

# Real-Time Physically Guided Hair Interpolation

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**Fig. 1.** Interpolated rendered hairs from the given guide hairs. (a) the hair model with 128 guide hairs; (b) 106K rendered hairs with 1.7M vertices interpolated from the guide hairs using Linear Hair Skinning (LHS) taking 0.28 ms per frame; (c) rendered hairs interpolated using our method taking 0.34 ms per frame. This is especially challenging for interpolation as almost no two guide hairs are the same shape.

Strand-based hair simulations have recently become increasingly popular for a range of real-time applications. However, accurately simulating the full number of hair strands remains challenging. A commonly employed technique involves simulating a subset of guide hairs to capture the overall behavior of the hairstyle. Details are then enriched by interpolation using linear skinning. Hair interpolation enables fast real-time simulations but frequently leads to various artifacts during runtime. As the skinning weights are often pre-computed, substantial variations between the initial and deformed shapes of the hair can cause severe deviations in fine hair geometry. Straight hairs may become kinked, and curly hairs may become zigzags.

This work introduces a novel physical-driven hair interpolation scheme that utilizes existing simulated guide hair data. Instead of directly operating

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on positions, we interpolate the internal forces from the guide hairs before efficiently reconstructing the rendered hairs based on their material model. We formulate our problem as a constraint satisfaction problem for which we present an efficient solution. Further practical considerations are addressed using regularization terms that regulate penetration avoidance and drift correction. We have tested various hairstyles to illustrate that our approach can generate visually plausible rendered hairs with only a few guide hairs and minimal computational overhead, amounting to only about 20% of conventional linear hair interpolation. This efficiency underscores the practical viability of our method for real-time applications.

CCS Concepts: • Computing methodologies → Physical simulation; Procedural animation.

Additional Key Words and Phrases: Hair Interpolation, Cosserat Rod

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## 1 INTRODUCTION

Hair simulations contribute significantly to believable characters and immersive environments in film, video games, and virtual reality. However, achieving efficient and realistic hair simulations remains an open problem because, on average, a human scalp has about 100k - 150k hair follicles, and simulating, storing, and transferring complex geometries at such scales poses significant challenges to both computational efficiency and robustness.

A widely used solution is to pre-select a fraction of hair strands as *guide hairs* and only simulate those hair strands [Bertails et al. 2008; Yuksel and Tariq 2010]. Subsequently, all remaining hair strands, referred to as *rendered (or interpolated) hairs*, are synthesized from the guide hairs via interpolation. Yet, conventional methods [Chai et al. 2014; Epic 2024; Rosu et al. 2022; Yuksel et al. 2009] rely solely on the geometric information of guide hairs to determine the shape of rendered hairs. Unfortunately, this approach is prone to severe visual artifacts when guide hairs undergo large deformations, which is not uncommon. An example of this is shown in Fig. 1b, where rendered hairs are unnaturally stretched due to geometric differences of their interpolated guide hairs. Though guide hairs can often adequately represent large-scale hair motion, the resulting rendered hairs may be highly unrealistic when generated through geometric interpolation alone.

In this paper, we propose a novel hair interpolation scheme that utilizes physical information directly obtained from the simulation. Rather than directly interpolating positions, we operate on internal forces by interpolating them from guide hairs and then solve for rendered hair shapes that could reproduce these forces. Aiming for real-time applications, we develop a fast Gauss-Seidel solver that can converge with very few iterations. We introduce an efficient drift correction scheme to stabilize solutions and penalty energies to avoid penetrations between rendered hairs and other geometry (such as the face and shoulders). Our approach can entirely avoid visual artifacts caused by conventional geometric interpolation and reproduce individual rendered hair motion using distinct physical properties. Notably, our method does not require any pre-computation or training. We use only readily available runtime simulation data from guide hairs, and our interpolation can be computed independently for each rendered strand with only a minor computational overhead. We have tested various hairstyles to illustrate that our approach can generate visually plausible rendered hairs with only 20% additional computation time over conventional linear hair interpolation. This efficiency underscores the practical value of our method for real-time applications.

## 2 RELATED WORK

In this section, we briefly summarize prior work on hair simulation and hair interpolation, followed by the interpolation methods with reconstruction.

### 2.1 Hair Simulation

Hair simulation is computationally expensive due to the large number of hair strands. Over the years, various reduced representations of hair bundles have been proposed to achieve cost-effective approximations. These representations encompass 2D strips [Koh and Huang 2001], cubic lattice structures [Volino and Magnenat-Thalmann 2006], short hair strips [Guang and Zhiyong 2002], and volumetric representations [Lee et al. 2019; Wu and Yuksel 2016]. These representations are transformed into full hairs using baked textures or procedural functions during rendering.

Strand-based representations have recently gained prevalence over card/polygon-based representations due to their superior ability to capture high-fidelity hair details. In earlier works, hair strands

have often been modeled utilizing techniques such as mass-spring chains [Rosenblum et al. 1991], rigid multi-body chains [Anjyo et al. 1992; Chang et al. 2002], and the incorporation of ghost particles [Umetani et al. 2015] or altitude springs [Selle et al. 2008] to address the twisting effects, particularly pertinent in simulating curly hair. Several elastic rod models have been introduced to achieve a physically accurate representation of hair strands. These models include the super-helix model [Bertails et al. 2006], Cosserat rod elements (CoRdE) [Spillmann and Teschner 2007], discrete elastic rods (DER) [Bergou et al. 2008], damped exponential time integrator (DETI) model [Michels et al. 2015], and position-based Cosserat rods [Kugelstadt and Schömer 2016]. Recently, several works have been introduced to accelerate the strand-based hair simulation scheme, e.g., resolving collisions on a background Eulerian grid [Fei et al. 2021; Han et al. 2019; Hsu et al. 2023; Huang et al. 2023; McAdams et al. 2009] and accelerating the computation using ADMM solver [Daviet 2020, 2023].

### 2.2 Hair Interpolation

To address the computational demands associated with simulating individual hair strands, a common strategy is to simulate a limited number of guiding hair strands before employing interpolation to reconstruct the dense hair model. Currently, the predominant approach involves the manual authoring strand-based hairstyles, with hair interpolation achieved through Linear Blend Skinning, also known as Linear Hair Skinning (LHS). LHS is extensively used in both gaming [Epic 2024] and film production [Somasundaram 2015]. Unfortunately, LHS may introduce undesirable artifacts, such as zigzagging shapes and shortened/stretched strands, especially when the associated guide hairs exhibit disparate shapes and motions (see Fig. 1b), which only becomes more prominent the more complex the hairstyle, particularly with those involving curly hair.

As these artifacts are often the result of poorly selected LHS weights, several approaches have been proposed to address weight computation. Chai et al. [2014] proposed a data-driven solution reliant on full hair simulation as training data. However, its efficacy heavily depends on having a similar range and motion between full simulation at training and guide simulation at runtime. Since these simulations often do not match behavior, ground truth can be challenging to obtain, limiting the generalization of data-driven methods. As a result, subsequent data-driven approaches [Chai et al. 2017; Lyu et al. 2022] still face challenges related to the need for extensive training and potential artifacts when guide hairs deviate from the training data. Chai et al. [2017] proposed the dynamic selection of weights at runtime to allow for local weight adaptations. However, this approach only considers large-scale motion similarity and fails to account for any runtime fine geometry deviations (e.g., curls) between the guide and interpolated hairs. This is especially true with sparse guide hairs that each has drastically different shapes, as shown in Fig. 1b.

To further account for changes in geometry, Lyu et al. [2022] introduced a neural interpolator for dynamic weight prediction, addressing previous generalization issues at the cost of computation time. In the same vein, Rosu et al. [2022] employed a pre-trained Variational Autoencoder (VAE) to convert the shape of guide hairs

into latent vectors, generating full hairs by decoding these interpolated latent vectors. Strand-VAE [Shen et al. 2023; Sklyarova et al. 2023] has extended this to reconstructing full hairs from a limited number of hair strands. However, the long inference times associated with this method hinder its real-time application, and its outcomes are constrained by the limitations of the training dataset, particularly concerning curly hair.

### 2.3 Interpolation Methods with Reconstruction

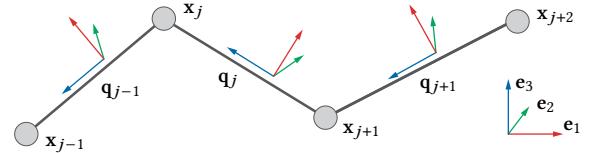
Our method is conceptually similar to the class of techniques known as gradient-domain reconstruction [Huang et al. 2006, 2010; Levin et al. 2004; Zheng 2013]. These methods apply various modifications to the gradient field of images and meshes and then reconstruct the images or meshes by solving a linear system, during which the spurious noise in the gradient domain is eliminated. We observe that the gradient field in a physical simulation corresponds exactly to the forces derived from physical strains and, thus, can be trivially obtained from existing simulations. As such, we propose an interpolation that instead operates on material-aware internal forces. This retains the benefits of gradient-domain reconstruction while making our method aware of physical properties like differing rest shapes and materials.

Physical material properties have been known to integrate well with physical systems. Specifically, approaches based on *differential coordinates* often utilize material-strain-based mesh reconstruction techniques reminiscent of gradient-domain reconstruction. For example, guided simulation methods [Barbić et al. 2009; Schumacher et al. 2012] define penalties based on differences in material strains to match target keyframes or poses in simulation. Strain-based interpolation methods for shells [Fröhlich and Botsch 2011; Heeren et al. 2014; Winkler et al. 2010] minimize differences in strains to produce interpolated poses. However, there are several important distinctions from our technique. Specifically, our method is designed to interpolate deformations between many inherently different hairs instead of the same mesh but with different poses. As such, we do not obtain strains from pre-made poses but rather directly from a running simulation. Furthermore, instead of operating in seconds, our solver is designed to operate in microseconds without the expensive and complex process in computing geodesic paths [Heeren et al. 2014], for example. Our solver is custom-tailored to the non-linear hair reconstruction problem that addresses the practical concerns for stability and performance.

## 3 STRAND-BASED HAIR SIMULATION

We employ Cosserat Rods to simulate hair dynamics due to their capability to capture complex behavior with an efficient position-based dynamics (PBD) solver [Kugelstadt and Schömer 2016], alongside their widespread adoption in modern game engines, e.g., Unreal Engine Groom [Epic 2024]. Here, we provide a very brief overview of our guide hair simulation framework.

Cosserat theory considers stretching, shearing, twisting, and bending resistance along the rod. Under the discretized representation, each strand segment is attached with a frame, denoted as a quaternion  $\mathbf{q}_j$ , with two ending vertices at  $\mathbf{x}_j$  and  $\mathbf{x}_{j+1}$ . We use the subscript  $j$  to index an ordered vertex or segment on each hair.



**Fig. 2.** Discretized Cosserat rod with position  $\mathbf{x}$  on vertices and orientation  $\mathbf{q}$  on segments.  $\mathbf{e}_\alpha$  is the axis-aligned orthonormal basis

For each reference frame, we denote the  $\alpha$ th axis as a 3D vector  $\mathbf{d}_{j,\alpha} = \mathbf{q}_j \mathbf{e}_\alpha \bar{\mathbf{q}}_j$ , where  $\bar{\mathbf{q}}$  indicates quaternion conjugation and 3D vector  $\mathbf{e}_\alpha$  is the  $\alpha$ th axis-aligned basis. By convention, we use  $\alpha = 3$  as the tangent axis along the segments of hair strands. The arrangements of variables are illustrated in Fig. 2.

Under this notation, Cosserat Rod formulates the rod material with two types of constraints: the *stretching and shearing* constraints  $\mathbf{C}^{\text{ss}}$  and the *bending and twisting* constraints  $\mathbf{C}^{\text{bt}}$ .  $\mathbf{C}^{\text{ss}}$  penalizes stretching with respect to the rest length  $l_j$  and shearing from the tangent direction as:

$$\mathbf{C}_j^{\text{ss}} \triangleq \mathbf{C}^{\text{ss}}(\mathbf{x}_j, \mathbf{x}_{j+1}, \mathbf{q}_j) = \frac{1}{l_j} (\mathbf{x}_{j+1} - \mathbf{x}_j) - \mathbf{d}_{j,3}. \quad (1)$$

To model the bending and twisting behaviors,  $\mathbf{C}_j^{\text{bt}}$  is introduced to penalize the difference between the scaled Darboux vector at current and rest pose as:

$$\mathbf{C}_j^{\text{bt}} \triangleq \mathbf{C}_j^{\text{bt}}(\mathbf{q}_j, \mathbf{q}_{j+1}) = \bar{\mathbf{q}}_j \mathbf{q}_{j+1} - \phi \mathbf{q}_j^0, \quad (2)$$

$$\phi \triangleq \begin{cases} +1 & \text{for } \|\bar{\mathbf{q}}_j \mathbf{q}_{j+1} - \mathbf{q}_j^0\|^2 \leq \|\bar{\mathbf{q}}_j \mathbf{q}_{j+1} + \mathbf{q}_j^0\|^2 \\ -1 & \text{for } \|\bar{\mathbf{q}}_j \mathbf{q}_{j+1} - \mathbf{q}_j^0\|^2 > \|\bar{\mathbf{q}}_j \mathbf{q}_{j+1} + \mathbf{q}_j^0\|^2 \end{cases}. \quad (3)$$

where quaternion  $\mathbf{q}_j^0 = \bar{\mathbf{q}}_j \mathbf{q}_{j+1}^0$  represents the scaled Darboux vector at the rest pose. Note that further scaling the stiffness  $k^{\text{bt}}$  by  $l_j^{-2}$  makes our  $\mathbf{C}_j^{\text{bt}}$  equivalent to that used by Kugelstadt and Schömer [2016] with discrete Darboux vectors. The energy potential  $E$  is further specified in terms of constraint functions  $E_j^\star = \frac{1}{2} k^\star \mathbf{C}_j^{\star T} \mathbf{C}_j^\star$ , where  $\star$  indicates constraint type and  $k^\star$  indicates the corresponding stiffness. Finally, we obtain the force and torque due to  $\mathbf{C}_j^{\text{ss}}$  on consecutive vertices  $j$  and  $j+1$  as follows:

$$\mathbf{f}_{j,j}^{\text{ss}} = \frac{k^{\text{ss}}}{l_j} \left( \frac{\mathbf{x}_{j+1} - \mathbf{x}_j}{l_j} - \mathbf{d}_{j,3} \right), \quad (4)$$

$$\mathbf{f}_{j,j+1}^{\text{ss}} = -\frac{k^{\text{ss}}}{l_j} \left( \frac{\mathbf{x}_{j+1} - \mathbf{x}_j}{l_j} - \mathbf{d}_{j,3} \right), \quad (5)$$

$$\tau_{j,j}^{\text{ss}} = -2k^{\text{ss}} \left( \frac{\mathbf{x}_{j+1} - \mathbf{x}_j}{l_j} - \mathbf{d}_{j,3} \right) \mathbf{q}_j \mathbf{e}_3. \quad (6)$$

Similarly, the torque from  $\mathbf{C}_j^{\text{bt}}$  on consecutive segments  $j$  and  $j+1$  reads:

$$\tau_{j,j}^{\text{bt}} = -k^{\text{bt}} \left( \mathbf{q}_j - \phi \mathbf{q}_{j+1} \bar{\mathbf{q}}_j^0 \right), \quad (7)$$

$$\tau_{j,j+1}^{\text{bt}} = -k^{\text{bt}} \left( \mathbf{q}_{j+1} - \phi \mathbf{q}_j \mathbf{q}_j^0 \right). \quad (8)$$

The extended position-based dynamics (XPBD) time integrator [Macklin et al. 2016] is used to apply the forces and torques to update each vertex's orientation  $\mathbf{q}_j$ , angular velocity  $\omega_j$ , position

$\mathbf{x}_j$ , and velocity  $\mathbf{v}_j$ . At the end of each iteration, the quaternion is normalized. We refer readers to the previous work [Kugelstadt and Schömer 2016] for more details on the XPBD integration of Cosserat rods. Then, to handle collisions, hair vertices are coupled with material point particles on an auxiliary Eulerian grid [Fei et al. 2021; Hsu et al. 2023; Huang et al. 2023]. For additional implementation details, we follow and refer readers to Hsu et al. [2023].

#### 4 PHYSICALLY GUIDED STRAND RECONSTRUCTION

In this section, we introduce our novel hair interpolation scheme utilizing real-time hair simulation data to reconstruct visually plausible rendered hair shapes.

To motivate our method, consider the simple case of two hair strands under gravity. No matter their shapes, the strands will exhibit similar internal forces in resistance to the same gravity field. Notably, the forces themselves do not specify a particular hair shape. So, as long as we obtain similar internal forces from nearby guides, the rendered hairs should be able to deform naturally according to their rest shapes. Hence, internal forces should be interpolated before reconstructing positions. We call this process as *force-based position reconstruction*.

Though intuitive, performing such an interpolation robustly and efficiently is challenging. Unlike conventional gradient-domain shape reconstruction [Huang et al. 2006; Levin et al. 2004], which amounts to solving a linear system, the position of a Cosserat rod is related non-linearly to forces due to the incorporation of the quaternion  $\mathbf{q}_i$ . Therefore, the position is typically solved using a non-linear global optimization [Winkler et al. 2010]. However, these optimizations cannot be performed at real-time in our hair interpolation scenario.

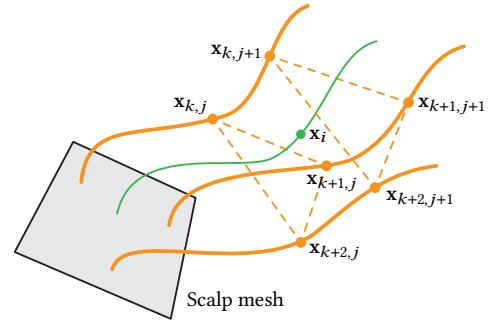
From another perspective, there exists a natural correspondence between conventional rod models and differential coordinates approaches in force-based position reconstruction. Since most rod models [Bergou et al. 2008; Bertails et al. 2006; Kugelstadt and Schömer 2016] consider quadratic potentials with respect to strain, the potential energy derivative (i.e., force) is a simple scalar multiple of the strain. As such, our method can also be interpreted as interpolating strains prior to position reconstruction.

In the following, we begin with Sec. 4.1 by formulating our constraint-based shape reconstruction scheme, which computes positions and orientations that generate our desired internal forces. We further propose several techniques to improve the robustness and visual quality of our solver, including penetration resolution (Sec. 4.2), drift correction (Sec. 4.3), and warm-starting (Sec. 4.4).

##### 4.1 Force-based Reconstruction

Our method requires an existing method to compute interpolated forces on each rendered hair. To this end, we employ Conventional Linear Hair Skinning (LHS). We use the double subscript  $k,j$  to denote the  $j$ th ordered segment on the  $k$ th guide hair. With this notation, LHS uses a linear interpolation stencil to derive the displacement of rendered hair as:

$$\mathbf{x}_i - \mathbf{x}_i^0 = \sum_{k \in \mathcal{N}} \sum_j w_{ijk} (\mathbf{x}_{k,j} - \mathbf{x}_{k,j}^0), \quad (9)$$



**Fig. 3.** Conventional Linear Hair Skinning (LHS). Segments from three guide hairs (orange) form a triangular prism and are used to interpolate the rendered hair (green) in a linear skinning fashion.

which is locally supported on the small neighborhood set  $\mathcal{N}$  of adjacent guide hairs, and we again use superscript  $0$  to indicate rest pose. Fig. 3 demonstrates the conventional interpolation scheme using three guide hairs forming a triangular prism for linear skinning fashion. The barycentric weights  $w_{ijk}$  denote the contribution from the  $j$ th vertex of the  $k$ th guide hair to the  $i$ th vertex of a rendered hair, which is precomputed for each rendered hair vertex  $\mathbf{x}_i^0$ . Instead of interpolating positions, however, we adopt the linear interpolation stencil for stretching forces:

$$\mathbf{f}_i^{\text{sim}} = \sum_{k \in \mathcal{N}} \sum_j w_{ijk} \mathbf{f}_{k,j}^{\text{ss}}, \quad (10)$$

where  $\mathbf{f}_{k,j}^{\text{ss}}$  is the force provided by the simulator on the  $j$ th vertex of the  $k$ th guide hair. The superscript  $\text{sim}$  denotes a variable provided by the simulator and used for reconstruction.

Our goal is then to find the set of segment positions and orientations that reproduce the target force  $\mathbf{f}_i^{\text{sim}}$ . This problem, however, is significantly under-determined in general since multiple sets of positions and orientations can reproduce the target force. To resolve this ambiguity, we utilize the observation that orientations typically converge very rapidly. As a result, non-zero net torques can contain spurious noises, especially in a less-accurate time-integration scheme such as XPBD [Macklin et al. 2016]. We thus decide to further constrain our problem by assuming that the net torque  $\tau_i^{\text{net}} = 0$  within each rendered hair strand. Note that individual bending and torque can still emerge as a part of our interpolation. We only specify the net torque at each segment. Put together, vertex positions can be computed as the solution that matches force with zero net torque under unit quaternion orientations. To write constraints more precisely, we have:

$$\forall i : \begin{cases} \mathbf{f}_i^{\text{ss}} \triangleq \frac{k^{\text{ss}}}{l_i} (\frac{\mathbf{x}_{i+1} - \mathbf{x}_i}{l_i} - \mathbf{d}_{i,0}) = \mathbf{f}_i^{\text{sim}} \\ \tau_i^{\text{net}} \triangleq \tau_i^{\text{ss}} + \tau_{i,i-1}^{\text{bt}} + \tau_{i,i}^{\text{bt}} = \lambda_i \mathbf{q}_i \\ \|\mathbf{q}_i\| = 1 \end{cases}, \quad (11)$$

where the Lagrangian multiplier  $\lambda_i$  is used to satisfy the unit quaternion constraints. As any extraneous torque along  $\mathbf{q}_i$  cannot move the same unit quaternion  $\mathbf{q}_i$  itself, the changing of  $\lambda_i$  does not affect the overall torque balance. Although these constraints are independent for each rendered hair, finding a solution for this nonlinear system is still highly non-trivial.

To devise an efficient solver, we first note that the first set of constraints,  $\mathbf{f}_i^{\text{ss}} = \mathbf{f}_i^{\text{sim}}$ , forms a tridiagonal linear system in terms of the vertices  $\mathbf{x}_i$ . Indeed, given the tangents  $\mathbf{d}_{i,3}$ , we can fix  $\mathbf{x}_{i-1}$  and solve for  $\mathbf{x}_i$  to satisfy the  $i$ th equation. With the first vertex  $\mathbf{x}_0$  fixed on the scalp, the linear system is fully determined and can be solved starting at the hair root and working towards the hair tips, leading to the following succinct formula for the vertex positions:

$$\mathbf{x}_i = \mathbf{x}_0 + \sum_{m=0}^{i-1} l_m \left( \frac{\mathbf{f}_m^{\text{sim}} l_m}{k^{\text{ss}}} + \mathbf{d}_{m,3} \right). \quad (12)$$

The bulk of our solver then lies in finding the correct segment orientation with tangent  $\mathbf{d}_{i,3}$ , which satisfies our constraint  $\tau_i^{\text{net}} = 0$  and in turn fully determines  $\mathbf{x}_i$ .

Expanding the full equations for torque (Eq. 6, Eq. 7, and Eq. 8) and removing any scalar terms of  $\mathbf{q}_i$ , we arrive at the following equivalent nonlinear system of equations to Eq. 11:

$$\begin{cases} -2l_i \mathbf{f}_i^{\text{sim}} \mathbf{q}_i \mathbf{e}_3 + k^{\text{bt}} \phi_{i-1} \mathbf{q}_{i-1} \bar{\mathbf{q}}_{i-1}^0 + k^{\text{bt}} \phi_i \mathbf{q}_{i+1} \bar{\mathbf{q}}_i^0 - \lambda_i \mathbf{q}_i = 0 \\ \|\mathbf{q}_i\| = 1 \end{cases} \quad (13)$$

in which  $\mathbf{f}_i^{\text{sim}} \mathbf{q}_i \mathbf{e}_3$  is a 4D vector. Since we only use the solution for rendering hairs instead of simulation, we do not require solving Eq. 13 exactly. As such, we devise an approximate solution using local constraint projections in a Gauss-Seidel fashion. Instead of considering the entire global system at once, we satisfy the segment orientations and their associated constraints individually on a per-segment basis in each local step.

Although the global system is nonlinear, treating the segments locally allows us to take advantage of the linear nature of quaternion multiplication. We arrange the torque terms into a linear system of  $\mathbf{q}_j$  and rewrite the torque-balancing condition as:

$$-2l_i \mathbf{f}_i^{\text{sim}} \mathbf{q}_i \mathbf{e}_3 \triangleq \mathbf{A}_i \mathbf{q}_i = \mathbf{b}_i \triangleq -k^{\text{bt}} \left( \phi_{i-1} \mathbf{q}_{i-1} \bar{\mathbf{q}}_{i-1}^0 + \phi_i \mathbf{q}_{i+1} \bar{\mathbf{q}}_i^0 \right), \quad (14)$$

where the left-hand side is encoded as a  $4 \times 4$  linear matrix  $\mathbf{A}_i$ , and the right-hand side is encoded as a 4D vector  $\mathbf{b}_i$ . If we assume that  $\mathbf{q}_{i-1}$  and  $\mathbf{q}_{i+1}$  are fixed, Eq. 13 takes the following form:

$$\begin{cases} (\mathbf{A}_i - \lambda_i \mathbf{I}_4) \mathbf{q}_i = \mathbf{b}_i \\ \|\mathbf{q}_i\| = 1. \end{cases} \quad (15)$$

Solving the 4-dimensional sub-system Eq. 15 yields an update rule for the orientation of a single rendered hair segment. Recall that solving this system exactly amounts to finding the scalar  $\lambda_i$  leading to a unit quaternion solution, which, in turn, requires solving the quartic polynomial:

$$\|(\mathbf{A}_i - \lambda_i \mathbf{I}_4)^{-1} \mathbf{b}_i\| = 1. \quad (16)$$

Although robust algorithms such as the bisection method exist for solving quartic polynomials, doing so for every segment of the rendered hair is highly inefficient on the GPU. As such, we instead propose a heuristic approach to first over-estimate  $\lambda_i$  by taking  $\lambda_i = \|2l_i \mathbf{f}_i^{\text{sim}}\| + \|\mathbf{b}_i\|$ , leading to a  $\|\mathbf{q}_i\| < 1$ , and then normalize  $\mathbf{q}_i$ . To explain this approach, we introduce the following theorem:

**THEOREM 4.1.**  $\mathbf{A}_i$  is a symmetric matrix with two pairs of eigenvalues at  $\pm \|2l_i \mathbf{f}_i^{\text{sim}}\|$ . Furthermore, the inversion of  $\mathbf{A}_i - \lambda_i \mathbf{I}_4$  takes the

following closed form:

$$\begin{cases} \mathbf{v} \triangleq -2l_i \mathbf{f}_i^{\text{sim}} \\ (\mathbf{A}_i - \lambda_i \mathbf{I}_4)^{-1} = \frac{1}{\|\mathbf{v}\|^2 - \lambda^2} \begin{pmatrix} \lambda + \mathbf{v}_2 & 0 & -\mathbf{v}_0 & \mathbf{v}_1 \\ 0 & \lambda + \mathbf{v}_2 & -\mathbf{v}_1 & -\mathbf{v}_0 \\ -\mathbf{v}_0 & -\mathbf{v}_1 & \lambda - \mathbf{v}_2 & 0 \\ \mathbf{v}_1 & -\mathbf{v}_0 & 0 & \lambda - \mathbf{v}_2 \end{pmatrix}. \end{cases}$$

**Theorem 4.1** can be verified via the attached WxMaxima code. Using an Eigen analysis, we can see that setting  $\lambda_i = \pm(\|2l_i \mathbf{f}_i^{\text{sim}}\| + \|\mathbf{b}_i\|)$  would always lead to a  $\|\mathbf{q}_i\| < 1$ , i.e., the magnitude of  $\lambda_i$  is over-estimated. Note that although the choice of either  $\lambda_i$  does not affect the torque-equilibrium condition,  $\lambda_i$  can affect the local stability of the hair strand near the configuration of  $\mathbf{q}_i$ . Indeed, if the interpolated result is used in a hypothetical simulation, a large positive  $\lambda_i$  would have a stabilizing effect that pushes a deviated hair strand back to the configuration  $\mathbf{q}_i$ , i.e., our approximate solution slightly exaggerates the stabilizing effect.

Put together, we propose the following closed-form solution for  $\mathbf{q}_i$ :

$$\begin{cases} \lambda_i \triangleq \|2l_i \mathbf{f}_i^{\text{sim}}\| + \|\mathbf{b}_i\| \\ \mathbf{q}_i \triangleq \frac{(\mathbf{A}_i - \lambda_i \mathbf{I}_4)^{-1} \mathbf{b}_i}{\|(\mathbf{A}_i - \lambda_i \mathbf{I}_4)^{-1} \mathbf{b}_i\|}, \end{cases} \quad (17)$$

which is very efficient to implement using the closed-form inversion of  $\mathbf{A}_i - \lambda_i \mathbf{I}_4$  in Theorem 4.1. Although we slightly underestimate the effect of the target force using this  $\lambda_i$ , in practice, we find the impact to be minimal. Our approximate solver then only has to solve the sub-systems from root to tip until termination conditions hold. In the following, we propose several extensions to our interpolation framework to improve visual quality and performance.

## 4.2 Penetration Correction

Penetration correction can be necessary for protruding surface features, like ears and noses. Although our guide hair simulator already incorporates collisions, it cannot guarantee that interpolated hairs are penetration-free. One naive solution for resolving penetration is to project the final position outside any colliders using a Signed Distance Field (SDF), denoted as  $\psi$ . However, as shown in Fig. 13, projecting the final positions directly often invariably causes similar visual artifacts in rendered hair geometry, leading to poor render quality. This is because the orientations of hair segments are not properly modified to reflect the shift in position due to the projection.

To make collisions handling for individual rendered hair to be properly reflected in hair reconstruction, we introduce a SDF-based penetration energy  $E_i^{\text{pen}}$  with stiffness  $k^{\text{pen}}$ , which is defined vertex-wise as:

$$E_i^{\text{pen}} = \frac{k^{\text{pen}}}{2} \min(0, \psi(\mathbf{x}_i))^2. \quad (18)$$

We then plug the position reconstruction Eq. 12 into  $E_i^{\text{pen}}$ , casting it as a function on the segment orientations. As a result, the vertex-wise penetration energy imposes torque locally as:

$$\tau_{i,i}^{\text{pen}} = -2k^{\text{pen}} l_i \min(0, \psi(\mathbf{x}_i)) \nabla \psi(\mathbf{x}_i) \mathbf{q}_i \mathbf{e}_3. \quad (19)$$



**Fig. 4.** Given guide hairs, while LHS introduces zig-zag artifacts, force-based reconstruction would lead to undesired hair shapes that are far from the guide hairs. At the rightmost, we show that simply blending those two solutions in half would not resolve the artifacts.

Following the same logic as Sec. 4.1, we can then incorporate this term into  $\tau_i^{\text{ss}}$  in Eq. 11 by the following redefinition:

$$\tau_i^{\text{net}} \triangleq \tau_i^{\text{ss}} + \tau_{i,i-1}^{\text{bt}} + \tau_{i,i}^{\text{bt}} + \tau_{i,i}^{\text{pen}} = \lambda_i \mathbf{q}_i. \quad (20)$$

As we typically only use a single Gauss-Seidel sweep in practice, the SDF value of each vertex can be unknown before positions are computed. Therefore, we choose to first solve each vertex assuming that all  $\psi(\mathbf{x}_j) = 0$ , i.e., without considering  $E^{\text{pen}}$ . We then query  $\psi(\mathbf{x}_j)$  at the reconstructed positions according to Eq. 12, before performing a second solve with  $E^{\text{pen}}$ , if needed. In practice, this procedure can be implemented very efficiently on GPU with marginal overhead. While this approach can inherit known temporal coherence issues from sharp SDF discontinuities, we found the performance gain advantageous for our particular use case. In general, we found the issues with SDF-caused temporal incoherence to be minor to negligible in all our examples, as shown in our supplemental materials.

#### 4.3 Drift Correction

Due to the discretized nature of our hair and the approximate nature of our solutions, errors will accumulate in each hair segment as we solve from root to tip. Since internal force is a local measure, it is translation invariant and does not penalize translations. As such, some hairs can drift undesirably far from the guide hairs along the strand. This is especially problematic for strands with little internal stress as the entire strand becomes dependent on the initial root orientation. While we want to preserve the shape of the hair, we also want the interpolated hair shapes to be consistent with those of the guide hairs. A common approach would be to correct this error by directly blending a stable solution with the output. Unfortunately, directly blending the reconstructed position of our method with that from LHS would re-introduce the artifacts of conventional interpolation schemes and diminish the benefit of our method (see Fig. 4).

Instead, we propose a blending scheme within our force-reconstruction framework. Note that if the interpolated force  $\mathbf{f}_i^{\text{sim}} = 0$ , Eq. 15 has the following trivial solution, denoted as  $\hat{\mathbf{q}}_i$ :

$$\hat{\mathbf{q}}_i \triangleq \frac{-\mathbf{b}_i}{\|\mathbf{b}_i\|} \quad \text{and} \quad \hat{\mathbf{d}}_{i,3} \triangleq \hat{\mathbf{q}}_i \mathbf{e}_3 \bar{\mathbf{q}}_i. \quad (21)$$

Plugging this solution into the definition of  $\mathbf{f}_i^{\text{ss}}$  in Eq. 11, we derive an estimation of the stretch force  $\hat{\mathbf{f}}_i^{\text{ss}}$  as:

$$\hat{\mathbf{f}}_i^{\text{ss}} \triangleq \frac{k^{\text{ss}}}{l_i} \left( \frac{\mathbf{x}'_{i+1} - \mathbf{x}_j}{l_i} - \hat{\mathbf{d}}_{i,3} \right), \quad (22)$$

where  $\mathbf{x}'_{i+1}$  can be any desirable position. For example,  $\mathbf{x}'_{i+1}$  can be taken from LHS-based prior works, e.g., Chai et al. [2017], to address

finer collisions. An interesting consequence is that our force-based reconstruction can then act as a filter for physically plausible hair geometries for any given  $\mathbf{x}'_{i+1}$ . However, here, we choose to use a fast static weight LHS scheme with weights based on the closest polyline segments. This is to avoid the requirement for training data and for performance. Our drift correction is then achieved by blending  $\hat{\mathbf{f}}_i^{\text{ss}}$  and  $\mathbf{f}_i^{\text{sim}}$  as:

$$\mathbf{f}_i^{\text{sim}} \leftarrow \alpha \hat{\mathbf{f}}_i^{\text{ss}} + (1 - \alpha) \mathbf{f}_i^{\text{sim}}, \quad (23)$$

where  $\alpha$  is taken as a small blending weight (of  $0.05 \sim 0.1$  in our examples).

#### 4.4 Warm Starting

As we use a very small number of iterations to solve Eq. 13 in practice for performance, the quality of the resulting quaternion significantly relies on a reasonable initialization. One typical solution is to use the orientation from a previous frame as the initial guess. However, significant overheads would have to be introduced to write back and update new solutions. Instead, we would like to opt for a solution that allows us to discard updates without performing memory writes. Our strategy is to assume that the bending energy of the next segment lies in its local minimum, which is reached when:

$$\mathbf{q}_{i+1} \bar{\mathbf{q}}_i^0 = \mathbf{q}_i. \quad (24)$$

Since the torque along  $\mathbf{q}_i$  does not affect the imaginary components, this simply results in the corresponding term in Eq. 13 to be taken out. This approach results in a faster hair interpolation scheme.

Finally, as an interesting side effect of our choice of warm starting, we can safely assume that  $\phi = 1$  at all times in  $\mathbf{C}_j^{\text{bt}}$ . When using our choice of  $\lambda$ ,  $\mathbf{A}_i - \lambda_i \mathbf{I}_4$  will always have negative eigenvalues that result in a solution closer to the positive pole, making our implementation slightly less complex in practice.

## 5 RESULTS

We implement both our simulation and interpolation using C++ and CUDA. Unless otherwise stated, we measure performance on an NVIDIA RTX 4090 GPU. For our simulation, we measure about 0.2 ms per 1 ms timestep with only 128 guide hairs. For our interpolation, we split the algorithm into two CUDA kernel calls. The first kernel call computes the internal force on each guide hair segment. The second kernel call then uses one thread per hair to compute their final positions in a single pass from the root to the tip. For drift correction and as a baseline, we implement a traditional static weight LHS scheme with weights based on the closest polyline segments.

**Algorithm 1:** Pseudocode for our hair interpolation looped over one hair strand.

```

foreach  $i \in [0, \text{Num Vertex in Hair} - 1]$  do
    // Compute target force
     $\mathbf{f}_i^{\text{sim}} \leftarrow \text{LHS based force (Eq. 10)}$ 
    // Compute drift correction
     $\mathbf{x}'_{i+1} \leftarrow \text{LHS based position (Eq. 9)}$ 
     $\hat{\mathbf{f}}_i^{\text{ss}} \leftarrow \text{Eq. 22 given } \mathbf{x}'_{i+1}$ 
     $\mathbf{f}_i^{\text{sim}} \leftarrow (1 - \alpha)\mathbf{f}_i^{\text{sim}} + \alpha\hat{\mathbf{f}}_i^{\text{ss}}$ 
    // Solve for  $\lambda$ 
     $\mathbf{b}_i \leftarrow -k^{\text{bt}}\phi_{i-1}\mathbf{q}_{i-1}\mathbf{q}_{i-1}^0$ 
     $\mathbf{v} \leftarrow -2l_i\mathbf{f}_i^{\text{sim}}$ 
     $\lambda \leftarrow \|\mathbf{v}\| + \|\mathbf{b}_i\|$ 
    // Use Theorem 4.1 given  $\mathbf{v}$ ,  $\mathbf{b}_i$ , and normalize
     $\mathbf{q}_i \leftarrow [\mathbf{A}_i - \lambda_i \mathbf{I}_4]^{-1}\mathbf{b}_i$ 
     $\mathbf{q}_i \leftarrow \mathbf{q}_i / \|\mathbf{q}_i\|$ 
    // Solve for  $\mathbf{x}_{i+1}$ 
     $\mathbf{x}_{i+1} \leftarrow \mathbf{x}_i + l_i [\mathbf{f}_i^{\text{sim}}l_i/k^{\text{ss}} + \mathbf{d}_{i,3}]$ 
    // Check SDF for collision
    if  $\psi(\mathbf{x}_{i+1}) < 0$  then
        // Update  $\mathbf{v}$  and resolve
         $\mathbf{v} \leftarrow \mathbf{v} - 2k^{\text{pen}}l_i\psi(\mathbf{x}_{i+1})\nabla\psi(\mathbf{x}_{i+1})$ 
         $\lambda \leftarrow \|\mathbf{v}\| + \|\mathbf{b}_i\|$ 
         $\mathbf{q}_i \leftarrow [\mathbf{A}_i - \lambda_i \mathbf{I}_4]^{-1}\mathbf{b}_i / \|[\mathbf{A}_i - \lambda_i \mathbf{I}_4]^{-1}\mathbf{b}_i\|$ 
         $\mathbf{x}_{i+1} \leftarrow \mathbf{x}_i + l_i [\mathbf{f}_i^{\text{sim}}l_i/k^{\text{ss}} + \mathbf{d}_{i,3}]$ 
    end
end

```

In contrast to prior works that use training [Chai et al. 2017; Lyu et al. 2022], our method requires no pre-computation, no training data, and is simple to implement. In particular, the force reconstruction only represents some dozen extra lines of code on top of any existing interpolation, as shown in Algorithm 1. Correspondingly, the overhead is extremely small. To further maximize performance, we packed the data required for force reconstruction together. For each vertex, this consists of  $\mathbf{q}_{r,j}$ ,  $l_j$ , and  $k^{\text{norm}}$ , which is the normalized stiffness computed by  $k^{\text{norm}} = k^{\text{bt}}/k^{\text{ss}}$ . Conceptually, we divide both sides of Eq. 13 by  $k^{\text{ss}}$  such that we only need to load one stiffness value for each segment. For all our scenes,  $k^{\text{pen}}$  is set to  $1e4$  as if it were a simple quadratic contact penalty energy.

### 5.1 Comparisons to LHS

We demonstrate our method on various real-world hairstyles captured from Unreal Metahumans [Epic 2024], multi-view 3D reconstruction [Luo et al. 2013], and computed tomography [Shen et al. 2023]. As our interpolation is designed specifically for real-time applications, we use low-resolution simulations of only 128 to 256 guide hairs each. This proves to be a very challenging use case for traditional LHS, especially in cases involving curly hair.

Fig. 1 demonstrates this challenge. As the curls stretch, bend, and unwind, the non-linear motion causes significant artifacts in the

fine geometry of the hair. In contrast, our method can efficiently recreate plausible interpolated rendered hairs that visually preserve the original hairstyle. It is true even when the same hairstyle is simulated with  $16\times$  the number of guide hairs, as shown in Fig. 5, which takes 1.6 ms per frame for the simulation and is too expensive for most real-time applications. Since the issue fundamentally arises from the shape of each individual rendered hair, adding more guide hairs does little to rectify the artifacts. On the other hand, our method can produce artifact-free interpolations with extremely sparse guide hairs. Note that, as our interpolation solves for the quasistatic shape of rendered hairs with interpolated forces, it does not depend on or affect the dynamic state of the simulator.

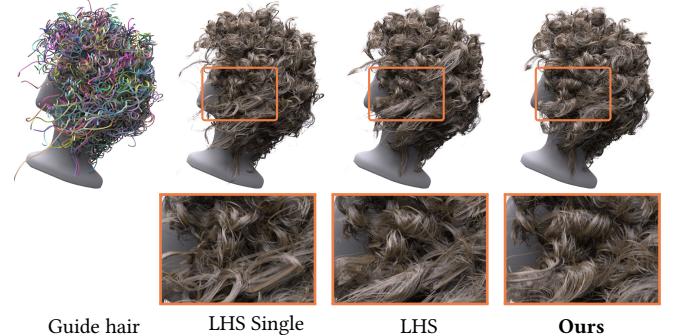


Fig. 5. Artifacts can still easily occur when the hairstyle is simulated with a large number of guide hairs. Here, we use 2048 guide hairs.

Fig. 6 demonstrates the robustness of our method to hair length. In this example, traditional LHS creates significant artifacts as the long strands unwind. Even only using a single guide hair for each rendered hair (LHS single), the simple motion of unwinding distorts the shapes of the interpolated strands into unrecognizable zig-zags. Our method produces artifact-free interpolations while remaining stable despite the fast and complex swinging motions of long hairs.

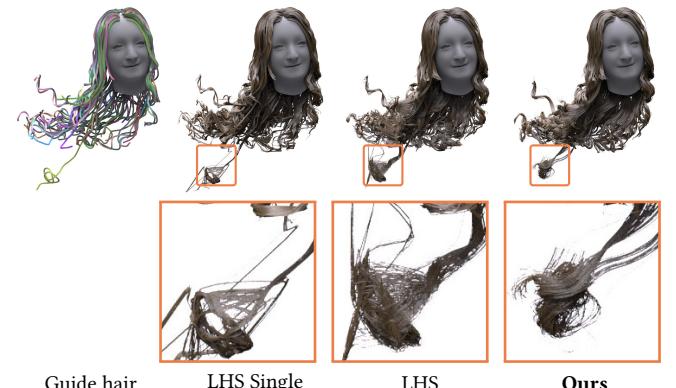
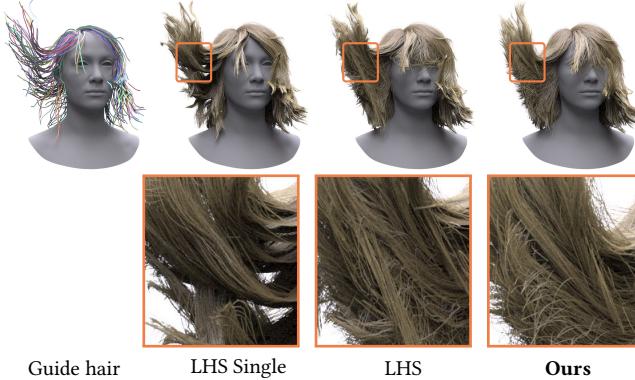


Fig. 6. When long curly hair unwinds and rotates in unpredictable ways, even interpolating rendered hair with only one guide hair can cause significant artifacts in hair geometry. Our method is able to handle this case robustly and efficiently.

The visual improvements of our method are also not limited to curly hair. The straight hairstyle in Fig. 7 exhibits significant

artifacts with LHS, as guide hairs separate. Although this can be remedied by restricting each rendered hair to only use a single guide hair (as in Fig. 7 LHS single), the result creates obvious clumping in motion. In cases where this clumping is undesirable, obtaining robust weights without relying on training data is highly difficult. Despite relying on the same exact interpolation method in both force interpolation and drift correction, our method successfully avoids the many artifacts from LHS in all our examples.



**Fig. 7.** Even with straight hairstyles, both one (LHS single) and triple (LHS) guides per rendered hair introduce odd clumping. Despite the reliance on the same LHS scheme for interpolating forces, our method can effectively remove the various artifacts in geometry.

To further demonstrate the robustness of our method under realistic motions, we test our interpolation using motion capture and animation data in Fig. 8 and Fig. 10. As shown, animations with large and sudden head motions very rapidly create chaotic movements that can be unaccounted for during training or pre-computation. Despite this, our interpolation can produce realistic interpolations with very few guide hairs required. Fig. 9 demonstrates that visual artifacts caused by LHS still exist even with a slow motion, while our method remains resistant to geometric artifacts.

**Performance.** We present the cost of our interpolation in Table 1. Compared to the LHS interpolation that our examples are based on, our method only presents a 20% overhead in total interpolation time. Even for the largest example with over 100K hair strands, our method never required more than half a millisecond, satisfying the real-time requirement.

**Table 1.** Performance of our method against LHS using three guide hairs. Timings in microseconds ( $\mu\text{s}$ ) per frame are measured on an Nvidia RTX 4090 GPU. Overhead is measured by our method compared against LHS using the same number of guide hairs per rendered hair. Guide and rendered hairs have the same number of vertices per strand.

	Guides/Hairs	Vertices	LHS	Ours	Overhead
Josh (Fig. 1)	128 / 106,686	1,706,976	283 $\mu\text{s}$	346 $\mu\text{s}$	22%
Alice (Fig. 6)	128 / 30,307	1,939,648	360 $\mu\text{s}$	425 $\mu\text{s}$	17%
Hadley (Fig. 7)	256 / 64,663	1,034,608	163 $\mu\text{s}$	199 $\mu\text{s}$	22%
Danielle (Fig. 8)	256 / 46,706	747,296	111 $\mu\text{s}$	137 $\mu\text{s}$	23%

**Ablation studies.** As demonstrated in Fig. 11, the decision not to use the solution of prior frames does not significantly impact the quality of the final results. The overall appearance of the hairstyle remains faithful to the original from the first iteration and onwards. Even fully allowing our method to converge, the differences are minor. Furthermore, by eliminating the extra data movement, we observe an over 52% speedup in interpolation time. Compared to traditional LHS, this represents an approximate drop in overhead from 85% to our 20%.

We perform further ablation studies in Fig. 12 and 13. In Fig. 12, without our drift correction, strands can easily veer off course, depending on the initial orientations at the hair root. This is especially true with hairs experiencing weightlessness. With drift correction, this issue is largely resolved with minimal degradation in final hair geometry.

Fig. 13 demonstrates the importance of incorporating our penetration energy. For sharp SDF discontinuities, simple position projections can fail to improve the result meaningfully compared to no collisions. In contrast, our penetration energy can consider the rest shapes for a higher-quality result.

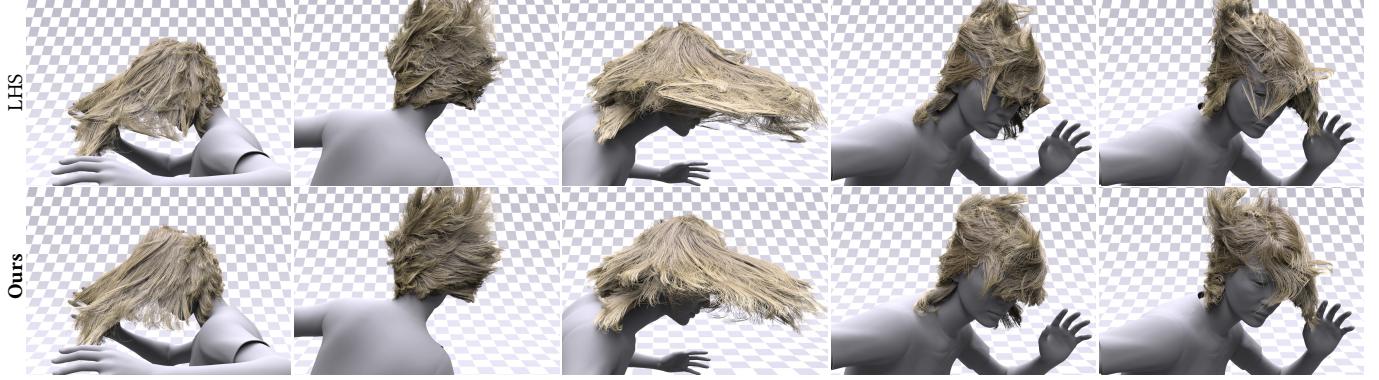
## 5.2 Comparison with Neural Hair Interpolation

We compare our interpolation method with the only available open-source neural interpolation work [Shen et al. 2023], in which a variational autoencoder (VAE) is pre-trained to encode guide hairs into latent vectors. These latent vectors are then interpolated based on barycentric coordinates on the scalp and decoded into rendered hairs. Fig. 14 presents a side-by-side comparison of a curly hairstyle interpolated using 2048 guide hairs. The results show that our interpolation can faithfully reproduce the hairstyle, while the neural interpolation simply enriches the hair count through interpolation without considering the rest pose of the hairstyle. Additionally, as an offline method, Shen et al. [2023] take 358 seconds on an Nvidia RTX 3080 to interpolate 59220 hair strands with 256 vertices per strand, several orders of magnitude slower than ours. Furthermore, when compared to the real-time neural interpolation proposed by Lyu et al. [2022], which takes 151 ms to interpolate 1M vertices, our method requires only 1.6 ms to interpolate 1M vertices (for Hadley) when measured on the same hardware (Nvidia GTX 1080), achieving about two orders of magnitude faster results. Notably, our method does not necessitate the pre-simulation of a large dataset for training.

## 6 CONCLUSION

We have presented a novel, robust, and efficient physical-guided hair interpolation scheme for real-time applications. Our method uses LHS to interpolate the physical parameters and forces already readily available in real-time simulations, which are then used to reconstruct the hair vertex positions. This results in an interpolator that requires no training data and no pre-computation. We have demonstrated the effectiveness of our approach in challenging real-world scenarios with interpolation times far faster than alternatives, affirming our suitability for real-time applications.

**Future work and limitations.** An interesting future direction would be generalizing our method to other hair simulation frameworks, e.g., discrete elastic rods [Bergou et al. 2008] and



**Fig. 8.** Large separations in guide hairs can often cause errors in LHS weights to amplify. Although we do not use any dynamic guide or weight selection, our method remains resistant to geometric artifacts.



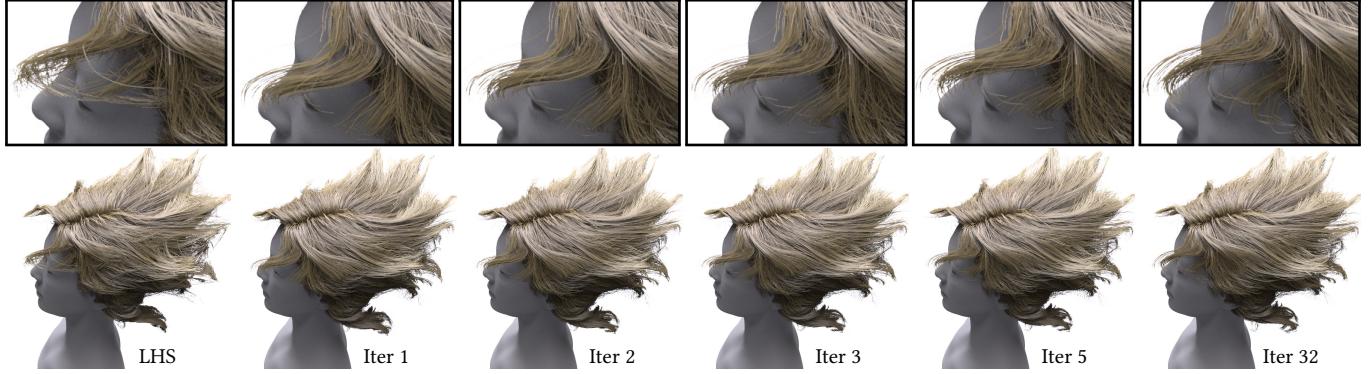
**Fig. 9.** Even with a slow motion, visual artifacts caused by LHS still exist, while our method remains resistant to geometric artifacts robustly.



**Fig. 10.** Despite only using 128 guide hairs, our interpolation remains robust under the large perturbations common in motion capture data.

altitude springs [Selle et al. 2008]. Although our core ideas still apply, significant work is needed to recreate our efficient constraint solver for each framework, which is non-trivial. Our interpolation

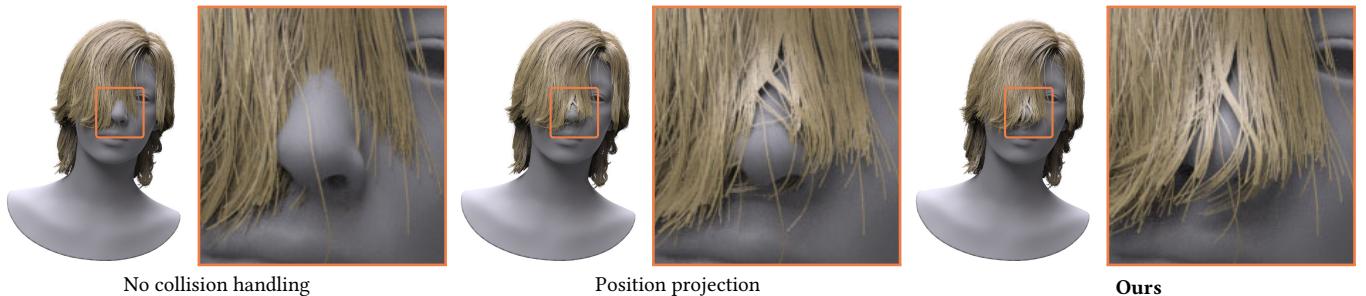
can also be incompatible with sag-free initialization methods [Hsu et al. 2023] that modify the rest shapes of hair strands to eliminate sagging at the beginning of simulations. Given that our method



**Fig. 11.** We show the result of our interpolation at various iterations starting with our initial guess in Sec. 4.4. The differences are minor, although there are some minor differences between the first and final converged iteration. Most importantly, compared to the leftmost LHS result, our solutions are artifact-free from the first iteration onwards, demonstrating the effectiveness of our initial guess.



**Fig. 12.** Comparison between LHS and ours with different drift correction blending parameters. Without drift correction, the flow of hairs that experience weightlessness (with little internal stress) become almost completely dependent on the root orientation.



**Fig. 13.** Directly projecting positions may result in vertices on alternating sides of a protrusion. By taking bending energies into consideration, our SDF penalty energy avoids this issue and produces strands that favor a consistent projection direction.



**Fig. 14.** Comparison with neural interpolation [Shen et al. 2023]: given 2048 guide hairs, our interpolation can faithfully reproduce the hairstyle, while the neural interpolation simply enriches the hair count through interpolation without considering the rest pose of the hairstyle.

relies on the natural rest shape of the hair, any modifications introduced by sag-free initialization techniques would require extra

consideration during initialization to preserve the style and ensure robustness. Finally, our method can exhibit less natural solutions due to the approximate solution scheme. For real-time performance, in particular, we do not consider the inter-segment coupling due to the penetration constraints. Efficient and more accurate solution techniques are left as future works.

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