## Flexy bility Matrix method.

flexability is the deformation at a point due to a unit load at the same (or) a different point.

WKT S= PL for an axial member [a][F] = (A-AL)

where [a] = Flexibility matrix of Size (nxn)

[F]: Redundant force Vector of Size (nx1)

△ = final displacement vector of Size (nx1)

where  $\Delta_{i} = \Delta_{i,i} + S_{i,i} - F_{0,i} + S_{i,k} F_{0,i} + S_{i,k} F_{0,k} + S_{$ 

(OR) Δ9 = Δ91 + α91 F, + α18 F2 + α13F3 + .... α10 Fn

A; = Displacement vector of size (nx1) due to loads.

1) Analyze the continous Beam as shown in the tig by flexibility matrix method. Flexural origidity 95 Constant throughout.

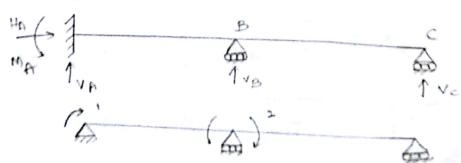
\$ 1-6m - 4m - 50 km

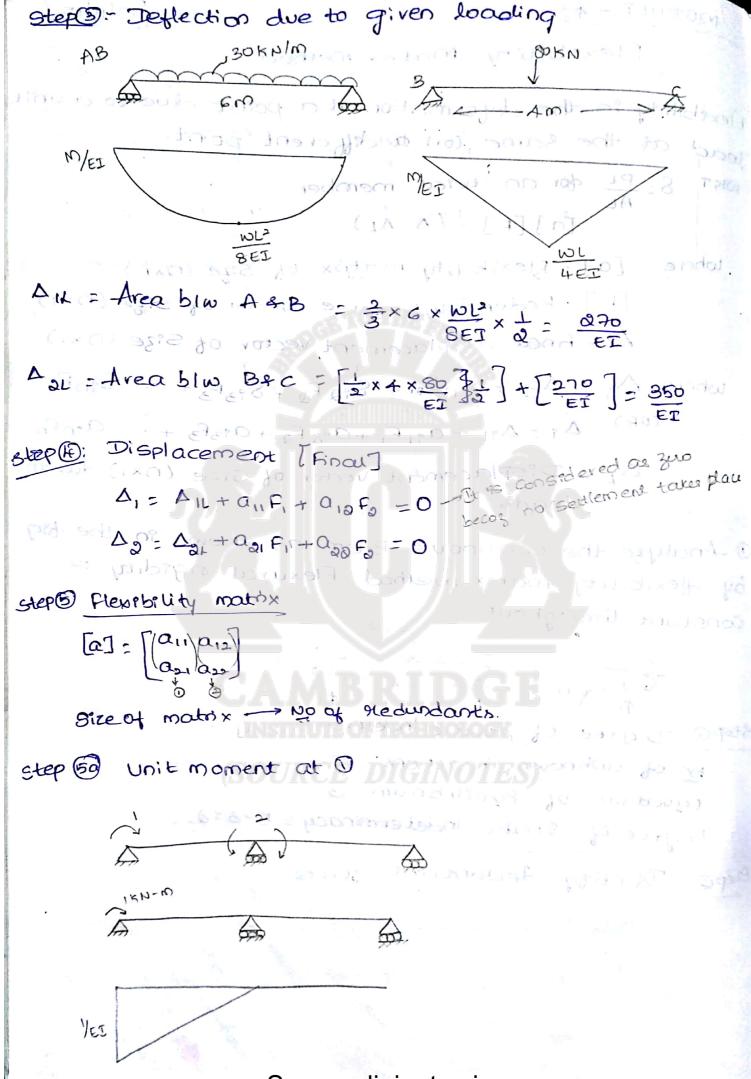
Stapo: Degree of static Indeterminacy

100 of unknown reactions = 5 Equation of Equilibrium = 3

Degree of Static Indeterminacy = 5-3=8.

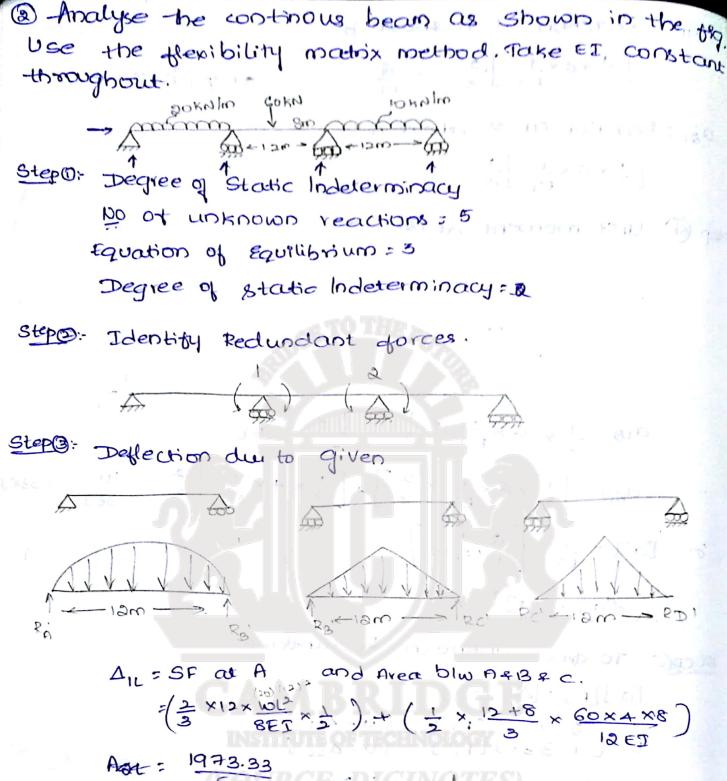
Step @: Identity Reduntant forces.





an = Reaction at A about B and syllong Step (7) BMD 97.16 azi : Reaction at B about A  $= \left[\frac{1}{3} \times 6 \times \frac{1}{5}\right] \frac{1}{3} = \frac{1}{5}$ step 6 Unit moment at 3 · YEI /EI aia = (1 × 6× = T) × (3) + 3× = ET  $a_{22} = \begin{bmatrix} \frac{1}{2} \times 6 \times \frac{1}{EI} \times \frac{2}{3} \end{bmatrix} + \begin{bmatrix} \frac{1}{2} \times 4 \times \frac{1}{EI} \end{bmatrix} = \frac{10}{3} = 3.33 \text{ ep}$ [a] = = 3.33 [a] = [a] T step (): To dind unknown Redundants [a][F]:[A-AL]  $\frac{1}{EI} \begin{bmatrix} 2 & 1 \\ 1 & 3.33 \end{bmatrix} \begin{bmatrix} F_1 \\ F_2 \end{bmatrix} = \begin{bmatrix} 0 - \Delta_{1L} \\ 0 - \Delta_{2L} \end{bmatrix}$  $\frac{1}{\text{EI}} \begin{bmatrix} 3 & 1 \\ 1 & 3.33 \end{bmatrix} \begin{bmatrix} F_1 \\ F_2 \end{bmatrix} = \begin{bmatrix} -350/\text{EI} \\ -350/\text{ET} \end{bmatrix}$  $\begin{bmatrix} F_1 \\ F_2 \end{bmatrix} = \begin{bmatrix} 1 \\ EI \\ 3.33 \end{bmatrix} - \begin{bmatrix} -270/EI \\ -350/EI \end{bmatrix}$ [F] = [0.58/EI -0.176/EI] [-270/EI] [-350/EI]  $= \begin{bmatrix} -15876 + 61.6 \\ EI > \end{bmatrix} = \begin{bmatrix} -97.16 \\ -76.03 \end{bmatrix}$ Source diginotes.in

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$$A_{\text{OL}} = \left(\frac{1}{3} \times 12 \times \frac{1012}{8ET} \times \frac{1}{3}\right) + \left(\frac{1}{2} \times \frac{12+8}{3} \times \frac{60 \times 4 \times 8}{12 ET}\right)$$

$$A_{\text{OL}} = \frac{1973.33}{ET}$$

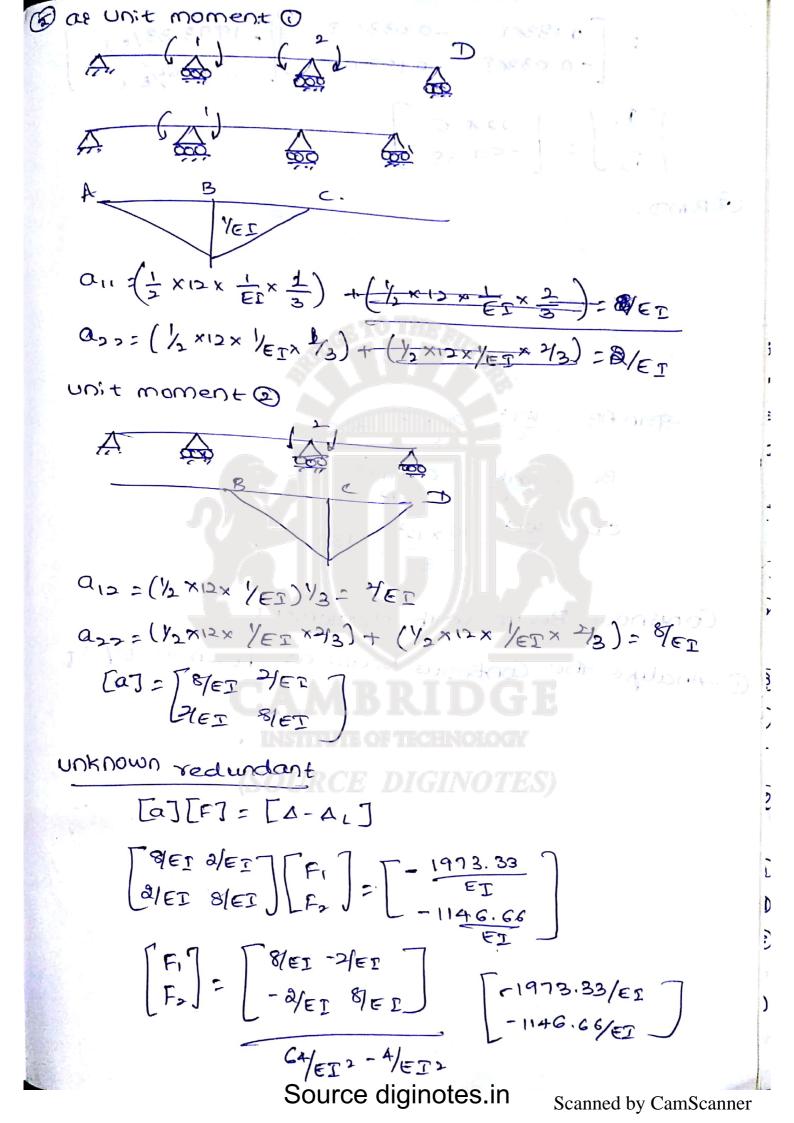
$$A_{\text{OL}} = \left(\frac{1}{2} \times \frac{12+4}{3} \times \frac{60 \times 4 \times 8}{12 ET}\right) + \left(\frac{1}{3} \times 12 \times \frac{10 \times 12^{2}}{8ET} \times \frac{1}{2}\right)$$

$$A_{\text{OL}} = \frac{1146.6c}{ET}$$

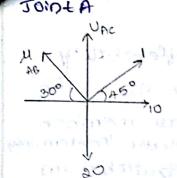
Final displacement

A:=0

A:=0



maysis of pin jointed frames. Analyse the touss shown in the tig by flexebility matrix method. Choosing the force member AD as the gredundant. Assume EA 95 constant for au members. Step 0:- Find degree of static Indeterminary Equations of Equilibrium DST : 3-3 =0 Internal static Determinacy m = 3m-2j+91 3 = 1 Internal= 2 20KN 91 = 3 External =0 step D: Identity Redundant force member. AD - Pedundant - makes it statically Indeterminate Released strochere. steps: To dind member forces. Joint A, EH=0 10-FABCOS 30=0 FAB = 11.54 KN 20 EV=0 FAC-20+ FABSIN30=0 FAC = 14-23 KN Btep@: Apply unit load & find forces members Source diginotes.in Scanned by CamScanner



Member	P(F)	- C	k	PUL AE	10°L AE	P+Ru
AB: U	11.55	0.816	8	75.39	5.32	10.82
Ac	14.85	-1-115	74	-63.55	AE	I hta.
AD		†	5.65	AE	4.97 AE	13.52
		A		5-66/AE		-0.73
		1 4	4	= = 11.84 =	=1594	9

$$COSH5 = \frac{AC}{AD} = \frac{A}{AD}$$

Analyse the pin jointed plane trame as shown anth Agg by flexibility matrix method & tabulate the member dorces. Assume MAF of each member = 0.005 mm/KN PRN 1B Step 1: No of members = 6 No of joints = 4 External 3-3=x m-2j+8=1 Considering Ac as a reductant 40 40 member Reduntant 3 Identity 10KN 5KN