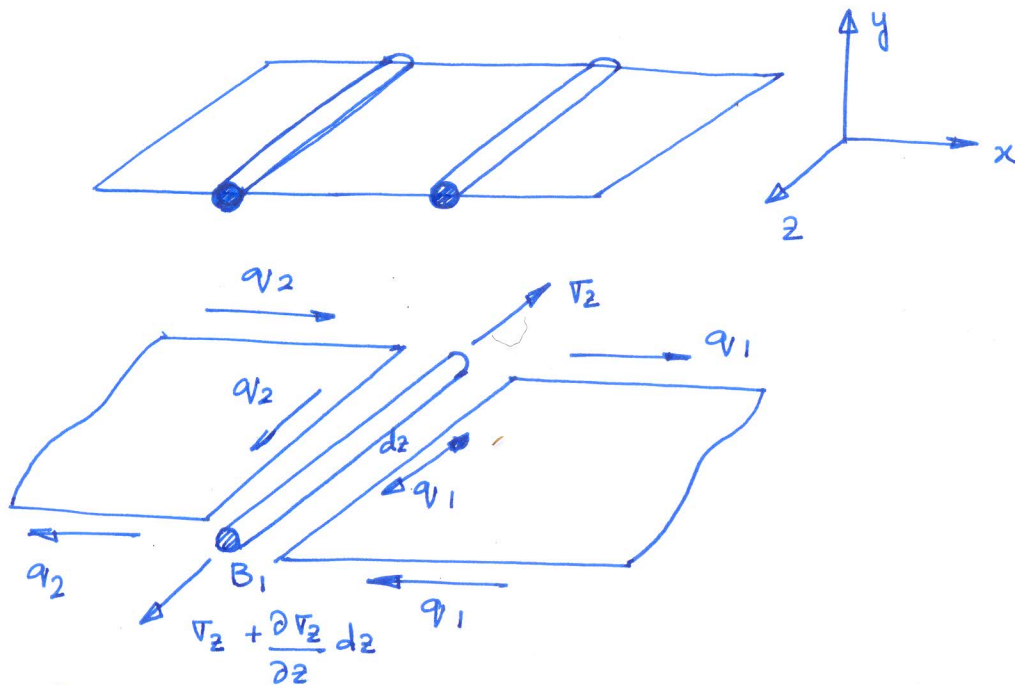


①

Shear of open section (skin-stringer) idealized beam



Considering force equilibrium in z-dir.

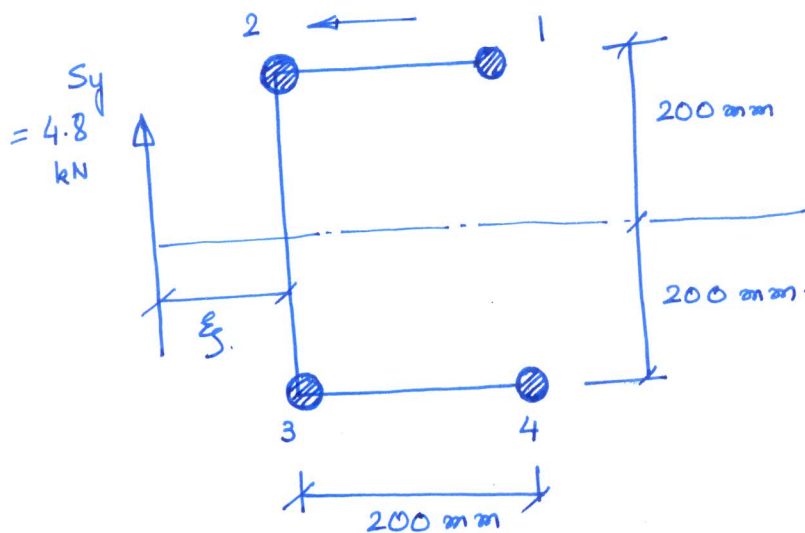
$$\left(\tau_2 + \frac{\partial \tau_2}{\partial z} dz \right) B_1 - \tau_2 B_1 - q_1 dz + q_2 dz = 0$$

$$\Rightarrow q_2 - q_1 = - \frac{\partial \tau_2}{\partial z} B_1$$

$$\Rightarrow q_2 - q_1 = - \left[\frac{\frac{\partial M_y}{\partial z} I_{xx} - \frac{\partial M_x}{\partial z} I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right] B_{1x} - \left[\frac{\frac{\partial M_x}{\partial z} I_{yy} - \frac{\partial M_y}{\partial z} I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right] B_{1y}$$

$$= - \left[\frac{S_x I_{xx} - S_y I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right] B_{1x} - \left[\frac{S_y I_{yy} - S_x I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right] B_{1y}$$

Ex
Shear flow in open c/s beam



Area of each boom = 300 mm^2

$$I_{xx} = 4 \times 300 \times (200)^2 = 48 \times 10^6 \text{ mm}^4$$

$$q_2 - q_1 = - \left[\frac{S_x I_{xx} - S_y I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right] B_r x_r - \left[\frac{S_y I_{yy} - S_x I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right] B_r y_r$$

$I_{xy} = 0$ and $S_x = 0$

$$q_2 - q_1 = - \frac{S_y}{I_{xx}} B_r y_r$$

For flange 12

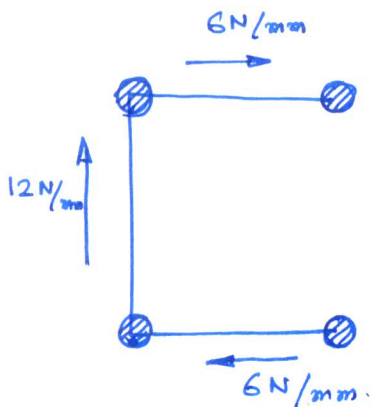
$$q_{12} = \frac{-4.8 \times 10^3}{48 \times 10^6} \times 300 \times 200 = -6 \text{ N/mm}$$

For web 23

$$q_{23} = \frac{-4.8 \times 10^3}{48 \times 10^6} \times 300 \times 200 - 6 = -12 \text{ N/mm}$$

For flange 34

$$q_{34} = \frac{-4.8 \times 10^3}{48 \times 10^6} \times 300 \times (-200) - 12 = -6 \text{ N/mm}$$



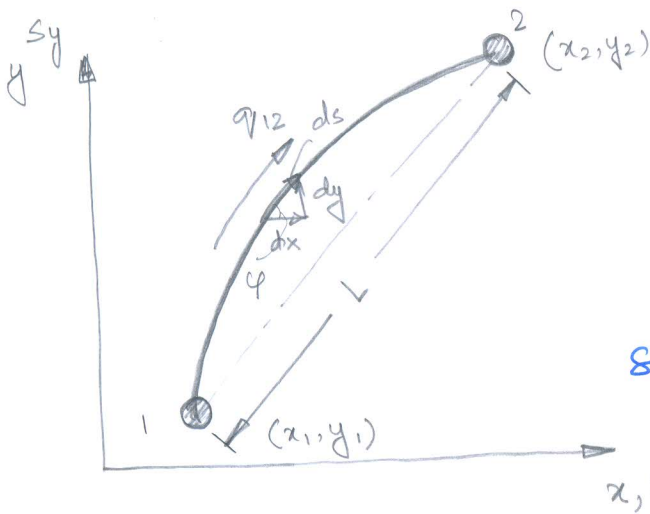
Shear center Let us assume that shear center is at a distance \bar{x}_s from the web as shown.

Taking moment about 3, we get

$$S_y \bar{x}_s = 6 \times 200 \times 400 = 480000$$

$$\Rightarrow \bar{x}_s = 100 \text{ mm}$$

(3)



$$S_x = \int q_{12} ds \cos \phi$$

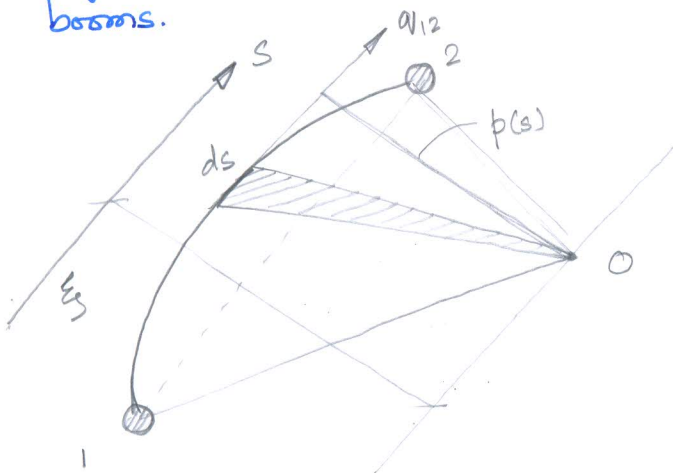
$$= q_{12} \int_{x_1}^{x_2} dx = q_{12} (x_2 - x_1)$$

Similarly,

$$S_y = q_{12} (y_2 - y_1)$$

$$S = \sqrt{S_x^2 + S_y^2} = q_{12} \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} = q_{12} L$$

∴ The resultant of the shear flow is equal to the shear flow multiplied by the straight line length between the booms.



Moment about O

$$\int q_{12} ds p(s) = 2 q_{12} A$$

Shear center

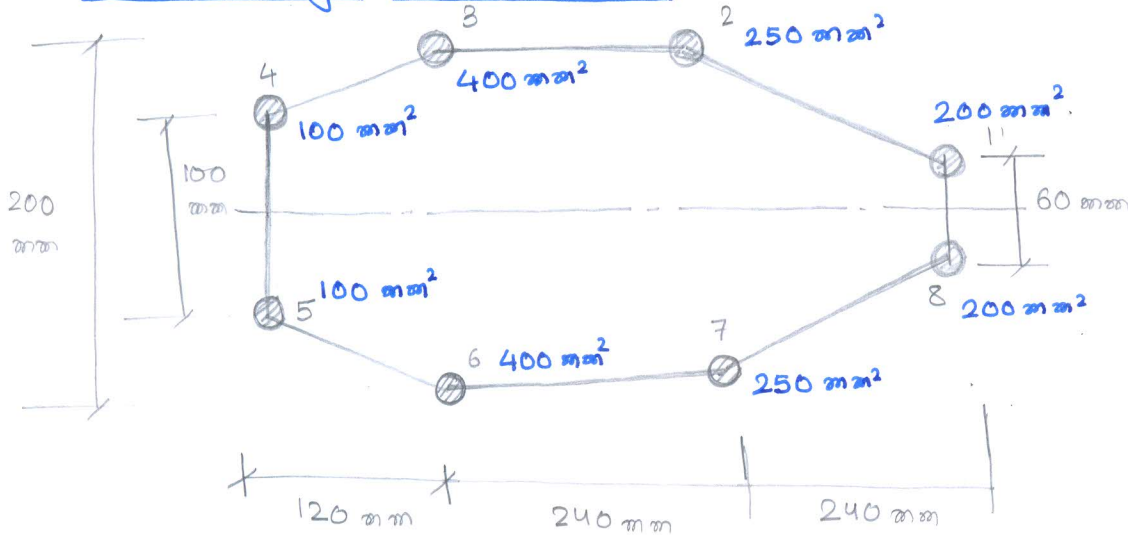
$$S e_s = 2 q_{12} A$$

$$= \frac{2 S}{L} A$$

$$\Rightarrow \boxed{e_s = \frac{2A}{L}}$$

(4)

Shear loading in closed c/s beam



Find the shear flow for $S_y = 10 \text{ kN}$ and the location of shear center

$$I_{xx} = 2 \left[200 \times (30)^2 + 250 \times (100)^2 + 400 \times (100)^2 + 100 \times (50)^2 \right]$$

$$= 13.86 \times 10^6 \text{ mm}^4$$

$$q_2 - q_1 = -\frac{S_y}{I_{xx}} B_r y_r \quad \text{Assuming } q_{23} = q_0$$

$$q_{34} = \frac{-10 \times 10^3}{13.86 \times 10^6} (400 \times 100) = -28.9 \text{ N/mm} + q_0$$

$$q_{45} = \frac{-10 \times 10^3}{13.86 \times 10^6} (100 \times 50) = \frac{-5 \times 10^7}{13.86 \times 10^6} - 28.9 + q_0 = -32.5 + q_0$$

$$q_{56} = \frac{-10 \times 10^3}{13.86 \times 10^6} (100 \times -50) + q_{45} = -28.9 + q_0$$

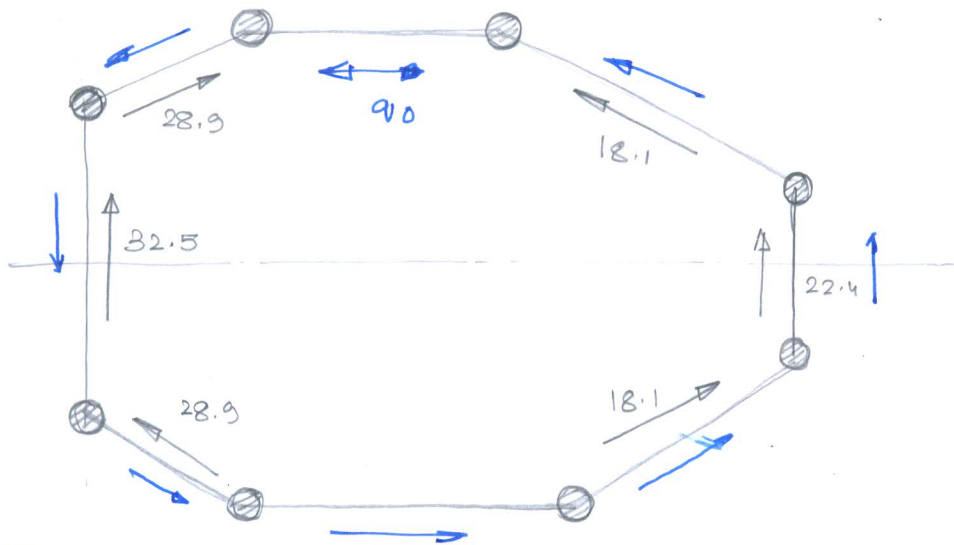
$$q_{67} = \frac{-10 \times 10^3}{13.86 \times 10^6} (400 \times -100) + q_{56} = q_0$$

$$q_{78} = \frac{-10 \times 10^3}{13.86 \times 10^6} (250 \times -100) + q_{67} = 18.1 + q_0$$

$$q_{81} = \frac{-10 \times 10^3}{13.86 \times 10^6} (200 \times -30) + q_{78} = 22.4 + q_0$$

$$q_{12} = 18.1 + q_0$$

(2)



$$\int Z ds = 0$$

$$\Rightarrow q_0 \left[2 \times 240 + 60 + 100 + 2 \sqrt{120^2 + 50^2} + 2 \times \sqrt{70^2 + 240^2} \right] - 28.9 \times 2 \times \sqrt{120^2 + 50^2} - 32.5 \times 100 + 22.4 \times 60 + 2 \times 18.1 \times \sqrt{70^2 + 240^2} = 0$$

$$\Rightarrow q_0 \left[480 + 160 + 2 \times 130 + 2 \times 250 \right] - 28.9 \times 2 \times 130 - 32.5 \times 100 + 22.4 \times 60 + 2 \times 18.1 \times 250 = 0$$

$$\Rightarrow 1400 q_0 - 7514 - 3250 + 1344 + 9050 = 0$$

$$\Rightarrow q_0 = 0.264 \text{ N/mm}$$