

Documentation for TULIP 2

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Abstract

This booklet gives an introduction to the TULIP, which is a program for fitting interatomic potentials to physical data of different phases and lattices.

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1 Introduction

The program TULIP tries to fit a interatomic potential to *e.g.* given physical properties of compounds *etc.*. Physical properties are for instance lattice parameters, cohesive energy, bulk modulus and elastic constants.

Input is essentially an initial guess for potential parameters, a list of compounds and their desired properties (lattice parameters, cohesive energy, mixing energy, bulk modulus, elastic constants, ...), and technical specifications to guide the fitting. Using the parametrization, compounds are relaxed in a molecular dynamics (MD) simulation (MDS), and then the specified physical properties are calculated. The fitting routine tries to minimize the merit function. The fitting method can be selected.

2 Source code

0. Prerequisites: Install the `spglib` package from <http://spglib.sourceforge.net/> in a standard location and remember the location of installed files.

1. Local users only: Download the `libutils` source code into a folder:

```
git clone /home/phys-data/people/koehenri/repos/libutils.git
```

The `libutils` directory will be created. Descend into it and follow the instructions in the Readme file to make and install the library.

2. Local users only: Download the `tulip2` source code into a folder:

```
git clone /home/phys-data/people/koehenri/repos/tulip2.git
```

The `tulip2` directory will be created. Descend into it and follow the instructions in the Readme file to make and install the fitting code.

3. The static version `tulip_static` can be copied to other computer systems having the same architecture and be run there without any additional effort. The shared library version requires adding the `libutils` library to the library path.

* * *

To download updated versions of these codes descend into the root directories (e.g. `tulip2`) and execute

```
git pull
```

This will fetch and merge updated code with your local copy.

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The `tulip2/examples` directory contains some ready-made examples, which can be run without additional editing to get a better feel for how the code works.

3 Program arguments

```
TULIP version 2 (c) Krister Henriksson 2013-
Purpose: Fit data to an interatomic potential.
Usage:
    tulip arguments [options]
Arguments:
    -pf file           Path to file containing potential information.
    -gf file           Path to file containing geometry information.
Options:
    -sf file           Path to file containing technical specifications about the calculations.
    -ro               Only calculate properties of reference compounds, then exit. Default: not used.
    -nof              Only calculate properties of reference and read-in compounds, then exit. Default: not used.
    -xyz              Use traditional XYZ format when writing XYZ files. Default: not used.
                     The extended XYZ format (http://jrkermode.co.uk/quippy/io.html#extendedxyz)
                     is used by default.

    -dfitpropn        Show information about fitting of properties. Here 'n' must be
                     an integer. Supported: 0-4. 0: debug fitting method. 1-4: debug deeper.
                     lying methods used by the fitting method. Default: not used
                     NOTE: 0 also shows some info about the initial Chi^2 object.

    -dfitpotn         Show information about fitting of potentials. Here 'n' have a similar
                     role as for fitting of the properties.
                     NOTE 1: 0 also shows some info about the initial Chi^2 object.
                     NOTE 2: 'fitpot0' is always set to true, others are false by default.

    -dforces          Debug the forces. Default: not used
    -dpressure        Debug the pressure. Default: not used
    -dmdsprop         Debug MDS runs of the structures. Default: not used
    -dall             Activate all debugging options (top level only). Default: not used

    -mif              Suggest an initial fit and exit. Default: not used

    -omp              Request maximal number of threads (8) for any OpenMP parts.
    -omp_nt num       Request 'num' number of threads for any OpenMP parts. Default: 1
```

Main arguments:

<code>-pf potinfofile</code>	This file contains info about the elements and interactions.
<code>-gf geominfofile</code>	This file contains the info about the compounds which are to be fitted.

Recommended options to always use:

<code>-sf specsinfofile</code>	This file contains settings steering the calculation of properties of read-in compounds and the fitting process.
--------------------------------	--

Useful options:

<code>-ro</code>	Calculate properties of reference (single-species) compounds and quit.
<code>-nof</code>	Calculate properties of reference and read-in compounds and quit. This is useful when parametrization is finalized and high-accuracy values of properties are desired (use long MD relaxation times!).

-mif	Obtain an initial partial fit to start from.
-dmdsprop	Show progress of all MD relaxations of all compounds.

Note: The OpenMP options can be used, but the OpenMP parallelization has not been extensively debugged. Some cache trashing is likely to occur, degrading performance.

4 Potentials

In TULIP the following potentials are subject to fitting: (i) the ABOP (Analytical Bond Order Potential). The EAM (Embedded Atom Method) potential is understood by the program, but this type of interactions cannot be fitted.

4.1 ABOP potential

The Abell-Brenner-Tersoff [1, 4, 8] or ABOP [5] potential gives the total energy of a system of atoms as

$$V = \frac{1}{2} \sum_i \sum_j f_{c,ij} (V_{R,ij} - B_{ij} V_{A,ij}) = \sum_i \sum_{j>i} f_{c,ij} (V_{R,ij} - \bar{B}_{ij} V_{A,ij}), \quad (1)$$

Here

$$\bar{B}_{ij} = \frac{B_{ij} + B_{ji}}{2} \quad (2)$$

Note:

$$V_{ij} \equiv f_{c,ij} (V_{R,ij} - B_{ij} V_{A,ij}) \quad (3)$$

may not be equal to V_{ji} .

The repulsive (R) and attractive (A) parts are

$$V_{R,ij} = \frac{D_0}{S-1} \exp \left[-\beta \sqrt{2S} (r_{ij} - r_{0,ij}) \right] \quad (4)$$

$$V_{A,ij} = \frac{SD_0}{S-1} \exp \left[-\beta \sqrt{2/S} (r_{ij} - r_{0,ij}) \right] \quad (5)$$

with

$$r_{ij} = |\mathbf{r}_{ij}| = |\mathbf{r}_i - \mathbf{r}_j| \quad (6)$$

The Tersoff [8] cutoff function is

$$f_c(r) = \begin{cases} 1, & r \leq R - D, \\ \frac{1}{2} \left(1 - \sin \left(\frac{\pi}{2} \frac{r-R}{D} \right) \right), & R - D < r < R + D \\ 0, & r \geq R + D \end{cases} \quad (7)$$

Hence, full interaction is felt when $r < R - D$, and no interaction when $r > R + D$, making the cutoff distance $r_c = R + D$. The derivative is

$$f'_c(r) = \begin{cases} 0, & r \leq R - D, \\ \frac{1}{2} \left(1 - \frac{\pi}{2D} \cos \left(\frac{\pi}{2} \frac{r-R}{D} \right) \right), & R - D < r < R + D \\ 0, & r \geq R + D \end{cases} \quad (8)$$

The bond-order parameter is defined as

$$B_{ij} = (1 + \chi_{ij})^{-p_{ij}} \quad (9)$$

The usual ABOP has $p_{ij} \equiv 1/2$.

Here

$$\chi_{ij} = \sum_{k, k \neq i, k \neq j} f_{c,ik} g_{ijk}(\theta_{ijk}) \omega_{ijk} \exp [\alpha_{ijk}(r_{ij} - r_{ik})] \quad (10)$$

We have now three different possibilities:

(V1) α_{ijk} and ω_{ijk} are used as parameters.

(V2) If α_{ijk} is used but ω_{ijk} is not, then the Brenner form is used for the latter:

$$\omega_{ijk} = \exp [-\alpha_{ijk}(r_{0,ij} - r_{0,ik})] \quad (11)$$

and ω_{ijk} is **not** a separate parameter.

(V3) If α_{ijk} is not used and $2\mu_{ik}$ is used, then the whole factor

$$\omega_{ijk} \exp [\alpha_{ijk}(r_{ij} - r_{ik})] \quad (12)$$

is replaced in its entirety by

$$\exp [2\mu_{ik}(r_{ij} - r_{ik})] \quad (13)$$

The function $g_{ijk}(\theta_{ijk})$ is given by the expression

$$g_{ijk}(\theta_{ijk}) = \gamma_{ik} \left(1 + \frac{c_{ik}^2}{d_{ik}^2} - \frac{c_{ik}^2}{d_{ik}^2 + (h_{ik} + \cos \theta_{ijk})^2} \right) \quad (14)$$

where θ_{ijk} is the angle between the bonds ij and ik .

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The Perriot cutoff/screening method [7] can be used instead of the Tersoff function. In this method the total potential energy is given by

$$V = \frac{1}{2} \sum_i \sum_j K_{ij} (V_{R,ij} - B_{ij} V_{A,ij}) \quad (15)$$

The bond-order is modified in the following way:

$$\chi_{ij} = \sum_{k, k \neq i, k \neq j} f_{c,ik}^{(P)} K_{ik} g_{ijk}(\theta_{ijk}) \omega_{ijk} \exp[\alpha_{ijk}(r_{ij} - r_{ik})] \quad (16)$$

The Perriot method contains the following functions:

$$K_{ij} = \exp \left[- \sum_{s, s \neq i, s \neq j} T_{ijs}^{n_{ij}} \right] \quad (17)$$

$$T_{ijs} = \begin{cases} -\frac{1}{2} + \frac{r_{ij}}{X_{is} + X_{js} - r_{ij}}, & X_{is} + X_{js} < 3r_{ij} \\ 0, & \text{otherwise} \end{cases} \quad (18)$$

$$X_{is} = \frac{r_{is}}{1 - (r_{is}/r_{c,is})^{m_{is}}} \quad (19)$$

$$X_{js} = \frac{r_{js}}{1 - (r_{js}/r_{c,js})^{m_{js}}} \quad (20)$$

$$f_{c,ik}^{(P)} = \begin{cases} 1, & r_{ik} < r_{ik,min} \\ 1 - q_{ik}^3(6q_{ik}^2 - 15q_{ik} - 10), & r_{ik,min} \leq r_{ik} \leq r_{ik,max} \\ 0, & r_{ik} > r_{ik,max} \end{cases} \quad (21)$$

$$q_{ik} = \frac{r_{ik} - r_{ik,min}}{r_{ik,max} - r_{ik,min}} \quad (22)$$

Here $n, m, r_c, r_{min}, r_{max}$ are parameters.

Technically, if r_{is} or r_{js} equals r_c then the corresponding X is infinite and T_{ijs} becomes 0. This can be exactly handled by the following rule: If neighbor s of atom i is beyond the cutoff radius $r_{c,is}$ or $r_{c,js}$, then $T_{ijs} = 0$ and it does not contribute at all to the K_{ij} . This does not account for the following situation: If r_{is} or r_{js} is larger than r_c then the corresponding X is negative. Mathematically, it can still satisfy $X_{is} + X_{js} < 3r_{ij}$ so it should be considered for the sum T_{ijs} . As of now, this case is ignored due to the rule above.

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The ABOP potential is inadequate for small interatomic distances. To ensure a more correct description a repulsive potential $V_{\text{rep}}(r)$ — e.g. the ZBL potential — describing interactions at small distances should be used. The original potential presented above is then modified to

$$V(r) = (1 - F(r))V_{\text{rep}}(r) + F(r)V_{\text{orig}}(r) \quad (23)$$

where $F(r)$ is the Fermi function

$$F(r) = 1/(1 + e^{-b_f(r-r_f)}) \quad (24)$$

and b_f, r_f are parameters that need to be supplied.

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All parameters that can be used with the ABOP potential are:

Parameter	Notes
D_0 r_0 β S γ c d h p b_f r_f	Defaults to 1/2. Defaults to 10. Defaults to 1.
D R	Tersoff cutoff parameters Cutoff radius is $r_c = R + D$.
n m r_c r_{\min} r_{\max}	Perriot cutoff parameters
(V1) α_{ijk} and ω_{ijk} (V2) α_{ijk} (V3) $2\mu_{ik}$	ω_{ijk} given by Eq. (11).

4.2 EAM potentials

EAM potentials can as of now not be fitted, but only be used as read-in potentials.

The total energy of a solid is in the EAM formalism

$$V = \frac{1}{2} \sum_i \sum_{j, j \neq i} V_2(r_{ij}) + \sum_i a_s F_s(\rho_{s,i}^a) + \sum_i a_p F_p(\rho_{p,i}^a) + \sum_i a_d F_d(\rho_{d,i}^a). \quad (25)$$

Here a_i is 1 if the band i is included, else it is 0. Also,

$$\rho_i^a = \sum_{j=1, j \neq i} \rho(r_{ij}), \quad (26)$$

where $\rho(r)$ is the atomic electron density at distance r from an atom. The program recognized the EAM versions displayed in table 1.

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The EAM potentials are read in from files. The format of these is shown in tables 2-4.

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Note: The N_r points (r, V_2) in the EAM files are read in as $r = 0, \dots, (N_r-1)dr$. To avoid any problems, we must have $N_r \times dr > r_{cut}$. For instance, use $N_r \times dr = r_{cut} + 10 \times dr$.

Table 1: Recognized EAM flavors.

EAM-s	EAM with only s embedding energy
EAM-p	EAM with only p embedding energy
EAM-d	EAM with only d embedding energy
EAM-sp	EAM with s and p embedding energies
EAM-sd	EAM with s and d embedding energies
EAM-sp d	EAM with s , p , and d embedding energies

Table 2: EAM file format when a single embedding energy is used. Note: First and second lines are ignored.

Comment line
Z1 Z2 mass1 mass2 latpar1 latpar2 latname1 latname2
Nrho drho Nr dr rcut
(Nrhod points of F_s or F_p or F_d)
(Nr points of V_2)
(Nr points of ρ_s or ρ_p or ρ_d)

Table 3: EAM file format when two embedding energies are used. Example is for s and d embedding energies. Note: First and second lines are ignored.

Comment line
Z1 Z2 mass1 mass2 latpar1 latpar2 latname1 latname2
Nrhod drhod Nr dr rcut Nrhos drhos
(Nrhod points of F_d)
(Nr points of V_2)
(Nr points of ρ_d)
(Nrhos points of F_s)
(Nr points of ρ_s)

Table 4: EAM file format when three embedding energies are used. Note: First and second lines are ignored.

Comment line
Z1 Z2 mass1 mass2 latpar1 latpar2 latname1 latname2
Nrhod drhod Nr dr rcut Nrhos drhos Nrhop drhop
(Nrhod points of F_d)
(Nr points of V_2)
(Nr points of ρ_d)
(Nrhos points of F_s)
(Nr points of ρ_s)
(Nrhop points of F_p)
(Nr points of ρ_p)

5 Read-in files

All specifications about the fitting procedure, physical properties, and calculations in general are given in read-in files: (i) file containing settings for the potentials, (ii) file containing physical properties, and (iii) file containing technical specifications about the calculations. The last file is optional.

The delimiters separating tokens in the read-in files are: tabulator, space, and the following characters: `:`, `(`, `)`, `[`, `]`, `=`. The point is not a delimiter. Character strings which are not part of the input value for an option are simply ignored.

5.1 File: Elements and interactions information

An overview of which potentials that can be read in from tabulated data in (x, y) format and those which can be specified via parameters only is shown in Table 5.

* * *

Complete example:

Table 5: R = Can be read in from data file. A = Can be specified by parameters.

Potential	R	A
EAM-*	Yes	No
ABOP	No	Yes

```

# MUST BE FIRST:
# Number of elements:
nelem = 3

# MUST BE SECOND:
# Element names:
elem(1) = Fe
elem(2) = Cr
elem(3) = C

# Optional:
atomtype(Fe) = 1
atomtype(Cr) = 2
atomtype(C) = 3

# Masses
mass(Fe) = 55.8470
mass(Cr) = 51.9961
mass(C) = 12.0110

# Reference lattices:
lat(Cr, Cr) = skip BCC Calc. for this will be skipped, we will have EcoH(Cr)=0.0.
lat(Fe, Fe) = BCC
lat(C, C) = GRA

# Supported ref. lattices:
# DIM1 (homomer), DIM2 (heteromer), SC, BCC, BCC-P, FCC, FCC-P,
# DIA, HCP, GRA, GRP (graphene)
# The ...-P versions refer to alternate structures with
# non-Cartesian primitive vectors.

a(Cr, Cr) = 2.87
a(Fe, Fe) = 2.87
#####
# Use accurate values for C, otherwise the graphite might explode due
# to massive pressure!!! Also, use small enough time step!!!
#####
a(C, C) = 1.46 rNN for graphite (GRA) DIA: 3.55647765821
c(C, C) = 6.689
# Also possible:
# bpa(C, C) = ...
# cpa(C, C) = ...

```

```
# Interaction types:
iac(Fe, Fe) = ABOP
iac(Cr, Cr) = ABOP
iac(C, C) = ABOP
iac(Fe, Cr) = ABOP    symmetric
iac(Fe, C) = ABOP    symmetric
iac(Cr, C) = ABOP    symmetric

# Fit this interaction? The interaction must be analytical.
fit(Fe, Cr) = yes    symmetric

# Repulsive potentials (ZBL):

use_rep_core( Fe, Fe ) = yes
use_rep_core( Cr, Cr ) = yes
use_rep_core( C, C ) = yes
use_rep_core( Fe, Cr ) = yes
use_rep_core( Fe, C ) = yes
use_rep_core( Cr, C ) = yes

# Parameters for fixed interactions

potpar( Fe, Fe ):D0 = 1.5
potpar( Fe, Fe ):r0 = 2.29
potpar( Fe, Fe ):beta = 1.4
potpar( Fe, Fe ):S = 2.0693109
potpar( Fe, Fe ):gamma = 0.0115751
potpar( Fe, Fe ):c = 1.2898716
potpar( Fe, Fe ):d = 0.3413219
potpar( Fe, Fe ):h = -0.26
potpar( Fe, Fe ):bfermi = 10
potpar( Fe, Fe ):rfermi = 1

potpar( Fe, Fe ):option: rcut_fun = perriot
potpar( Fe, Fe ):n = 5
potpar( Fe, Fe ):m = 48
potpar( Fe, Fe ):rcut = 3.3
potpar( Fe, Fe ):rmin = 3.0
potpar( Fe, Fe ):rmax = 3.3

potpar(Cr, Cr ):D0 = 4.04222081
potpar(Cr, Cr ):r0 = 2.13018547
potpar(Cr, Cr ):beta = 1.62158721
potpar(Cr, Cr ):S = 3.36793914
potpar(Cr, Cr ):gamma = 0.02388562
potpar(Cr, Cr ):c = 1.03288255
potpar(Cr, Cr ):d = 0.13813230
potpar(Cr, Cr ):h = -0.28569237
potpar(Cr, Cr ):R = 3.2
potpar(Cr, Cr ):D = 0.20
```

```

potpar( Cr, Cr ):bfermi = 12
potpar( Cr, Cr ):rfermi = 1.7

potpar(C, C ):D0 = 6.0
potpar(C, C ):r0 = 1.39
potpar(C, C ):beta = 2.1
potpar(C, C ):S = 1.22
potpar(C, C ):gamma = 2.0813e-4
potpar(C, C ):c = 330.0
potpar(C, C ):d = 3.5
potpar(C, C ):h = 1.0
potpar(C, C ):R = 1.85
potpar(C, C ):D = 0.15
potpar( C , C ):bfermi = 8
potpar( C , C ):rfermi = 0.6

potpar(Fe, C ):D0 = 3.95000634
potpar(Fe, C ):r0 = 1.53426579
potpar(Fe, C ):beta = 1.82109816
potpar(Fe, C ):S = 1.43035110
potpar(Fe, C ):gamma = 0.07485571
potpar(Fe, C ):c = 1.11674155
potpar(Fe, C ):d = 0.94663188
potpar(Fe, C ):h = -0.18665305
potpar(Fe, C ):R = 2.6
potpar(Fe, C ):D = 0.20
potpar( Fe, C ):bfermi = 10
potpar( Fe, C ):rfermi = 1

potpar( Cr, C ):D0          = 2.77620074
potpar( Cr, C ):r0          = 1.81289285
potpar( Cr, C ):beta        = 2.00816371
potpar( Cr, C ):S           = 2.04637644
potpar( Cr, C ):gamma       = 0.00068830
potpar( Cr, C ):c           = 3.93353757
potpar( Cr, C ):d           = 0.17497204
potpar( Cr, C ):h           = -0.17850001
potpar( Cr, C ):R           = 2.95
potpar( Cr, C ):D           = 0.1
potpar( Cr, C ):bfermi = 8
potpar( Cr, C ):rfermi = 1.2

# Parameters for fittable interactions

      potpar( Fe, Cr ):D0 = 3.48049488
min: potpar( Fe, Cr ):D0 = 0.1
max: potpar( Fe, Cr ):D0 = 10.0

      potpar( Fe, Cr ):r0 = 2.16998952
min: potpar( Fe, Cr ):r0 = 1.0
max: potpar( Fe, Cr ):r0 = 5.0

      potpar( Fe, Cr ):beta = 1.75467567
min: potpar( Fe, Cr ):beta = 1.0
max: potpar( Fe, Cr ):beta = 5.0

```

```

        potpar( Fe, Cr ):S = 2.28661503
min: potpar( Fe, Cr ):S = 1.1
max: potpar( Fe, Cr ):S = 5.0

        potpar( Fe, Cr ):gamma = 0.15766130
min: potpar( Fe, Cr ):gamma = 1e-5
max: potpar( Fe, Cr ):gamma = 1e5

        potpar( Fe, Cr ):c = 0.48531613
min: potpar( Fe, Cr ):c = -1e5
max: potpar( Fe, Cr ):c = 1e5

        potpar( Fe, Cr ):d = 0.31427413
min: potpar( Fe, Cr ):d = -1e5
max: potpar( Fe, Cr ):d = 1e5

        potpar( Fe, Cr ):h = -0.69
min: potpar( Fe, Cr ):h = 1.0
max: potpar( Fe, Cr ):h = 1.0

        potpar( Fe, Cr ):R = 3.10
min: potpar( Fe, Cr ):R = 2.0
max: potpar( Fe, Cr ):R = 2.0

        potpar( Fe, Cr ):D = 0.15
min: potpar( Fe, Cr ):D = 1.0
max: potpar( Fe, Cr ):D = 1.0

        potpar( Fe, Cr ):bfermi = 10
min: potpar( Fe, Cr ):bfermi = 5
max: potpar( Fe, Cr ):bfermi = 15

        potpar( Fe, Cr ):rfermi = 1
min: potpar( Fe, Cr ):rfermi = 0.1
max: potpar( Fe, Cr ):rfermi = 5

# ABOP alpha and omega parameters

#####
##
## NOTE: There are NO ABOP alpha, omega, 2mu parameters used by default.
## Only the specified ones are used.
## Defaults: alpha=2mu=0.0 and omega=1.0 as constants.
##
## If an omega parameter is specified it is taken as an
## independent parameter (non-Brenner form), otherwise
## it is constructed from alpha parameters --- if they are
## specified --- as
##
## "omega_ijk" = exp( alpha_ijk*(r0_ij - r0_ik) )
##
#####

```

```
# Fixed:

abop_alpha( Fe, Fe, Fe ) = 0.0
abop_omega( Fe, Fe, Fe ) = 1.0

abop_alpha( Cr, Cr, Cr ) = 1.39662066
abop_omega( Cr, Cr, Cr ) = 1.0

abop_alpha( C, C, C ) = 0.0
abop_omega( C, C, C ) = 1.0

abop_alpha( Cr, Cr, C )      = 0.8640643600
abop_alpha( Cr, C , Cr )    = -1.7520448300
abop_alpha( C, Cr, Cr )     = 0.6122158900
abop_alpha( C, C , Cr )     = 0
abop_alpha( C, Cr, C )      = 0
abop_alpha( Cr, C, C )      = 0

abop_omega( Cr, Cr, C )     = 1.6402877600
abop_omega( Cr, C , Cr )   = 0.2939996300
abop_omega( C, Cr, Cr )    = 0.4190507900
abop_omega( C, C , Cr )    = 1
abop_omega( C, Cr, C )     = 1
abop_omega( Cr, C, C )     = 1

# Fittable:

      abop_alpha( Fe, Fe, Cr ) = 1.0
min: abop_alpha( Fe, Fe, Cr ) = 100.0
max: abop_alpha( Fe, Fe, Cr ) = 100.0

      abop_alpha( Fe, Cr, Fe ) = 1.0
min: abop_alpha( Fe, Cr, Fe ) = 100.0
max: abop_alpha( Fe, Cr, Fe ) = 100.0

      abop_alpha( Cr, Fe, Fe ) = 1.0
min: abop_alpha( Cr, Fe, Fe ) = 100.0
max: abop_alpha( Cr, Fe, Fe ) = 100.0

      abop_alpha( Cr, Fe, Cr ) = 1.0
min: abop_alpha( Cr, Fe, Cr ) = 100.0
max: abop_alpha( Cr, Fe, Cr ) = 100.0

      abop_alpha( Fe, Cr, Cr ) = 1.0
min: abop_alpha( Fe, Cr, Cr ) = 100.0
max: abop_alpha( Fe, Cr, Cr ) = 100.0

      abop_alpha( Cr, Cr, Fe ) = 1.0
min: abop_alpha( Cr, Cr, Fe ) = 100.0
max: abop_alpha( Cr, Cr, Fe ) = 100.0
```

```

        abop_omega( Fe, Fe, Cr ) = 1.0
min: abop_omega( Fe, Fe, Cr ) = 100.0
max: abop_omega( Fe, Fe, Cr ) = 100.0

        abop_omega( Fe, Cr, Fe ) = 1.0
min: abop_omega( Fe, Cr, Fe ) = 100.0
max: abop_omega( Fe, Cr, Fe ) = 100.0

        abop_omega( Cr, Fe, Fe ) = 1.0
min: abop_omega( Cr, Fe, Fe ) = 100.0
max: abop_omega( Cr, Fe, Fe ) = 100.0

        abop_omega( Cr, Fe, Cr ) = 1.0
min: abop_omega( Cr, Fe, Cr ) = 100.0
max: abop_omega( Cr, Fe, Cr ) = 100.0

        abop_omega( Fe, Cr, Cr ) = 1.0
min: abop_omega( Fe, Cr, Cr ) = 100.0
max: abop_omega( Fe, Cr, Cr ) = 100.0

        abop_omega( Cr, Cr, Fe ) = 1.0
min: abop_omega( Cr, Cr, Fe ) = 100.0
max: abop_omega( Cr, Cr, Fe ) = 100.0

# Not used:
#     abop_2mu( Fe, Cr ) = 1.0
#     abop_2mu( Cr, Fe ) = 1.0

```

5.2 File: Compounds information

In order to specify a physical property to be fitted, the keywords in example below must be used.

Keywords are grouped into sets than begin with the string LAT on a separate line. Properties in each set refer to the same structure/lattice/geometry.

All properties that are specified (=set) are activated as fitting targets.

Complete listing of options for a lattice: Note that . . . means that numerical values (single or several ones) are expected, and *** means that a string is needed.

```

LAT                               <= starts readin of new lattice info

name                             = ...   string
csystem                         = ...   OPTIONAL, crystal system
file                           = ...   LAT file, string
elements                       = ...   element names (e.g. W H), strings
Ndesired                       = ...   number of cells in direction a, three integers

```

```
Neven_desired = ...    0 for false, 1 for true, three integers
Nodd_desired  = ...    0 for false, 1 for true, three integers

# Lattice parameters
a              = ...
w_a           = ...      weight
b              = ...
u_b           = ...      uncertainty
c              = ...      default: weight: 1.0

# weight for any property: w_***
# uncertainty for any property: u_***

# Lattice parameter relationships:
bpa           = ...
cpa           = ...

# Dimer bond distance (only for dimers):
# r0           = ...

# Angles (radians):
angle_ab      = ...
angle_ac      = ...
angle_bc      = ...

# Atomic volume (cubic Angstroms):
Vatom         = ...

# This compound should be considered ground/reference state when calculating
# cohesive energies:
Ecoh_delta_refcomp = true
# If no cohesive energies used, then skip this setting.

# Change in cohesive energy relative to reference:
Ecoh_delta    = ... (>0.0, i.e. more unstable than reference)

# Formation energy Ef in 'mixing energy' Emix = Ef/natoms form:
Emix          = ...

# Bulk modulus B (GPa):
B              = ...

# Pressure derivative of B:
Bp            = ...

# Elastic constants (all):
C11           = ...
C12           = ...
C13           = ...
C14           = ...
C15           = ...
C16           = ...
C22           = ...
C23           = ...
C24           = ...
C25           = ...
```



```
C26          = ...
C33          = ...
C34          = ...
C35          = ...
C36          = ...
C44          = ...
C45          = ...
C46          = ...
C55          = ...
C56          = ...
C66          = ...
# A SPGLIB call will determine space group and which Cij are correct.
# Wrong ones will be turned off.

# Options:
option: no_heating           Do not use temperatures > 0 K.
option: fixed_geometry       Do not allow atom positions in compounds to change.
option: quench_always        Always scale velocities to 0.

# Force handling:
frc_file      = *** string
# => use atomic forces, get them from specified file
frc_use       = *** boolean
# => use atomic forces
frc_use_w     = *** boolean, use weights for force components (default)
# frc_use_u   = *** boolean, use uncertainties for force components
#
# Format of forces file: Lines of
#   fx fy fz wufx wufy wufz
# in eV/fs, where wufx, wufy, wufz is interpreted as weights/uncertainties,
# depending on which of frc_use_w/frc_use_u is set.
#

# Options that still exist (?) but are deprecated:
# Fmax        = ...    try to achieve this largest atomic force
#                in relaxed compound
# Pmax        = ...    try to achieve this largest Cartesian pressure
#                in relaxed compound
# displmax    = ...    try to achieve this largest atomic displacement
#                in relaxed compound
# Rationale: Prefer parametrizations that minimize forces, pressures, and
# displacements.
# Note: Usually the MD relaxation achieves these goals already, and specifying
# these options may interfere with the fitting (see the merit function discussion).

# Compound-specific MD options, overrides any others specified elsewhere:
# Complete list (example values):

mds_skint     = 1.0      # Angstrom
mds_seed      = 12345
mds_ndump     = 10       # dump info every ndump steps (if -dmdsprop option)

mds_tstart    = 0.0
mds_tend      = 2000.0
```

```

mds_dt          = 3.0
mds_max_dt      = 3.0

mds_Tstart      = 0.5  starting temperature T (K)

# Negative values or missing settings turn off control:
mds_btc_tau     = 10.0  Berendsen time constant for T control (fs)
mds_btc_T0      = 0.0  desired T (K)

# Negative values or missing settings turn off control:
mds_bpc_tau     = 80.0  Berendsen time constant for P control (fs)
mds_bpc_P0      = 0.0  desired P (GPa)
mds_bpc_scale   = 50.0  scaling constant, usually on the order of bulk modulus (GPa)

# mds_quench_tstart = 2000
# mds_quench_rate   = 1.0  # quenching rate (K/fs), negative value => heating

# Some default values are always used, even if no settings here:
mds_error_T_gt   = 1e6  Fatal error if T gets over this limit (K).
mds_error_dt_lt  = 0.01 Fatal error if dt gets under this limit (fs).
mds_error_boxlen_gt = 1e4 Fatal error if any boxlen gets over this limit (Angstrom).

```

* * *

Ignoring elastic constants: The space group is determined by a call to the `spglib` library. The SPG information is used to determine which elastic constants C_{ij} that can be calculated. If elastic constants are not used, and especially if the compound *e.g.* contains defects that complicate the determination of the space group, use

```
cssystem = any
```

This setting makes the program skip the determination of the space group for that compound. This skipping is also performed if the compound is non-periodic in any dimension.

* * *

Providing logical true or false: If a boolean value of logical true is to be input, use `yes`, `Yes`, `true`, `True`, `set`, or `Set`. Only the first letter is significant. The string `on` or a mixed version of lower- and upper-case also translates to logical true. In addition, the digit `1` also means logical true. Any other string or character evaluates to logical false.

* * *

Default behavior for weights and uncertainties: If neither weight nor uncertainty is specified for any property a default weight of 1 is used. The weights w_i are normalized: $\sum_i w_i = 1$, where the sum goes over properties with weights only, properties with uncertainties are not taken into account.

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Example:

```

LAT                                     <= triggers readin of new compound data

name      = dimer
file      = in/dimer.lat
elements  = W H

r0 = 1.5                                Desired bond distance in dimer
w_r0 = 0.0001                           weight

Ecoh      = -0.123
u_Ecoh    = 0.0068                      uncertainty (w and u can be freely mixed
                                         for different properties)

option: no_heating                      Do not use temperatures > 0 K.

LAT                                     <= triggers readin of new compound data

name      = bcc
file      = in/bcc.lat
elements  = W
a         = 2.9
w_a       = 1.0
Ecoh_delta_refcomp = true
C11       = 80.1605326176
w_C11     = 20
C12       = 20.4233027208
w_C12     = 20
C44       = 25.072362326
w_C44     = 20

LAT                                     <= triggers readin of new compound data

name      = octa
file      = in/octa.lat
elements  = W H
Ndesired  = 2 2 2
Neven_desired = 1 1 1
Nodd_desired = 0 0 0
a         = 2.9
Emix      = 0.001

mds_seed  = 123
mds_tend  = 5000.0
mds_dt    = 3.0
mds_max_dt = 3.0

mds_Tstart = 0.5  starting temperature T (K)

```

```

mds_btc_tau = 10.0 Berendsen time constant for T control (fs)
mds_btc_T0 = 0.0 desired T (K)

mds_bpc_tau = 80.0 Berendsen time constant for P control (fs)
mds_bpc_P0 = 0.0 desired P (GPa)
mds_bpc_scale = 50.0 scaling constant, usually on the order of bulk modulus (GPa)

```

5.3 LAT files

5.3.1 Basic structure

Format of LAT file:

Comment	Arbitrary comment.
S	Overall scaling constant.
a1 a2 a3 optional-string	Components of the first primitive vector U1.
b1 b2 b3 optional-string	Components of the second primitive vector U2.
c1 c2 c3 optional-string	Components of the third primitive vector U3.
format	internal or direct
Nbasis	number of basis vectors
E1 B11 B12 B13 constr1	Element name and vector components of first basis atom.
E2 B21 B22 B23 constr2	Element name and vector components of second basis atom.
...	

The real primitive vectors are

$$\mathbf{v}_i = S\mathbf{u}_i \quad (27)$$

The strings E_i — e.g. Cr, H, W — specify the element/species of the basis atom.

If optional-string is present and is pbc, then the corresponding direction is considered periodic, i.e. it is a true primitive vector in an infinite lattice. Other strings are ignored.

If the format keyword is scaled or Scaled or letter s or S then e.g. the j :th basis vector is

$$\mathbf{b}_j = SB_{j1}\mathbf{e}_x + SB_{j2}\mathbf{e}_y + SB_{j3}\mathbf{e}_z = \sum_i SB_{ji}\mathbf{e}_i \quad (28)$$

This is equivalent to **Cartesian** in VASP.

If instead the format keyword is internal or Internal or letter i or I then the basis vector is

$$\mathbf{b}_j = SB_{j1}\mathbf{u}_x + SB_{j2}\mathbf{u}_y + SB_{j3}\mathbf{u}_z = \sum_i SB_{ji}\mathbf{u}_i \quad (29)$$

This is equivalent to **Direct** in VASP.

5.3.2 Constraints

The `constr1`, `constr2`, *etc.* are atomic constraint strings (each atom can be given constraints). There are three possible constraint types:

1. Fix atom: `fix`
2. Constrain atom to move in one direction only: `freedir u1 u2 u3`, where the u_i are coordinates. Example: `freedir 0 0 1` allows motion in z direction only.
3. Constrain atom to move in a plane only: `freeplane u1 u2 u3`, or `freeplanevecs v1 v2 v3 w1 w2 w3`, where the u_i are coordinates of the plane's normal vector, and the v_i, w_i are coordinates of two vectors lying in the plane.

All direction vectors are normalized automatically. Only one option is valid for any atom.

5.3.3 Specifying the origin

An explicit origin can be specified on the line after the last basis atom. The first string has to start with lower- or upper-case O, then three coordinates must be given. This origin will be used when the simulation cell is created.

5.3.4 Examples

Example 1: Fe-Y dimer in vacuum, non-periodic boundaries:

```
Fe-Y dimer
10.0  <= scaling constant
1.0  0.0  0.0    primitive vector U1
0.0  1.0  0.0    primitive vector U2
0.0  0.0  1.0    primitive vector U3
Scaled
2
Y    0.0000000000  0.0000000000  0.0000000000
Fe   0.2000000000  0.0000000000  0.0000000000 freedir 1 0 0
origin: 0.0 0.0 0.0
```

Example 2: CrC in the NaCl crystal form:

```
#
4.0741512214
0.0  0.5  0.5    pbc    primitive vector U1
0.5  0.0  0.5    pbc    primitive vector U2
0.5  0.5  0.0    pbc    primitive vector U3
Internal
2
C    0.0  0.0  0.0
Cr   0.5  0.5  0.5
```

Scripts are provided to convert between POSCAR, XYZ and LAT formats.

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A simulation box with box lengths $L_i = N_i |\mathbf{v}_i|$ is constructed from a compound with primitive vectors $\mathbf{v}_i = S\mathbf{u}_i$, so that all box lengths are more than twice the largest cutoff radius for the elements occuring in the compound:

$$L_i = N_i v_i \geq 2r_c \quad (30)$$

Here N_i is initially the corresponding value in the `Ndesired` setting, if specified.

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Predicted lattice parameter \tilde{a} is calculated as

$$\tilde{a} = (\tilde{L}_1 / L_1) a, \quad (31)$$

where a is the read-in lattice parameter in the file listing the compounds, L_1 is the initial length of the simulation box in the \mathbf{v}_1 direction, and \tilde{L}_1 is the relaxed length of the simulation box in the same direction.

Q: Why are read-in values for a, b, c not equal to v_1, v_2, v_3 ? Why are predicted values for a, b, c not equal to relaxed values of v_1, v_2, v_3 ?

A: Primitive vectors for compounds may be given in many different ways. The current scheme avoids keeping track of them all, lightening the work burden for the user and minimizes additional coding.

The tradeoff is that for e.g. cubic phases $a = b = c$, but now a is taken from the change in v_1 , changes in v_2, v_3 are not taken into account.

★ ★ ★

Note: There must always be at least one basis vector. The following example for bcc Fe should be helpful:

```

Comment: BCC Fe with primitive vectors.
-0.25  0.25  0.25  pbc
 0.25 -0.25  0.25  pbc
 0.25  0.25 -0.25  pbc
Internal
1
Fe 0.0 0.0 0.0
```

Using a conventional cubic cell, the lattice is

```

Comment: BCC Fe.
 1.0  0.0  0.0  pbc
 0.0  1.0  0.0  pbc
 0.0  0.0  1.0  pbc
  Internal
  2
Fe   0.0  0.0  0.0
Fe   0.25 0.25 0.25

```

5.4 Optional file: Technical specifications

```

# -----
# Calculating properties of compounds
# -----

# Bulk modulus
prop:BM_rel_sys = yes      relax a strained frame
prop:BM_fmin    = -0.01
prop:BM_fmax    =  0.01
prop:BM_Nf      =  10      number of points to use for (V,E) curve
prop:BM_ef      = 1e-10    error ratio for each energy valve

# Elastic constants
prop:C_rel_sys  = yes
prop:C_fmin     = -0.01
prop:C_fmax     =  0.01
prop:C_Nf       =  10
prop:C_ef       = 1e-10

# -----
# Fitting properties of compounds
# -----

prop:fitmet      = LM      options: CG, PM, GN, LM, DL, SM, DE, PS, BC, GS, or SA
prop:nitermin    =  5      do at least this many iterations
prop:nitermax    = 100     do a maximum of this many iterations
prop:niterrestart = 20     restart every 20th iteration

#### Negative values means that it will not be used when testing for convergence:
prop:functolabs  = 1e-5    convergence when absolute merit function value is less
                           than this
prop:functolrel  = -1e-5   ... change in merit function value ...
prop:gradtolabs  = 1e-5    ... absolute gradient value ...
prop:steptolabs  = 1e-5    ... absolute step size ...
prop:steptolrel  = -1e-5   ... change in step size ...

prop:dogleg_radius    = 0.2    initial trust region radius
prop:dogleg_minradius = 1e-5   exit when radius gets this low
prop:barrier_scale     = 0.0    scaling constant for barrier penalty function,
                                to keep parameter values inside min/max interval
prop:simann_delta_rel  = 0.2    initial displacements in coordinate directions

```

```
prop:use_data_scales = false use/do not use scaled values in the merit function

# -----
# General MDS settings
# -----
prop:mds_skint = 1.0      Angstrom
prop:mds_seed  = 12345
prop:mds_ndump = 10      dump info every ndump steps (if -dmdsprop option)

prop:mds_tstart = 0.0
prop:mds_tend   = 2000.0
prop:mds_dt     = 0.5
prop:mds_max_dt = 1.0

prop:mds_Tstart = 300.0  starting temperature T (K)

# Negative values or missing settings turn off control:
prop:mds_btc_tau = 20    Berendsen time constant for T control (fs)
prop:mds_btc_T0  = 0     desired T (K)

# Negative values or missing settings turn off control:
prop:mds_bpc_tau = 100   Berendsen time constant for P control (fs)
prop:mds_bpc_P0  = 0     desired P (GPa)
prop:mds_bpc_scale = 100 scaling constant, usually on the order of bulk modulus
                        (GPa)

prop:mds_quench_tstart = 100
prop:mds_quench_rate   = 1.0 quenching rate (K/fs), negative value => heating

# -----
# MDS settings for reference compounds
# -----

# Use this to copy MDS settings for reference compounds from the general settings
# specified above:
# prop:ref:mds = prop:mds

prop:ref:mds_skint = 1.0      Angstrom
prop:ref:mds_seed  = 12345
prop:ref:mds_ndump = 10      dump info every ndump steps (if -dmdsprop option)

prop:ref:mds_tstart = 0.0
prop:ref:mds_tend   = 3000.0
prop:ref:mds_dt     = 5.0
prop:ref:mds_max_dt = 5.0

prop:ref:mds_Tstart = 1.0    starting temperature T (K)

# Negative values or missing settings turn off control:
prop:ref:mds_btc_tau = 20    Berendsen time constant for T control (fs)
prop:ref:mds_btc_T0  = 0     desired T (K)

# Negative values or missing settings turn off control:
prop:ref:mds_bpc_tau = 80    Berendsen time constant for P control (fs)
```



```
prop:ref:mds_bpc_P0      = 0      desired P (GPa)
prop:ref:mds_bpc_scale = 80      scaling constant, usually on the order of bulk modulus
                                (GPa)

prop:ref:mds_quench_tstart = 100
prop:ref:mds_quench_rate  = 1.0   # quenching rate (K/fs), negative value => heating

# #####
# Fitting potential(s)
# #####

pot:fitmet               = DL      options: CG, PM, GN, LM, DL, SM, DE, PS, BC, GS, or SA
pot:nitermin              = 5
pot:nitermax              = 100
pot:niterrestart         = 20      restart every 10th iteration

#### Negative values means that it will not be used when testing for convergence:
pot:functolabs            = 1e-5
pot:functolrel            = -1e-5
pot:gradtolabs            = 1e-5
pot:steptolabs            = 1e-5
pot:steptolrel            = -1e-5

pot:dogleg_radius         = 0.2
pot:dogleg_minradius      = 1e-5
pot:barrier_scale         = 0.0     barrier value
pot:simann_delta_rel      = 0.2
pot:use_data_scales       = false   scaling option

INFO:

# Gradient-based fitting methods:
# -----
# CG = conjugate gradients (ls)
# PM = Powell's method (ls)
# GN = Gauss-Newton (mi)
# LM = Levenberg-Marquardt (mi)
# DL = Powell's dog-leg method (mi) (usually most robust)
# SA = simulated annealing

#
# Population-based fitting methods:
# -----
# SM = simplex method
# DE = differential evolution
# PS = particle swarm method
# BC = bee colony method
# GS = gravitational search method

# mi: uses matrix inversion
# ls: uses line-search, usually implies slow fitting
```

The keyword `prop` is relevant to the calculations in which lattice parameter, cohesive energy, bulk modulus and other properties are calculated and/or fitted for the read-in structures using a given potential parameter set.

On the other hand, the keyword `pot` is relevant to the potential fitting itself, *i.e.* the evolution of the potential parameters.

6 Calculation of physical properties

Temperature T is obtained from the equipartition theorem:

$$\frac{3}{2}NkT = \sum_{i=1}^N \frac{1}{2}m_i v_i^2 \quad (32)$$

The pressure is obtained from the general stress tensor σ_{ab} ,

$$\sigma_{ab} = \frac{1}{2} \sum_i \sum_j F_{ij,a} r_{ij,b} \quad (33)$$

where $\mathbf{F}_{ij} \propto \mathbf{r}_{ij}$ and $\mathbf{r}_{ij} = \mathbf{r}_i - \mathbf{r}_j$. The Cartesian pressure components are $P_x = \sigma_{xx}, \dots$, and $P = (P_x + P_y + P_z)/3$.

Temperature and pressure is controlled according to the method of Berendsen et al. [2].

7 Calculation of fittable properties

Predicted value of a property with the read-in value P is written \tilde{P} . In order to simplify notation in this section the tilde will be omitted, with the understanding that all values used are based on the relaxed compounds. If a read-in value is used, it is written P^{ri} .

Predicted lattice parameter \tilde{a} (Ångströms) is calculated as

$$\tilde{a} = (\tilde{L}_1/L_1) \times a, \quad (34)$$

where a is the read-in lattice parameter in the compounds file (the file listing all the compounds to be used), L_1 is the initial length of the simulation box in the \mathbf{v}_1 direction, and \tilde{L}_1 is the relaxed length of the simulation box in the same direction.

L_i are determined from \mathbf{v}_i as $L_i = N_{\text{desired}}(i) \times v_i$, if the `Ndesired` option is used. Otherwise N_i is determined from the requirement $L_i = N_i v_i \geq 2\max(r_c)$, where $\max(r_c)$ is the largest cutoff radius between species present in the compound. In this calculations the

options `Neven_desired` and `Nodd_desired` are considered, if given in the compounds file.

Predicted lattice parameters $\widetilde{b}, \widetilde{c}$ are calculated in a similar way:

$$\widetilde{b} = (\widetilde{L}_2/L_2) \times b \quad (35)$$

$$\widetilde{c} = (\widetilde{L}_3/L_3) \times c \quad (36)$$

$$(37)$$

Ratios of lattice parameters:

$$\widetilde{b/a} = \frac{\widetilde{L}_2/L_2}{\widetilde{L}_1/L_1} \times b/a \quad (38)$$

$$\widetilde{c/a} = \frac{\widetilde{L}_3/L_3}{\widetilde{L}_1/L_1} \times c/a \quad (39)$$

Dimer bond length (Ångströms)::

$$\widetilde{r}_o = |\widetilde{\mathbf{r}}_2 - \widetilde{\mathbf{r}}_1| \quad (40)$$

Angle $\widetilde{\gamma}$ (in degrees), i.e. angle between primitive vectors $\widetilde{\mathbf{a}} = \widetilde{\mathbf{v}}_1$ and $\widetilde{\mathbf{b}} = \widetilde{\mathbf{v}}_2$:

$$\widetilde{\gamma} = \arccos \left(\frac{\widetilde{\mathbf{L}}_1 \cdot \widetilde{\mathbf{L}}_2}{\widetilde{L}_1 \widetilde{L}_2} \right) \cdot 1/(2\pi) \cdot 360 \quad (41)$$

Angle $\widetilde{\beta}$ (in degrees), i.e. angle between primitive vectors $\widetilde{\mathbf{a}} = \widetilde{\mathbf{v}}_1$ and $\widetilde{\mathbf{c}} = \widetilde{\mathbf{v}}_3$:

$$\widetilde{\beta} = \arccos \left(\frac{\widetilde{\mathbf{L}}_1 \cdot \widetilde{\mathbf{L}}_3}{\widetilde{L}_1 \widetilde{L}_3} \right) \cdot 1/(2\pi) \cdot 360 \quad (42)$$

Angle $\widetilde{\alpha}$ (in degrees), i.e. angle between primitive vectors $\widetilde{\mathbf{b}} = \widetilde{\mathbf{v}}_2$ and $\widetilde{\mathbf{c}} = \widetilde{\mathbf{v}}_3$:

$$\widetilde{\alpha} = \arccos \left(\frac{\widetilde{\mathbf{L}}_2 \cdot \widetilde{\mathbf{L}}_3}{\widetilde{L}_2 \widetilde{L}_3} \right) \cdot 1/(2\pi) \cdot 360 \quad (43)$$

Atomic volume (cubic Ångströms):

$$\widetilde{V}_a = \widetilde{V}_{tot}/N \quad (44)$$

where N is the number of atoms in the cell.

Cohesive energy (eVs):

$$\widetilde{E}_{coh} = \widetilde{E}_P/N < 0 \quad (45)$$

$$\widetilde{\Delta E}_{coh} = \widetilde{E}_{coh} - \widetilde{E}_{coh}^{ref} \quad (46)$$

Here N is the number of atoms in the compound, \widetilde{E}_P is the potential energy of the compound, and $\widetilde{E}_{coh}^{ref}$ is the cohesive energy of the reference compound, if used.

Formation energies are read in and calculated as "mixing energies", which is simply the formation energy normalized with the number of atoms in the cell. Hence the mixing energy (eVs) is:

$$\widetilde{E}_{mix} = \widetilde{E}_f/N \quad (47)$$

$$\widetilde{E}_f = \widetilde{E}_p - \sum_s N(s) \widetilde{E}_{coh}(s) \quad (48)$$

Here $N(s)$ is the number of atoms of species s in the compound, and $\widetilde{E}_{coh}(s)$ is the cohesive energy of the ground state of species s . Parametrization for species s must be given. For instance, if s is C, then ground state might be GRA (graphite).

Bulk modulus B (GPa) and its pressure derivative $B'(P)$ is calculated from $(V(\varepsilon), E_p(\varepsilon))$ data using the Birch-Murnaghan equation of state [3, 6]

$$E = E_0 + \frac{9}{16} V_0 B_0 \left(\left(\frac{V_0}{V} \right)^{2/3} - 1 \right)^2 \times \left[\left(\left(\frac{V_0}{V} \right)^{2/3} - 1 \right) B'_0 + 6 - 4 \left(\frac{V_0}{V} \right)^{2/3} \right] \quad (49)$$

The volume is $V(\varepsilon) = (1 + \varepsilon)V_0 = (1 + f)^3 L_1(0) L_2(0) L_3(0)$, with $f \in [-f_{max}, f_{max}]$, usually $f_{max} \sim 0.01$.

Each box — for a given value of f — may be allowed to relax (`prop:BM_rel_sys = yes`), or not (`prop:BM_rel_sys = no`).

Elastic constants C_{ij} (GPa) are calculated using volume-non-conserving strains ε_{ij} . Given a strain matrix

$$[\varepsilon_{ij}] = \begin{bmatrix} \varepsilon_{11} & \varepsilon_{12} & \varepsilon_{13} \\ \varepsilon_{21} & \varepsilon_{22} & \varepsilon_{23} \\ \varepsilon_{31} & \varepsilon_{32} & \varepsilon_{33} \end{bmatrix} \quad (50)$$

the transformation matrix is

$$F = 1_3 + [\varepsilon_{ij}] = \begin{bmatrix} 1 + \varepsilon_{11} & \varepsilon_{12} & \varepsilon_{13} \\ \varepsilon_{21} & 1 + \varepsilon_{22} & \varepsilon_{23} \\ \varepsilon_{31} & \varepsilon_{32} & 1 + \varepsilon_{33} \end{bmatrix} \quad (51)$$

Any ε_{ij} can take only three values: $-\varepsilon, 0, \varepsilon$. The exact structure of F depends on which elastic constants are being calculated.

The atomic positions are in essence transformed as

$$r' = Fr, \quad (52)$$

where r is a column vector containing the Cartesian coordinates x, y, z . From the calculations the data points $(\varepsilon, E_p(\varepsilon))$ are obtained. A second degree polynomial in strains is fitted to this data to obtain the elastic constants.

Each box — for a given value of ε — may be allowed to relax (`prop:C_rel_sys = yes`), or not (`prop:C_rel_sys = no`).

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The physical properties are not independent: e.g. a and V_a are dependent for a cubic lattice, since $V_a \propto a^3$. Specifying properties which are dependent on each other as fitting targets will most likely give rise to singular matrices when using a fitting method relying on matrix inversion, due to presence of zero-valued rows/columns.

8 Data fitting

Given compounds and their desired properties, as well as technical specifications on how to compute them, the program tries to obtain a best fit of potential parameters. The best fit is achieved by minimizing the merit/cost function

$$\chi^2 = \frac{1}{2} \sum_i f_i^2 \quad (53)$$

$$f_i = t_i \frac{\tilde{Y}_i - Y_i}{s_i} \quad (54)$$

Here

- the \tilde{Y}_i is the predicted value of property i which has the read-in (desired) value of Y_i ;
- the t_i is either a weight ($t_i = w_i$ if weight is used) or an inverse uncertainty ($t_i = 1/u_i$ if uncertainty is used); and
- the $s_i = 1$ if scales are not used (`use_data_scales = false` in the specifications file), and $s_i = Y_i$ if scales are used.

Defaults:

- Weights are used, with $w_i = 1$ for all i . Specifying weight or uncertainty for any property i overrides any default.
- Scales are used. If a property value is positive and less than machine accuracy then it is replaced by the machine accuracy. By using scaled properties all are on an equal footing.

Note: The weights w_i are normalized: $\sum_i w_i = 1$, so that properties using uncertainties have zero weight in this normalization sum.

★ ★ ★

Assume the predicted value is $\tilde{Y}_i = Y_i + \delta Y_i$, then $f_i = t_i(\tilde{Y}_i - Y_i)/s_i = t_i \delta Y_i / Y_i$ if scales are used, and $f_i = t_i \delta Y_i$ otherwise.

Suppose the relative deviation $\delta Y_i / Y_i \approx \delta Y_j / Y_j \approx 10\%$ for two properties i, j , e.g. lattice parameter, formation energy. If they are equally important to the fitting then $t_i = t_j$ and $f_i \approx f_j$ and these properties give equal contributions to the merit function.

Now consider the general case that the read-in values are vastly different, e.g. $Y_i = 1$ and $Y_j = 10^{-3}$. Using the former choice of scaling there is no dependence on the absolute values of the read-in property values, and we have no problems. If scales are not used, then the contributions to the merit function are $f_i = t_i$ and $f_j = t_j \times 10^{-3} = t_i 10^{-3}$ and there is a considerable relative difference, although both properties were assumed to be equally important. In this case property i will have a larger impact on the fitting process (assuming $J_{ik} \equiv \partial f_i / \partial x_k \approx J_{jk}$).

★ ★ ★

Consider now the use of any of the deprecated options, e.g. `Fmax`. This option may be used to try to guide the fitting process to accept parametrizations giving small forces of relaxed compounds. Assume $t_i = 1$ and that scaling is used, so $s_i = Y_i$.

(1) Case $\tilde{Y}_i \gg Y_i$: Now

$$f_i = \frac{\tilde{Y}_i - Y_i}{Y_i} = \tilde{Y}_i / Y_i - 1 \sim \tilde{Y}_i / Y_i \gg 1 \quad (55)$$

E.g. `Fmax` = 10^{-10} and the predicted value is e.g. 10^{-5} :

$$f_i \sim 10^{-5}/10^{-10} = 10^5 \quad (56)$$

i.e. probably much larger than for any of the conventional properties. In a gradient-based search the moves in parameter space will tend to focus on minimizing the forces, paying less attention to other properties, e.g. differences in cohesive energies.

(2) Case $\tilde{Y}_i \ll Y_i$: Now

$$f_i = \frac{\tilde{Y}_i - Y_i}{Y_i} = \tilde{Y}_i/Y_i - 1 \sim 1 \quad (57)$$

E.g. $F_{\max} = 10^{-3}$ and the predicted value is e.g. 10^{-5} . Only in this case will the contribution be manageable.

In the general case the predicted forces could be very small. And in the general case we also want force values close to zero (read-in force values). Involving very small values and especially their ratios in the calculations is not desirable.

Conclusion: Do not use F_{\max} , P_{\max} or $displ_{\max}$. Rely on the MD relaxation instead, to provide zero forces and zero pressure. In fact, the MD run can be made to scale the pressure to any desired value (`mds_bpc_P0`), so it's better to use that one.

★ ★ ★

The **gradient** of the merit function is

$$g_j = \frac{\partial \chi^2}{\partial x_j} = \sum_i f_i \frac{\partial f_i}{\partial x_j} \equiv \sum_i f_i J_{ij} = \sum_i J_{ji}^T f_i = -h_j \quad (58)$$

where h_j are components of the **antigradient**, and

$$J_{ij} = \frac{\partial f_i}{\partial x_j} = \frac{t_i}{s_i} \frac{\partial \tilde{Y}_i}{\partial x_j} \quad (59)$$

9 Convergence conditions

Convergence criteria in the technical specifications file are of the form (`prop`, for fitting compound properties):

<code>prop:functolabs = 1e-5</code>	convergence when absolute merit function value is less than this
<code>prop:functolrel = -1e-5</code>	... change in merit function value ...
<code>prop:gradtolabs = 1e-5</code>	... absolute gradient value ...
<code>prop:steptolabs = 1e-5</code>	... absolute step size ...
<code>prop:steptolrel = -1e-5</code>	... change in step size ...

Note: A **negative** value means that criterion is **not used**.

- `functolabs` refers to $\min(|\chi^2|)$
- `functolrel` refers to $\min(|\Delta\chi^2|/|\chi^2|)$, where Δ signifies the change (in the merit function in this case) during the last step.
- `gradtolabs` refers to $\min(|\nabla_x\chi^2|)$, where $\nabla_x\chi^2$ is the gradient of the merit function with respect to the parameters.
- `steptolabs` refers to $\min(|\mathbf{h}|)$, where \mathbf{h} is the last step taken in parameter space.
- `steptolrel` refers to $\min(|\Delta\mathbf{h}|/|\mathbf{h}|)$

10 Parameters

The parameters are x_1, x_2, \dots, x_M .

Parameter limits $x_i^{\min} = x_i^{\max} = 0$ means that the parameter is **unconstrained** and can vary freely in the interval $(-\infty, \infty)$.

The limits $x_i^{\min} = x_i^{\max} \neq 0$ means that the parameter is **fixed**. The default for any parameter is $x_i^{\min} = x_i^{\max} = 1$.

The limits $x_i^{\min} < x_i^{\max}$ means that the parameter is **constrained** in the given interval.

11 Constraint method

In order to forcibly constrain parameter values a barrier penalty function can be used. The option `barrier_scale = μ` with a value > 0 switches on the penalty function U :

$$U = - \sum_i \mu \ln \left\{ \frac{1}{s_i} \left(\left[\frac{1}{2}(x_i^{\min} - x_i^{\max}) \right]^2 - \left[x_i - \frac{1}{2}(x_i^{\min} + x_i^{\max}) \right]^2 \right) \right\} < 0 \quad (60)$$

The total cost function is then

$$\chi_{\text{tot}}^2 = \chi^2 + U \quad (61)$$

A complication with this scheme is that with small weights w_i one may get $\chi_{\text{tot}}^2 = \chi^2 + U < 0$. This may interfere with the convergence criteria $\min(|\chi^2|)$, since $\chi_{\text{tot}}^2 < 0 < \min(|\chi^2|)$ as soon as $|U|$ starts to dominate over $|\chi^2|$.

With $\mu = 0$ the program still tries to stop parameter values from going outside their limits, but a penalty function is not used.

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