

Describing Functions

The describing function of a nonlinear element is its approximate transfer function if the nonlinearity is in cascade with a linear process that acts as a low pass filter. It is useful for finding limit cycles in the system.

Let's continue with detailed examples of computing the describing function of some nonlinearities.

Example: Compute the describing function of an ideal relay:

The input-output curve of the ideal relay is shown below. Note that it is an odd function. Here in detail are the steps toward the solution:

1. **Draw the output.** First we need to get the output given a sinusoidal input. Shown below is the result.

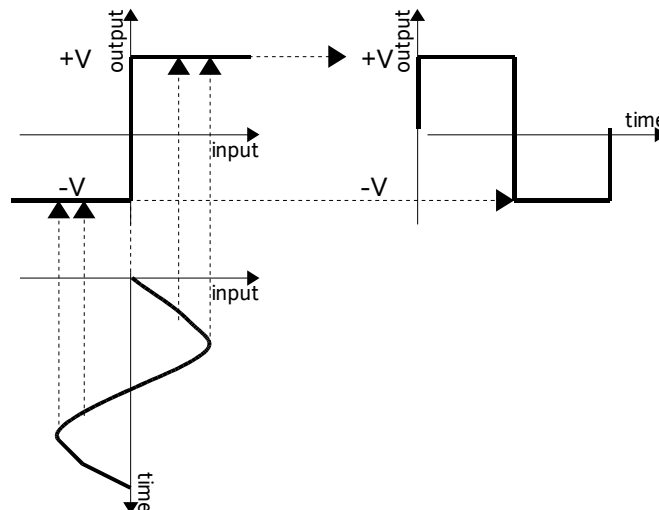


Illustration 1 Output of an Ideal Relay.

2. **Equate $n(t)$ to the first terms of the Fourier expansion.** Remember that with $G(s)$ acting as low pass the higher order terms vanish. That is

$$n(t) = A_1 \cos(\omega t) + B_1 \sin(\omega t) \quad (1)$$

3. **Calculate coefficients A_1 and B_1 .**

From definition

$$A_1 = \frac{2}{T} \int_{t_0}^{t_0+T} n(t) \cos(\omega t) dt \quad (2)$$

$$B_1 = \frac{2}{T} \int_{t_0}^{t_0+T} n(t) \sin(\omega t) dt \quad (3)$$

where $T = \frac{2\pi}{\omega}$

The integral is evaluated over one full period from the starting time t_0 (which can be any time).

Graphically, to get A_1 we first multiply $n(t)$ to $\cos(\omega t)$ then get the area under the curve over one full period. Shown below is the $n(t)\cos(\omega t)$.

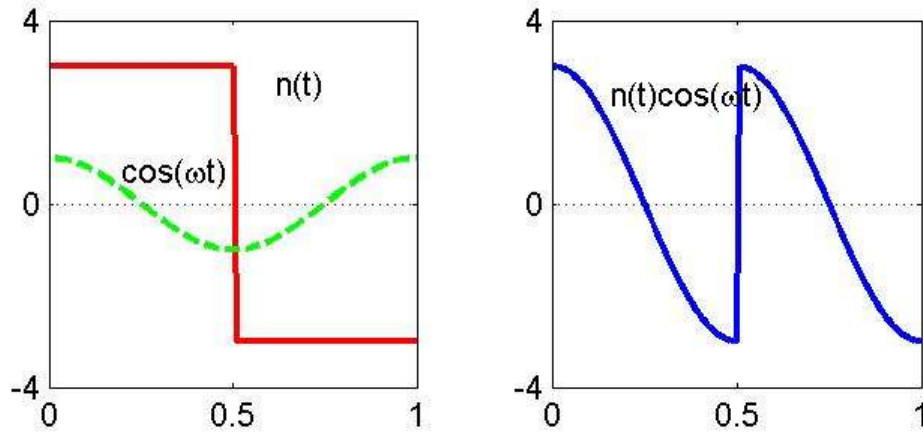


Illustration 2 Product of $n(t)$ and $\cos(\omega t)$. In this example $|V| = 3$

Since $n(t)$ is an odd function and $\cos(\omega t)$ is an even function, the integral of their product over one full period is zero. Therefore, A_1 in this case is zero.

If we apply the same analysis to B_1 we see that area under the curve is not zero because $n(t)$ and $\sin(\omega t)$ are both odd.

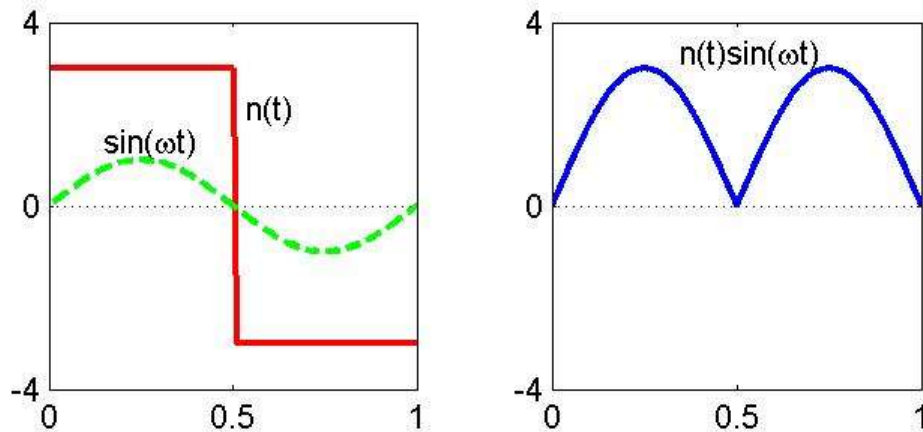


Illustration 3 Product of $n(t)$ and $\sin(\omega t)$.

Therefore from (1) $n(t)$ becomes

$$n(t) = B_1 \sin(\omega t) \quad (4)$$

In solving for B_1 we note that the integration can be carried over a half period (from $t_0 = 0$ to $T/2$) so long as we multiply the integral by 2. With that

$$B_1(t) = \frac{4}{T} \int_0^{T/2} V \sin(\omega t) dt \quad (5)$$

$$B_1(t) = \frac{4V}{T} \left[\frac{-\cos(\omega t)}{\omega} \right], t=0 \text{ to } T/2 \quad (6)$$

$$= \frac{4V}{T\omega} [-\cos(\omega T/2) + \cos(0)] \quad (7)$$

Substituting

$$T = \frac{2\pi}{\omega}$$

$$B_1 = \frac{4V}{2\pi} [-\cos(\pi) + \cos(0)] = \frac{4V}{\pi} \quad (8)$$

4. Solve for $N(M, \omega)$.

$$N(M, \omega) = \frac{B_1 + jA_1}{M} = \frac{B_1}{M} \quad (9)$$

$$N(M, \omega) = \frac{4V}{\pi M} \quad (10)$$

Try it.

Exercise:

1. Compute the describing function of a Saturation (also known as a “Limiter”).
2. Compute the describing function of a Dead Zone.

Finding Limit Cycles

A nonlinear system in a feedback loop will have a limit cycle with the output approximately sinusoidal if the sinusoid at the input regenerates itself in the loop.

Consider the unity feedback loop below with a nonlinearity.

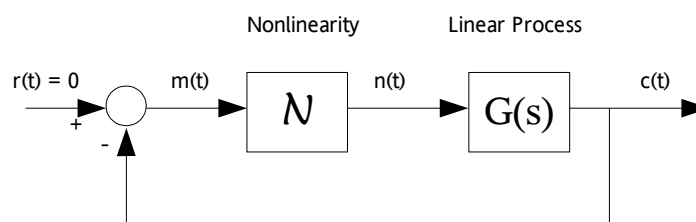


Illustration 4 A unity feedback loop with nonlinearity.

We can replace the nonlinearity with a describing function. The condition for the existence of a limit cycle means that $m(t) = -c(t)$.

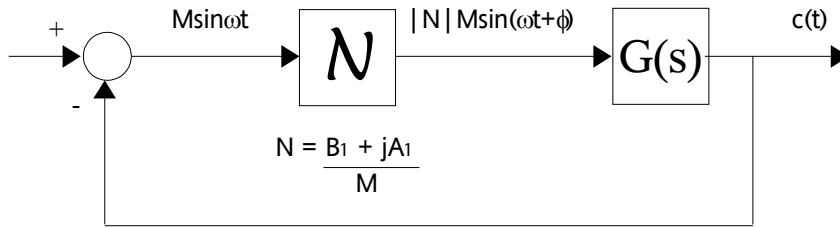


Illustration 5 Nonlinearity replaced with describing function in finding limit cycles.

This means

$$M \sin(\omega t) = -|G(j\omega)| |N(M, \omega)| M \sin(\omega t + \phi + \theta) \quad (11)$$

The negative sign is due to the negative sign in the summing junction.

For sustained oscillation, equate the phases.

$$M = -G(j\omega) N(M, \omega) M \quad (12)$$

$$1 = -G(j\omega) N(M, \omega) \quad (13)$$

$$1 + N(M, \omega) G(j\omega) = 0 \quad (14)$$

Or

$$G(j\omega) = \frac{-1}{N(M, \omega)} \quad (15)$$

Any M (input sinusoid amplitude) and ω (sinusoid frequency) which satisfies Eq. (15) will produce a limit cycle.

Example

In Illustration 5, let $G(s) = \frac{4}{s(1+s)^2}$ and the nonlinearity an ideal relay. Will there be a limit cycle?

1. Express $G(s)$ as a frequency response, $G(j\omega)$.

$$G(j\omega) = \frac{4}{j\omega(1+j\omega)^2} \quad (16)$$

$$= \frac{4}{j(\omega - \omega^3) - 2\omega} \frac{(-j(\omega - \omega^3) - 2\omega)}{(-j(\omega - \omega^3) - 2\omega)} \quad (17)$$

$$= \frac{-8\omega + 4j(\omega - \omega^3)}{4\omega^2 + (\omega - \omega^3)^2} \quad (18)$$

2. Remove possible phase differences by zeroing the imaginary component

$$\omega - \omega^3 = 0 \quad (19)$$

$$\omega = 1 \quad (20)$$

Replacing $\omega = 1$ in Eq. 18 We get

$$G(j1) = \frac{8\omega}{4\omega^2} = -2 \quad (21)$$

3. Solve for $G = \frac{-1}{N}$

For an ideal relay $N = \frac{4V}{\pi M}$

$$G = \frac{-1}{N}$$

$$2 = \frac{-\pi M}{4V} \quad (22)$$

$$\frac{8V}{\pi} = M \quad (23)$$

Conclusion: There's a limit cycle when $\omega = 1$ and $M = 8V/\pi$.