

# Lab-9 Report

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Q1

(a)

$$\begin{aligned} \textcircled{a} \quad x[n] &= \frac{1}{2\pi} \int_{-\pi}^{\pi} X(\omega) e^{j\omega n} d\omega \quad [\text{IDTFT}] \\ &= \frac{1}{2\pi} \int_{-\pi/6}^{\pi/6} e^{-j\omega n_0} e^{j\omega n} d\omega = \frac{1}{2\pi} \int_{-\pi/6}^{\pi/6} e^{j\omega(n-n_0)} d\omega \\ &= \frac{1}{2\pi} \left[ \frac{e^{j\omega(n-n_0)}}{j(n-n_0)} \right]_{-\pi/6}^{\pi/6} \\ &= \frac{1}{\pi(n-n_0)} \left[ \frac{e^{j(\pi/6)(n-n_0)} - e^{-j(\pi/6)(n-n_0)}}{2j} \right] \\ &= \frac{1}{\pi(n-n_0)} \sin\left(\frac{\pi}{6}(n-n_0)\right) \\ &= \boxed{\frac{1}{6} \times \text{sinc}\left(\frac{(n-n_0)\pi}{6}\right)} \end{aligned}$$

**(b)**

No, the phase is not linear but has a zig-zag phase.

**(d)**

Blackman filter gives better result. Rectangular window is seen to have some ripples after the cut-off frequency but the blackman window has dip to -100 dB after the cut-off frequency.

**(f)**

The given filter is a high-pass filter. It allows high frequency to pass and low frequencies are attenuation.

This can be clearly observed in the magnitude plot.

## **Q2**

**(d)**

Changing  $r_0$  value changes the location of poles of the transfer function, thus eventually affecting the output.

As  $r_0$  value increases sharpness of the notch increases thus making it better.

## **Q3**

**(d)**

Changing the design method to least square from equiripple gives a similar output.

Equiripple filter is a better filter as it has constant and lesser amplitude ripples after cut-off frequency.