

Lab Number 4  
EEE 108L – Electronics I - Laboratory  
Diode Circuits (One week)

Background

The purpose of this laboratory is to introduce what is most likely your first semiconductor device. The diode is the simplest two terminal semiconductor in common use. While there are many types of diodes, this laboratory will investigate the nonlinear characteristics of a small signal diode.

Preliminary Calculations:

1. Find the majority carrier (n) and minority carrier (p) concentration of in n-type silicon that has been doped with a donor level of  $N_D = 1 \times 10^{15} / \text{cm}^3$ .
2. Find the majority carrier (p) and minority carrier (n) concentration of p-type silicon that has been doped with an acceptor level of  $N_A = 1 \times 10^{17} / \text{cm}^3$ .
3. Assume you are making a PN diode from the p and n-type semiconductors discussed above; Calculate the built-in potential.
4. Use the exponential diode model of diode. Assume  $I_S = 2 \times 10^{-14}$  A. Plot  $I_D$  vs  $V_D$  from  $100\text{mV} \leq V_D \leq 900\text{mV}$ . Take at least 50 points.
5. Calculate  $r_d$  at  $V_D = 0.4, 0.5, 0.6, 0.7$ , and  $0.8\text{V}$ .
6. For the circuit of Figure 1, find an expression for the diode currents  $I_{D1}$  and  $I_{D2}$  in terms of  $V_{BIAS}$ ,  $R_{BIAS}$  and  $R$ . You may assume that  $V_D = 0.7\text{V}$  and that the  $C_S$  prevents DC current from flowing through the function generator.
7. Find an expression for the small-signal gain  $V_{OUT}/V_{IN}$  for the circuit of Figure 1 in terms of the diode small-signal resistance (let  $r_d = r_{d1} = r_{d2}$ ) and  $R$ . Ignore  $R_{BIAS}$  here since it is much greater than any of the other resistances in the circuit.

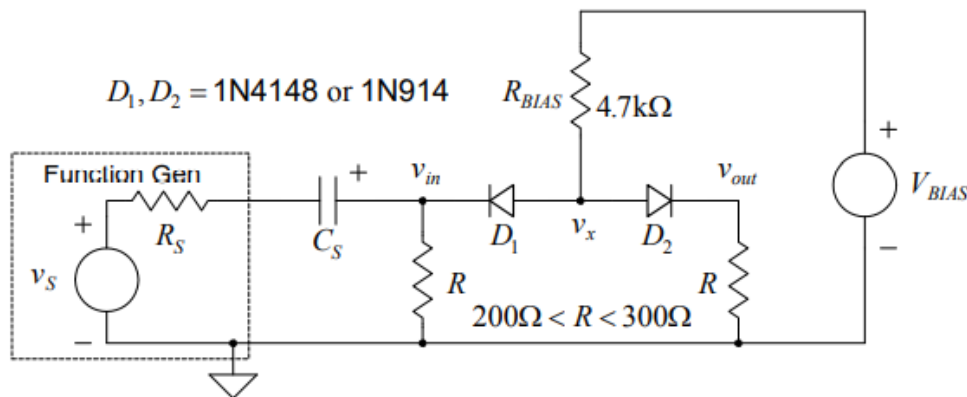


Figure 1.

### SPICE Simulations:

1. Enter the circuit of Figure 1 into SPICE. Select  $C_S$  between 2  $\mu\text{F}$  and 10  $\mu\text{F}$ . Set  $V_{\text{BIAS}} = 6\text{V}$ . Set  $v_s$  to zero for this step. The default value for  $R$  is 240  $\Omega$ . Make sure that the simulation setup enables the bias point detail.
2. Run Bias point simulation, compare the simulated diode bias current to the values calculated in preliminary calculation.
3. Now for transient, set  $V_{\text{BIAS}} = 6\text{V}$ ,  $v_s = 50\text{mV}$  peak sine wave at 10kHz, and  $R_S = 50\Omega$ , final time =  $4 \times 10^{-4}$  seconds and the maximum step size to  $1 \times 10^{-7}$  seconds.
4. Perform transient analysis. Display  $v_{\text{in}}$  and  $v_{\text{out}}$ .
5. Calculate the small-signal gain  $v_{\text{out}}(\text{p-p}) / v_{\text{in}}(\text{p-p})$  (not  $v_{\text{out}}/v_s$ ).

### Laboratory Measurements:

1. Construct the circuit of Figure 1. Connect the +ve side of  $C_S$  to  $V_{\text{in}}$ . Set  $V_{\text{BIAS}}$  to +6V. (-V= -1V and +V=5V total 6V)
2. With no AC signal applied, verify that the DC bias voltages  $V_{\text{IN}}$  and  $V_{\text{OUT}}$  are within  $\pm 5\text{mV}$  of each other. This check will make sure that the diodes are well matched.
3. Verify that the currents  $I_{D1}$  and  $I_{D2}$  are reasonably close to their calculated values.
4. Set  $V_{\text{in}}$  a triangle waveform, equal to  $160\text{mV}_{\text{pp}}$  at 10 kHz.
5. Vary  $V_{\text{BIAS}}$  and observe how do the AC magnitudes at  $V_{\text{in}}$  and  $V_{\text{out}}$  change as  $V_{\text{BIAS}}$  is changed? How to the DC voltages  $V_{\text{in}}$  and  $V_{\text{out}}$  change as  $V_{\text{BIAS}}$  is changed?
6. For at least 10 values of  $V_{\text{BIAS}}$ , measure  $\text{Gain} = V_{\text{out}}/V_{\text{in}}$ . Make a table and sketch a plot of measured gain as a function of  $V_{\text{BIAS}}$ .
7. With  $V_{\text{BIAS}} = 4\text{V}$ , increase the amplitude of the input signal until  $V_{\text{out}}$  shows noticeable clipping at the top and bottom peaks.
8. For at least 10 values of  $V_{\text{BIAS}}$ , record the positive and negative clipping levels corresponding to each value of  $V_{\text{BIAS}}$ . Make a table.

## SOME USEFUL EQUATIONS

### Background:

The diode is a nonlinear device with defined regions of operation. For the diode, we should define at least three regions of operation

- reverse current saturation,
- forward current operation up to the “knee”
- forward current after the “knee”.

The ideal diode equation is: 
$$i_D = I_S \left( e^{\frac{v_D}{nV_T}} - 1 \right)$$

- $I_S$  is the reverse saturation current up to the breakdown voltage for the diode.
- $n$  is the ideality factor for the diode (ideal = 1, normal is  $1 \leq n \leq 2$ )
- $V_T$  is the “thermal voltage” given by  $V_T = kT/q = 26 \text{ mV}$  at room temperature.

### The diode large-signal model

The large-signal model relates the diode current  $I_D$  to the diode voltage  $V_D$ . A good large signal model for a diode in forward bias is given by:

$$I_D = I_S \exp\left(\frac{V_D}{nV_T}\right) \quad \text{OR} \quad V_D = nV_T \ln\left(\frac{I_D}{I_S}\right).$$

- Where  $I_S$  is the diode saturation current and is about  $25 \times 10^{-9} \text{ A}$  for the 1N914
- $V_T$  is the thermal voltage (at room temperature, about 26mV and PSPICE defaults to 25.8mV),
- $n = 1.836$ .
- if the voltage across the resistor is more than about 2 volts.  $V_D = 0.7 \text{ V}$  is acceptable for most purposes.

### The diode small-signal model

The small-signal model relates the change in the diode current  $I_D$  to the change in the diode voltage  $V_D$ . This property can be modeled by the diode's small-signal resistance, defined as

$r_d = \frac{\Delta V_D}{\Delta I_D} = \frac{v_d}{i_d}$ . The small-signal conductance can be derived from the large-signal model above

as follows:  $g_d = \frac{dI_D}{dV_D} = \frac{I_D}{nV_T}$ , hence  $r_d = \frac{1}{g_d} = \frac{nV_T}{I_D}$ .

The diode's small-signal resistance could be expressed as a function of  $V_D$ , but the calculations are less sensitive to error when  $r_d$  is calculated from  $I_D$ .