

## Torsion of non-circular shaft

$$\begin{aligned} u &= -\theta y z \\ v &= \theta x z \\ w &= 0 \end{aligned}$$

for circular c/s



$$\begin{aligned} u &= -\theta y z \\ v &= \theta x z \\ w &= \theta \psi(x, y) \end{aligned}$$

non-circular c/s

Saint Venant's solution

undergoes out-of-plane

warping function. warping unlike circular c/s

$$\begin{aligned} \tau_{xz} &= G\theta \left( \frac{\partial \psi}{\partial x} - y \right) \\ \tau_{yz} &= G\theta \left( \frac{\partial \psi}{\partial y} + x \right) \end{aligned} \quad \left| \quad \begin{aligned} \tau_x &= \tau_y = \tau_z = 0 \\ \tau_{xy} &= 0 \end{aligned} \right.$$

Eqn. of equlib

⇒

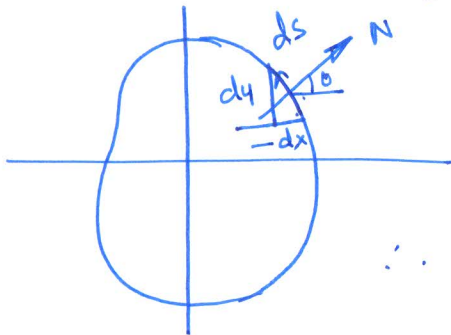
$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = 0$$

①

Boundary condns on the lateral surfaces

$$\tau_{xz} l + \tau_{yz} m = 0$$

$$\Rightarrow G\theta \left( \frac{\partial \psi}{\partial x} - y \right) l + G\theta \left( \frac{\partial \psi}{\partial y} + x \right) m = 0$$



$$\cos(Nx) = l = \frac{dy}{ds}$$

$$\cos(Ny) = m = -\frac{dx}{ds}$$

$$\therefore G\theta \left( \frac{\partial \psi}{\partial x} - y \right) \frac{dy}{ds} - G\theta \left( \frac{\partial \psi}{\partial y} + x \right) \frac{dx}{ds} = 0$$

∴ Saint Venant's solution requires a warping function satisfying eqns. ① and ②

## Torsion of non-circular shaft

- (i) cross-sectional shape is not distorted
- (ii) out-of-plane warping governed by  $\psi(x, y)$
- (iii) warping is constant along the length of the shaft
- (iv)  $\frac{d\phi}{dz} = \theta$  is constant
- (v) it is in pure shear

## Praedtl's stress function

$$\tau_{xz} = \frac{\partial \phi}{\partial y} \leftarrow \text{Praedtl's stress function}$$

$$\tau_{yz} = -\frac{\partial \phi}{\partial x}$$

Egns. of equilon

$$\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + \frac{\partial \tau_{xz}}{\partial z} = 0$$

$$\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + \frac{\partial \tau_{xz}}{\partial z} = 0$$

$$\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \tau_{xz}}{\partial z} = 0$$

$$\frac{\partial \phi}{\partial x \partial y} - \frac{\partial \phi}{\partial x \partial y} = 0$$

Egns. of equilon  
are satisfied.

$$\tau_{xz} = \frac{\partial \phi}{\partial y} = G\theta \left( \frac{\partial \phi}{\partial y} + y \right)$$

$$\tau_{yz} = -\frac{\partial \phi}{\partial x} = G\theta \left( \frac{\partial \phi}{\partial x} - x \right)$$

$$\boxed{\frac{\partial^2 \phi}{\partial y^2} + \frac{\partial^2 \phi}{\partial x^2} = -2G\theta} \quad \text{--- (1)}$$

Boundary condns on lateral surfaces

$$\tau_{xz} l + \tau_{yz} m = 0 \Rightarrow \frac{\partial \phi}{\partial y} \cdot \frac{dy}{ds} + \frac{\partial \phi}{\partial x} \cdot \frac{dx}{ds} = 0$$

$$\Rightarrow \boxed{\frac{d\phi}{ds} = 0} \quad \text{--- (2)}$$

$\phi$  is taken as zero on the boundary.

Praedtl's stress function should satisfy eqns. (1) and (2)

BCs on top and bottom surfaces

$$\hat{X} = \tau_{xz} \quad \text{and} \quad \hat{Y} = \tau_{yz}$$

Resultant

force in x-dir due to BC

on top and bottom surfaces.

$$\begin{aligned} S_x &= \iint_{xy} \hat{X} dx dy = \iint \tau_{xz} dx dy = \iint \frac{\partial \varphi}{\partial y} dx dy \\ &= \int dx \int \frac{\partial \varphi}{\partial y} dy = \oint \varphi dx \quad [\text{using Green's theorem}] \\ &= 0 \quad \text{as } \varphi \text{ is zero on the boundary.} \end{aligned}$$

$$\begin{aligned} S_y &= \iint_{xy} \hat{Y} dx dy = \iint \tau_{yz} dx dy = - \iint \frac{\partial \varphi}{\partial x} dx dy \\ &= - \int dy \int \frac{\partial \varphi}{\partial x} dx = - \oint \varphi dy \\ &= 0 \end{aligned}$$

Torsional moment  $M_t = \iint_{xy} (\hat{Y}x - \hat{X}y) dx dy$

$$= \iint_{xy} (\tau_{yz}x - \tau_{xz}y) dx dy = \iint -\frac{\partial \varphi}{\partial x} x dx dy - \iint \frac{\partial \varphi}{\partial y} y dx dy$$

$$= - \iint \frac{\partial}{\partial x} (\varphi x) dx dy - \iint \frac{\partial}{\partial y} (\varphi y) dx dy + 2 \iint \varphi dx dy$$

$$= - \oint \varphi x dy \Big|_{y=0}^{y=h} - \oint \varphi y dx \Big|_{x=0}^{x=b} + 2 \iint \varphi dx dy = 2 \iint \varphi dx dy$$

$$\therefore \boxed{M_t = 2 \iint \varphi dx dy}$$