

## COMMON EMITTER CONFIGURATION

Output Characteristic:

The output characteristic is the curve between  $V_{CE}$  and  $I_C$  for various values of  $I_B$ . For fixed value of  $I_B$  and is shown in **fig. 3**. For fixed value of  $I_B$ ,  $I_C$  is not varying much dependent on  $V_{CE}$  but slopes are greater than CE characteristic. The output characteristics can again be divided into three parts.

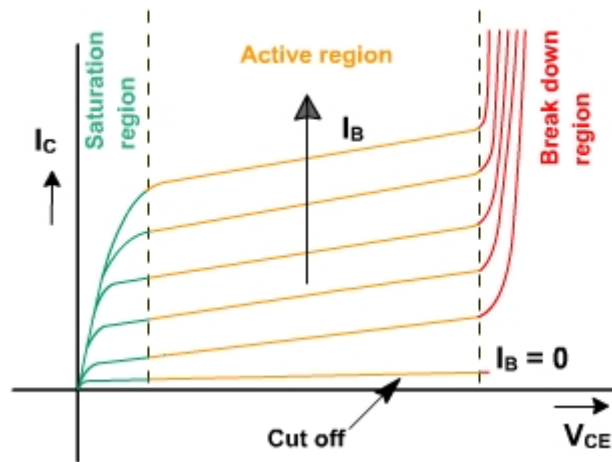


Fig. 3

### (1) Active Region:

In this region collector junction is reverse biased and emitter junction is forward biased. It is the area to the right of  $V_{CE} = 0.5$  V and above  $I_B = 0$ . In this region transistor current responds most sensitively to  $I_B$ . If transistor is to be used as an amplifier, it must operate in this region.

$$I_E = I_C + I_B$$

Since,  $I_C = I_{C0} + \alpha_{dc} I_E$

$$I_C = I_{C0} + \alpha_{dc} (I_C + I_B)$$

or  $(1 - \alpha_{dc}) I_C = \alpha_{dc} I_B + I_{C0}$

or  $I_C = \left( \frac{\alpha_{dc}}{1 - \alpha_{dc}} \right) I_B + \left( \frac{1}{1 - \alpha_{dc}} \right) I_{C0}$

Let,  $\beta_{dc} = \frac{\alpha_{dc}}{1 - \alpha_{dc}}$

$$\therefore I_C = (1 + \beta_{dc}) I_{C0} + \beta_{dc} I_B$$

$\beta_{dc}$  is defined as current gain of the transistor is given by

$$\beta_{dc} = \frac{I_C - I_{C0}}{I_B + I_{C0}}$$

If  $a_{dc}$  is truly constant then  $I_C$  would be independent of  $V_{CE}$ . But because of early effect,  $a_{dc}$  increases by 0.1% (0.001) e.g. from 0.995 to 0.996 as  $V_{CE}$  increases from a few volts to 10V. Then  $\beta_{dc}$  increases from  $0.995 / (1 - 0.995) = 200$  to  $0.996 / (1 - 0.996) = 250$  or about 25%. This shows that small change in  $a$  reflects large change in  $\beta$ . Therefore the curves are subjected to large variations for the same type of transistors.

## (2) Cut Off:

Cut off in a transistor is given by  $I_B = 0$ ,  $I_C = I_{C0}$ . A transistor is not at cut off if the base current is simply reduced to zero (open circuited) under this condition,

$$I_C = I_E = I_{C0} / (1 - \alpha_{dc}) = I_{CEO}$$

The actual collector current with base open is designated as  $I_{CEO}$ . Since even in the neighborhood of cut off,  $a_{dc}$  may be as large as 0.9 for Ge, then  $I_C = 10 I_{C0}$  (approximately), at zero base current. Accordingly in order to cut off transistor it is not enough to reduce  $I_B$  to zero, but it is necessary to reverse bias the emitter junction slightly. It is found that reverse voltage of 0.1 V is sufficient for cut off a transistor. In Si, the  $a_{dc}$  is very nearly equal to zero, therefore,  $I_C = I_{C0}$ . Hence even with  $I_B = 0$ ,  $I_C = I_E = I_{C0}$  so that transistor is very close to cut off.

In summary, cut off means  $I_E = 0$ ,  $I_C = I_{C0}$ ,  $I_B = -I_C = -I_{C0}$ , and  $V_{BE}$  is a reverse voltage whose magnitude is of the order of 0.1 V for Ge and 0 V for Si.

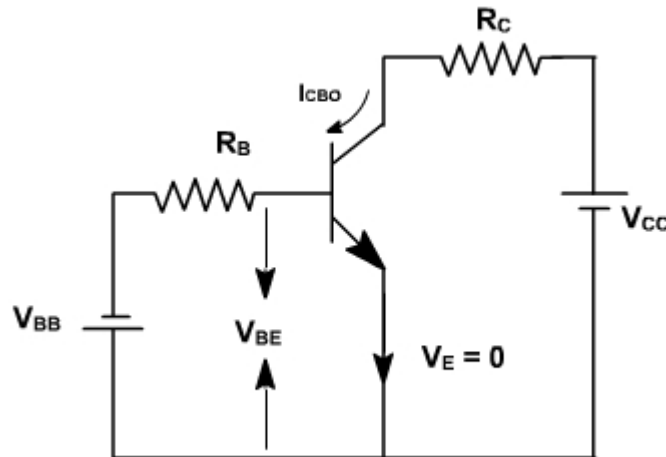
**Reverse Collector Saturation Current  $I_{CBO}$ :**

When in a physical transistor emitter current is reduced to zero, then the collector current is known as  $I_{CBO}$  (approximately equal to  $I_{CO}$ ). Reverse collector saturation current  $I_{CBO}$  also varies with temperature, avalanche multiplication and variability from sample to sample. Consider the circuit shown in **fig. 4**.  $V_{BB}$  is the reverse voltage applied to reduce the emitter current to zero.

$$I_E = 0, \quad I_B = -I_{CBO}$$

If we require,  $V_{BE} = -0.1 \text{ V}$

$$\text{Then } -V_{BB} + I_{CBO} R_B < -0.1 \text{ V}$$



**Fig. 4**

If  $R_B = 100 \text{ K}$ ,  $I_{CBO} = 100 \text{ m A}$ , Then  $V_{BB}$  must be 10.1 Volts. Hence transistor must be capable to withstand this reverse voltage before breakdown voltage exceeds.

**(3).Saturation Region:**

In this region both the diodes are forward biased by at least cut in voltage. Since the voltage  $V_{BE}$  and  $V_{BC}$  across a forward is approximately 0.7 V therefore,  $V_{CE} = V_{CB} + V_{BE} = -V_{BC} + V_{BE}$  is also few tenths of volts. Hence saturation region is very close to zero voltage axis, where all the

current rapidly reduces to zero. In this region the transistor collector current is approximately given by  $V_{CC} / R_C$  and independent of base current. Normal transistor action is lost and it acts like a small ohmic resistance.

### common emitter current gain

#### Large Signal Current Gain $\beta_{dc}$ :-

The ratio  $I_C / I_B$  is defined as transfer ratio or large signal current gain  $\beta_{dc}$

$$\beta_{dc} = \frac{I_C}{I_B}$$

Where  $I_C$  is the collector current and  $I_B$  is the base current. The  $\beta_{dc}$  is an indication of how well the transistor works. The typical value of  $\beta_{dc}$  varies from 50 to 300.

In terms of h parameters,  $\beta_{dc}$  is known as dc current gain and is designated  $h_{FE}$  ( $\beta_{dc} = h_{FE}$ ).

Knowing the maximum collector current and  $\beta_{dc}$  the minimum base current can be found which will be needed to saturate the transistor.

$$I_{C(max)} = \frac{V_{CC} - V_{CE(sat)}}{R_C} = I_{C(sat)}$$

$$I_{B(min)} = \frac{I_{C(sat)}}{\beta_{dc}}$$

This expression of  $\beta_{dc}$  is defined neglecting reverse leakage current ( $I_{CO}$ ).

Taking reverse leakage current ( $I_{CO}$ ) into account, the expression for the  $\beta_{dc}$  can be obtained as follows:

$\beta_{dc}$  in terms of  $\alpha_{dc}$  is given by

$$\begin{aligned}
 \beta_{dc} &= \frac{\alpha_{dc}}{1 - \alpha_{dc}} \\
 &= \frac{\frac{I_C - I_{CO}}{I_E}}{1 - \frac{I_C - I_{CO}}{I_E}} = \frac{I_C - I_{CO}}{I_E - I_C + I_{CO}} \\
 &= \frac{I_C - I_{CO}}{I_B + I_{CO}}
 \end{aligned}$$

Since,  $I_{CO} = I_{CBO}$

$$\therefore \beta_{dc} = \frac{I_C - I_{CBO}}{I_B + I_{CBO}}$$

Cut off of a transistor means  $I_E = 0$ , then  $I_C = I_{CBO}$  and  $I_B = -I_{CBO}$ . Therefore, the above expression  $\beta_{dc}$  gives the collector current increment to the base current change from cut off to  $I_B$  and hence it represents the large signal current gain of all common emitter transistor.