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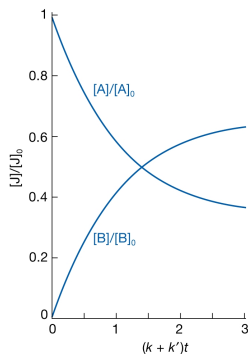
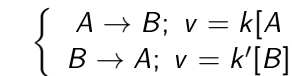
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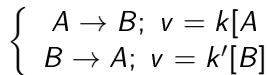
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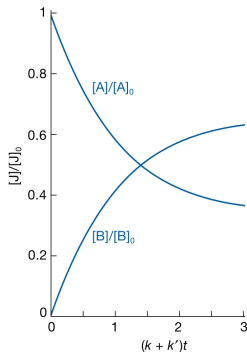
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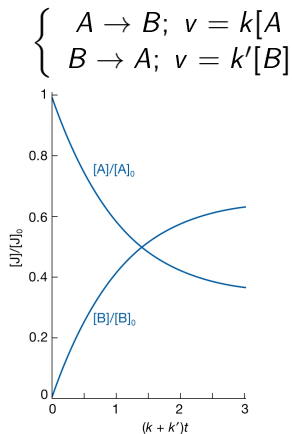
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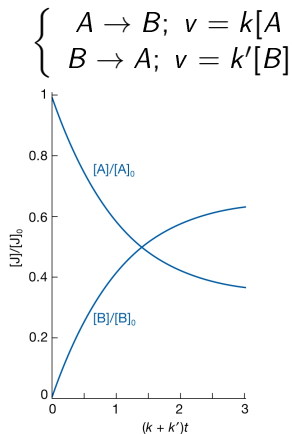
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more generally, $K = \frac{k_a}{k'_a} \cdot \frac{k_b}{k'_b} \cdot \frac{k_c}{k'_c} \cdot \dots$



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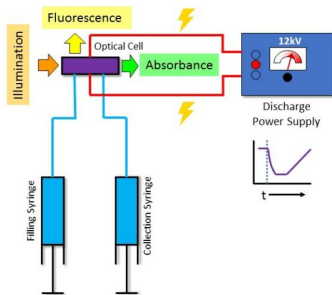
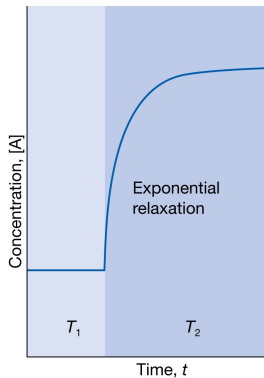
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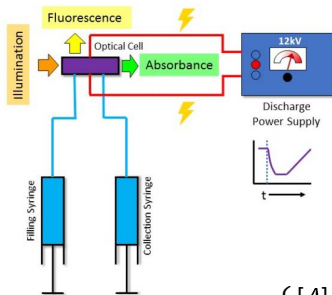
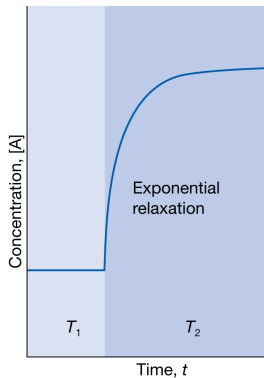


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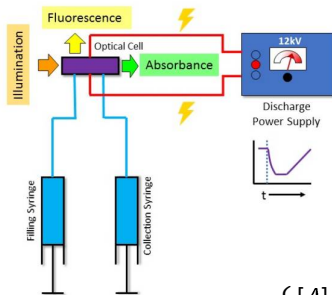
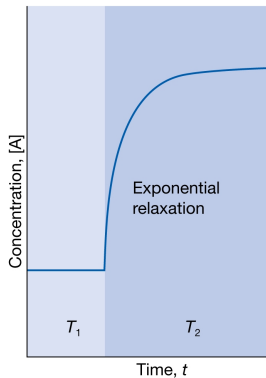


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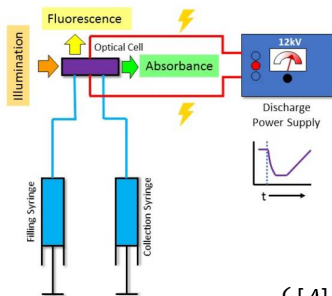
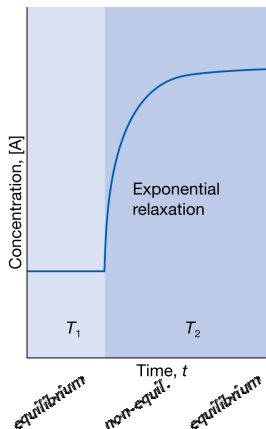
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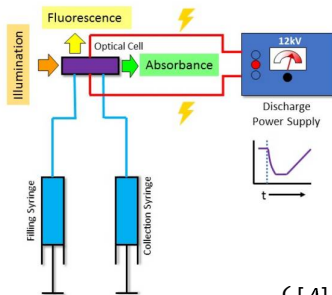
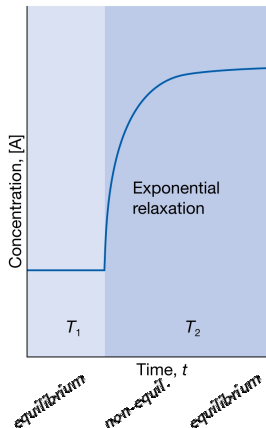
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Some equilibria are also sensitive to pressure : pressure-jump techniques also used

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find $k_2 = 1.4 \times 10^{11} \text{ dm}^3 \text{mol}^{-1} \text{s}^{-1}$ and $k_1 = 2.4 \times 10^{-5} \text{ s}^{-1}$

Temperature dependence of rate constant: Arrhenius behaviour

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$$k = Ae^{-\frac{E_a}{RT}}$$

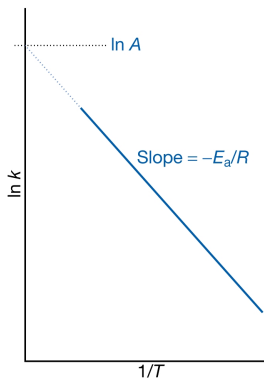
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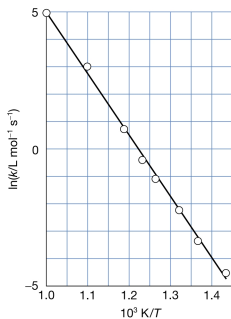
Activation energy:

$$E_a = RT^2 \left(\frac{d \ln k}{dT} \right)$$



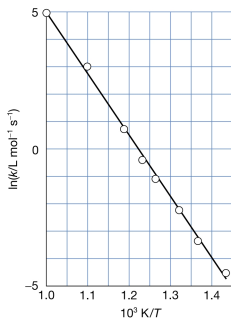
second-order decomposition of acetaldehyde (ethanal, CH_3CHO)

T/K	700	730	760	790	810	840	910	1000
$k/(\text{dm}^3 \text{mol}^{-1} \text{s}^{-1})$	0.011	0.035	0.105	0.343	0.789	2.17	20.0	145
$(10^3 \text{ K})/T$	1.43	1.37	1.32	1.27	1.23	1.19	1.10	1.00
$\ln(k/\text{dm}^3 \text{mol}^{-1} \text{s}^{-1})$	-4.51	-3.35	-2.25	-1.07	-0.24	0.77	3.00	4.98



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slope = -22.7

intercept = 27.7 $\Rightarrow E_a = 22.7 \times 8.3145 \text{ J K}^{-1} \text{mol}^{-1} \times 10^3 \text{ K}$

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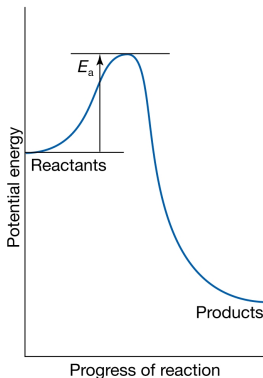
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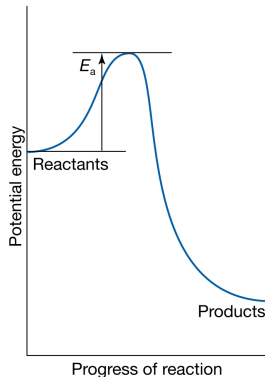
Potential energy profile for exothermic reaction



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Potential energy profile for exothermic reaction



activated complex
versus
transition state

Effect of catalyst

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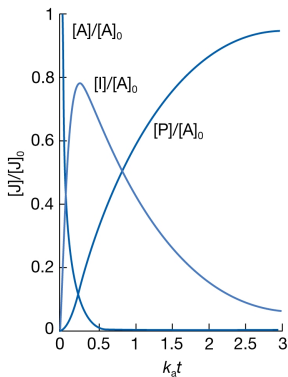
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$$\implies [I] = \frac{k_a}{k_b - k_a} (e^{-k_a t} - e^{-k_b t}) [A]_0$$



$$k_a = 10k_b$$

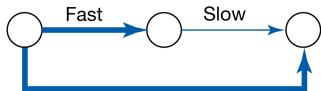
Reactants Products



(a)

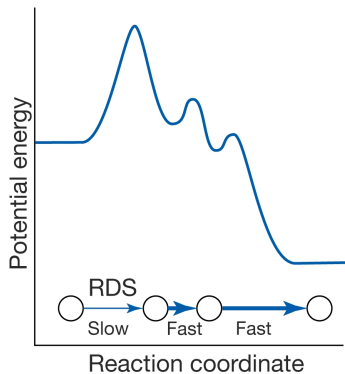


(b)



(c)

slow step is rate determining [not in (c)]



steady state approximation: $\frac{d[I]}{dt} = 0$

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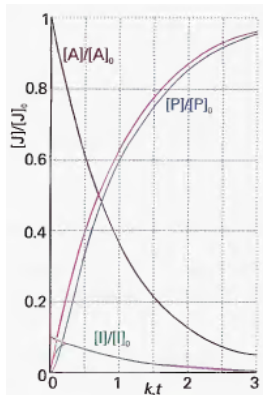
$$\Rightarrow [I] = \left(\frac{k_a}{k_b}\right) [A]$$

The concentrations of the intermediates remains small and hardly changes during reaction.

$$\Rightarrow \frac{k_a}{k_b} \ll 1$$

$$\Rightarrow \frac{d[P]}{dt} = k_b[I] = k_a[A]$$

$$\Rightarrow [P] = (1 - e^{-k_a t}) [A]_0$$

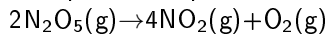


$$k_b = 20k_a$$

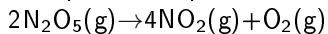
exact (black) versus s.s. (red)

example: decomposition of N_2O_5 :

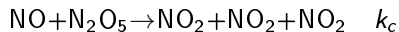
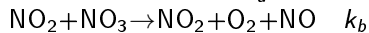
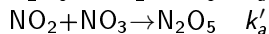
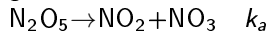
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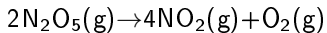
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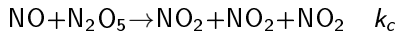
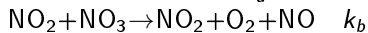
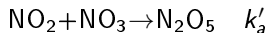
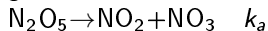
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rate law?

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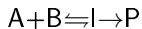
$$\begin{aligned}\frac{d[N_2O_5]}{dt} &= -k_a[N_2O_5] + k'_a[NO_2][NO_3] - k_c[NO][N_2O_5] \\ &= -k_a[N_2O_5] + k'_a \frac{k_a[N_2O_5]}{k'_a + k_b} - k_b \frac{k_a[N_2O_5]}{k'_a + k_b} = -\frac{2k_a k_b[N_2O_5]}{k'_a + k_b}\end{aligned}$$

Kinetic and thermodynamic control

When rate of decay of intermediate back into reactants much faster than rate of product formation ($k'_a \gg k_b$)

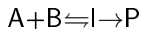
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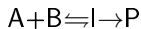
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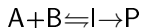


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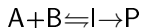
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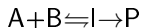
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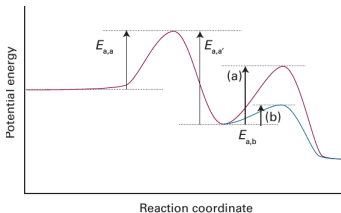
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3 activation energies to take into account:

two referring to reversible steps of pre-equilibrium and one for final step

relative magnitudes of activation energies determine

overall activation energy (a) > 0 or (b) < 0



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same as before for $k'_a \gg k_b$