

## AMPLIFIER DESIGN

### Example-2 (Emitter-Resistor Amplifier Design)

Design an emitter-resistor amplifier as shown in fig. 2 to drive a  $2\text{ K}\Omega$  load using a pnp silicon transistor,  $V_{CC} = -24\text{V}$ ,  $\beta = 200$ ,  $A_v = -10$ , and  $V_{BE} = -0.7\text{ V}$ . Determine all element values and calculate  $A_i$ ,  $R_{in}$ ,  $I_{CQ}$  and the maximum undistorted symmetrical output voltage swing for three values of  $R_C$  as given below:

1.  $R_C = R_{load}$
2.  $R_C = 0.1 R_{load}$
3.  $R_C = 10 R_{load}$

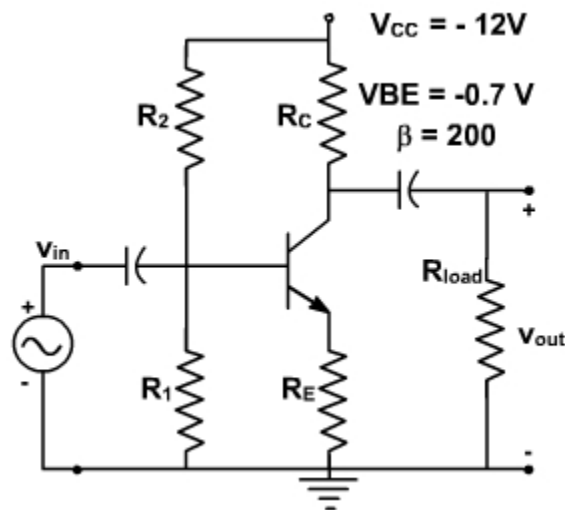


Fig. 2

Solution:

(a)  $R_C = R_{load}$

We use the various equations derived in previous lecture in order to derive the parameters of the circuit.

From the voltage gain, we can solve for  $R'_E$ .

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$$A_v = -10 = -\frac{R_{load} \parallel R_C}{r_e + R_E} = -\frac{2K\Omega \parallel 2K\Omega}{r_e + R_E}$$

$$\text{So } R'_E = r_e + R_E = 100 \Omega$$

We can find the quiescent value of the collector current  $I_C$  from the collector-emitter loop using the equation for the condition of maximum output swing.

$$I_{CQ} = \frac{V_{CC}}{R_{dc} + R_{ac}} = 7.5 \text{ mA}$$

$$\text{Therefore, } r'_E = \frac{25 \times 10^{-3}}{7.5 \times 10^{-3}} = 3.33 \Omega$$

This is small enough that we shall ignore it to find that  $R_E = 100 \Omega$ . Since we now know  $\beta$  and  $R_E$ . We can use the design guideline.

$$R_B = 0.1 \beta R_E = 2 \text{ k } \Omega$$

As designed earlier, the biasing circuitry can be designed in the same manner and given by

$$V_{BB} = -1.52 \text{ V}$$

$$R_1 = 2.14 \text{ K } \Omega$$

$$R_2 = 3.6 \text{ K } \Omega$$

The maximum undistorted symmetrical peak to peak output swing is then

$$V_{out} (P-P) = 1.8 I_{CQ} (R_{load} \parallel R_C) = 13.5 \text{ V}$$

$$\text{Thus current gain } A_i = -9.1$$

$$\text{and input impedance } R_{in} = 1.82 \text{ K } \Omega$$

(b)  $R_C = 0.1 R_{load}$

we repeat the steps of parts (a) to find

$$R_C = 200 \, \Omega$$

$$R_i = 390 \, \Omega$$

$$I_{CQ} = -57.4 \, \text{mA}$$

$$R_2 = 4.7 \text{K} \, \Omega$$

$$r'_e = 0.45 \, \Omega$$

$$v_{out(p-p)} = 18.7 \, \text{V}$$

$$R_B = 360 \, \Omega$$

$$A_i = -1.64$$

$$V_{BB} = -1.84 \, \text{V}$$

$$R_{in} = 327 \, \Omega$$

(C)  $R_C = 10 R_{load}$

Once again, we follow the steps of part (a) to find

$$R_C = 20 \text{K} \, \Omega$$

$$R_i = 3.28 \text{K} \, \Omega$$

$$I_{CQ} = -1.07 \, \text{mA}$$

$$R_2 = 85.6 \text{K} \, \Omega$$

$$r'_e = 24.2 \, \Omega$$

$$v_{out(p-p)} = 3.9 \, \text{V}$$

$$R_B = 3.64 \text{K} \, \Omega$$

$$A_i = -14.5$$

$$V_{BB} = -0.886 \, \text{V}$$

$$R_{in} = 2.91 \text{K} \, \Omega$$

We now compare the results obtained Table-I for the purpose of making the best choice for  $R_C$ .

	$I_{CQ}$	$A_i$	$R_{in}$	$v_{out}(p-p)$
$R_C = R_{load}$	-7.5 mA	-9.1	1.82K W	13.5 V
$R_C = 0.1 R_{load}$	-57.4 mA	-1.64	327 W	20.8 V
$R_C = 10 R_{load}$	-1.07mA	-14.5	2.91W	3.9 V

Table - 1 Comparsion for the three selections of  $R_C$ 

It indicates that of the three given ratios of  $R_C$  to  $R_{load}$ ,  $R_C = R_{load}$  has the most desirable performance in the CE amplifier stage.

It can be used as a guide to develop a reasonable designs. In most cases, this choice will provide performance that meets specifications. In some applications, it may be necessary to do additional analysis to find the optimum ratio of  $R_C$  to  $R_{load}$ .