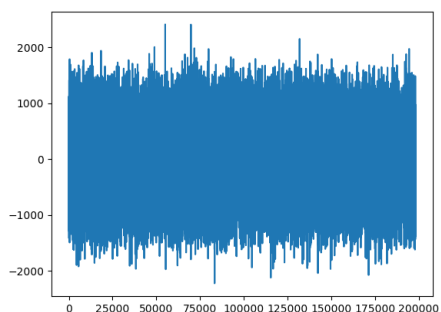


HEXANE WATER RESULTS LOG SUMMER 2018 (AUGUST-PRESENT)

KIRK SWANSON

1. 8/6/2018

- (1) Downloaded pressure_scalar-press-NPT-1bead-water-lammps to dash_work/interface on laptop. Used pressure_analysis_UPDATE.py leaving out first 2000 records and used 198 blocks 5 ps to get average pressure of 1.41, SE 0.94, SD 511.08:



- (2) Because we accidentally used restart/traj every 1,000 for fulldata-NPT-298 and then restart/traj 10,000 for fulldata-NPT-298-restart1, we will re-do this calculation again using the updated interface file collecting restart/traj every 1,000.
- (3) Submitted simulation no. 1.
- (4) To check pressures in a non-vacuum interfacial system, in DASH we are going to run simulation no. 2, which does NPT equilibration for 200,000 steps and then does an NVT simulation of the interface. Filename press-nonexpanded.
- (5) Submitted simulation no. 2.
- (6) We want to compare the above simulation to LAMMPS, so we will first run the equilibration step in LAMMPS as simulation no. 3. Note, however, that the mixing rules currently used in the LAMMPS file are arithmetic. Also NOTE: to use depablo-tc, must type module load openmpi into terminal first, even if it is already in submit script. After this, we need to run the NVT portion of the simulation for 6M steps.
- (7) Running simulation no. 3.
- (8) Now, let's turn to how pressure is typically computed in DASH. In general, an ideal gas mechanical equation of state is given by

$$P = \frac{Nk_B T}{V} = \rho k_B T \quad (1.1)$$

This assumes that molecules in the gas are point-like and do not interact with each other. However, if interactions between the particles and a finite particle volume is allowed. The virial expansion is a perturbation theory around the ideal gas used when the interactions in the real gas are dominated by two-body interactions. One uses a virial expansion in powers of the density, keeping the temperature dependence of the coefficients. We can then apply manipulations of the time derivative of the classical virial to arrive at

$$P = \rho k_B T - \left[\frac{1}{3V} \left\langle \sum_{i < j}^N r_{ij} F_{ij} \right\rangle \right] \quad (1.2)$$

where the second term is called the virial correction.

- (9) In DASH, it appears as though `DataComputerPressure.cu` is responsible for scalar pressure values. On line 92, we have

$$pressureScalar = (tempScalar_loc * ndf_loc * boltz + sumVirial) / (dim * volume) * state - > units \quad (1.3)$$

`tempScalar_loc` appears to be the temperature of the system, `boltz` is the boltzmann coefficient, `sumVirial` is that second virial correction, `dim` is the dimension of the system. `ndf` I calculated to be 3 per atom, including M sites for the water model (printed values using interface file). So, it does make sense to divide by `dim`, i.e. divide by 3, because that gets us to N. However, we are also including M-sites in the pressure value. So, we are at the very least overcounting the ideal gas term for the pressure. The amount of overcorrection for 3650 water molecules is given by:

$$P_c = \frac{N k_B T}{V} = \frac{3650 \times 1.38 \times 10^{-23} \times 298}{50 \times 10^{-10} \times 50 \times 10^{-10} \times 150 \times 10^{-10}} \quad (1.4)$$

Actually, would it even be incorrect to have four sites per atom? Maybe that's actually the correct ideal model here?

2. 8/7/2018

- (1) First, we will begin by compiling the most recent version of DASH, which should contain Mike's edits to the TIP4P/F fix for accurate pressure computation (avoiding M-site in ideal gas term). Compiling version in folder DASH-8-7-2018.
- (2) DASH pressure computations:

NVT with vacuum: `run_UPDATE_8-7-2018.sh` and `interface_UPDATE_8-7-2018.py`, z length 149.2717, x length 58.45467, y length 58.67825, 3650 TIP4P/F water molecules, 500 hexane molecules, waldman-hagler mixing between the water and hexane molecules, NVT with Andersen thermostat with parameters `nu = 0.01` (a parameter describing the collision frequency of the system with the heat bath) and applying every 10 steps, 298 K, 1M steps equilibration and 1M steps production, `PI false`, `restart/traj` every 10,000, -20/+20 for z change as accounted above, filename `newpress-expanded`, tensor information commented out in input script. This is simulation no. 4.

We will do the same as above, except we will not expand the box by 20 Å in each z direction, and we will apply NPT equilibration for 1M steps and then 1M steps of NVT. This is simulation no. 6.

(3) LAMMPS pressure computations:

NVT with vacuum: interface.sbatch and in.taffi_tip4pF_waldman, x length 149.2717, y length 58.67825, z length 58.45467, 3650 TIP4P/F water molecules, 500 hexane molecules, waldman-hagler mixing, NVT with NoseHoover, 298 K, 1M steps equilibration and 1M steps production, PI false, restart/traj every 10,000, filename newpress-expanded-lammps. We will start with 500,000 steps and restart from there, which is simulation no. 5.

Same as above, except we will not expand the box by 20 Å in each z direction, and we will apply NPT equilibration for 1M steps and then 1M steps of NVT. The first 500,000 steps will be simulation no. 7.

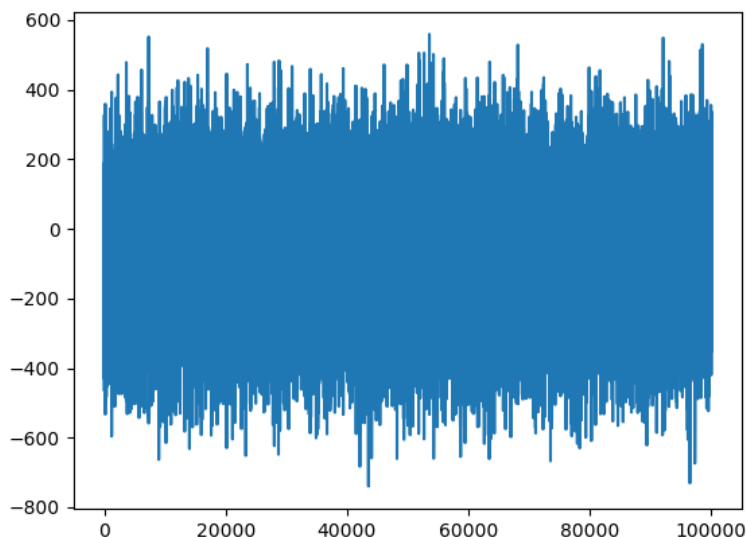
Simulation no. 8 is filename newpress-expanded-lammps-restart1, restarting from newpress-expanded-lammps.restart for 1.5M steps

Simulation no. 9 is filename newpress-nonexpanded-lammps-restart1, restarting from newpress-nonexpanded-lammps.restart for 500K steps

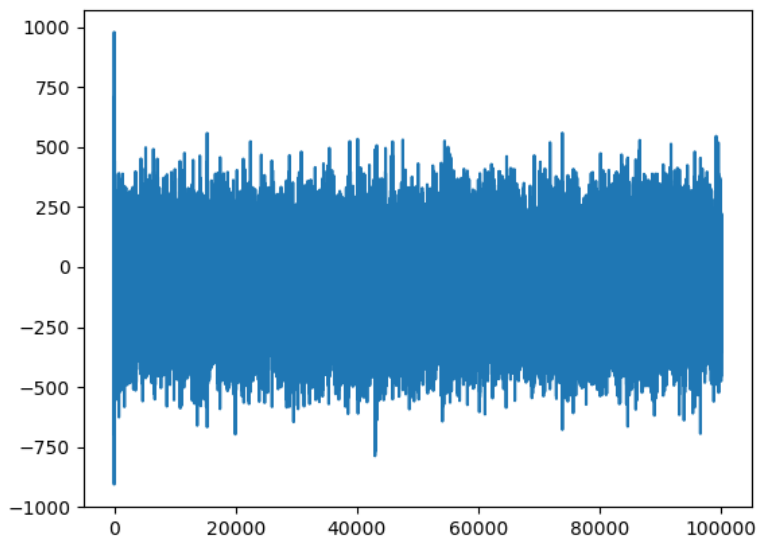
Simulation no. 10 is filename newpress-nonexpanded-lammps-restart2, restarting from newpress-nonexpanded-lammps-restart1.restart, and going for 1M NVT steps.

3. 8/8/2018

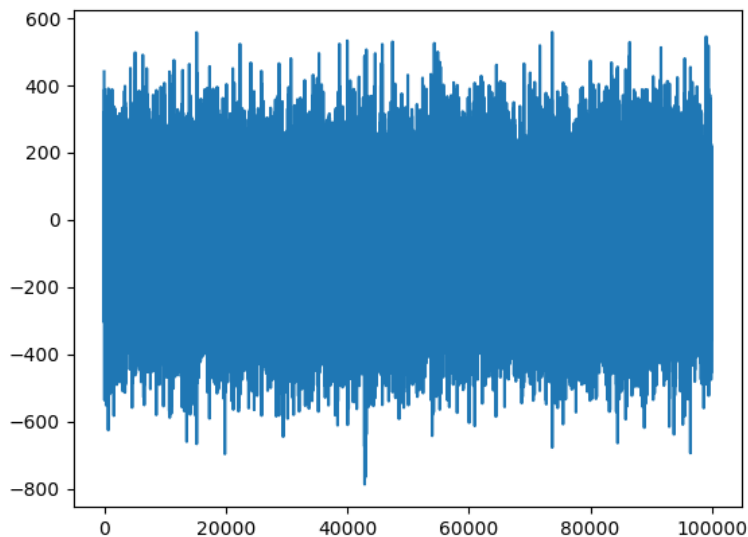
- (1) From simulation no. 8, we use pressure_analysis_UPDATE.py on laptop in dash_work/interface folder to analyze pressures_scalar-newpress-expanded-lammps-restart.txt. We use indices 50,000 to 150,000 and 100 SE blocks of size 5 ps. This gives us a mean pressure of -83.443 atm, SE of the mean 1.578 atm, and SD of the distribution 154.699 atm. Here is a plot of these values over time:



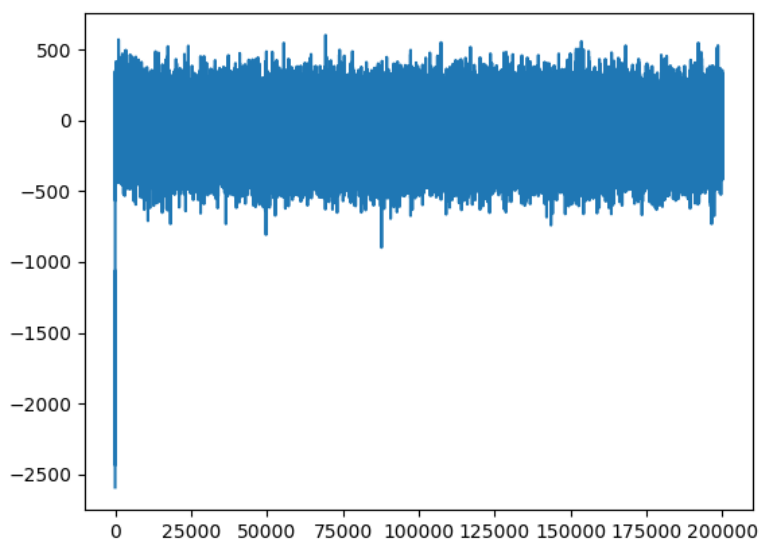
- (2) From simulation no. 4, we use `pressure_analysis_UPDATE.py` on laptop in `dash_work/interface` to analyze `pressure_scalar-newpress-expanded.txt`. We use indices 100,000 to 200,000 and 100 SE blocks of size 5 ps. This gives us a mean pressure of -70.603 atm, SE of the mean 1.487 atm, and SD of the pressures 154.854. Here is a plot:



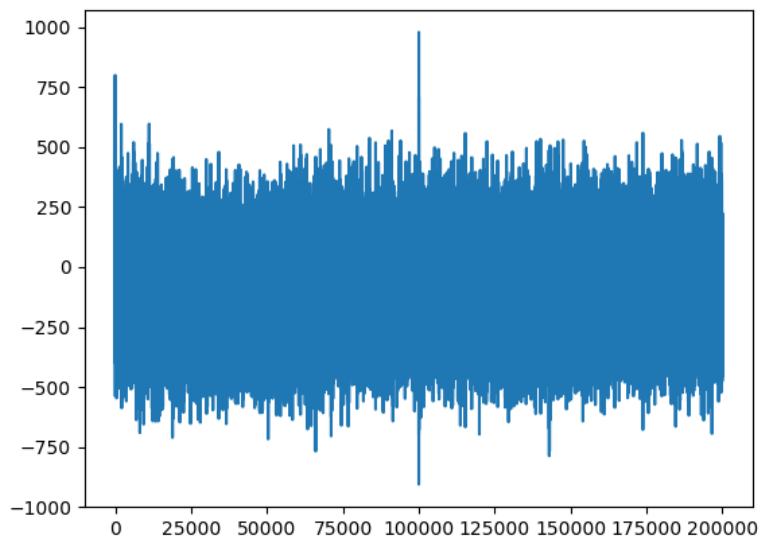
Removing the first 100 values for better comparison to the above plot, we have:



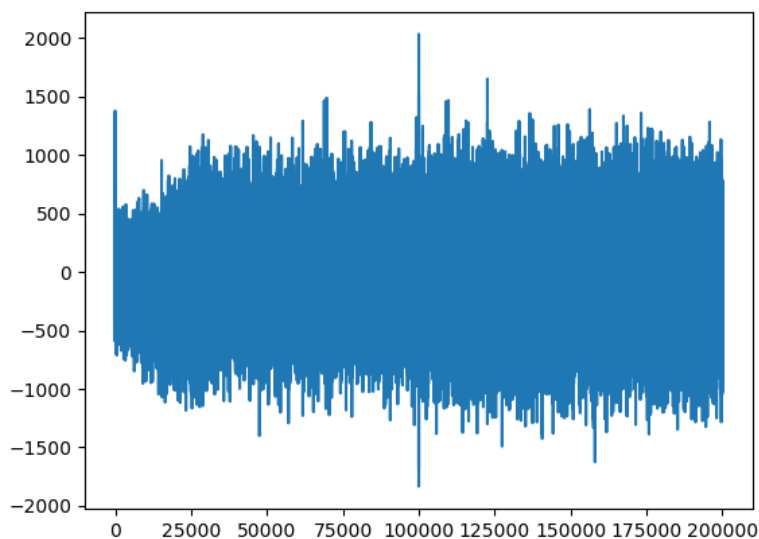
- (3) If we combine pressures_scalar-newpress-expanded-lammps.txt and pressures_scalar-newpress-expanded-lammps-restart1.txt, then we have all 2M steps covered. We call this file pressures_scalar-newpress-expanded-lammps-combined.txt. Analyzing all points in this file, using 200 blocks of size 5 ps, we get an average pressure of -80.945, SE of the mean 1.237, and SD of values 156.056:



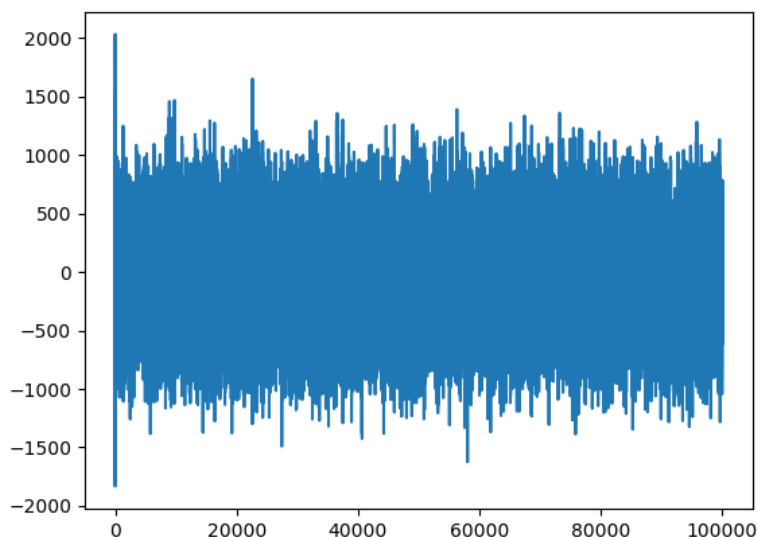
- (4) Using all values from pressures_scalar-newpress-expanded.txt from DASH, using 200 blocks as well, we get a mean pressure of -77.716, SE of the mean 1.337, and SD of values 155.610:



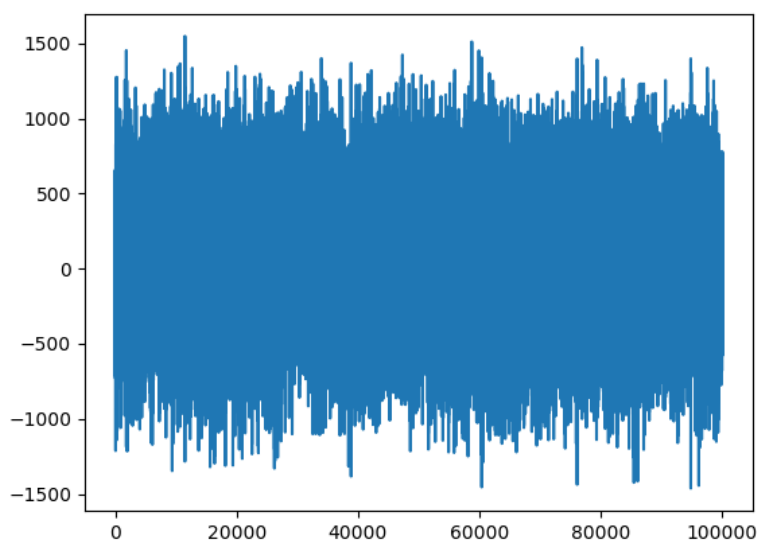
- (5) Andersen Thermostat: Rescales velocities at regular timesteps to control the temperature
- (6) NoseHoover Thermostat: Integrates equations of motion derived from a Hamiltonian that has an extra degree of freedom for the heat bath
- (7) From simulation no. 6, in DASH, we did 1M NPT steps followed by 1M NVT steps so that we can analyze pressure from the NVT which will not have vacuum, in theory. The box dimensions we get from this simulation are: x length 48.875, y length 49.061, z length 91.3641. Downloading pressure_scalar-newpress-nonexpanded.txt to dash_work/interface on laptop for analysis as above. Using the 1M NPT plus 1M NVT data and 200 blocks, we have a mean pressure of -31.943, SE of the mean 3.174, and SD of values 333.460:



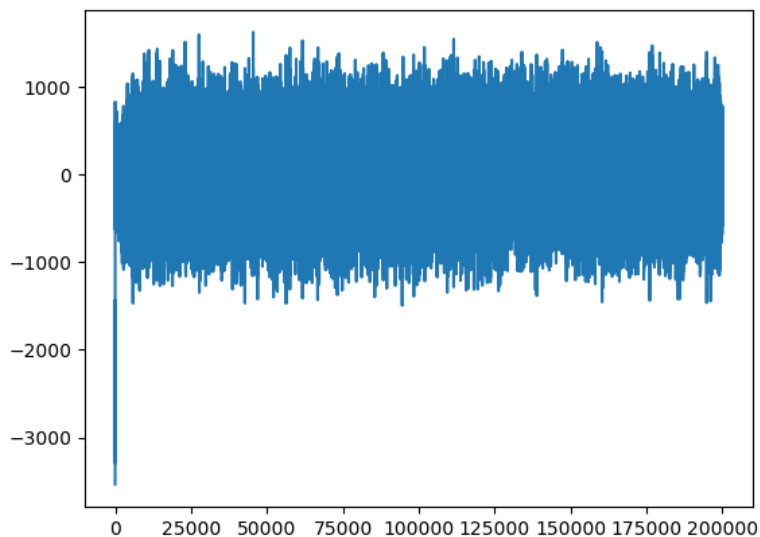
Using only the 1M NVT steps, and 100 blocks, we have a mean pressure of -32.501, SE of the mean 3.592, SD of values 364.244:



- (8) From simulation no. 10, in LAMMPS, we did 1M NVT steps after 1M NPT equilibration. The box dimensions are: x length 90.498, y length 48.597, z length 48.412. These lengths are slightly different from the above DASH simulation. The NVT component of the simulation, from pressures_scalar-newpress-nonexpanded-lammps-restart2.txt, we get a mean pressure of 54.504, SE of the mean 4.47, and SD of values 375.729, using 100 blocks:

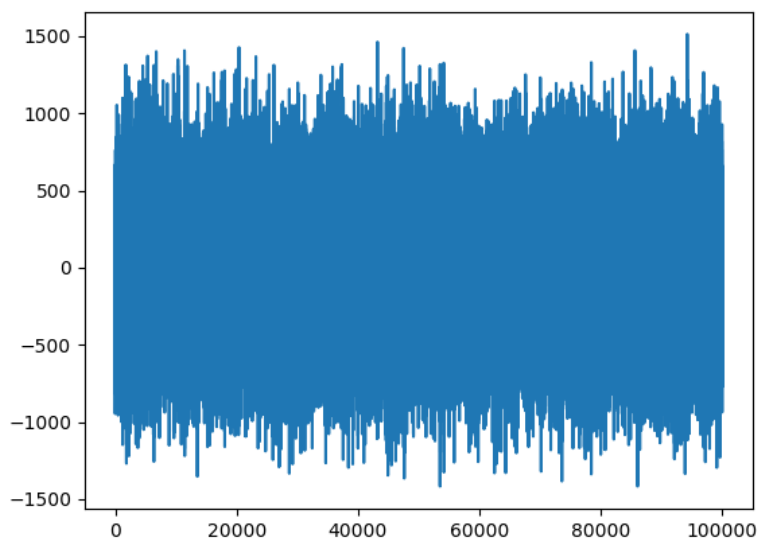
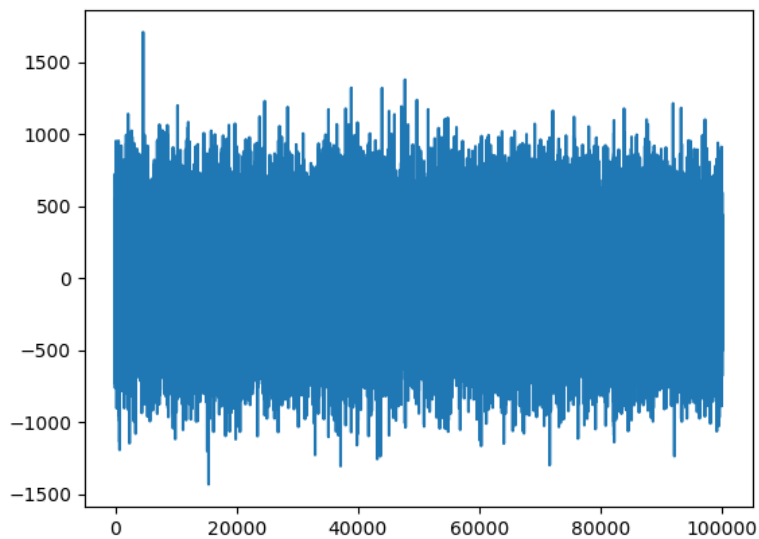


Combining the NPT steps into pressures_scalar-newpress-nonexpanded-lammps-combined.txt, we get a mean pressure of 25.947, SE 3.152, and SD 374.379 using 200 blocks:



- (9) It is possible that we have differing values here because the volumes are slightly different. To test the hypothesis that the vacuum is responsible for the negative pressure, let's try decreasing the volume by only putting 10 Angstroms on each side of the simulation box.
- (10) Simulation no. 11 in DASH will take care of this filename newpress-smallexpanded, and simulation no. 12 in LAMMPS will do the same.
- (11) Simulation no. 13 will be DASH 2M NPT of the interface
- (12) Simulation no. 14 will be LAMMPS NPT of the interface
- (13) Simulation no. 15 will be DASH 2M NVT at 0.997 of TIP4P/F 3650 molecules
- (14) Simulation no. 16 will be 2M NPT at 1 atm of 3650 molecules in DASH

4. 8/9/2018



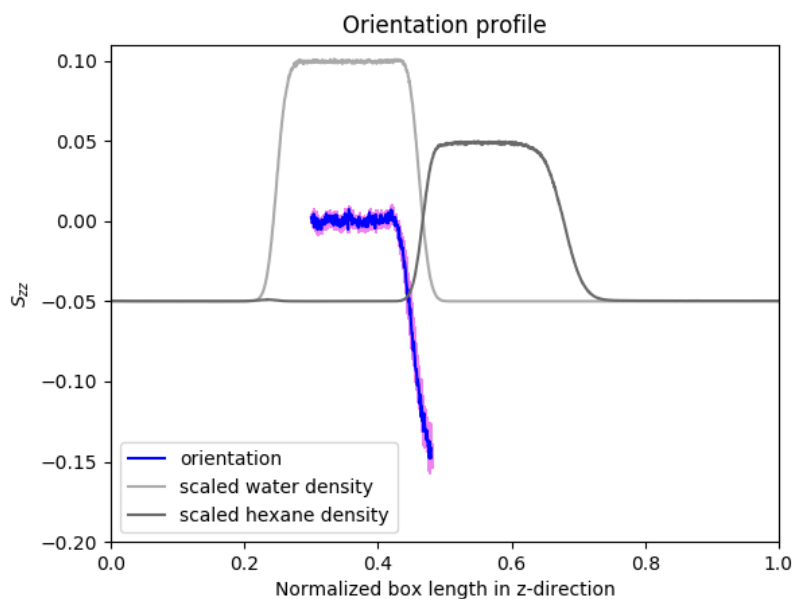
(1)

5. 8/11/2018

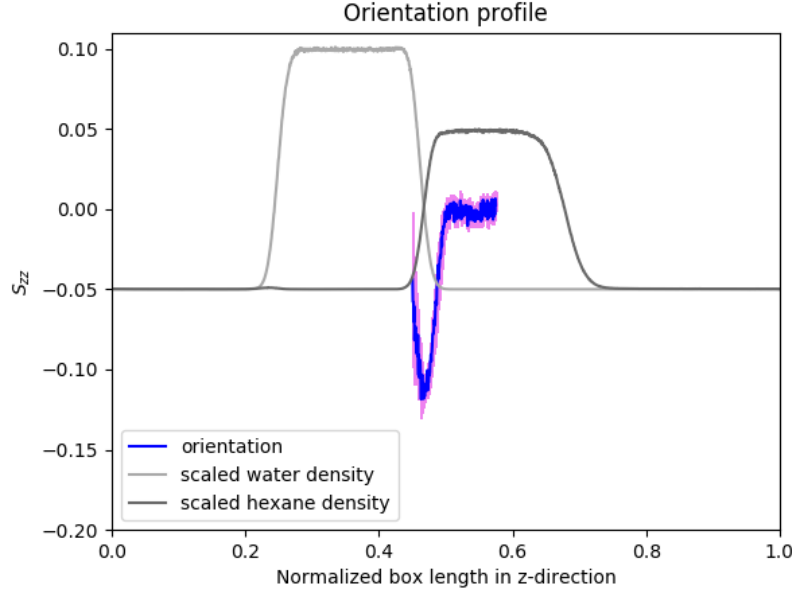
- (1) First, we need to re-do molecular orientation plots. The file `molecular_orientation_water_postproduc` contains the unwrap update that is necessary for accurate analysis. In this file, we correctly unwrap molecules based on the location of the oxygen atom. In

dash_work/interface on Midway, we will use orientation_postproduction.sbatch to do water orientation postproduction profiles from the 1bead trajectory, full-298-1bead, and the 32 bead trajectory, full-298-32bead-combined.xyz. The filename for 1bead is orientations_water_unwrap.txt, which once downloaded to laptop was copied as orientations_water_full-298-1bead-orientations-water.txt. The filename for 32bead is orientations_water_32bead-water-unwrap.txt.

- (2) For full-298-1bead, we used indices 600 to 960:



- (3) We also corrected molecular_orientation_hexane_postproduction_UPDATE.py to have the appropriate unwrapping procedure. We use this in orientation_postproduction_hexane.sbatch to analyze the same trajectory files as above for hexane. The 1bead file is orientations_hexane_full-298-1bead-orientations-hexane-corrected.txt. We download this onto laptop and use indices 900 to 1150 to obtain:



We are also running the 32 bead version, named as above, orientations_hexane_full-298-32bead-orientations-hexane-corrected.txt.

- (4) We recently resolved the negative pressure issue. Let's start from Section 2.5 of The Molecular Theory of Capillarity, by J. S. Rowlinson and B. Widom. The assumption we begin with is that it is possible to consistently define local values of the thermodynamic fields p, T, μ even in an inhomogeneous system. At a planar fluid-fluid interface, confined to a cube of sidelength l and interfacial area $A = l^2$, these fields and densities are functions only of the z dimension, defined as normal to the interfacial plane. We call the pressure in either bulk phase the scalar quantity p . Near the interface the pressure is a tensor since its tangential components, parallel with a dividing surface, include the tension of the interface, and so differ from the normal component. Mechanical stability requires that the gradient of this tensor is zero everywhere in the fluid, $\nabla \cdot \vec{p} = 0$, and the symmetry of the surface requires that \vec{p} is a diagonal tensor, $\vec{p}(\vec{r}) = p_{xx}(\vec{r})e_x e_x + p_{yy}(\vec{r})e_y e_y + p_{zz}(\vec{r})e_z e_z$ with $p_{xx}(\vec{r}) = p_{yy}(\vec{r})$. Substitution of this equation into the gradient equation yields $p_{zz}(z) = p_{yy}(z) = p_T(z)$ and $p_{zz}(z) = p_N(z) = p$, where p_N and p_T are the normal and transverse components of the pressure. If a side-wall of the cube is displaced isothermally and reversibly so as to increase the area by δA , then the tangential work done on the system is $\delta W_T = -\delta A \int_{-l/2}^{l/2} p_T(z) dz$. A similar displacement of the top or bottom wall by a distance $\delta A/l$ serves to maintain the volume constant, and requires further (normal) work $\delta W_N = A(\delta A/l)p = l\delta A p$. Thus, the total work done, and hence the increase in free energy, is $\delta F = \delta W_T + \delta W_N = \delta A \int_{l/2}^{l/2} [p - p_T(z)] dz$. Using $dF = -SdT - pdV + \gamma dA + \mu dN$. So, we can associate this integral with the interfacial tension.

- (5) This brings us to the following. We define the interfacial tension as $\gamma = \int_0^{L_z} [p_N(z) - p_T(z)] dz$. Since at a stable planar interface the gradient of the pressure tensor must be zero, the tensor must be symmetric, and the bulk pressures have scalar value p , we can define $p_N(z) = p_{zz} = p$ and $p_T(z) = \frac{p_{xx}(z) + p_{yy}(z)}{2}$. Using the mean value theorem, we can write the average pressure tensor elements obtained from an MD simulation, $\langle p_{xx} \rangle = p_{xx}$ and $\langle p_{yy} \rangle = p_{yy}$ as $p_{xx} = \frac{1}{L_z} \int_0^{L_z} p_{xx}(z) dz$ and $p_{yy} = \frac{1}{L_z} \int_0^{L_z} p_{yy}(z) dz$. We can then carry out the integration that defines γ and rewrite the interfacial tension as $\gamma = (p - \frac{p_{xx} + p_{yy}}{2}) L_z$, which is the standard formula for computing interfacial tension in molecular simulations. In our simulation box, we have two interfaces, so the interfacial tension associated with a single interface can be given by dividing by two: $\gamma = \frac{1}{2} (p - \frac{p_{xx} + p_{yy}}{2}) L_z$. We assume that the bulk phases are at their equilibrium densities corresponding to $p \approx 1 \text{ atm}$, either by measuring the bulk densities in an NVT simulation or by applying a barostat in the z dimension to maintain $p \approx 1 \text{ atm}$. For hexane-water, the experimental interfacial tension is $50 \frac{mN}{m} = 4,900 \text{ atm} \cdot \text{\AA}$. Our simulation box is approximately 100 \AA in the z dimension, so, we have $4,900 \text{ atm} \cdot \text{\AA} = (1 \text{ atm} - \frac{p_{xx} + p_{yy}}{2}) \cdot 100 \text{ \AA}$. We can solve this to get $p_{xx} + p_{yy} = -194$. Since the scalar pressure in an MD simulation is computed as $P_{tot} = \frac{p_{xx} + p_{yy} + p_{zz}}{3}$, we have $P_{tot} = -64.33$. What happens to these negative scalar pressures in the thermodynamic limit? In ambient conditions, γ would still be $50 \frac{mN}{m}$ and $p = 1 \text{ atm}$, but $L_z \rightarrow \infty$, so $\lim_{L_z \rightarrow \infty} \frac{\gamma}{L_z} = 0$, which implies that $\frac{p_{xx} + p_{yy}}{2}$ converges to p and $P_{tot} \rightarrow 1$.

$$\gamma = \int_0^{L_z} [p_N(z) - p_T(z)] dz \quad (5.1)$$

$$p_N(z) = p_{zz} = p \quad (5.2)$$

$$p_T(z) = \frac{p_{xx}(z) + p_{yy}(z)}{2} \quad (5.3)$$

$$= \frac{1}{2} \left(p - \frac{p_{xx} + p_{yy}}{2} \right) L_z \quad (5.4)$$

$$p_{xx} = \langle p_{xx}(z) \rangle = \frac{1}{L_z} \int_{-L_z/2}^{L_z/2} p_{xx}(z) dz \quad (5.5)$$

$$4,900 \text{ atm} \cdot \text{\AA} \approx \frac{1}{2} (1 \text{ atm} - \frac{p_{xx} + p_{yy}}{2}) \cdot 100 \text{\AA} \quad (5.6)$$

$$p_{xx} + p_{yy} \approx -194 \quad (5.7)$$

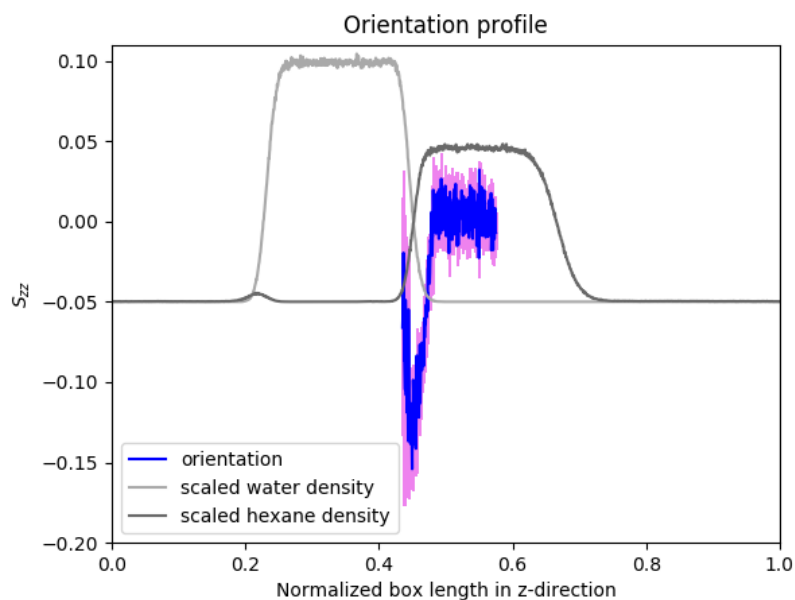
$$P_{\text{tot, MD sim.}} = \frac{p_{xx} + p_{yy} + p_{zz}}{3} \approx -65 \text{ atm} \quad (5.8)$$

$$\lim_{L_z \rightarrow \infty} \frac{\gamma}{L_z} \rightarrow 0 \quad (5.9)$$

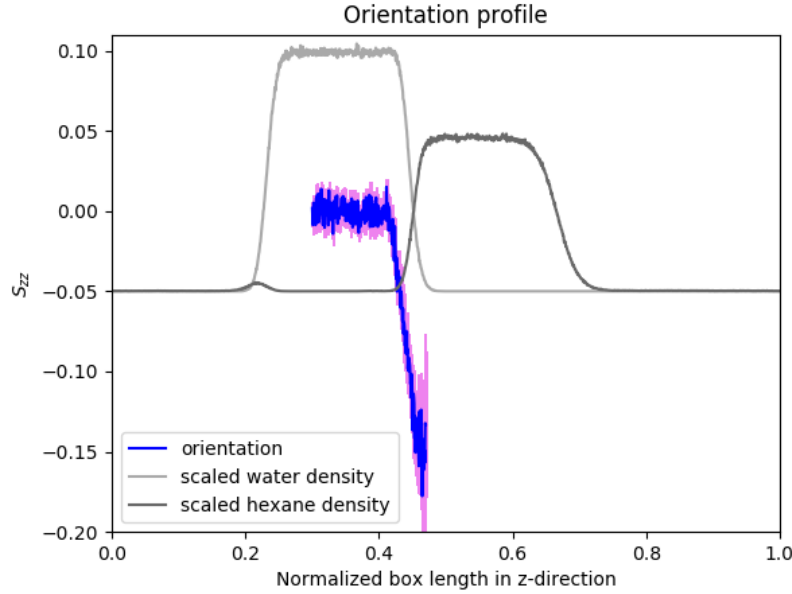
$$\frac{p_{xx} + p_{yy}}{2} \rightarrow p \quad (5.10)$$

6. 8/12/2018

- (1) Working on slides explaining capillary theory contributions for candidacy ppt.
- (2) We download orientations_hexane_full-298-32bead-hexane-orientations-corrected.txt and analyzed:



- (3) Download orientations_water_32bead-water-unwrap.txt. Had issues with nan in orientation_profile_analysis_UPDATE for some strange reason, nans in the SE measurements, so used nan_policy='omit' for stats.sem. Finally, it works: used zlo 600 zhi 940:



7. 8/13/2018

- (1) PIMC barostat acceptance criterion:

$$A(V'/V) = \min[1, e^{-\beta P(V'-V)} e^{-\beta[(U(r')-U(r))/nBeads]} e^{N \ln(V'/V)}] \quad (7.1)$$

- (2) Developing ppt slide on density fluctuations:

$$\begin{aligned} \rho_W(z) &= \frac{1}{2}\rho_W + \frac{1}{2}\rho_W \operatorname{erf}\left(\frac{z - \langle h_W \rangle}{\sqrt{2}\sigma_c}\right) \\ \rho_H(z) &= \frac{1}{2}\rho_H - \frac{1}{2}\rho_H \operatorname{erf}\left(\frac{z - \langle h_H \rangle}{\sqrt{2}\sigma_c}\right) \end{aligned} \quad (7.2)$$

$$\begin{aligned} \sigma_0 &= \langle h_H \rangle - \langle h_W \rangle \\ \sigma_c^2 &= \frac{k_B T}{2\pi\gamma} \ln\left(\frac{L_{||}}{l_b}\right) \end{aligned} \quad (7.3)$$

8. 8/14/2018

- (1)

$$\leq \quad (8.1)$$

9. 8/23/2018

- (1) Test 1: P_16 on midway-113b-21, printing to test.xyz but not output right away. About 175,000 printings to .xyz (about 10,000 steps) but none to output. Started printing to output after about 4:00 minutes. Stopped printing and said "Turn 3271000 15.86 per" without finishing line. At about 8 minutes it printed again to output file, catching up...and immediately got stuck again.
- (2) Test2: P_16 on midway2-gpu06, printing to output right away, no problem.

(3) Test 3: P_16 on midway-113b-21, printing to test.xyz but not output right away.

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