BONAFIDE CERTIFICATE

This is to certify that the project report entitled "Production of THERMOPLASTIC POLYURETHANE" submitted by Kritika Kashyap, Shreya Sengupta, Karan Sarpal in partial fulfillment of the requirements for the award of the Degree Bachelor of Technology in Chemical Engineering is a bonafide record of the work carried out under the guidance and supervision of Professor Dr. G.S. Nirmala at VIT University, Vellore.

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PREFACE

This Design Project includes various aspects of chemical product development right from the market condition evaluation to estimation of cost of the plant setup.

Chapter 1 deals with the introduction of the product Thermoplastic Polyurethane - its properties both physical and chemical. It also provides the application of TPU in various areas.

Chapter 2 contains a study of TPU in the global as well as Indian market. The gap between demand and supply is studied. The statistical data regarding the demand and supply pertaining to Indian market is studied.

Chapter 3 has a brief explanation of various processes available for the manufacture of TPU. The reason for going for the process is cited. The detailed process description along with solid works process sheet is given.

Chapter 4 includes the material balance over all the equipment and for each component for the basis of 8.4 TPD production of TPU production. Both the component and overall Mass balance has been provided. The flow rate along with % composition of each component along each stream is mentioned.

Chapter 5 contains the enthalpy balance for all the streams in the plant for each component. The total input and output energy is calculated.

Chapter 6 contains design of the polyol reactor.

Chapter 7 deals with the cost estimation of the polyol reactor and also the overall cost of the plant. The total income and profit is also calculated.

Chapter 8 summarizes the important results and conclusion.

Process flow sheet is also provided at the end of the report.

CHAPTER1

Introduction

1.1Thermoplastic polyurethane

- Thermoplastic polyurethane (TPU) is a unique category of plastic created when a polyaddition reaction occurs between a diisocyanate and one or more diols. The underlying chemistry behind polyurethane was first developed by Professor Dr. Otto Bayer. He invented the Diisocyanate Polyaddition Process which is the base patent in the polyurethane industry.
- First developed in 1937, this versatile polymer is soft and processable when heated, hard when cooled and capable of being reprocessed multiple times without losing structural integrity. Used either as a malleable engineering plastic or as a replacement for hard rubber, TPU is renowned for many things including its: high elongation and tensile strength; its elasticity; and to varying degrees, its ability to resist oil, grease, solvents, chemicals and abrasion. These characteristics make TPU extremely popular across a range of markets and applications. Inherently flexible, it can be extruded or injection molded on conventional thermoplastic manufacturing equipment to create solid components typically for footwear, cable & wire, hose and tube, film and sheet or other industry products. It can also be compounded to create robust plastic moldings or processed using organic solvents to form laminated textiles, protective coatings or functional adhesives.
- Aliphatic TPUs based on isocyanates like H12 MDI, HDI and IPDI are light stable and offer excellent optical clarity. They are commonly employed in automotive interior and exterior applications and as laminating films to bond glass and polycarbonate together in the glazing industry. They are also used in projects where attributes like optical clarity, adhesion and surface protection are required.
- Thermoplastic Polyurethane is a rubber-like material that is often used in shoes, mobile device cases, sporting goods, medical devices, and drive belts.

1.2 Physical Properties

• Appearance: Transparent, spherical pellets, rubber like

Colour: Black

• Odour: odourless

• Density: 1.15-1.19 g/cm3

• Tensile strength: 30-40 Mpa ~ 5076 psi

• Tear Strength: 285 pli

Compression Set/ 70h @ 23C 34%
 Compression Set/ 24h @ 70C 48%

• Abrasion Loss: 20-35 mm3

• Glass transition: -30 to -45 'C

• Specific Gravity: 1.18

• Boiling Point : not available

Melting Point: 130-300'C
 154-419 F (over range of different grades)

• Solubility in water : not available

• Viscosity: 14850 to 35000 mPa.s ASTM D445

• Flash Point : not applicable

• Vapour Pressure:

• Water Absorption (73°F, 24 hr): 0.3 - .4 % ASTM D570

• Surface Resistivity: 1.0E+6 to 2.5E+10ohms ASTM D257

• High wear resistance

- Flexibility over a wide range of temperature
- High elasticity over the entire hardness rang
- Excellent resistance to oils, greases and many solvents
- Good resistance to weathering
- Intrinsically soft, no plasticiser needed
- Excellent resistance to high-energy radiation

1.3 Chemical Properties

- During handling and use,product can cause static discharge. In the presence of flammable materials a fire and/or explosion may occur. Molten material may cause thermal eye burns. Molten material may cause thermal skin burns. Processing vapors may cause respiratory tract irritation
- General Only normally needed for thermal burns and for inhalation of smoke from burning material
- Eye contact: Check for and remove any contact lenses. In case of contact, immediately flush eyes with plenty of water for at least 15 minutes. Get medical attention.
- Skin contact: Molten material can cause severe burns. Do NOT try to peel molten polymer from the skin. Immediately immerse in or flush with large amounts of cold water to dissipate heat. Cover with gauze and get prompt medical attention.
- Inhalation: Remove patient from exposure, keep warm and at rest. Obtain medical advice IMMEDIATELY.

1.4 Application and Uses

From the gear knobs in our hand, athletic shoes or ski boots on our feet to materials in construction, agriculture or other industries we depend on daily – product designers, engineers and manufacturers rely on our diverse portfolio of thermoplastic polyurethanes. See for yourself and learn about our most important industries and applications.

Automotive

- Gear Knobs
- TPU-Surface (Skin) for instrument panels
- Chassis spring seatings
- Tamber doors
- Door handles, Cupholders
- Pedal covers
- Door damper, Sealing

Industrial Mechanical

- Wearing parts: mine screens, strippers, cyclones
- Wheels and solid tyres: wheels with polyamide or metal hubs for machines, trucks, escalators
- Rollers: transport, support and guide rollers, rollers for office equipment
- Seals: U- and V-packing rings, O-rings, cup seals, inverted cup seals and V-shaped seals
- Damping components: spacers and grippers, pickers, handles for pneumatic drills
- Drive elements: clutch components, timing belts, round belts, cog wheels.

Agriculture

In addition to animal identification tags there are several more TPU applications in the field of agriculture. Desmopan® TPU also helps farmers to sow and harvest their crops. All kinds of different harrows and picking prongs, for example, are made of TPU.

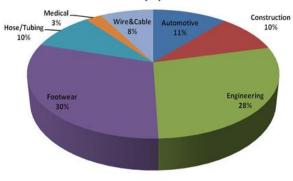
Sport & Leisure

- Ski boots, inline skates
- Ice Hockey Boots
- Hiking and climbing boots
- Flexible soles for sports shoes
- Parts for ski bindings
- Roller skate wheels
- Ski edges
- Ski and snow board surfaces
- Motorcross boots

Other applications

- Household and electrical appliances
- **Tools**
- Medicl Technology
- Toys
- Fabric Coating
- Films

Global TPU Consumption by End Use 2010 (%) Medical Wire&Cable



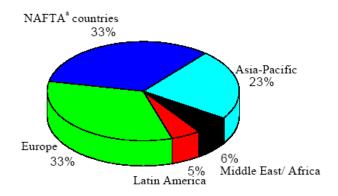
1.5 End Use Consumption

Thermoplastic Polyurethane has a variety of applications in the industry. It can be used for Furniture, Automobile seats, Houses, sculptures, and decorations, Filling of spaces and cavities, Water vessels, Flexible plastics, Varnish, Wheels, Automotive Parts, Electronic components, Adhesives , Abrasion resistance , Architectural Glass Lamination , Auto-Body Side Molding Automotive Lumbar Supports ,Caster Wheels ,Cattle Tags ,Constant Velocity Boots (Automotive) ,Drive Belts ,Film and Sheet, Fire Hose Liner ,Flexible Tubing ,Food Processing Equipment, Footwear—sport shoe soles, Hydraulic Hoses, Hydraulic Seals, Inflatable Rafts, In-Line Skates , Magnetic Media.

CHAPTER 2

2.1 Market Analysis

World's largest market store-RESEARCH AND MARKETS has made a report regarding the identification of the performance of Thermoplastic Polyurethane (TPU) in the overall market. This report is subdivided by application, end user industries and also by geographical analysis in terms of both volume and revenue from 2010 till 2018. By application the global TPU market includes injection molding, extrusion, adhesives and sealants, and paints and coatings in terms of kilo tons as volume and USD million in terms of revenue from 2010 and forecasted till 2018.



^a North American Free Trade Agreement

Worldwide Consumption of PU.

According to Transparency Market Research, the TPU market by end users includes industries such as automotive, construction, electronics and appliances, hose and tubing, footwear, wire and cable and others which includes industrial insulation Engineering because of their high tensile strength, abrasion resistance, and low temperature properties. In addition, thermoplastic polyurethanes possess a number of physical properties that no other TPEs can provide.

Some of the key players of the TPU market profiled in this report are BASF, Bayer AG, Huntsman Corporation, Dow Chemicals, and Lubrizol and so on.

In terms of volume, the Global Thermoplastic Polyurethane market shipped 0.448 million tons in 2014 and is expected to increase to 0.560 million tons by 2019, growing at a CAGR of 4.56 percent.

Increased demand from the Automotive industry is one of the major drivers of increasing production of TPU. Thermoplastic polyurethane is replacing the metals used in the manufacture of automobile parts because it is light in weight and has higher impact resistance. Increased use of thermoplastic polyurethane in medical applications is another growth driver.

IROGRAN®, AVALON®, KRYSTALGRAN® and IROSTIC® are the four main TPU brands produced by the polyurethanes division of Huntsman. Available in an array of different grades, each has its individual characteristics and can be tailored for either basic plastic product applications or more complex engineering projects.

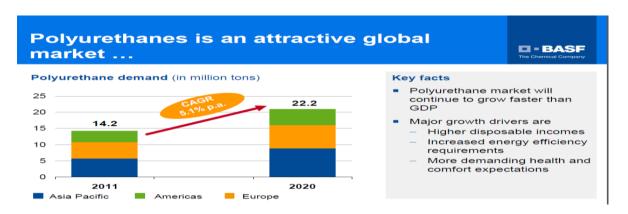
Regardless of brand, all TPU grades have some common performance traits that set them apart from other plastic materials. These typically include:

- High abrasion resistance
- High elasticity across the entire hardness range
- Excellent low-temperature and impact strength
- Resilience to oils, greases and numerous solvents
- Good flexibility over a wide temperature range
- Robust weather and high-energy radiation resistance
- Pleasant tactile properties
- Suitability for bonding and welding
- Ease of coloring
- Recyclability

For applications with specific requirements, it is possible to change a TPU's physical attributes and production values. Distinct performance properties can be achieved by:

- Varying the type of polyol used
- Adjusting the ratio of other raw materials
- Changing the reaction conditions under which processing takes place
- Using additives like UV stabilizers, mold release agents and flame-retardants.

BASF is the leading global player in MDI and TDI with regional world scale plants.



In South India, Bayer TPU Private Limited, a growth oriented Bayer AG, Germany subsidiary, manufactures Thermoplastic Polyurethane (TPU), marketed under the registered Bayer AG brand name Desmopan. The company's manufacturing facility at Cuddalore, Tamil Nadu, contributes more than 2000 MT annual capacity to feed both the domestic market as well as Europe and Far East customers through BayeCs international marketing network. While the majority of sales are still generated through exports, local sales are expected to pick up. The quality of Desmopan (TPU) manufactured at Cuddalore conforms to specification laid down by Bayer AG and testing these products periodically enforces strict quality control.

The company has pioneered the development of TPU applications in wide ranging industry segments viz. injection moulded components in automotive, textile, shoe, castor wheels- extrusion of cable sheathing, pneumatic tubing, solution coatings, adhesives etc. Bayer TPU Private also represents Wolff Waisrode, another Bayer Group Company, in India for their thermoplastic elastomer films used in a range of applications viz. automotive industry, tank lining, conveyor belts, membrane packaging, medical/surgical drapes etc.

Another TPU manufacturing company in southern India, **G-STAR POLYMERS PLASTICS** in Tiruvallur, Tamil Nadu, has acquired a reputed name in the realm of offering comprehensive range of all Thermoplastics plastic products. They are a trusted Manufacturer and Supplier of high quality range of Recycling, Colouring and Compounding of all Thermoplastics such as LDPE Granules, Recycled LDPE Granules, Polyethylene Granules, HDPE Granules, LDPE Polyethylene, Nylon, Polypropylene, Polystyrene, Polycarbonates, Acrylonitrile-Butadiene-Styrene, Thermoplastic Rubber, Thermoplastic polyrethane. Moreover, they are also engaged in

rendering value added services like Thermoplastic Recycling, Coloring & Compounding Job Works Can Done etc.

With the support of a sound manufacturing unit and a competent workforce, they have been catering to the needs of various domains like automobile, electronic, home appliances, etc.

2.2 Global Producers

BASF (Germany)

Bayer (Germany)

Huntsman

Gala Industries

CHAPTER 3

3.1 Production Processes

Polyol, MDI and 1, 4-Butanediol are the main reactants for the formation of TPU.

Polyol Reactor: Adipic acid and 1, 4-Butanediol are made to react to produce polyester Polyol. Water liberated from the reaction is condensed and treated as effluent. Along with the water some amount of organic material also gets produced which needs to be analysed for the presence of monomers and oligomers.

Polyol Blend Tank: Prepared polyol is melted to liquid state and is fed to the blend tank with additives in a very negligible amount as per application.

The flowrate of raw materials is calibrated to avoid polymer build up. The calibrated reactants cannot be reused again as it gets exposed to air and gets a colour due to oxygen presence.

MDI and **BDO** Charging: MDI and BDO supplied to the tanks are charged after melting. The flowrate is maintained to maintain the polymer consistency and final quality of the product.

FettAlkohol Tank: Fettalkohol C-8 98% is a chain terminating agent which controls the side reaction of a product which is not desired to be formed.

Extruder: Co-rotating twin reactive screw extruder is used. Mixer product and BDO are sent to the extruder and are fed one by one, with few minutes gap and the material is collected in waste drums till all raw material are mixed and uniform polymer is formed before sending the polymer to pelletisation process. The technique used for making the pellets from the resin is called *Under water pelletisation*. Resin from the extruder passes through a DIE and then pulled out in the required cross sectional area and is cut by the blades of the pelletiser, then cooled by chilled water. A lot of waste is also removed due to pelletiser upset as a result of improper polymer build up.

Dryers: A centrifugal dryer is used. Here the pellets and water gets separated. This water is recycled. The final moisture content present in the pellets after dehumidification (hot air dryer) is 0.05%.

Sieving: The desired shape of pellets is between 3-5mm. Hence the bigger sizes are left on the upper sieves and the required size of pellets are obtained. **Packing:** The final product is packed and dispatched to various industries.

3.3 PROCESS CHEMISTRY

Polyurethane (**PUR** and **PU**) is a polymer composed of a chain of organic units joined by carbamate (urethane) linkages. Polyurethanes are produced by reacting an isocyanate containing two or more isocyanate groups per molecule (R-(N=C=O)n \geq 2) with a polyol containing on average two or more hydroxy groups per molecule (R'-(OH)n \geq 2), in the presence of a catalyst. Polyurethane products often are simply called "urethanes".

$$O = C = N$$

$$C = O + HO$$

$$C =$$

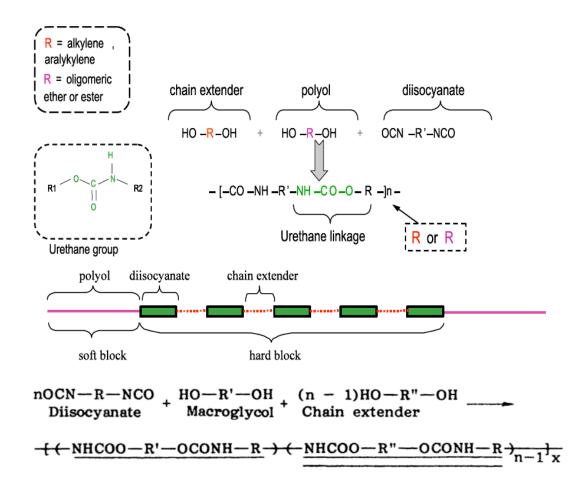
Fig: Polyurethane synthesis, wherein the urethane groups — NH-(C=O)-O- link the molecular units.

Polyurethanes are in the class of compounds called reaction polymers, which include epoxies, unsaturated polyesters, and phenolics. The properties of a polyurethane are greatly influenced by the types of isocyanates and polyols used to make it. Long, flexible segments, contributed by the

polyol, give soft, elastic polymer. High amounts of crosslinking give tough or rigid polymers. Long chains and low crosslinking give a polymer that is very stretchy, short chains with lots of crosslinks produce a hard polymer while long chains and intermediate crosslinking give a polymer useful for making foam.

A TPU is a multi-phase block copolymer that is created when three basic raw materials are combined together in a specific way. The individual components required to produce a TPU are:

- A polyol or long-chain diol
- A chain extender or short-chain diol
- A diisocyanate



Generalized urethane reaction

The polymerization reaction makes a polymer containing the urethane linkage, - RNHCOOR'- and is catalyzed by tertiary amines, such as 1,4-diazabicyclo[2.2.2]octane (also called DABCO or TEDA), and metallic compounds, such as dibutyltin, dilaurate, orbismuth, octanoate. This is often referred to as the gellation reaction or simply gelling.

If water is present in the reaction mixture (it is often added intentionally to make foams), the isocyanate reacts with water to form a urea linkage and carbon dioxide gas and the resulting polymer contains both urethane and urea linkages. This reaction is referred to as the blowing reaction and is catalyzed by tertiary amines like bis-(2-dimethylaminoethyl)ether.

One of the most desirable attributes of polyurethanes is their ability to be turned into foam. Making a foam requires the formation of a gas at the same time as the urethane polymerization (gellation) is occurring. The gas can be carbon dioxide, either generated by reacting isocyanate with water or added as a gas or produced by boiling volatile liquids. In the latter case heat generated by the polymerization causes the liquids to vaporize. The liquids can be HFC-245fa (1,1,1,3,3-pentafluoropropane) and HFC-134a (1,1,1,2- tetrafluoroethane), and hydrocarbons such as n-pentane.

Carbon dioxide gas formed by reacting water and isocyanate

When water is used to produce the gas, care must be taken to use the right combination of catalysts to achieve the proper balance between gellation and blowing. The reaction to generate carbon dioxide involves water molecule reacting with an isocyanate first forming an unstable carbamic acid, which then decomposes into carbon dioxide and an amine. The amine reacts with more isocyanate to give a substituted urea. Water has a very low molecular weight, so even though the weight percent of water may be small, the molar proportion of water may be high and considerable amounts of urea produced. The urea is not very soluble in the reaction mixture and tends to form separate "hard segment" phases consisting mostly of polyurea. The concentration and organization of these polyurea phases can have a significant impact on the properties of the polyurethane foam.

carbon dioxide gas formed by reacting water and isocyanate

$$R-N=C=O + H_2O \xrightarrow{\text{step 1}} R-N-\overset{O}{C}-O-H \xrightarrow{\text{step 2}} R-NH_2 + CO_2^{\text{gas}}$$

$$R-N=C=O + R-NH_2 \xrightarrow{\text{step 3}} -R-\overset{O}{N}-R-\overset{O}{H} \overset{O}{H}$$

Thermoplastic Polyurethane is soft and processable when heated, hard when cooled and capable of being reprocessed multiple times without losing structural integrity.

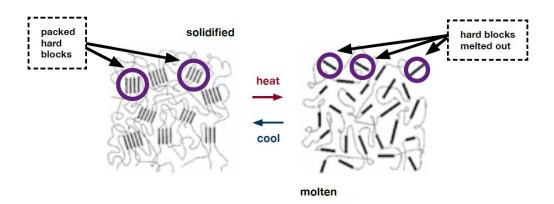


Figure provides a graphic illustration of the morphology of a TPU. It shows how physical cross-links melts out under heat and repack when the material is cooled.

RAW MATERIALS

Urethane functional groups are based in isocyanate and alcohol reaction:

The use of bifunctional isocyanates and diols will produce the so called polyurethanes. The first commercial production of flexible PU foams, based on the reaction between an aromatic isocyanate and a polyester polyol, was carried out in 1954.

However, these foams were unable to withstand the severe humidity and temperature conditions in which they were used, and thus foams based on polyether polyols were developed. This second generation foams provided better durability as well as comfort. A major advancement in PU technology was the introduction of the "one-shot" system using new catalysts and silicone-based surfactants. In the one-shot process; the isocyanate, polyol, water, and other ingredients are rapidly and intensively mixed and immediately poured to carry out the foaming.

Isocyanates

The polyurethane industry is mostly based on isocyanate chemistry. The functional group of isocyanates, -NCO, is capable of undergoing several different types of chemical reactions and is highly reactive toward proton-bearing nucleophiles such as alcohols, water, amines and urethanes [39]. The isocyanate, which provides the NCO groups that are essential to the PU production reaction, is quite important to the final physical and chemical properties of the foam. Although there are many isocyanates available in the market, most all of the PUs are based only on two of them. These are toluene diisocyanate (TDI), and the diphenylmethane diisocyanate (MDI) and its derivatives. The first is used mainly in the production of low-density foams, but its use under certain working conditions was not advisable for safety issues, giving therefore rise to the development of MDI.

The MDI used in PU production is a dark colored liquid, less hazardous than TDI due to its lower vapor pressure at normal temperatures. Despite this, MDI is still a very reactive and toxic reagent. MDI is prepared from aniline, formaldehyde, and phosgene.

TDI and MDI are generally less expensive and more reactive than other isocyanates. Industrial grade TDI and MDI are mixtures of isomers and MDI often contains polymeric materials. They are used to make flexible foam (for example slabstock foam for mattresses or molded foams for car seats), rigid foam (for example insulating foam in refrigerators) elastomers (shoe soles, for example), and so on. The isocyanates may be modified by partially reacting them with polyols or introducing some other materials to reduce volatility (and hence toxicity) of the isocyanates, decrease their freezing points to make handling easier or to improve the properties of the final polymers. Aliphatic and cycloaliphatic isocyanates are used in smaller volumes, most often in coatings and other applications where color and transparency are important since polyurethanes made with aromatic isocyanates tend to darken on exposure to light. The most important aliphatic and cycloaliphatic isocyanates are 1,6-hexamethylene diisocyanate (HDI), 1- isocyanato-3-isocyanatomethyl-3,5,5-trimethyl-cyclohexane (isophorone diisocyanate, IPDI), and 4,4'-diisocyanato dicyclohexylmethane, (H12MDI or hydrogenated MDI).

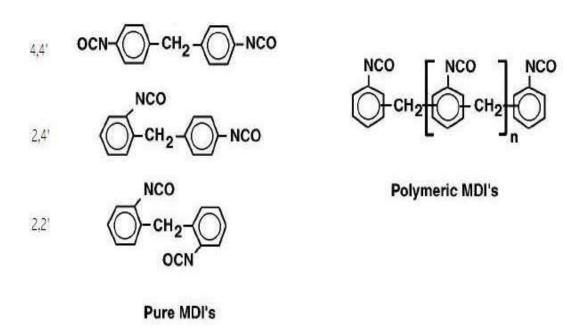


Figure: The aromatic methylene diphenyl diisocyanate, MDI

Polyols

Polyother polyols are mostly made by polymerizing ethylene oxide and propylene oxide. Polyester polyols are made similarly to polyester polymers. The polyols used to make polyurethanes are not "pure" compounds since they are often mixtures of similar molecules with different molecular weights and mixtures of molecules that contain different numbers of hydroxyl groups, which is why the "average functionality" is often mentioned. Despite them being complex mixtures, industrial grade polyols have their composition sufficiently well controlled to produce polyurethanes having consistent properties. As mentioned earlier, it is the length of the polyol chain and the functionality that contribute much to the properties of the final polymer. Polyols used to make rigid polyurethanes have molecular weights in the hundreds, while those used to make flexible polyurethanes have molecular weights up to ten thousand or more.

$$R(COOH)_2 + 2R(OH)_2 \rightarrow HO - [R - COO - R - COO - R] - OH + 2H_2O$$

Acid number is defined as the number of milligrams of potassium hydroxide (KOH) required for neutralizing the acid in 1 gram of resin (mg of KOH/ g of polyol). The used indicator was phenolphthalein. This is a direct measure of the degree of polyesterification, since acid groups which have react to form ester groups will not react with KOH. Acid number is the physical constant most frequently used as a process control during the synthesis of a resin. It is observed that as the reaction proceeds, the acid number decreases in a regular manner becoming constant as the reaction reaches toward completion. The acid number is inversely proportional to the MW of a polyol chain.

CHAPTER 4

Material Balance

The process shows a maximum conversion rate of 96%.

Production of TPU: 350 Kg/hr = 8400 Kg/day = 8.4 tons/day

Composition of the TPU pellets (excluding water content)

POLYOL	48.06%
BDO	10.14%
MDI	41.04%
Additives	0.76%

The additives used are:

Finawax	0.36%
Edenol	0.25%
Irgonax	0.10%
Carbodiimid	0.05%

Calculations:

Since the mass flow rate is 350 kg/hr for TPU pellets. It has 0.05% of moisture and 99.95% of solids and the percentage composition of BDO is 10.14% of the solids. Therefore, the mass flow rate of **stream 9** = 10.14% x 99.95% x 350

$$= 0.1014 \times 0.9995 \times 350$$

= 35.47 Kg/hr = 0.851 tons/day.

The percentage composition of polyol is 48.06% of solids. Therefore, the mass flow rate of **stream 4** = 48.04% x 99.95% x 350 = 0.4806 x 0.9995 x 350

$$= 168.125 \text{ kg/hr} = 4.035 \text{ tons/day.}$$

Now according to the reaction:

$$R(COOH)_2 + 2R(OH)_2 \rightarrow HO - [R - COO - R - COO - R] - OH + 2H_2O$$

Adipic acid

1,4-butanediol

butanediol adipate

water

(polyester polyol)

Where $\mathbf{R} = \mathbf{C}_4 \mathbf{H}_8$

1 mole Adipic acid—2 moles BDO—1 mole polyol—2 moles water

Therefore, mass flow rate of Adipic acid i.e **stream 1** = (168.125/290) x (1x146)

= 84.642 kg/hr = 2.031 tons/day.

Mass flow rate of BDO i.e **stream 2** = $[(168.125/290) \times 2] \times (2 \times 90)$

= 208.7 kg/hr = 5.009 tons/day.

Similarly, mass flow rate of water effluent i.e stream $3 = (168.125/290)x2 \times (2x18)$

= 41.74 kg/hr = 1.0017 tons/day.

The percentage composition of MDI is 41.04% of solids. Therefore, the mass flow rate of **stream 6** = 41.04% x 99.95% x350 = 0.4104 x 0.9995 x 350 = 143.568 kg/hr.

we know that there is a loss of 2.25% of 4% of 350 i.e 0.315 kg/hr. Therefore (143.568 - 0.315)

= 143.25 kg/hr = 3.43 tons/day.

Stream 5 is a blend of polyol and additives. The percentage composition of additives is 0.76% of solids.

Therefore mass flow rate of **stream 5** = $(0.76\% \times 99.95\% \times 350) + 168.125$

 $= (0.0076 \times 0.9995 \times 350) + 168.125$

= 170.78 kg/hr = 4.098 tons/day.

Therefore, now mass flow rate of **stream 7=stream 8** = 170.78 + 143.25

= 314.037 kg/hr = 7.536 tons/day.

The mass flow rate of stream 10 = 314.037 + 35.47 = 349.51kg/hr =8.388 tons/day.

Since the extruder startup loss and pelletiser upset loss contribute to a total loss of 10.1% of 4% of 350 = 11.34 + 2.016 = 13.356 kg/hr.

Therefore, mass flow rate of **stream 11** = 349.51 - 13.356

= 336.154kg/hr = 8.067 tons/day.

Now with 21000 kg/hr of chilled water for wash of pellets from extruder and 20% absorption of water by the pellets.

Therefore mass flow rate of stream 12 = 21000 kg/hr = 504 tons/day

and that of stream 13 = 80% of 210 00kg/hr = 16800 kg/hr = 403.2 tons/day.

Mass flow rate of **stream 14 = stream 15** = 336.154 + (20% of 21000 kg/hr)

= 336.154 + 4200

= 4536.154 kg/hr = 108.86 tons/day.

Since the centrifugal dryer is efficient in removing 60% of the moisture content, therefore mass flow rate of **stream 16** = 60% of 4200

= 2520 kg/hr = 60.4 tons/day.

After removing 60% moisture, the mass flow rate of stream 17 = stream 18 = (4536.154 - 2520) = 2016.154 kg/hr = 48.387 tons/day.

The hot air dryer removes moisture upto 0.05% of 350 i.e. the moisture content in stream 20 is $0.05\% \times 350 = 0.175$ and moisture content in stream 18 = (4200 - 2520) = 1680.

This implies mass flow rate of **stream 19** = (1680 - 0.175) = 1679.82 kg/hr

= 40.315 tons/day.

Mass flow rate of **stream 20** = (2016.154 - 1679.82) = 336.329 kg/hr

= 8.07 tons/day.

Therefore % conversion = $336.329 / 350 \times 100 = 96.09\%$

	T12 ▼ (Temp. of reactor (K)												
⊿	А	В	С	D	Е	F	G	Н	-1	J	K	L	
1	Streams	Mass Fl.rate	Mass Fl.rate	AA %	BDO %	additives %	polyol %	polyolblend %	MDI %	water %	TPU %	Known variables	
2		(Kg/hr)	(tons/day)	w/w	w/w	w/w	w/w	w/w	w/w	w/w	w/w		
3	Stream 1	84.642713	2.0314251	100	0	0	0	0	0	0		%age of moisture in stream19	0.05
4	Stream 2	208.70806	5.0089934	0	100	0	0	0	0	0			
5	Stream 3	41.741612	1.0017987	0	0	0	0	0	0	100		production rate in Kg/hr	350
6	Stream 4	168.12594	4.0350225	14.53	88.32	0	100	0	0	0		% of water removed by centrifugal dyer	60
7	Stream 5	170.78461	4.0988306	0	0	1.5575053	98.4425	0	0	0		amount of chilled water used (kg/hr)	21000
8	Stream 6	143.25322	3.4380772	0	0	0	0	0	100	0		% of water absorption in during wash	20
9	Stream 7	314.03782	7.5369078	0	0	0	0	29.57559804	20.81	0		%polyol	48.06
10	Stream 8	314.03782	7.5369078	0	0	0	0	29.57559804	20.81	0		% MDI	41.04
11	Stream 9	35.472264	0.8513343	0	100	0	0	0	0	0		%BDO	
12	Stream 10	349.51009	8.3882421	0	10.14	0.8089696	48.06	48.86896958	41.04	0	100	% Additives	
13	Stream 11	336.15409	8.0676981	0	10.14	0.8089696	48.06	48.86896958	41.04	0	100	amount of additives(kg/hr)	2.66
14	Stream 12	21000	504	0	0	0	0	0	0	100	0	mol.wt of adipic acid(stream1)	
15	Stream 13	16800	403.2	0	0	0	0	0	0	100	0	mol.wt of 1,4 butanediol(stream2)	
16	Stream 14	4536.1541	108.8677	0	0	0	0	0	0	92.5894	7.411	mol.wt of polyol(stream4)	290
17	Stream 15	4536.1541	108.8677	0	0	0	0	0	0	92.5894	7.411	mol.wt of water(stream 3)	18
18	Stream 16	2520	60.48	0	0	0	0	0	0	100	0	moles of adipic acid(by stoichiometry)	1
19	Stream 17	2016.1541	48.387698	0	0	0	0	0	0	83.327	16.67	oles of 1,4butanediol(by stoichiometr	2
20	Stream 18	2016.1541	48.387698	0	0	0	0	0	0	83.327	16.67	noles of polyol formed(by stoichiometr	1
21	Stream 19	1679.8249	40.315798	0	0	0	0	0	0	100	0	noles of water formed(by stoichiometry	2
22	Stream20	336.32917	8.0719002	0	0	0	0	0	0	0.05	99.95		
23													
24												% conversion	96
25	Total Loss	14	0.336									%Loss	4
26	Polyol loss	0.315	0.00756									%Polyol charging and metering loss	2.25
27	MDI loss	0.315	0.00756									%MDI charging and metering loss	2.25
28	Extruder loss	11.34	0.27216									%Extruder startup loss	81
29	elletiser los	2.016	0.048384									%Pelletiser upset loss	14.4

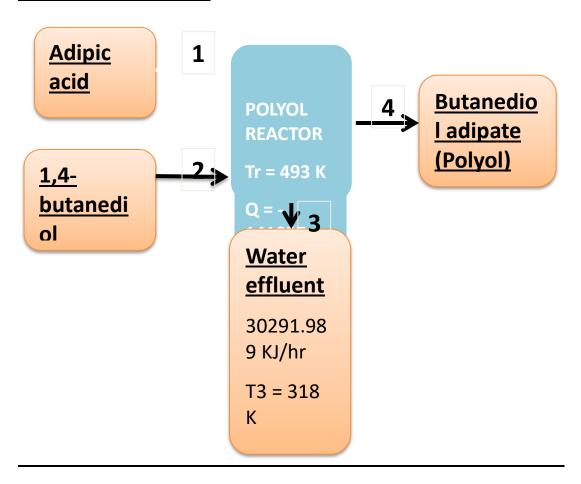
CHAPTER 5

ENERGY BALANCE

Temp	specific heat, Cp	ΔH_f
(K)	(KJ/kg)	(KJ/mol)
298	4.18	-242
298	2.43694	-994.3
298	2.219263205	-503.25
363	1.89	-1250
338	1.8	-360
333	1.65946	-1393
	(K) 298 298 298 363 338	(K) (KJ/kg) 298 4.18 298 2.43694 298 2.219263205 363 1.89 338 1.8

493
523
368
318
373
1.78
-1483
385.5
298

Energy Balance on Reactor:



For Adipic Acid

$$\Delta H_1 = \Delta H^0 + m_1 C p_1 (T_r - T_1) = (-994.3) + (84.685)(2.4369)(493-298) = 39228.19656 \text{ KJ/hr}$$

For 1,4 Butandiol

$$\Delta H_2 = \Delta H^0 + m_2 \, C p_2 (T_r - T_2) = -503.25 + (208.812)(2.219)(493-298) = 89816.482 \text{ KJ/hr}$$

For Water

$$\Delta H_3 = \Delta H^0 + m_3 \, C p_3 (T_3 - T_r) = (-242) + (41.74)(\ 4.18\)\ (493 -\ 318) = 30291.98912\ \mathrm{KJ/hr}$$

For Polyol

$$\Delta H_4 = \Delta H^0 + m_4 \, C p_4 (T_4 - T_r) = (-1250 \,) + (168.12)(1.89 \,) \, (363 - 493) = -42558.542 \, \, \mathrm{KJ/hr}$$

Heat Loss In Reactor

$$\Delta H_1 + \Delta H_2 + Q1 = \Delta H_4 + \Delta H_3$$

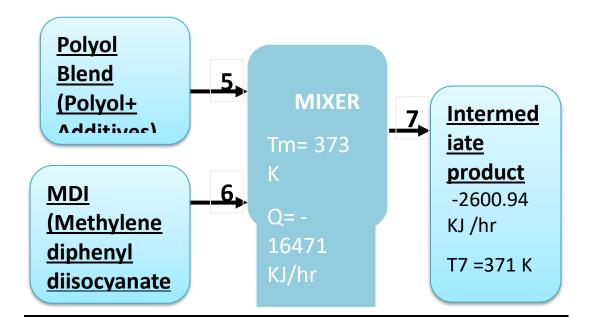
 $Q_1 = -141311.23 \text{ KJ/hr}$

Energy Balance On Blending Tank

A blending action is observed. The polyol released from the polyol reactor is mixed with additives like Iragnox and Carbodiimid with the help of an agitator which results in a 10% loss in energy.

$$Q_2 \ = \ Q_1 - 0.1 * Q_1 = \text{-} \ 126951 \ KJ/hr$$

Energy Balance On Mixer



For Polyol

$$\Delta H_5 = \Delta H^0 + m_5 C p_5 (T_m - T_5) = (-1250) + (170.78)(1.89)(373 - 353) =$$
5205.658 KJ/hr

For Methylene Diamine Isocyanate

$$\Delta H_6 = \Delta H^0 + m_6 C p_6 (T_m - T_6) = (-360) + (143.25)(1.8) (373-338) = 8664.952593 \text{ KJ/hr}$$

For Stream 7

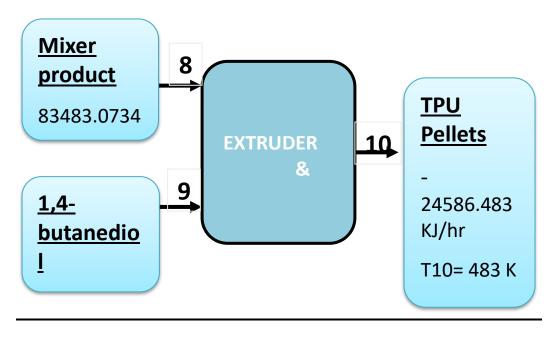
$$\Delta H_7 = \Delta H^0 + m_7 C p_7 (T_7 - T_m) = (-1483) + (314.03)(1.78)(371-373) = -2600.9746 \text{ KJ/hr}$$

Heat Loss In Mixer

$$\Delta H_5 + \Delta H_6 + Q3 = \Delta H_7$$

 $Q_3 = -16471.585 \text{ KJ/hr}$

Energy Balance On Extruder



For Stream 8

$$\Delta H_8 = \Delta H^0 + m_8 \, C p_8 (T_e - T_8) = (-1483) + (314.03)(1.78) \, (523-371) = \textbf{83483.07348 KJ/hr}$$

For 1,4 Butandiol

$$\Delta H_9 = \Delta H^0 + m_9 \, C p_9 (T_e - T_9) = (-503.25) + (35.47)(2.219) \, (523 - 298) = \textbf{17209.26523 KJ/hr}$$

For Stream 10

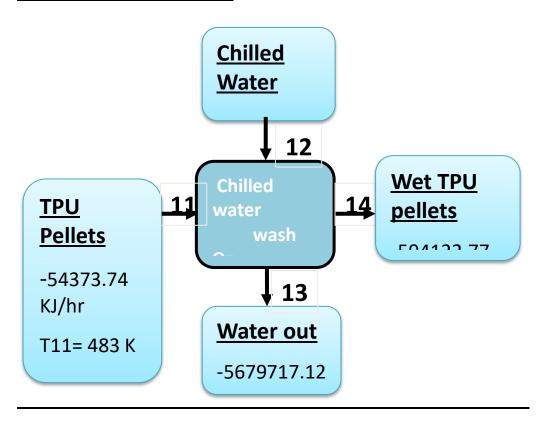
$$\Delta H_{10} = \Delta H^0 + m_{10} \, C p_{10} (T_{10} - T_e) = (-1393 \,) + (349.51)(1.659 \,) \, (483 - 523) = \textbf{-24592.9 KJ/hr}$$

Heat Loss In Extruder

$$\Delta H_8 + \Delta H_9 + Q4 = \Delta H_{10}$$

$Q_4 = -125285.26 \text{ KJ/hr}$

Energy Balance of Water Wash



For Extruder Pellet

$$\Delta H_{11} = m_{11} C p_{11} (T_w - T_{11}) = (336.154)(1.659) (385.5-473) = -54388.84049 \text{ KJ/hr}$$

For Inlet Chilled Water

$$\Delta H_{12} = m_{12} \, C p_{12} (T_w - T_{12}) = (21000) (4.18 \,) \, (385.5 \text{--} \, 288) = \textbf{8558550 KJ/hr}$$

For Outlet Water

$$\Delta H_{13} = m_{13} C p_{13} (T_{13} - T_w) = (16800)(4.18) (304.62-385.5) = -5679717.12 \text{ KJ/hr}$$

For Wet TPU Pellets

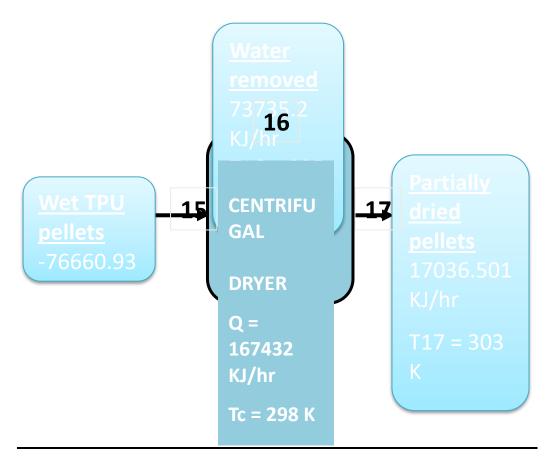
$$\Delta H_{14} = m_{14} C p_{14} (T_{14} - T_w) = (4536.154)(1.69) (308-385.5) = -583386.3853 \text{ KJ/hr}$$

Heat Loss In Water Wash

$$\Delta H_{11} + \Delta H_{12} + Q5 = \Delta H_{13} + \Delta H_{14}$$

$$Q_5 = -14767265$$

Energy Balance On Centrifugal Dryer



For Wet TPU Pellets

$$\Delta H_{15} = m_{15} C p_{15} (T_c - T_{15}) = (4536.15)(1.69) (298-308) = -75275.66261 \text{ KJ/hr}$$

For Outlet Water

$$\Delta H_{16} = m_{16} C p_{16} (T_{16} - T_c) = (2520)(4.18) (305-298) = 73735.2 \text{ KJ/hr}$$

For Dry TPU

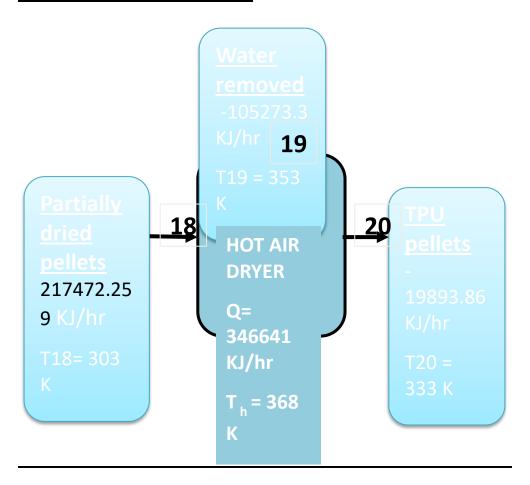
$$\Delta H_{17} = m_{17}Cp_{17}(T_{17} - T_c) = (2016.154)(1.69)(303-298) =$$
16728.6 KJ/hr

Heat Loss In Centrifugal Dryer

$$\Delta H_{15} + Q6 = \Delta H_{16} + \Delta H_{17}$$

$$Q_6 = 165739.498 \text{ KJ/hr}$$

Energy Balance On Hot Air Dryer



For Dry TPU Pellets

$$\Delta H_{18} = m_{18}Cp_{18}(T_h - T_{18}) = (2016.15)(1.69)(368-303) = 217472.259$$
KJ/hr

For Hot Water Exit

$$\Delta H_{19} = m_{19}Cp_{19}(T_{19} - T_h) = (1679)(4.18)(353-368) = -105325.022\text{KJ/hr}$$

For Dried TPU

$$\Delta H_{20} = m_{20} C p_{20} (T_{20} - T_h) = (336.329)(1.69) (333-368) = -19534.36843 \text{KJ/hr}$$

Heat Loss In Hot Air Dryer

$$\Delta H_{18} + Q7 = \Delta H_{19} + \Delta H_{20}$$

 $Q_{20} = -342331.65 \text{ KJ/hr}$

l	M	N	0	Р	Q	R	S	T	U	V	W
				(K)	KJ/hr	KJ/hr					
%age of moisture in stream19	0.05		Stream 1	298	39228.19656	in reactor		stream	Temp	specific heat, Cp	ΔH _f
			Stream 2	298	89816.48284	-141311.23			(K)	(KJ/kg)	(KJ/mol)
production rate in Kg/hr	350		Stream 3	373	30291.98912			water	298	4.18	-242
% of water removed by centrifugal dyer	60		Stream 4	363	-42558.54269			adipic acid	298	2.43694	-994.3
amount of chilled water used (kg/hr)	21000		Stream 5	353	5205.658165	in mixer		BDO	298	2.219263205	-503.25
% of water absorption in during wash	20		Stream 6	338	8664.952593	-16471.585		polyol	363	1.89	-1250
%polyol	48.06		Stream 7	371	-2600.974651			MDI	338	1.8	-360
% MDI	41.04		Stream 8	371	83483.07348	in extruder		TPU	333	1.65946	-1393
%BDO	10.14		Stream 9	298	17209.26523	-125285.26					
% Additives	0.76		Stream 10	483	-24592.92037			Temp. of reactor (K)	493		
amount of additives(kg/hr)	2.66		Stream 11	483	-54388.84049	in water		Temp. of Extruder (K)	523		
mol.wt of adipic acid(stream1)	146		Stream 12	288	8558550	wash		Temp. in hot air dyer(K)	368		
mol.wt of 1,4 butanediol(stream2)	90		Stream 13	304.62	-5679717.12	-14767265		Temp of water effluent(K)	318		
mol.wt of polyol(stream4)	290		Stream 14	308	-583386.3853			Temp of mixer(K)	373		
mol.wt of water(stream 3)	18		Stream 15	308	-75275.66261	in centrifugal		specific heat of mixer outlet(KJ/kg)	1.78		
moles of adipic acid(by stoichiometry)	1		Stream 16	305	73735.2	dryer		enthalpy of mixer outlet stream	-1483		
moles of 1,4butanediol(by stoichiometry)	2		Stream 17	303	16728.63531	165739.498		Temp of chilled water wash (K)	385.5		
moles of polyol formed(by stoichiometry)	1		Stream 18	303	217472.259	hot air dryer		temp in centrifugal dryer(K)	298		
moles of water formed(by stoichiometry)	2		Stream 19	353	-105325.022	-342331.65					
			Stream20	333	-19534.36843						

CHAPTER 6

6.1 EQUIPMENT DESIGN- POLYOL REACTOR

CONDENSATION POLYMERISATION REACTOR DESIGN

Model selection reference of reaction kettle

Composition	Туре							
Specification (L)	50-50000							
Design Pressure (Mpa)	Atmospheric Pressure or under pressure							
Material	Titanium Clad steel							
Heating Forms	Electrical heating with medium in jacket, external half coil steam heatin g, external half conduction oil heating, hot water infrared heating							
Cooling Forms	Refrigeration medium in the internal pipe jacket							
Blending Power	Model selection is made according to material viscosity, liquid- solid ratio, liquid specific gravity, solid specific gravity, solid granularit y, rotation speed, paddle type, with or without baffle or internal coil.							
Stirring blade Forms	Ribbon Type							
Seal	Mechanical seal							
Inner Surface Treatmen t	Polished							
Discharge Valve	Open downward discharge valve							
Technological Pipe Hol	Manhole, pressure							
e	gauge port, temperature, mouth							

All parts of the equipment that contact with the material are all made by stainless steel (SS304)

WORKING MECHANISM:

Batch Reactor has been used. These are exclusively used for polymerization reactions. The reactants are added to the empty vessel and the contents are removed after completion of the reaction via discharge valve. The reactor temperature is maintained at 220 degrees celcius which is the condition requirement for polyol formation. A polymerization condensation reaction occurs during polyol formation which leads to the formation of water product along with polyol. This water boils at 220 degrees celcius reactor temperature and escapes out of the reactor as vapors

from the vent present on the upper portion of the reactor vessel. A Double Helical Ribbon (DHR) agitator is used for mixing the highly viscous polyol being formed. DHR ensures efficient mixing of the polyol at higher rates in the laminar region. The velocity field produced by DHR exerts a stretching and folding action which forms Lagrangian Hyperbolic Structured cells of viscous component. A mechanical seal is used for firm attachment of the agitator. The reactor temperature is maintained via the cooling jacket around the reactor vessel. An ellipsoidal reactor head has been used along with a dished bottom. The stirrer should be started at the same time or 3-4 minutes after heating and should continue throughout the synthesis process. The total time cycle of the polyesterification reaction in this second phase can be reduced in 3 different ways:

- The flow of nitrogen can be increased with careful monitoring of glycol loss;
- The speed of the stirrer can be increased;
- Reduced pressure can be applied with special care to prevent foam rising.

REACTOR FUNCTIONING:

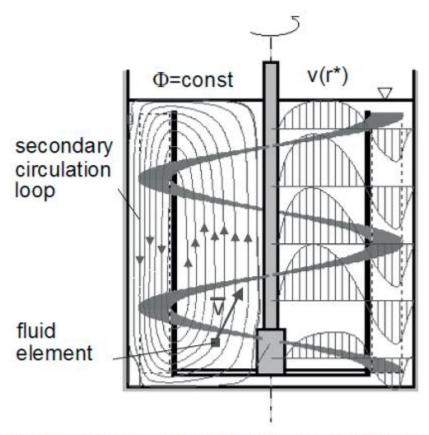


Fig. 1. Secondary circulation in a mixer, where: Φ – lines connecting points of equal dimensionless average axial velocity, r^* – dimensionless radius

MECHANICAL DESIGN OF REACTOR:

Technical parameter

代号Code 規格Type	500L	1000L	1500L	2000L	3000L	4000L	5000L	6000L
简体尺寸 Cylinder Size (mm)	900×800	1100 × 1200	1300 × 1200	1400×1500	1600×1500	1700×1800	1800×2000	1900×2000
实际客积 Actual Capacity (L)	699	1400	2166	3000	4066	5400	6600	7700
外管规格 Outer Tube Size (mm)	φ76/2	φ76/2	φ76/2	φ76/2	ф89/2	ф89/2	ф89/2	ф89/2
加热面积 Heating Area(m²)	1.7	2.6	3.8	4.5	5.8	7	7.5	8.7
内盘管规格 Inner Coll Size(mm)	ф38	ф45	ф45	ф45	ф45	ф57	ф57	ф57
冷却面积 Cooling Area (m²)	1.6	2.7	3.6	4.3	5.7	6,8	8	9
电机功率 Motor Power (kw)	3	4	5.5	5.5	7.5	11	11	15
减速机型号 Reducer Model	XLB4-17-3	XLB4-17-4	XLB4-17-5.5	XLB5-17-5.5	XLB5-17-7.5	XLB6-23-11	XLB6-23-11	XLB7-23-15
机架Frame	JXLD4-45	JXLD4-45	JXLD5-55	JXLD5-55	JXLD6-55	JXLD6-65	JXLD6-65	JXLD7-80

Production of polyol per batch = 350 * 6 = 2100 kg

Adipic Acid per batch = 507.85 kg

Volume of adipic acid per batch = $507.85/1344 = 0.3778 \text{ m}^3 = 377 \text{ L}$

BDO per batch = 1252.24 kg

Volume of BDO per batch = $1252.24/1017 = 1.231 \text{ m}^3 = 1231 \text{L}$

Hence total volume required = 377+1231 = 1608 L

Volume of the reactor = $V = 2166 L= 2.166 m^3$

Assuming L/D = 1.125

$$V = (\Pi D^2/4) \times L = (\pi/4) \times 1.125*(D)^3$$

$$\Rightarrow$$
 Diameter, $D_i = (4V/1.125\pi)^{1/3} = [4 \times 0.699 / (1.125 \times \pi)]^{1/3} = 1.348 \text{ m}$

$$\Rightarrow$$
 Height, L = V*4/(π x D²) = 1.518 m

AGITATOR DESIGN:

The diameter of helical impeller varies from 85 % of tank diameter.

Assuming that turbine operates at 70 rpm

Diameter of reactor = 1.348 m

Diameter of agitator = $85/100*D_i = 0.85 \times 1.348$

$$= 1.146 \text{ m}$$

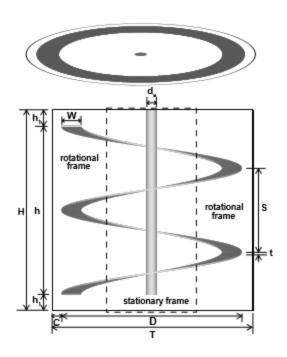
i.e using 85% of diameter of reactor as impeller diameter

$$W/D_a = 0.25$$

Width of the blade= $0.25*D_a$ = 0.25*1.146 = 0.2865m (Optimised Blade: giving optimum performance)

Thickness of Blade= 0.005 m

Clearance= $0.01*D_a$ = 0.01*1.146= 0.0146 m



VORANOL Diol Polyether Polyols

The diol line of VORANOL polyether polyols are well suited for use in numerous applications, including microcellular reaction injection molding (RIM), prepolymers, sealants, and other polyol blends.

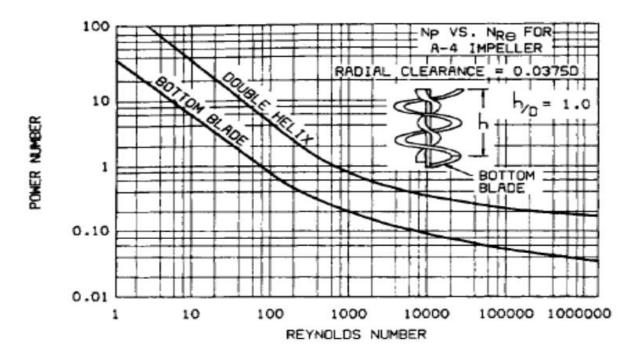
OH Number 8 28	Function- ality 2.0	Average Mol. Wt. 4,000	Initiator	Flash Point® °F (°C)	Density lb/gal (g/cc)	Viscosity [®] @ 77°F	Viscosity @ 100°F	Viscosity @ 150°F	Viscosity @ 210°F
	2.0	4,000	nronylana						
(N. E/			glycol	446 (230)	8.36 (1.00)	880	465	140	53
6N 56	2.0	2,000	propylene glycol	390 (199)	8.34 (1.00)	300	160	60	23
4 94	2.0	1,200	propylene glycol	435 (224)	8.43 (1.01)	175	92	31	13
0N 110	2.0	1,000	propylene glycol	360 (182)	8.37 (1.00)	160	80	28	11
0 260	2.0	432	propylene glycol	330 (165)	8.43 (1.01)	75	33	12	4.7
0 530	2.0	212	aniline	325 (163)	8.39 (1.00)	solid	6,000	200	13
9 29	2.0	4,000	propylene glycol	420 (216)	8.49 (1.02)	790	410	168	62
6 56	2.0	2,000	propylene glycol	>420 (>216)	8.46 (1.01)	321	168	63	25
	0N 110 0 260 0 530 9 29	4 94 2.0 ON 110 2.0 0 260 2.0 0 530 2.0 9 29 2.0	4 94 2.0 1,200 ON 110 2.0 1,000 O 260 2.0 432 O 530 2.0 212 9 29 2.0 4,000	glycol 4 94 2.0 1,200 propylene glycol ON 110 2.0 1,000 propylene glycol 0 260 2.0 432 propylene glycol 0 530 2.0 212 anilline 9 29 2.0 4,000 propylene glycol 6 56 2.0 2,000 propylene	glycol (199) (199)	glycol (199) (1.00) 4 94 2.0 1,200 propylene 435 8.43 glycol (224) (1.01) 0N 110 2.0 1,000 propylene 360 8.37 glycol (182) (1.00) 0 260 2.0 432 propylene 330 8.43 glycol (165) (1.01) 0 530 2.0 212 aniline 325 8.39 (163) (1.00) 9 29 2.0 4,000 propylene 420 8.49 glycol (216) (1.02) 6 56 2.0 2,000 propylene >420 8.46	glycol (199) (1.00) 4 94 2.0 1,200 propylene 435 8.43 175 glycol (224) (1.01) ON 110 2.0 1,000 propylene 360 8.37 160 glycol (182) (1.00) 0 260 2.0 432 propylene 330 8.43 75 glycol (165) (1.01) 0 530 2.0 212 aniline 325 8.39 solid (163) (1.00) 9 29 2.0 4,000 propylene 420 8.49 790 glycol (216) (1.02) 6 56 2.0 2,000 propylene >420 8.46 321	Second Columbia	glycol (199) (1.00) 4 94 2.0 1,200 propylene 435 8.43 175 92 31 ON 110 2.0 1,000 propylene 360 8.37 160 80 28 O 260 2.0 432 propylene 330 8.43 75 33 12 O 530 2.0 212 aniline 325 8.39 solid 6,000 200 9 29 2.0 4,000 propylene 420 8.49 790 410 168 Glycol (216) (1.02) 6 56 2.0 2,000 propylene >420 8.46 321 168 63

Density of polyol mixture, $\rho = 1000 \text{ kg/m}3$

Viscosity of mixture, $\mu = 53 \text{ cP}$

 $N_{Re} = \rho N Da^2/\mu = \left[1000x~70/60~x~(1.486)^2\right]/~53 = 48.6~\text{(Confirming low Reynolds No. for viscous fluids)}$

From M.V. Joshi, Process Equipment Design,



From power curve, Np = 10 for Reynolds number 48.6

Power, $P = Np*\rho* N^3*Da^5 = (10 \times 1000 \times (70/60)^3 \times (1.486)^5) = 115062.6616 \text{ W}$

Power losses (10%) = 11506.2 W (helical gears have efficiency of power transmission 90%)

Power input = 115062.66 + 11506.2 = 126568.861 W

Transmission system losses $(20\%) = 126568.861 \times 0.2 = 25313.78 \text{ W}$

Total Power= 126568.861 + 25313.78 = 151882.64 W

This will be taken as 152000 W to allow for fitting losses. It is advisable to use 152000 W motor.

Tab. 1. Parameters of helical-ribbon impellers

Impeller	Diameter of impeller d [m]	d/D [-]	Height h [m]	h/D [-]	A number of coils <i>i</i> [-]	Pitch of ribbon p [m]	<i>p/d</i> [-]	The ribbon angle β
R1	0.28	0.959	0.26	0.890	1	0.260	0.929	72.6
R2	0.28	0.959	0.26	0.890	2	0.130	0.464	80.6
R3	0.28	0.959	0.26	0.890	3	0.087	0.311	83.7
R4	0.27	0.925	0.26	0.890	2	0.130	0.481	80.2
R5	0.26	0.890	0.26	0.890	2	0.130	0.5	79.8

SHAFT DESIGN:

Continuous average rated torque on the agitator shaft,

$$Tc = P/2 \pi N =$$

 $152000/(2 \pi 70/60) = 20746.132 \text{ Nm}$

Where Tm is maximum torque= 1.5*Tc= 1.5*20746.132 = 31119.2 Nm

Polar modulus of the shaft cross section is, Zp = Tm/fs

fs =shear stress =550 kg/cm2

 $Zp = 31119.2*100/550 = 5658 \text{ cm}^3 \text{ d} = 10.3 \text{ cm}$

 $\Pi * D_s^3 / 16 = 5658$

 $D_s=30\ cm=0.3\ m$

CRITICAL SPEED:

Actual speed is 40% of the critical speed

Critical speed $N_c = 70/0.4$

= 175 rpm

Since actual shaft speed is 70 rpm which is 40% of the critical speed.

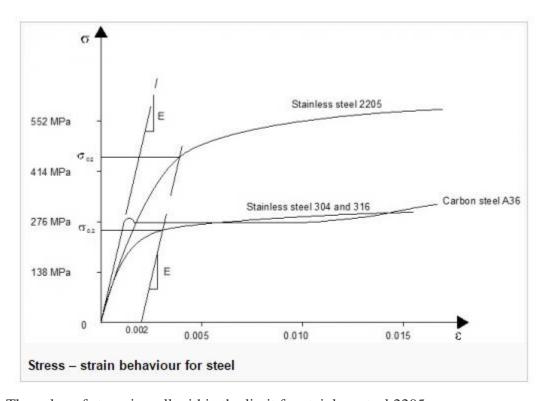
BLADE DESIGN:

No. of blades = 4 (for efficiency, typically 2 are used)

Using blade width, w = 0.2865m

Blade thickness, t = 0.005 m

Stress in the blade, $F = (maximum torque)/(tw^2/n) = (31119.2)/(0.005 \times 0.0.2865^2/4)$ =303306042N/m²= 303.3MPa < 414MPa (Ultimate Strength of Stainless Steel 2205)



The value of stress is well within the limit for stainless steel 2205.

MECHANICAL SEAL:

It consists of two surfaces (rings), one on the rotating shaft and the other is stationary. It has a rotary ring made of steel which is held on the shaft by a flexible O-ring made of Teflon. A

stationary ring made of carbon (low coefficient of friction) is placed in a box through another Oring. O-ring compensates for lack of alignment, thermal expansion and shaft vibration.

THICKNESS OF VESSEL:



304 Stainless Steel



	304	FSW		
	Transverse Ter	nsile Properties		
Sample	Yield Strength 0.2 % offset KSI (MPa)	Ultimate Tensile Strength KSI (MPa)	Elongation %	
400 RPM, 3 IPM	51 (352)	95 (655)	54	
Base Metal	55 (379)	98 (675)	56	

[•]Tensile failures occurred in HAZ

Allowable stress value, $f = 650 \text{ kg/cm}^2$ (upto 6679 kg/cm^2 for Stainless Steel 304)

Thickness of reactor, $t = (PD_i)/[(2fj)-P] + C$

Where

'j' is joint efficiency = 0.85

'P' is the design pressure

P = 1.1*30

 $= 1.1 \times 30$

 $= 33 \text{ kg/cm}^2$

 $t = (33 \times 1348)/[(2 \times 650 \times 0.85)-33] + 3$

= 44.496 mm with corrosion allowance

Thickness of reactor vessel = t = 44.496 mm = 0.044 m

DESIGN OF REACTOR HEAD (ELLIPSOIDAL):

Using Flat head

Thickness of head, $t = (C*D_i/10)$

Where 'C' is taken as 0.5

(IS 2825 - 1969)

 $t = (0.5 \times 1348/10)$

= 67.4 mm

= 70.4 mm with 3mm allowance for corrosion

DISHED BOTTOM THICKNESS

 $T_h = PD_i/2 \times f \times J$

 $T_h = 33 \times 1348 / (2 \times 650 \times 0.85) + 3$

= 43.25 mm with corrosion allowance

JACKET DESIGN

Jacket Diameter= 1.045 * 1.392 = 1.455 m

Jacket Thickness= $(PD_i)/[(2f_j)-P] + C = 33*1455/(2*650*0.85-33) + 2 = 46.79 \text{ mm} = 0.046 \text{ m}$

Hence approximately 0.046 m is the jacket thickness

WEIGHT CALCULATIONS:

Length of reactor = 1.518 m

Outside diameter of reactor = 1.392496 m

Inner diameter of reactor = 1.348 m

Density of structure steel = $8000 \text{ kg/m}^3 \text{ (SS304)}$

Weight of reactor vessel,

$$W_1 = 8000 \text{ x } \pi/4 \text{ (1.392} - 1.348) \text{ x 1.518} = 419.453 \text{ kg}.$$

Weight of Adipic acid,

$$W_2 = \pi/4 \text{ (Di}^2\text{) L }\rho$$

= $\pi/4 \text{ x } 1.348^2 \text{ x } 1.518 \text{ x } 1344$
= 11640.73 kg

Weight of the head

$$W_3 = t \times L \times b \times \rho$$

= 70.4 x 10⁻³x 1.518 x 1.518 x 8000 = 1297.795 kg

Weight of the BDO

$$W_4 = \pi/4 \text{ (Di}^2) \text{ L } \rho = \pi/4 \text{ x } 1.348^2 \text{ x } 1.518 \text{ x } 1017 = 2202.1 \text{ kg}$$

Weight of Agitator Assembly

We have a motor power output of 115 kW

Matching this with the standard specifications we get the, W_5 = 400 kg

Total weight
$$W = W_1 + W_2 + W_3 + W_4 + W_5 = 15958 \text{ kg}$$

Design weight =
$$1.3 \times 15958$$

= 20746.5 kg .

PRIMARY STRESS ON VESSEL

$$\begin{split} &\sigma_b = PxD_i/2t = (33 \text{ kg/cm}^3 \text{ x } 1.348)/(2 \text{ x } 0.044) = 505.5 \text{ kg/cm}^2 \\ &\sigma_L = PxD_i/4t = 505.5/2 = 252.5 \\ &\sigma_W = W/\left(\pi \text{ x t x } (Di + t)\right) = \ 20746.5 \ /(\pi \text{ x } 0.044 \text{ x } (1.348 + 0.044)) = 105.31 \text{ kg/cm}^2 \\ &\sigma_Z \text{ Total Longitudinal stress} = \sigma_W + \sigma_b + \sigma_L = 863.31 \text{ kg/cm}^2 \end{split}$$

DESIGN OF SUPPORT

LEG SUPPORT

No. of legs = 4

Base to be circular and legs are cylindrical in shape.

Maximum ratio of leg support length to diameter of vessel = 2:1 (Assuming 0.5:1 for batch reactor configurations)

Thus, Length = 1. 348 m x 0.5= 0.674 m

 $\sigma_{\rm Z}/2 = 431.655 \text{ kg/cm}^2$

 $\sigma_{\rm Z}/4 = 215.827 \text{ kg/cm}^2$

 $\sigma_Z/6 = 143.885 \text{ kg/cm}^2 \text{ Stress per base plate}.$

Area of leg support = Outer Dimensions of leg support² (For square shaped plate type leg support)

 $= 0.07 \text{m x } 0.07 \text{m} = 0.0049 \text{ m}^2$

Width = $33 \times 0.674 / 2 \times 143.885 = 0.07 \text{ m} = PxL/2t$

CHAPTER 7

7.1 COST ESTIMATION OF POLYOL REACTOR

AGITATOR

Ribbon Blender (SS 304) costs = Rs 1525261.93 (\$22957)

REACTOR VESSEL

(Including Jacketing, Sealing and Gears)

For a capacity of 2.1m^3 and design pressure of 33 kg/cm^2 , $\cos t = \text{Rs } 13674803.39(\$205822)$

Hence total equipment cost = 1525261.93 + 13674803.39 = Rs 15,200,065.32

(Refered from Equipment Costs-Plant Design and Economics for Chemical Engineers 5th edition by Peter and Timmerhaus Tata Mcgraw Hills Publications)

7.2 ESTIMATION OF VARIABLE COST

RAW MATERIAL:

Cost of Adipic acid =Rs. 500 per kg =Rs. 5 lakhs per tonne

Cost of BDO =Rs. 199.23 per kg =Rs. 199230 per tonne

For one year, amount of Adipic acid required = 2.031 tonnes/day(from material balance)

Total raw material cost=(5lakh+1.99lakh)*2.031=**14.20 Crores**

7.3 COST ESTIMATION OF PLANT

Capacity of plant = 350 kg/hr= 8400 kg/day

Current selling Price=\$20/kg

We assume that operating percentage = 95%

Therefore, annual gross sales are the product of annual production rate and the selling price per unit of production.

Basic assumption is that all product made is sold.

Annual Gross sales= \$20/kg X 365 days X 0.95 X 8400 kg/days =\$ 5.82 X 10⁷

With the current economy, \$1=Rs. 66.41

Therefore, Annual Gross Sales = Rs. 386.502×10^7

The Turnover Ratio = 0.65 (Assumed to be of polymeric material)

Fixed capital investment = Annual Gross Sales /Turnover ratio

 $= (386.502 \times 10^7)/0.65$

 $= Rs.594.618 \times 10^7$

ESTIMATION OF TOTAL INVESTMENT COST:

- 1. Direct cost:
- a. Purchased equipment cost: (15 40% of FCI)

Assume 40% of FCI

=Rs. 237.84 X 10^7

b. Installation cost: (35 -45% of PEC)

Assume 45%

=Rs. 107.03 X 10⁷

c. Instrumentation and control installed: (6-30% of PEC)

Assume 30% of PEC

=Rs. 71.35 X 10^7

d. Piping installation cost: (10-80% of PEC)

Assume 80%

=Rs. 190.27 X 10^7

e. Electrical installation cost: (10-40% of PEC)

Assume 40% of PEC

$$=$$
Rs. 95.14 X 10^7

f. Building process and auxillary: (10-70% of PEC)

Assume 70% =Rs. 166.5×10^7

g. Service facilities: (30-80% of PEC)

Assume 80%

$$=$$
Rs 190.272 X 10^7

h. Yard improvement: (10-15% ofPEC)

Assume 15%

$$=$$
Rs. 35.67 X 10^7

i. Land: (4-8% of PEC)

Assume 8%

$$=$$
Rs. 19.02 X 10^7

Therefore direct cost = Rs. 1113.092×10^7

- 2. Indirect Costs: Expenses which are not directly involved with material and labour of actual installation or complete facility
- a. Engineering and supervision: (5-30% of DC)

Assume 30%

$$=$$
Rs. 333.92 X 10^7

b. Construction expenses: (10% of DC)

$$=$$
Rs. 111.31 X 10^7

c. Contractors fee: (2-7% of DC)

Assume 7%

$$=$$
Rs. 77.91 X 10^7

d. Contingency: (8-20% of DC)

Assume 20%

=Rs. 222.61 X 10^7

Therefore total indirect cost =Rs. 745.75×10^7

FIXED CAPITAL INVESTMENT:

Fixed capital investment (FCI): = DC+IC

=Rs. 1858.842 X 10^7

WORKING CAPITAL INVESTMENT:

(10-20% of FCI)

Assume 15%

=Rs. 278.826 X 10^7

TOTAL CAPITAL INVESTMENT: =FCI+WC

=Rs. 2137.668 X 10^7

ESTIMATION OF TOTAL PRODUCT COST (TPC):

FIXED CHARGES:

- a. Depreciation: (10% of FCI for machinery)
 - =Rs. 185.884 X 10^7
- b. Local taxes: (3-4% of FCI)

Assume 3%

=Rs. 55.765 X 10^7

c. Insurances: (0.4-1% of FCI)

Assume 0.4%

=Rs. 7.435 X 10^7

d. Rent: (8-12% of FCI)

Assume 8%

=Rs. 148.707 X 10^7

Therefore total fixed charges = Rs. 397.791×10^7

But, fixed charges = (10-20% OF TPC)

Assume 20%

Therefore total product cost=Rs. 1988.95 X 10⁷

DIRECT PRODUCTION:

a. Raw materials: (10-50% of TPC)

Assume 40%

=Rs. 795.58 X 10^7

b. Operating labour(OL): (10-20% of TPC)

Assume 15%

=Rs. 298.34 X 10^7

c. Direct supervisory and electric labour: (10-15% of OL)

Assume 13%

=Rs. 38.78 X 10^7

d. Utilities: (10-20% of TPC)

Assume 15%

=Rs. 298.342 X 10^7

e. Maintenance(M): (2 - 10% of FCI)

Assume 8%

=Rs. 148.707 X 10^7

f. Operating supplies(OS): (10-20% of maintenance)

Assume 15%

=Rs. 22.306 X 10^7

g. Laboratory charges: (10-20% of OL)

Assume 12%

=Rs. 35.80 X 10^7

h. Patent and royalties: (2-6% of TPC)

Assume 4%

=Rs. 79.558 X 10^7

PLANT OVERHEAD COST:

50-70% of (OL+OS+M)

Assume 65%

=Rs. 305.08 X 10^7

GENERAL EXPENSES

a. Administration cost: (40-60% of OL)

Assume 50%

=Rs. 149.17 X 10^7

b. Distribution and selling price: (2-30% of TPC)

Assume 20%

=Rs. 397.79 X 10^7

c. Research and development cost: (3% of TPC)

=Rs. 59.668 X 10^7

Therefore general expenses (GE) = Rs. 606.628×10^7

Therefore manufacturing cost(MC) = product cost + fixed charges + plant overhead expenses

TOTAL PRODUCTION COST= MC + GE
= Rs.
$$3298.45 \times 10^7$$

GROSS EARNING AND RATE OF RETURN:

The plant is working for say 345 days a year

Selling price = 20 x 66.41 =Rs.1328.2/kg

Total income =
$$1328.2 \times 345 \times 8400$$

= 3849.1×10^7

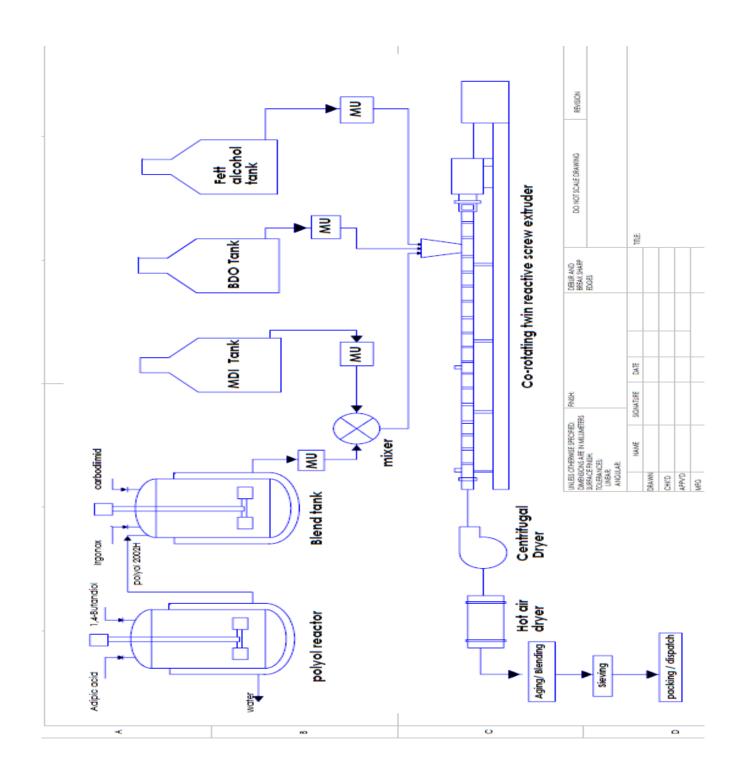
Gross income = total income – total product cost
=
$$(3849.1 \times 10^7) - (1988.95 \times 10^7)$$

=Rs. 1860.15×10^7

Assumption: Tax = 50%

Net profit =Rs. 930.075×10^7

Return on Investment (ROI) = Annual Net Profit (after taxes)/Total Capital Investment X100 = $930.075 \times 10^7/(2173.668 \times 10^7) \times 100$ = 42.78%



8. CONCLUSION

A thermoplastic polyurethane plant with a capacity of 8400 tons/day has been designed using adipic acid, 1,4—butanediol,MDI, Irgonox, carbodiimide, and others additives as raw material. A market survey was done to reach a concrete conclusion regarding the increasing demand of TPU globally and within the country. Thermoplastic Polyurethane has a variety of applications like it can be used for Furniture, Automobile seats, Houses, sculptures, and decorations, Filling of spaces and cavities, Water vessels, Flexible plastics, Varnish, Wheels, Automotive Parts, Electronic components, Adhesives, Abrasion resistance, Architectural Glass Lamination, Auto-Body Side Molding, Automotive Lumbar Supports, Caster Wheels. Its latest field of application includes usage as foams for oil absorption in water bodies to prevent pollution, taking advantage of the high hydrophobicity and oleophilicity that dimer acids impart to the final polyurethanes.

Polymerisation condensation reaction was selected as the first step of the manufacturing process after a careful study of the problems faced during manufacture, environment concerns. Efficient use of raw materials was considered to reach an optimum efficiency level. The detailed study of the process provided a clear insight into various stages and unit operations involved in the manufacture of TPU. The project led to an understanding on the need to manage plant processes and conditions to ensure optimal plant operation. This project involves energy and material balance which led to a clearer understanding of large scale production of TPU. Equipment design of reactor was done using basics of process equipment design along with total costing of the plant which made us appreciate the practical applications of the theory learnt and understood in classes.

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