

# The Fast Exact Closure for Jeffery’s Equation with Diffusion

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## Abstract

Jeffery’s equation with diffusion is widely used to predict the motion of fiber suspensions in fluid flows with low Reynold’s numbers. Solutions of the full form for the orientation fiber distribution function requires excessive computational effort, and a common approach is to solve the related second order moment tensor equation instead. This approach requires a so called ‘closure,’ that is, a method to approximate the fourth order moment tensor from components of the second order moment tensor. This paper presents the *Fast Exact Closure* (FEC), whereby conversion tensors are defined to obtain a pair of related ordinary differential equations which can be solved simultaneously, thus avoiding numerical approximations of higher order moment tensors. This form is exact in that when the diffusion terms are absent it exactly solves Jeffery’s equation. Results demonstrate that this form is computationally fast with speeds equivalent to or better than closure approximations commonly employed today in industrial simulations. Examples are provided to demonstrate the improved accuracy of the new closure, for both classical Folgar-Tucker (1984) diffusion and the recently proposed anisotropic rotary diffusion form of Phelps and Tucker (2009). We also provide a proof that for isotropic diffusion the solution to the FEC will remain physical.

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## 1. Introduction

The industrial demand has continued to increase for high-strength, low-weight, rapid production parts such as those made of short fiber composites with injection molding processes. For effective design, it is essential to understand the dependance of the final part performance of short-fiber injection molded composites with the variations in the microstructure due to the processing (see e.g. [1, 2]). The Folgar and Tucker model of isotropic diffusion [3] for fiber interactions within a suspension has been used for several decades to compute fiber orientation and has been implemented within most related industrial and research computer simulations. Unfortunately, direct computations of the isotropic diffusion model are computationally prohibitive, and most implementations employ the orientation tensor approach of Advani and Tucker [4] where the moments of the fiber orientation are solved, thus indirectly quantifying the fiber orientation distribution. The orientation tensor approach requires knowledge of the next higher-order moment tensor, thus requiring some form of a closure. The hybrid closure of Advani and Tucker [4] has been used extensively due to its computational efficiencies, but in implementation it will overpredict the alignment state in simple shear flow [5]. Cintra and Tucker [6] introduced the class of the orthotropic closures, which result

in significant improvements in accuracy when compared to the hybrid closure, but at an increase in computational costs.

With recent advances in part repeatability, the limitation of the isotropic diffusion model has become apparent [7]. Recent anisotropic diffusion models [8, 9, 10, 11] propose new forms with greater accuracies for modeling fiber collisions, but these anisotropic diffusion models pose a new set of computational complications. In particular is the concern that nearly all of the fitted orthotropic closures are obtained by fitting orientation information based on direct numerical solutions of the Folgar-Tucker diffusion model. The exception is the orthotropic closures of Wetzel [12] and VerWeyst [13] which were both constructed on distributions formed through the elliptic integral form for orientations encompassing the eigenspace [6].

The Exact Closure of Montgomery-Smith *et al.* [14] presents an alternative to the classical closure form, and provides an exact solution for pure Jeffery's motion (i.e., the dilute regime). The Exact Closure avoids the curve fitting process required to define fitted closures, by solving a set of related ODEs of the fiber orientation. In the present paper, we extend the Exact Closure form to systems of concentrated suspensions that are more relevant to modeling the processing of short-fiber composites. Furthermore, we introduce the new *Fast Exact Closure* (FEC) that defines conversion tensors that lead to a coupled system of ordinary differential equations that avoid costly closure computations. The FEC form is derived for both the isotropic diffusion model of Folgar and Tucker and the recent anisotropic diffusion model of Phelps and Tucker [9]. Results demonstrate the effectiveness of this alternative approach for modeling fiber orientation, both for accuracy and for computational speed.

## 2. Fiber Motion Basics

Jeffery's equation [15] has been used to predict the motion of the direction of axi-symmetric fibers under the influence of a low Reynold's number flow of a Newtonian fluid, whose velocity field is  $\mathbf{u} = \mathbf{u}(\mathbf{x}, t)$ . The directions of the fibers is represented by the fiber orientation distribution  $\psi = \psi(\mathbf{x}, \mathbf{p}, t)$ , where  $\mathbf{p}$  is an element of the orientation space, that is, the 2-dimensional sphere  $S = \{\mathbf{p} = (p_1, p_2, p_3) : p_1^2 + p_2^2 + p_3^2 = 1\}$ . Thus given a subset  $E$  of  $S$ , the proportion of fibers whose direction is in  $E$  is given by  $\int_E \psi(\mathbf{x}, \mathbf{p}, t) d\mathbf{p}$ , where  $d\mathbf{p}$  represents the usual integration over  $S$ . In particular, an isotropic distribution is represented by  $\psi = 1/4\pi$ . The Jeffery's equation for the fiber orientation distribution is

$$\frac{D\psi}{Dt} = -\frac{1}{2}\nabla_{\mathbf{p}} \cdot ((\Omega \cdot \mathbf{p} + \lambda\Gamma \cdot \mathbf{p} - \lambda\Gamma : \mathbf{p}\mathbf{p}\mathbf{p})\psi) \quad (1)$$

Here  $\Omega$  is the vorticity, that is, the anti-symmetric part  $\nabla\mathbf{u} - (\nabla\mathbf{u})^T$  of the Jacobian of the velocity field  $\nabla\mathbf{u} = (\partial u_i / \partial x_j)_{1 \leq i, j \leq 3}$ , and  $\Gamma$  is the rate of strain tensor, that is, the symmetric part  $\nabla\mathbf{u} + (\nabla\mathbf{u})^T$  of the Jacobean of the velocity field. Also,  $D/Dt = \partial/\partial t + \mathbf{u} \cdot \nabla$  represents the material derivative, and  $\nabla_{\mathbf{p}} = (I - \mathbf{p}\mathbf{p}) \cdot \left( \frac{\partial}{\partial p_1}, \frac{\partial}{\partial p_2}, \frac{\partial}{\partial p_3} \right)$  is the gradient operator restricted to the sphere.

Equation (1) is modified to incorporate the rotary diffusion expressed by Bird *et al.* [16], occasionally referred to as the generalized Fokker-Planck or the Smoluchowski equation [17], as

$$\frac{D\psi}{Dt} = -\frac{1}{2}\nabla_{\mathbf{p}} \cdot ((\Omega \cdot \mathbf{p} + \lambda\Gamma \cdot \mathbf{p} - \lambda\Gamma : \mathbf{p}\mathbf{p}\mathbf{p})\psi) + \Delta_{\mathbf{p}}(D_r\psi), \quad (2)$$

where  $D_r$  captures the effect of fiber interaction and depends upon the flow kinetics. Here  $\Delta_{\mathbf{p}} = \nabla_{\mathbf{p}} \cdot \nabla_{\mathbf{p}}$  represents the Beltrami-Laplace operator on the sphere. Folgar and Tucker [3] selected  $D_r = C_I \dot{\gamma}$  where  $\dot{\gamma} = (\frac{1}{2}\Gamma : \Gamma)^{1/2}$  and  $C_I$  is a constant that depends upon the volume fraction and aspect ratio of the fibers.

Other authors have considered a wider class of diffusion terms. For example, Koch [10], and Phelps and Tucker [9] considered anisotropic diffusion

$$\frac{D\psi}{Dt} = -\frac{1}{2}\nabla_{\mathbf{p}} \cdot ((\Omega \cdot \mathbf{p} + \lambda\Gamma \cdot \mathbf{p} - \lambda\Gamma : \mathbf{p}\mathbf{p}\mathbf{p})\psi) + \nabla_{\mathbf{p}} \cdot (I - \mathbf{p}\mathbf{p}) \cdot D_r \cdot \nabla_{\mathbf{p}}\psi \quad (3)$$

where  $D_r$  is the anisotropic diffusion matrix, calculated as a function of  $\psi$  and  $\nabla u$  (see, e.g., [9, 10]).

Since these are, in effect, partial differential equations in 5-spacial dimensions, numerically calculating solutions can be rather daunting. Hence Hinch and Leal [18] suggested to recast the equation in terms of moment tensors. For example, the second and fourth moment tensors are defined by

$$A = \int_S \mathbf{p}\mathbf{p}\psi \, d\mathbf{p}, \quad \mathbb{A} = \int_S \mathbf{p}\mathbf{p}\mathbf{p}\mathbf{p}\psi \, d\mathbf{p} \quad (4)$$

Then Jeffery's equation (1) for the second order moment tensor is

$$\frac{DA}{Dt} = \frac{1}{2}(\Omega \cdot A - A \cdot \Omega + \lambda(\Gamma \cdot A + A \cdot \Gamma) - 2\lambda\mathbb{A} : \Gamma) \quad (5)$$

and the equations (2) and (3) with diffusion terms become

$$\frac{DA}{Dt} = \frac{1}{2}(\Omega \cdot A - A \cdot \Omega + \lambda(\Gamma \cdot A + A \cdot \Gamma) - 2\lambda\mathbb{A} : \Gamma) + \mathcal{D}[A] \quad (6)$$

where for equation (2)

$$\mathcal{D}[A] = D_r(2I - 6A) \quad (7)$$

and for equation (3) (see [9])

$$\mathcal{D}[A] = 2D_r - 2(\text{tr } D_r)A - 5(A \cdot D_r + D_r \cdot A) + 10\mathbb{A} : D_r \quad (8)$$

The difficulty with equations (5) and (6) is that they include the fourth order moment tensor. To circumvent this problem, various authors (for example, [1, 6, 18, 19, 20, 21, 22, 23, 24]) have proposed *closures*, that is, formulae to calculate the fourth order moment tensor  $\mathbb{A}$  from the second order moment tensor  $A$ . Many closures are approximate, involving coefficients obtained by fitting numerical data obtained by solving equation (2) using a finite element method (for example, Bay [25]).

### 3. The Fast Exact Closure

Verleye and Dupret [24] (see also [12, 13, 26, 27, 28]) noted that there is an exact closure for Jeffery's equation without diffusion terms, *in the particular case that the fiber orientation distribution is at some time isotropic*. This exact closure was stated explicitly in [14]. For the sake of labeling, we still call this the *Exact Closure*, even though it is only exact for Jeffery's equation without diffusion terms. The Exact Closure is computed by solving equation (6), where  $\mathbb{A}$  is computed from  $A$  using equations (38) and (39).

This approach only gives the exact answer to equations (2) and (3) when  $D_r = 0$  and when the orientation is isotropic at some time. Nevertheless it is reasonable to suppose that the exact closure should give a good approximation in general, even when  $D_r \neq 0$  as in Verweyst *et al.* [1, 13]. Their ORT closure is a polynomial approximation to the Exact Closure, and as we demonstrate below, gives answers that are virtually indistinguishable from the Exact Closure.

The *Fast Exact Closure* (FEC) performs the Exact Closure in a computationally efficient manner. A version of FEC is described in [14], but only when the diffusion terms are absent. In this section we describe the FEC, but leave the derivation until the appendix.

The idea behind the FEC is the computation of two rank 4 tensors,  $\mathbb{C}$  and  $\mathbb{D}$ , which we define as *conversion tensors*. They convert between  $DA/Dt$  and  $DB/Dt$  according to the formulae.

$$\frac{DA}{Dt} = -\mathbb{C} : \frac{DB}{Dt}, \quad \frac{DB}{Dt} = -\mathbb{D} : \frac{DA}{Dt} \quad (9)$$

What makes everything work is the formula that for any matrix  $M$ , we have

$$\mathbb{C} : (B \cdot M + M^T \cdot B) = (\text{tr } M)A + M \cdot A + A \cdot M^T - 2\mathbb{A} : M \quad (10)$$

where  $\mathbb{A}$  and  $A$  satisfy equations (38) and (39).

All the FEC's we present in this paper will be of the form:

$$\frac{DA}{Dt} = -\mathbb{C} : F(B) + G(A), \quad \frac{DB}{Dt} = F(B) - \mathbb{D} : G(A) \quad (11)$$

where  $F(B)$  and  $G(A)$  are given explicitly. We show later in this section how to calculate the conversion tensors  $\mathbb{C}$  and  $\mathbb{D}$ . In the appendix we will give a more mathematical formula for them, and a proof that they have these properties. It is important to note that  $\mathbb{C}$  and  $\mathbb{D}$  may be computed directly from  $A$  and  $B$  in a rather fast manner, involving nothing more than diagonalizing and inverting three by three symmetric matrices, general simple arithmetic, and occasionally invoking inverse trigonometric or inverse hyperbolic functions.

The FEC solves the ODEs of (11) simultaneously. If the initial fiber orientation is isotropic, then  $A = \frac{1}{3}I$  and  $B = I$  at  $t = 0$ . When the initial fiber orientation is not isotropic, then one can compute the initial condition for  $B$  from  $A$  by inverting equation (38), as described in [14].

It can be shown that the matrices  $A$  and  $B$  remain positive definite, simultaneously diagonalizable, and satisfy the equations  $\text{tr } A = \det B = 1$ .

For example, the FEC for the Jeffery's equation with isotropic diffusion given in equation (2) is given by:

$$\frac{DA}{Dt} = \frac{1}{2}\mathbb{C} : [B \cdot (\Omega + \lambda\Gamma) + (-\Omega + \lambda\Gamma) \cdot B] + D_r(2I - 6A) \quad (12)$$

$$\frac{DB}{Dt} = -\frac{1}{2}(B \cdot (\Omega + \lambda\Gamma) + (-\Omega + \lambda\Gamma) \cdot B) - D_r\mathbb{D} : (2I - 6A) \quad (13)$$

and the FEC for Jeffery's equation with anisotropic diffusion as shown in equation (3) is given by

$$\frac{DA}{Dt} = \frac{1}{2}\mathbb{C} : [B \cdot (\Omega + \lambda\Gamma) + (-\Omega + \lambda\Gamma) \cdot B] + 2D_r + 3(\text{tr } D_r)A - 5\mathbb{C} : (B \cdot D_r + D_r \cdot B) \quad (14)$$

$$\frac{DB}{Dt} = -\frac{1}{2}(B \cdot (\Omega + \lambda\Gamma) + (-\Omega + \lambda\Gamma) \cdot B) - \mathbb{D} : (2D_r + 3(\text{tr } D_r)A) + 5(B \cdot D_r + D_r \cdot B) \quad (15)$$

Now let us describe how to compute the conversion tensors, which are both computed with respect to the basis of orthonormal eigenvectors of  $B$ . With respect to this basis, the matrix  $B$  is diagonal with entries  $b_1$ ,  $b_2$  and  $b_3$ , and  $A$  is diagonal with entries  $a_1$ ,  $a_2$  and  $a_3$ . Note that if  $a_1 \geq a_2 \geq a_3$ , then  $b_1 \leq b_2 \leq b_3$ .

If the eigenvalues  $b_1$ ,  $b_2$  and  $b_3$  are not close to each other, then  $\mathbb{C}$  is the symmetric tensor calculated using the formulae

$$\begin{aligned} \mathbb{C}_{1122} &= \frac{a_1 - a_2}{2(b_2 - b_1)} & \mathbb{C}_{1111} &= \frac{1}{2}b_1^{-1} - \mathbb{C}_{1122} - \mathbb{C}_{1133} \\ \mathbb{C}_{1133} &= \frac{a_1 - a_3}{2(b_3 - b_1)} & \mathbb{C}_{2222} &= \frac{1}{2}b_2^{-1} - \mathbb{C}_{1122} - \mathbb{C}_{2233} \\ \mathbb{C}_{2233} &= \frac{a_2 - a_3}{2(b_3 - b_2)} & \mathbb{C}_{3333} &= \frac{1}{2}b_3^{-1} - \mathbb{C}_{1133} - \mathbb{C}_{2233} \\ \mathbb{C}_{ijkk} &= 0 \text{ if } i \neq j \neq k \end{aligned} \quad (16)$$

If two or more of the eigenvalues are close to each other, then these equations can give rise to large numerical errors, or even ‘divide by zero’ exceptions. So in this situation, we use different formulae to compute  $\mathbb{C}$ .

Suppose two of the eigenvalues are close to each other, for example,  $b_1 = b_0 + \epsilon$  and  $b_2 = b_0 - \epsilon$ , where  $\epsilon$  is small. Thus  $b_0 = \frac{1}{2}(b_1 + b_2)$  and  $\epsilon = \frac{1}{2}(b_1 - b_2)$ . Define the quantity  $\mathcal{I}_n$  by

$$\begin{aligned} \mathcal{I}_{n+1} &= \frac{2n-1}{2n(b_0 - b_3)} \mathcal{I}_n - \frac{\sqrt{b_3}}{nb_0^n(b_0 - b_3)} \text{ if } n \geq 1 \\ \mathcal{I}_1 &= \frac{2}{\sqrt{b_0 - b_3}} \cos^{-1} \left( \sqrt{\frac{b_3}{b_0}} \right) \text{ if } b_0 > b_3 \\ \mathcal{I}_1 &= \frac{2}{\sqrt{b_3 - b_0}} \cosh^{-1} \left( \sqrt{\frac{b_3}{b_0}} \right) \text{ if } b_0 < b_3 \end{aligned} \quad (17)$$

Then replace the first equation of equation (16) by

$$\mathbb{C}_{1122} = \frac{1}{4}\mathcal{I}_3 + \frac{3}{8}\mathcal{I}_5\epsilon^2 + O(\epsilon^4) \quad (18)$$

If all three of the eigenvalues are almost equal, that is  $b_1 = 1 + c_1$ ,  $b_2 = 1 + c_2$ ,  $b_3 = 1 + c_3$  with  $|c_1|, |c_2|, |c_3| \leq \epsilon$ , then

$$\begin{aligned} \mathbb{C}_{1122} &= \frac{1}{10} - \frac{3}{28}c_1 - \frac{3}{28}c_2 - \frac{1}{28}c_3 + \frac{5}{48}c_1^2 + \frac{1}{8}c_1c_2 + \frac{1}{24}c_1c_3 + \frac{5}{48}c_2^2 + \frac{1}{24}c_2c_3 + \frac{1}{48}c_3^2 \\ &\quad - \frac{35}{352}c_1^3 - \frac{45}{352}c_1^2c_2 - \frac{15}{352}c_1^2c_3 - \frac{45}{352}c_1c_2^2 - \frac{9}{176}c_1c_2c_3 \\ &\quad - \frac{9}{352}c_1c_3^2 - \frac{35}{352}c_2^3 - \frac{15}{352}c_2^2c_3 - \frac{9}{352}c_2c_3^2 - \frac{5}{352}c_3^3 + O(\epsilon^4) \end{aligned} \quad (19)$$

with similar formulae for  $\mathbb{C}_{1133}$  and  $\mathbb{C}_{2233}$ . The other entries of  $\mathbb{C}$  are computed using the last four equations from (16).

The rank 4 tensor  $\mathbb{D}$  is defined with respect to the basis of orthonormal eigenvectors of  $B$  by

$$\begin{aligned} \begin{bmatrix} \mathbb{D}_{1111} & \mathbb{D}_{1122} & \mathbb{D}_{1133} \\ \mathbb{D}_{2211} & \mathbb{D}_{2222} & \mathbb{D}_{2233} \\ \mathbb{D}_{3311} & \mathbb{D}_{3322} & \mathbb{D}_{3333} \end{bmatrix} &= \begin{bmatrix} \mathbb{C}_{1111} & \mathbb{C}_{1122} & \mathbb{C}_{1133} \\ \mathbb{C}_{2211} & \mathbb{C}_{2222} & \mathbb{C}_{2233} \\ \mathbb{C}_{3311} & \mathbb{C}_{3322} & \mathbb{C}_{3333} \end{bmatrix}^{-1} \\ \mathbb{D}_{ijji} &= \mathbb{D}_{ijji} = \frac{1}{4\mathbb{C}_{ijij}} \text{ if } i \neq j & \mathbb{D}_{ijkk} &= 0 \text{ if } i \neq j \neq k \end{aligned} \quad (20)$$

Note that there is no reason to suppose that  $\mathbb{D}$  is completely symmetric because in general  $\mathbb{D}_{ijij}$  will not be the same as  $\mathbb{D}_{iijj}$ .

In performing the numerical calculations, it is more efficient when forming  $DA/Dt$  and  $DB/Dt$  from equation (11) to calculate the right hand side in the coordinate system of the orthonormal eigenvectors of  $B$ , and then convert back to the standard coordinate system when solving for  $A$  and  $B$ .

For example, suppose  $\mathbb{B}$  is any rank four tensor such that  $\mathbb{B}_{ijkk} = 0$  if  $i \neq j \neq k$ , and  $\mathbb{B}_{ijkl} = \mathbb{B}_{jikl} = \mathbb{B}_{klij}$ . Suppose also that  $N$  is a symmetric matrix. Then  $\mathbb{B} : N$  can be calculated by first defining the matrices  $M_{\mathbb{B}}$  and  $\tilde{M}_{\mathbb{B}}$  as

$$M_{\mathbb{B}} = \begin{bmatrix} \mathbb{B}_{1111} & \mathbb{B}_{1122} & \mathbb{B}_{1133} \\ \mathbb{B}_{1122} & \mathbb{B}_{2222} & \mathbb{B}_{2233} \\ \mathbb{B}_{1133} & \mathbb{B}_{2233} & \mathbb{B}_{3333} \end{bmatrix}, \quad \tilde{M}_{\mathbb{B}} = \begin{bmatrix} 0 & \mathbb{B}_{1212} & \mathbb{B}_{1313} \\ \mathbb{B}_{1212} & 0 & \mathbb{B}_{2323} \\ \mathbb{B}_{1313} & \mathbb{B}_{2323} & 0 \end{bmatrix} \quad (21)$$

then decompose

$$N = \text{diag}(\mathbf{n}) + \tilde{N} \quad (22)$$

where  $\mathbf{n} = (N_{11}, N_{22}, N_{33})$ , and  $\tilde{N}$  is the matrix of the off-diagonal elements of  $N$ . It follows that

$$\mathbb{B} : N = \text{diag}(M_{\mathbb{B}} \cdot \mathbf{n}) + 2\tilde{M}_{\mathbb{B}} \circ \tilde{N} \quad (23)$$

where for any matrices  $U$  and  $V$  we define the entrywise product (also known as the Hadamard or Schur product) by  $(U \circ V)_{ij} = U_{ij}V_{ij}$ .

### 3.1. The Reduced Strain Closure

Wang *et al.* [8] described a method that slows down the rate of alignment of the fibers, which the paper calls the reduced strain closure model (RSC). The method is implemented by selecting a number  $0 < \kappa \leq 1$ , which is identified as the rate of reduction. The authors [8] define the tensor

$$\mathbb{M} = \sum_{i=1}^3 \mathbf{e}_i \mathbf{e}_i \mathbf{e}_i \mathbf{e}_i \quad (24)$$

where  $\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3$  are the orthonormal eigenvectors for  $A$ . The RSC replaces equations of the form

$$\frac{DA}{Dt} = F(A) \quad (25)$$

by

$$\frac{DA}{Dt} = F(A) - (1 - \kappa)\mathbb{M} : F(A) \quad (26)$$

It turns out this is simple to reproduce for the FEC. If equation (25) is represented by the FEC

$$\frac{DA}{Dt} = F(A, B), \quad \frac{DB}{Dt} = G(A, B) \quad (27)$$

then the effect of equation (26) is precisely modeled by the new FEC

$$\frac{DA}{Dt} = F(A, B) - (1 - \kappa)\mathbb{M} : F(A, B), \quad \frac{DB}{Dt} = G(A, B) - (1 - \kappa)\mathbb{M} : G(A, B) \quad (28)$$

Finally, from a computational point of view, it should be noticed that if we are working in the basis of orthonormal eigenvectors of  $B$ , then for any symmetric matrix  $N$  we have that  $\mathbb{M} : N$  is simply the diagonal part of  $N$ , that is,  $\text{diag}(N_{11}, N_{22}, N_{33})$ .

### 3.2. Is the solution to FEC always physical?

By the phrase “the solutions stay physical” we mean that  $A$  stays positive definite with trace one, that is, there exists a fiber orientation distribution  $\psi$  that satisfies equation (4). In fact, if  $A$  ever ceases to become positive definite, then not only is the Exact Closure going to give the wrong answer, it even ceases to have a meaning in that equation (38) cannot be solved. Thus another way to state “the solutions stay physical” is that  $B$  stays positive definite and finite, that is, none of the eigenvalues of  $B$  become zero, and none of them become infinite.

**Theorem 1.** *The FEC solution to the isotropic diffusion equations (12) and (13) have global in time physical solutions if  $\Omega$ ,  $\Gamma$  and  $D_r$  are bounded.*

**Theorem 2.** *The FEC solution to the anisotropic diffusion equations (14) and (15) have global in time physical solutions if  $D_r$  is positive definite, and  $\Omega$ ,  $\Gamma$ ,  $D(D_r)/Dt$ ,  $D_r$  and  $1/\|D_r^{-1}\|$  are bounded.*

Unfortunately Theorem 2 will not necessarily apply to the Koch model [10] nor to the Phelps-Tucker ARD model [9], as there is no guarantee that  $1/\|D_r^{-1}\|$  is bounded nor, in the ARD case, that  $D_r$  is positive definite, unless extra hypotheses are applied.

## 4. Numerical Results

Results are presented to demonstrate the accuracy improvements from employing the FEC closure, and just as important to demonstrate the computational speed advances over the similarly accurate orthotropic closures. All flows have an initial isotropic orientation state designated by  $A_{11} = A_{22} = A_{33} = 1/3$  and  $B_{11} = B_{22} = B_{33} = 1$ , with all other components of  $A$  and  $B$  being zero. The equations of motion are solved using the FEC closure for  $A$  and  $B$  from equations (12) and (13) for isotropic diffusion or from equations (14), (15) and (28) for the ARD model with the reduced strain closure from Phelps and Tucker [9]. For comparison, the classical equations of motion for the second-order orientation tensor  $A$  requiring a curve-fitted closure for the fourth-order orientation tensor  $\mathbb{A}$ , are solved using equations (6) and (7) for Folgar-Tucker diffusion and equations (6), (8) and (25) for the ARD-RSC diffusion model. Results are compared to solutions obtained using the Spherical Harmonic approach [29] for solving the full distribution function equations (2) and (3). Solutions using the Spherical Harmonic approach are only limited in their accuracy by machine precision and require considerably less computational effort than solutions using the control volume approach of Bay [25]. The Spherical Harmonic approach still requires more effort than does the orientation tensor approach, nor does it readily lend itself to an applicable form for coupling with commercial FEA solvers. We select three commonly employed closures for comparisons. The classical Hybrid closure of Advani and Tucker [4] is selected as it is regularly used in commercial and research codes due to its computational efficiency and ease of implementation. The orthotropic closures have found increasing use due to their considerable accuracy improvements over the Hybrid closure, and we select the ORT closure presented by VerWeyst and Tucker [1] based on the Wetzel closure [12] and the IBOF closure of Chung and Kwon [21] which is claimed to be a more computationally efficient orthotropic closure as it uses the invariants of  $A$  as opposed to the eigenvalues of  $A$  thus avoiding costly tensor rotations.



#### 4.1. Algorithm Summary

The algorithm to solve the FEC closure for the second-order orientation tensor  $A$  and the second-order tensor  $B$  can be summarized as:

1. Initialize  $A$  and  $B$ , and define  $\lambda$  and any constants needed for the diffusion model  $\mathcal{D}[A]$
2. At time  $t_i$ , rotate the tensors  $A$  and  $B$  into the principal frame of  $B$
3. When the eigenvalues are distinct, use equation (16) for  $\mathbb{C}$ . Otherwise when two eigenvalues are repeated, use equation (17) along with equation (18). When three eigenvalues are repeated, use equation (19).
4. Compute  $\mathbb{D}$  using equation (20) in the principal frame of  $B$ .
5. Compute  $DA/Dt$  and  $DB/Dt$  using either equations (12) and (13) for isotropic diffusion or equations (14), (15) and (28) for the anisotropic diffusion model, ARD-RSC. For the symmetric rank four tensor contractions with rank two tensors, use equation (23) to reduce the number of redundant multiplication operations.
6. Rotate  $DA/Dt$  and  $DB/Dt$  into the flow reference frame, and extrapolate  $A(t_{i+1})$  and  $B(t_{i+1})$  from time  $t_i$  using any standard ODE solver.

There are a number of coding issues that we feel it will be helpful to share as it will aid others in their computational implementations.

- There is a choice to compute the basis of orthonormal eigenvectors from either  $A$  or  $B$ , where in theory these should be identical. We compute the basis from  $B$ , arguing that the quantity  $B$  is somehow more ‘fundamental’ and  $A$  is ‘derived,’ which is true in the absence of diffusion.
- We solve a ten dimensional set of ODEs, five for  $A$ , and five for  $B$ , where one of the components of  $A$  and  $B$  can be obtained, respectively, from the relationships  $\text{tr } A = 1$  and  $\det B = 1$ .
- When computing  $A$  from the orthonormal eigenvector basis of  $B$ , it is important to force the off diagonal entries to be non-zero to limit numerical drifting. In our studies, we found that failing to do this could cause an adaptive ODE solver to completely freeze in select scenarios.
- We set the ODE solver to work with a relative tolerance of  $10^{-5}$ , and choose to use equations (18) or (19) when the eigenvalues were within  $10^{-4}$  of each other. This should cause  $\mathbb{C}$  to be computed with an accuracy of about  $10^{-8}$  when using equations (16), and nearly machine precision when using equations (18) or (19).

#### 4.2. Results: Simple Shear Flow

The first example is of a pure shearing flow, given by  $v_1 = Gx_3$  and  $v_2 = v_3 = 0$ . Pure shearing flow is commonly employed (see e.g., [6, 21, 30]) to demonstrate a particular closure problem due to the oscillatory nature of alignment inherent to the Jeffery fiber orbits. Two scenarios are presented, the first of the Folgar-Tucker isotropic diffusion model in equation (2) where  $D_r = C_I \dot{\gamma}$ , and the second scenario for the ARD-RSC anisotropic diffusion model. All results are compared to solutions obtained through the spherical harmonic solution approach [29], which in the present context is considered numerically exact.

In industrial simulations, the Folgar-Tucker isotropic diffusion model typically has interaction coefficients that range from  $C_I = 10^{-3}$  to  $C_I = 10^{-2}$ . The effective fiber aspect ratio ranges from 5 to 30 ( $a_e \simeq 1.4 \times a_r$ , which corresponds to a shape correction factor ranging from  $\lambda = 0.96$  to



$\lambda = 0.999$ ). Two simulation results using isotropic diffusion are presented in Figures 1(a) and (b), the first is for  $C_I = 10^{-3}$  with  $\lambda = 0.99$  and the later for  $C_I = 10^{-2}$  with  $\lambda = 0.95$ . Results for the IBOF closure are not shown as they are graphically indistinguishable from the ORT closure results. It is important to observe that the ORT and the FEC closure yield results that are graphically indistinguishable and reasonably close to the orientation state predicted from the numerically exact Spherical Harmonic solution. Conversely, the orientation results from the Hybrid closure tend to over predict the the true orientation state. It is important to point out the apparent oscillatory nature of the transient solution when  $C_I = 10^{-3}$  with  $\lambda = 0.99$ , which occurs to a lesser extent for  $C_I = 10^{-2}$ . These oscillations are expected due to the low amount of diffusion present. Equally important is to notice that the oscillations from the FEC closure, as well as the ORT, both damp out to the same steady state value. Note also that the FEC does not oscillate excessively for either of the isotropic flow conditions presented, which was a problem that plagued the early orthotropic closures (see e.g., [6] and [31]) and the early neural network closures [32]. There remains room for further accuracy improvements (see e.g., [33] for several preliminary higher accuracy closures). However, it is speculated based upon the discussion in Jack and Smith [34] that such improvements will be slight when solving the second-order moment equations, and higher order moment simulations, such as those that use sixth-order closures (see e.g., [23]) may need to be considered for significant accuracy improvements.

The Folgar-Tucker model has been used for decades, but tends to overstate the rate of alignment during the transient solution (see e.g., [7]). The ARD-RSC model [9] seeks to address these limitations, but few studies have focused on this new diffusion model and the dependance of computed results on the choice of closure. The ARD-RSC model serves as an excellent example of the effectiveness of the FEC approach for solving the tensor form of orientation as the ARD-RSC model will yield orientation states that are considerably different than that of the Folgar-Tucker model. Results from the various closures and the spherical harmonic results are presented in Figure 2 for the ARD-RSC flow with  $\kappa = 1/30$ . The value of  $\kappa = 1/30$  is taken from the results presented in Phelps and Tucker [9], which was based on their experimental observations. For a fiber aspect ratio of  $\sim 5$ , corresponding to  $\lambda = 0.95$ , each of the investigated closures produces graphically similar results. During the initial flow stages, the Hybrid tends to over predict alignment, whereas the ORT and the FEC tend to under predict alignment. As steady state is attained, the FEC and the ORT yield nearly identical results, both of which over predict  $A_{11}$  in the final orientation state whereas the Hybrid yields a reasonable representation of the orientation. For a long fiber, corresponding to  $\lambda \rightarrow 1$ , the trends are similar to those of the lower aspect ratio fibers, but in this case the FEC and the ORT better represent the final orientation state relative to the Hybrid.

The ORT is a polynomial approximation to the Exact Closure, as demonstrated in the preceding section, and it is not surprising that the two approaches yield graphically indistinguishable results for many of the flows investigated. On closer inspection of the transient solution of the ARD-RSC model for  $\kappa = 1/30$  and  $\lambda = 1$  there is a slight difference. This difference is shown in Figure 3(a) where a closeup view is provided of the  $A_{11}$  component. These results indicate how well the fitting was performed in the construction of the ORT. As the ORT is an approximation of the Exact Closure of Montgomery-Smith *et al.* [14] for pure Jeffery's flow, it is of interest to determine whether the slight deviation comes from the Jeffery's component or the diffusion component of equation (6). To this end, we performed a comparison between the derivative of  $A$  computed in two different ways. First, for each point in time  $t$ , we computed  $A(t)$  and  $B(t)$  using the FEC method. Then we computed four quantities:  $\frac{DA^{\text{FEC, Diff}}}{Dt}$  which contains the terms from the right

hand side of equation (14) that explicitly include  $D_r$ ,  $\frac{DA^{\text{FEC, Jeff}}}{Dt}$  which contains the terms from the right hand side of equation (14) that do not involve  $D_r$ ,  $\frac{DA^{\text{ORT, Diff}}}{Dt}$  the right hand side of equation (8), and  $\frac{DA^{\text{ORT, Jeff}}}{Dt}$  the right hand side of equation (6) when  $\mathcal{D}(A)$  is set to zero. In the latter two cases  $\mathbb{A}$  is computed using the ORT closure.

$$Err_{\text{Diffusion}} = \sqrt{\sum_{i=1}^3 \sum_{j=1}^3 \left( \frac{DA_{ij}^{\text{FEC, Diff}}}{Dt} - \frac{DA_{ij}^{\text{ORT, Diff}}}{Dt} \right)^2} \quad (29)$$

$$Err_{\text{Jeffery}} = \sqrt{\sum_{i=1}^3 \sum_{j=1}^3 \left( \frac{DA_{ij}^{\text{FEC, Jeff}}}{Dt} - \frac{DA_{ij}^{\text{ORT, Jeff}}}{Dt} \right)^2} \quad (30)$$

Each of the two errors are plotted in Figure 3(b). It is clear from the figure that although the ORT's derivative calculation from the diffusion component is not zero, it is minor in comparison to the error from the Jeffery's part of the orientation tensor equation of motion. This error is only a rough indication of the sources of error, but values of 0.04% at a given moment in flow time can account for an error as large as 40% for  $A$  for the flow times on the order 1,000. Since the errors from each of the possible sources probably do not drive the error in the solution toward the same direction, the total error would be expected to be less than the upper bound of 40%, where in reality the error is closer to 0.9% as steady state is approached.

Since the ORT and FEC differ by about 0.9%, it begs the question as to which is more accurate in computing the true exact closure. While the FEC in theory should exactly compute the exact closure, it is possible that numerical errors creep into the FEC. To test for this, we performed a consistency check. After finding the solution  $A(t)$  and  $B(t)$  using the FEC, we calculated

$$Err_{\text{Exact}} = \sqrt{\sum_{i=1}^2 \sum_{j=1}^3 (A(B)_{ij} - A_{ij})^2} \quad (31)$$

where  $A(B)$  was computed using equation (38). This calculation was performed by diagonalizing  $B$ , applying the elliptic integrals in equation set (47) using the software package [35], and then performing the reverse change of basis. The results for the ARD-RSC model with  $\kappa = 1/30$  and  $\lambda = 1.00$  show an error of less than  $10^{-8}$  throughout the transient solution, thus suggesting the implementation as presented in this paper for the FEC is quite accurate.

#### 4.3. Results: Error Summary

To quantify the errors observed in Figures 1(a) and (b) for the isotropic diffusion models, a series of fourteen flows are studied as outlined in table 1 where  $\lambda = 1$  for each of the flows. The solution is obtained using the classical closure methods and the FEC closure results are compared to solutions obtained from the Spherical Harmonic approach. To quantify the error, the Frobenius Norm of the difference between the true solution  $A_{ij}^{\text{Spherical}}(t)$  and the approximate solution obtained from a closure  $A_{ij}^{\text{Closure}}(t)$  is computed as

$$\|Err(t)\|_{\text{Closure}} = \sqrt{\sum_{i=1}^3 \sum_{j=1}^3 \left| A_{ij}^{\text{Spherical}}(t) - A_{ij}^{\text{Closure}}(t) \right|^2} \quad (32)$$

The Frobenius Norm is then integrated over all time to obtain the average error as

$$\overline{Err}_{\text{Closure}} = \frac{1}{t_{\text{end}} - t_{\text{start}}} \int_{t_{\text{start}}}^{t_{\text{end}}} ||Err(t)||_{\text{Closure}} dt \quad (33)$$

where  $t_{\text{start}}$  is the initial time where the fiber orientation is isotropic and  $t_{\text{end}}$  is the time when the steady state is attained, which in this example will be defined when the magnitude of the largest derivative of the eigenvalues of  $A$  is less than  $G \times 10^{-4}$ . This can be expressed as the smallest moment in time when the following is satisfied  $\left(\max_{i \in \{1,2,3\}} \left| \frac{DA(i)}{Dt}(t) \right| \right) \leq G \times 10^{-4}$ . The quantitative error metric in equation (33) yields a value for the simple shear flow of Figure 1(b) for the FEC, ORT and Hybrid closures of, respectively,  $4.74 \times 10^{-2}$ ,  $4.85 \times 10^{-2}$  and  $1.75 \times 10^{-1}$ . As the objective is to compare the relative accuracy improvements between the FEC closure and the existing closures we will normalize the error metric in equation (33) as

$$\overline{Err}_{\min} \equiv \min \overline{Err}_{\text{Closure}} \quad (34)$$

$$\overline{\varepsilon}_{\text{Closure}} \equiv \frac{\overline{Err}_{\text{Closure}}}{\overline{Err}_{\min}} \quad (35)$$

where the closure with the greatest accuracy will have a value of  $\overline{\varepsilon}_{\text{Closure}} = 1$ , and the remaining closures will have a value of  $\overline{\varepsilon}_{\text{Closure}}$  in excess of 1. For each of the flows studied, the normalized error of equation (34) is tabulated in Table 1 for the FEC, ORT, IBOF and the Hybrid closures. In each of the flows considered, the FEC performs as well as or better than the orthotropic closures.

#### 4.4. Results: Combined Flow

A classical flow to demonstrate the effectiveness and robustness of a closure is that of the combined flow presented in Cintra and Tucker [6]. This flow is often selected as the orientation state crisscrosses the eigenspace of possible orientations. The combined flow begins with pure shear in the  $x_1 - x_2$  direction for  $0 \leq Gt < 10$  defined by the velocity field  $v_1 = Gx_2$ ,  $v_2 = v_3 = 0$ . The flow then transitions to shearing flow in the  $x_2 - x_3$  plane with stretching in the  $x_3$  direction during the time  $10 \leq Gt < 20$  defined by the velocity field  $v_1 = -1/20Gx_1$ ,  $v_2 = -1/20Gx_2 + Gx_3$  and  $v_3 = 1/10Gx_3$ . The flow then transitions to a flow with a considerable amount of stretching in the  $x_1$  direction with a reduced amount of shearing in the  $x_2 - x_3$  plane for  $20 \leq Gt$  defined by the velocity field  $v_1 = Gx_1$ ,  $v_2 = -1/2Gx_2 + Gx_1$  and  $v_3 = -1/2x_3$ . The times where the flow transitions are chosen to prevent the orientation from attaining steady state, thus any error in the transient solution will be propagated to the next flow state. As observed in Figure 4 for flow results from the Folgar-Tucker model with  $C_I = 10^{-2}$  and  $\lambda = 1$ , the ORT and the FEC again yield similar results. This is significant as it further demonstrates the robustness and the accuracy of the FEC.

#### 4.5. Results: Center-gated Disk Flow

The final flow investigated is that of the center-gated disk, which regularly occurs in industrial processes [1, 36]. The flow enters the mold through the pin gate and flows radially outward. The velocity vector is a function of both the gap height  $2b$  and the radial distance from the gate  $r$ . The velocity and the velocity gradient for a Non-Newtonian fluid can be represented by [6]

$$v_r = \frac{3Q}{8\pi r b} \left( 1 - \left( \frac{z}{b} \right)^2 \right), \quad v_\theta = v_z = 0 \quad (36)$$

$$\frac{\partial v_i}{\partial x_j} = \frac{3Q}{8\pi r b} \begin{bmatrix} -\frac{1}{r}\left(1-\frac{z^2}{b^2}\right) & 0 & -\frac{2}{b}\frac{z}{b} \\ 0 & \frac{1}{r}\left(1-\frac{z^2}{b^2}\right) & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad (37)$$

where  $z$  is the gap height location between the mold walls,  $b$  is half the gap height thickness, and  $Q$  is the flow rate. Orientation results are presented in Figure 5 for a gap height of  $z/b = 4/10$  for isotropic diffusion with  $C_I = 10^{-2}$  and  $\lambda = 1$ . Again, the Hybrid overshoots the actual orientation state, whereas the ORT and the FEC behave in a graphically identical fashion. This last result further demonstrates the robustness of the FEC approach. Similar tests were performed for gap heights of  $z/b = 0, 1/10, 2/10, \dots, 9/10$  and similar conclusions were observed at all gap heights.

#### 4.6. Results: Computational Time Enhancement

An additional goal for any new closure is that of reducing the computational requirements for numerical solutions. Simulations are performed using in-house developed single threaded code using Intel's FORTRAN 90 compiler version 11.1. Computations are solved on a standard desktop with an Intel i7 processor with 8 GB of Ram. The solution of the ORT has been studied by the investigators for several years, and a reasonably efficient algorithm has been developed. Solutions for the IBOF were made using the FORTRAN 90 code discussed in Jack *et al.* [30].

Notice from Equations (12) and (13) that the operations  $\mathbb{C} : [\dots]$  and  $\mathbb{D} : [\dots]$  are independent of coordinate frame. As we explained in equation (23), in the principal frame there are a considerable number of terms in both  $\mathbb{C}$  and  $\mathbb{D}$  that are zero that are known prior to any calculations, and thus operations involving 0 can be avoided in the coding. In addition, computing  $DA/Dt$  and  $DB/Dt$  in the principle reference frame and then rotating the resulting  $3 \times 3$  tensors into the local reference frame will be more efficient than rotating the  $3 \times 3 \times 3 \times 3$  tensors  $\mathbb{C}$  and  $\mathbb{D}$  into the local reference frame and then computing  $DA/Dt$  and  $DB/Dt$ . All computations of the FEC utilize this characteristic, and thus greatly reduce the computational efforts. In addition, redundant calculations from Equations (12) and (13) are closely followed and performed only once. These computations are particularly frequent in the double contractions of the fourth-order tensors with the second-order tensors.

In the first study, computations were performed for the previous closure operations for the ORT and the Hybrid using algorithms similar to implementations discussed in the literature. In studies using an adaptive step size solver, solutions for the IBOF took nearly 10 times that of the ORT, whereas for the fixed step size the two closures required similar computational efforts. To avoid any computational comparisons introduced by an adaptive step size solver, computations were performed using a fixed step-size fourth-order Runge-Kutta (R-K) solver with a very small step size of  $\Delta Gt = 10^{-4}$ . Computational times are tabulated in Table 2 for both CPU time and normalized time. Normalized time is defined based off of the often employed Hybrid closure using the standard implementation for the Hybrid closure with the very small step size. The ORT required nearly 770 seconds, a factor of 31 times greater than that of the Hybrid. Conversely, the FEC required only 26 seconds, a slight increase in effort beyond the Hybrid, which required 25 seconds. This is very striking as the Hybrid closure is often selected in research and industrial codes due to its computational efficiency, while recognizing the sacrifice in computational accuracy. This is no longer the case with the FEC as it has the same accuracy of the orthotropic closures while providing computational speeds nearly identical to that of the Hybrid closure.

In the process of developing the FEC algorithm, it was observed that many redundant operations existed in the implementation of the ORT and the Hybrid closures. For existing implementation of

the classical closures, no special consideration was given to the  $\mathbb{A} : \Gamma$  term, but since the rank four tensor  $\mathbb{A}$  is symmetric, equation (23) can be used to reduce the number operations of the double contraction to that of a simple rank two tensor operations for both the hybrid closure and the ORT closure implementations. For the ORT, the computational problem can be further simplified by constructing the second-order tensor  $DA/Dt$  in the principal frame, and then performing the tensor rotation back into the reference frame. Thus the costly rotations of the fourth-order tensor  $\mathbb{A}$  are avoided. These optimized results for the Hybrid and the ORT are shown in Table 2, and it is clear that the computational times were greatly reduced. The optimized Hybrid implementation reduced the computational time to 30% of the original time, whereas the ORT implementation improved by over an order of magnitude. With these additional computational advances the ORT appears to be a more viable alternative to the Hybrid, but the FEC still has similar computational requirements. It is expected that with further studies, the FEC algorithm could be improved to further reduce its computational times.

## 5. Conclusion

The Fast Exact Closure is a robust, computationally efficient, approach to solve the fiber orientation equations of motion for the orientation tensors. This unique approach does not require any form of curve fitting based on orientation data obtained from numerical solutions of the full fiber orientation distribution. The results presented demonstrate that the FEC is as accurate and robust as the existing industrially accepted closures, while enjoying computational speeds equivalent to the industrial form of the hybrid closure.

## 6. Acknowledgments

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## Appendix: Justification and Proofs

By [14], the Exact Closure is this. Given  $A$ , compute the symmetric matrix  $B$  by solving

$$A = A(B) = \frac{1}{2} \int_0^\infty \frac{(B + sI)^{-1} ds}{\sqrt{\det(B + sI)}} \quad (38)$$

It was shown in [14] that  $B$  is unique with this property. Then compute  $\mathbb{A}$  using the formula

$$\mathbb{A} = \frac{3}{4} \int_0^\infty \frac{s \mathcal{S}((B + sI)^{-1} \otimes (B + sI)^{-1}) ds}{\sqrt{\det(B + sI)}} \quad (39)$$

Here  $\mathcal{S}$  represents the symmetrization of a rank 4 tensor, that is,  $\mathcal{S}(\mathbb{B})_{ijkl}$  is the average of  $\mathbb{B}_{mnpq}$  over all permutations  $(m, n, p, q)$  of  $(i, j, k, l)$ .

It can be shown that the following two statements are equivalent:

1. Equation (38) holds for all time.

2. Equation (38) holds at  $t = 0$ , and equation (9) holds for all time, where

$$\mathbb{C} = \frac{3}{4} \int_0^\infty \frac{\mathcal{S}((B + sI)^{-1} \otimes (B + sI)^{-1}) ds}{\sqrt{\det(B + sI)}} \quad (40)$$

Furthermore, it can be shown for every symmetric matrix  $M$  that

$$\text{tr}(B^{-1} \cdot M) = 2 \text{tr}(\mathbb{C} : M) \quad (41)$$

and hence it can be seen that  $\text{tr}(DA/Dt) = 0$  if and only if  $\text{tr}(B^{-1} \cdot (DB/Dt)) = 0$ , that is,  $\text{tr} A$  stays constant if and only if  $\det B$  stays constant.

Next, we have

$$\text{The linear map on symmetric matrices } M \mapsto \mathbb{C} : M \text{ is invertible} \quad (42)$$

that is, there exists a rank 4 tensor  $\mathbb{D}$  such that

$$\mathbb{C} : \mathbb{D} : M = \mathbb{D} : \mathbb{C} : M = M \text{ for any symmetric matrix } M \quad (43)$$

Indeed if we define the six by six matrix

$$\mathcal{C} = \begin{bmatrix} \mathbb{C}_{1111} & \mathbb{C}_{1122} & \mathbb{C}_{1133} & 2\mathbb{C}_{1112} & 2\mathbb{C}_{1113} & 2\mathbb{C}_{1123} \\ \mathbb{C}_{2211} & \mathbb{C}_{2222} & \mathbb{C}_{2233} & 2\mathbb{C}_{2212} & 2\mathbb{C}_{2213} & 2\mathbb{C}_{2223} \\ \mathbb{C}_{3311} & \mathbb{C}_{3322} & \mathbb{C}_{3333} & 2\mathbb{C}_{3312} & 2\mathbb{C}_{3313} & 2\mathbb{C}_{3323} \\ 2\mathbb{C}_{1211} & 2\mathbb{C}_{1222} & 2\mathbb{C}_{1233} & 4\mathbb{C}_{1212} & 4\mathbb{C}_{1213} & 4\mathbb{C}_{1223} \\ 2\mathbb{C}_{1311} & 2\mathbb{C}_{1322} & 2\mathbb{C}_{1333} & 4\mathbb{C}_{1312} & 4\mathbb{C}_{1313} & 4\mathbb{C}_{1323} \\ 2\mathbb{C}_{2311} & 2\mathbb{C}_{2322} & 2\mathbb{C}_{2333} & 4\mathbb{C}_{2312} & 4\mathbb{C}_{2313} & 4\mathbb{C}_{2323} \end{bmatrix} \quad (44)$$

then  $\mathbb{D}$  can be calculated using the formula

$$\begin{bmatrix} \mathbb{D}_{1111} & \mathbb{D}_{1122} & \mathbb{D}_{1133} & \mathbb{D}_{1112} & \mathbb{D}_{1113} & \mathbb{D}_{1123} \\ \mathbb{D}_{2211} & \mathbb{D}_{2222} & \mathbb{D}_{2233} & \mathbb{D}_{2212} & \mathbb{D}_{2213} & \mathbb{D}_{2223} \\ \mathbb{D}_{3311} & \mathbb{D}_{3322} & \mathbb{D}_{3333} & \mathbb{D}_{3312} & \mathbb{D}_{3313} & \mathbb{D}_{3323} \\ \mathbb{D}_{1211} & \mathbb{D}_{1222} & \mathbb{D}_{1233} & \mathbb{D}_{1212} & \mathbb{D}_{1213} & \mathbb{D}_{1223} \\ \mathbb{D}_{1311} & \mathbb{D}_{1322} & \mathbb{D}_{1333} & \mathbb{D}_{1312} & \mathbb{D}_{1313} & \mathbb{D}_{1323} \\ \mathbb{D}_{2311} & \mathbb{D}_{2322} & \mathbb{D}_{2333} & \mathbb{D}_{2312} & \mathbb{D}_{2313} & \mathbb{D}_{2323} \end{bmatrix} = \mathcal{C}^{-1} \quad (45)$$

$$\mathbb{D}_{ijkl} = \mathbb{D}_{jikl} = \mathbb{D}_{ijlk} \quad (46)$$

In the basis of orthonormal eigenvectors of  $B$ , since  $\mathbb{C}_{ijkk} = 0$  whenever  $i \neq j \neq k$ , this reduces to equation (20).

Next, if  $B$  is diagonal, then  $A$  is diagonal with entries

$$\begin{aligned} a_1 &= \frac{1}{2} \int_0^\infty \frac{ds}{(b_1 + s)^{3/2} \sqrt{b_2 + s} \sqrt{b_3 + s}} \\ a_2 &= \frac{1}{2} \int_0^\infty \frac{ds}{\sqrt{b_1 + s} (b_2 + s)^{3/2} \sqrt{b_3 + s}} \\ a_3 &= \frac{1}{2} \int_0^\infty \frac{ds}{\sqrt{b_1 + s} \sqrt{b_2 + s} (b_3 + s)^{3/2}} \end{aligned} \quad (47)$$

and

$$\begin{aligned} \mathbb{C}_{1111} &= \frac{3}{4} \int_0^\infty \frac{ds}{(b_1 + s)^{5/2} \sqrt{b_2 + s} \sqrt{b_3 + s}} & \mathbb{C}_{1122} &= \frac{1}{4} \int_0^\infty \frac{ds}{(b_1 + s)^{3/2} (b_2 + s)^{3/2} \sqrt{b_3 + s}} \\ \mathbb{C}_{2222} &= \frac{3}{4} \int_0^\infty \frac{ds}{\sqrt{b_1 + s} (b_2 + s)^{5/2} \sqrt{b_3 + s}} & \mathbb{C}_{2233} &= \frac{1}{4} \int_0^\infty \frac{ds}{\sqrt{b_1 + s} (b_2 + s)^{3/2} (b_3 + s)^{3/2}} \\ \mathbb{C}_{3333} &= \frac{3}{4} \int_0^\infty \frac{ds}{\sqrt{b_1 + s} \sqrt{b_2 + s} (b_3 + s)^{5/2}} & \mathbb{C}_{1133} &= \frac{1}{4} \int_0^\infty \frac{ds}{(b_1 + s)^{3/2} \sqrt{b_2 + s} (b_3 + s)^{3/2}} \end{aligned} \quad (48)$$

all the other coefficients of  $\mathbb{C}$  being zero. Furthermore

$$\mathbb{C} : I = \frac{1}{2}B^{-1} \quad (49)$$

Equations (16) now follow by an easy calculation. Equations (18) and (19) are obtained by expanding the fourth equation of (48) using Taylor's series, where

$$\mathcal{I}_n = \int_0^\infty \frac{ds}{(b_0 + s)^n \sqrt{b_3 + s}} \quad (50)$$

The proofs of various details now follow.

*Proof of equations (9) and (40):* Write  $\dot{A}$  and  $\dot{B}$  for  $\frac{DA}{Dt}$  and  $\frac{DB}{Dt}$  respectively. Use the formulae

$$\frac{D}{Dt}B^{-1} = -B^{-1} \cdot \dot{B} \cdot B^{-1} \quad \text{and} \quad \frac{D}{Dt} \det B = \text{tr}(B^{-1} \cdot \dot{B}) \det B \quad (51)$$

to obtain

$$\begin{aligned} \dot{A} &= -\frac{1}{2} \int_0^\infty \frac{(B + sI)^{-1} \cdot \dot{B} \cdot (B + sI)^{-1} ds}{\sqrt{\det(B + sI)}} - \frac{1}{4} \int_0^\infty \frac{[(B + sI)^{-1} : \dot{B}] (B + sI)^{-1} ds}{\sqrt{\det(B + sI)}} \\ &= -\mathbb{C} : \dot{B} \end{aligned} \quad (52)$$

since for any symmetric matrix  $K$  we have

$$\mathcal{S}(K \otimes K) : \dot{B} = \frac{1}{3}K \cdot \dot{B} \cdot K + \frac{2}{3}(K : \dot{B})K \quad (53)$$

*Proof of equation (10):* For any invertible symmetric matrix  $K$

$$\mathcal{S}(K^{-1}K^{-1}) : (K \cdot M) = \mathcal{S}(K^{-1}K^{-1}) : (M^T \cdot K) = \frac{1}{3}((\text{tr } M)K^{-1} + M \cdot K^{-1} + K^{-1} \cdot M^T) \quad (54)$$

Setting  $K = B + sI$ , we multiply both sides by  $3/(4\sqrt{\det(B + sI)})$ , and integrate with respect to  $s$  from zero to infinity, to obtain equation (10).

*Proof of equations (17) from (50):* To compute  $\mathcal{I}_1$ , use the formulae

$$\frac{d}{ds} \cos^{-1} \left( \sqrt{\frac{b_3 + s}{b_0 + s}} \right) = -\frac{\sqrt{b_0 - b_3}}{2(b_0 + s)\sqrt{b_3 + s}} \quad (55)$$

$$\frac{d}{ds} \cosh^{-1} \left( \sqrt{\frac{b_3 + s}{b_0 + s}} \right) = -\frac{\sqrt{b_3 - b_0}}{2(b_0 + s)\sqrt{b_3 + s}} \quad (56)$$

Next, integrating by parts, we obtain

$$\mathcal{I}_n = -\frac{\sqrt{b_3}}{2b_0^n} + \frac{n}{2} \int_0^\infty \frac{\sqrt{b_3 + s} ds}{(b_0 + s)^{n+1}} \quad (57)$$

and simple algebra gives

$$\int_0^\infty \frac{\sqrt{b_3 + s} ds}{(b_0 + s)^{n+1}} = \mathcal{I}_n + (b_3 - b_0)\mathcal{I}_{n+1} \quad (58)$$



*Proof of equation (41):* For any positive definite matrix  $X$ , if

$$A(X) = \frac{1}{2} \int_0^\infty \frac{(X + sI)^{-1} ds}{\sqrt{\det(X + sI)}} \quad (59)$$

then

$$\text{tr}(A(X)) = \frac{1}{2} \int_0^\infty \frac{\text{tr}((X + sI)^{-1}) ds}{\sqrt{\det(X + sI)}} = - \int_0^\infty \frac{d}{ds} \left( \frac{1}{\sqrt{\det(X + sI)}} \right) ds = \frac{1}{\sqrt{\det X}} \quad (60)$$

If  $\text{tr}(B^{-1} \cdot M) = \alpha$ , then (remembering that  $\det B = 1$ ) we have  $\det(B + \epsilon M) = 1 + \epsilon \alpha + O(\epsilon^2)$  as  $\epsilon \rightarrow 0$ . Hence  $1 - \frac{1}{2}\epsilon \alpha + O(\epsilon^2) = \text{tr}(A(B + \epsilon M)) = 1 - \epsilon \text{tr}(\mathbb{C} : M) + O(\epsilon^2)$ . Therefore  $\text{tr}(\mathbb{C} : M) = \frac{1}{2}\alpha$ .

*Proof of equation (42):* This follows because

$$M \text{ is a symmetric non-zero matrix} \Rightarrow M : \mathbb{C} : M > 0 \quad (61)$$

and hence  $M \neq 0 \Rightarrow \mathbb{C} : M \neq 0$ .

To see this, suppose that  $K$  is a positive definite three by three matrix, and let  $k_1, k_2$  and  $k_3$  be its eigenvalues. Then in the basis of corresponding orthonormal eigenvalues of  $K$ , we have that for any non-zero symmetric  $M$

$$M : \mathcal{S}(K \otimes K) : M = \frac{1}{3} \left( \sum_{i=1}^3 k_i M_{ii} \right)^2 + \frac{2}{3} \sum_{i,j=1}^3 k_i k_j M_{ij}^2 > 0 \quad (62)$$

Apply this to  $K = (B + sI)^{-1}$ , multiply by  $(\det(B + sI))^{-1/2}$ , and then integrate over  $s$  to obtain  $M : \mathbb{C} : M > 0$ .

*Proof of equation (49):* Without loss of generality  $B$  is diagonal. Hence we need to prove statements such as  $\mathbb{C}_{1111} + \mathbb{C}_{1122} + \mathbb{C}_{1133} = \frac{1}{2}b_1^{-1}$  when  $\mathbb{C}$  satisfies equation (48). But

$$\begin{aligned} \mathbb{C}_{1111} + \mathbb{C}_{1122} + \mathbb{C}_{1133} &= -\frac{1}{2} \int_0^\infty \frac{d}{ds} \left( \frac{1}{(b_1 + s)^{3/2} \sqrt{b_2 + s} \sqrt{b_3 + s}} \right) ds \\ &= \frac{1}{2} b_1^{-3/2} b_2^{-1/2} b_3^{-1/2} \end{aligned} \quad (63)$$

The result follows since  $b_1 b_2 b_3 = 1$ .

*Proof of equation (28):* From equation (9), we see that the RSC version of equation (27) is equation (28) and

$$\frac{DB}{Dt} = G(A, B) - (1 - \kappa) \mathbb{D} : \mathbb{M} : F(A, B) \quad (64)$$

Since  $\mathbb{D} : F(A, B) = G(A, B)$ , it follows that all we need to show is  $\mathbb{D} : \mathbb{M} : F(A, B) = \mathbb{M} : \mathbb{D} : F(A, B)$ . This is easily seen by working in the basis of orthonormal eigenvectors of  $B$ , noticing that then  $\mathbb{M} : N$  is simply the diagonal part of  $N$ , and applying equation (23).

*Proof of Theorem 1:* It follows from  $\det B = 1$  that the only way that the solutions can become non-physical is if  $B$  ‘blows up,’ that is, if one or more of the eigenvalues of  $B$  become infinite in finite time. (Also, [37, Theorem 1.4] can be used to show that the finiteness of the eigenvalues of  $B$  imply the differential equations have a unique solution.)

Substituting  $M = I$  into equation (10), we obtain  $\mathbb{C} : B = \frac{3}{2}A$ , that is,

$$\mathbb{D} : A = \frac{2}{3}B \quad (65)$$

Take the trace of equation (13) and use equation (65), to obtain

$$\frac{D}{Dt} \text{tr } B \leq c(\|\Omega\| + \|\Gamma\| + D_r)(\text{tr } B) - 2D_r(I : \mathbb{D} : I) \quad (66)$$

for some universal constant  $c > 0$ . Here  $\|\cdot\|$  denotes the spectral norm of a matrix, and we have used the inequality  $\text{tr}(X \cdot Y) \leq \|X\| \text{tr } Y$  whenever  $Y$  is positive definite. By equation (61), we have  $I : \mathbb{D} : I = M : \mathbb{C} : M \geq 0$ , where  $M = \mathbb{D} : I$ , and hence

$$\frac{D}{Dt} \text{tr } B \leq c(\|\Omega\| + \|\Gamma\| + D_r)(\text{tr } B) \quad (67)$$

Now we can apply Gronwall's inequality [37, Chapter 2.1.1] (in Lagrangian coordinates) to obtain

$$\text{tr } B \leq (\text{tr } B_0)e^{ctL} \quad (68)$$

where  $L$  is an upper bound for  $\|\Omega\| + \|\Gamma\| + D_r$ , and  $B_0$  is the value of  $B$  at  $t = 0$ . Therefore  $\text{tr } B$  remains finite, and since  $B$  is positive definite, no eigenvalue of  $B$  blows up to infinity in finite time.

*Proof of Theorem 2:* Note that the positive definiteness of  $D_r$ , and the boundedness of  $D_r$  and  $1/\|D_r^{-1}\|$  guarantee that the ratio of  $\text{tr } B$  and  $D_r : B$  is bounded from above and below. From equation (15), and using equation (65)

$$\frac{D}{Dt}(D_r : B) \leq c \left( \|\Omega\| + \|\Gamma\| + \|D_r\| + \left\| \frac{D(D_r)}{Dt} \right\| \right) (D_r : B) - 2(D_r : \mathbb{D} : D_r) \quad (69)$$

The rest of the proof proceeds by a similar argument as above.

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Flow #	$v_1$	$v_2$	$v_3$	$C_I$	$\lambda$	$\bar{\epsilon}_{\text{FEC}}$	$\bar{\epsilon}_{\text{ORT}}$	$\bar{\epsilon}_{\text{IBOF}}$	$\bar{\epsilon}_{\text{Hybrid}}$
1	$Gx_1$	$Gx_2$	$-2Gx_3$	$10^{-3}$	1	1	2.06	1.28	76.2
2	$2Gx_1$	$-Gx_2$	$-Gx_3$	$10^{-3}$	1	1.03	1.05	1	25.8
3a	$Gx_3$	0	0	$10^{-3}$	0.99	1	1.02	1.02	3.69
3b	$Gx_3$	0	0	$10^{-3}$	1	1	1.02	1.01	3.28
4	$-Gx_1 + 10Gx_2$	$-Gx_2$	$2Gx_3$	$10^{-3}$	1	1	2.25	1.36	12.9
5	$-Gx_1 + Gx_2$	$-Gx_2$	$2Gx_3$	$10^{-3}$	1	1.02	1	1.23	22.6
6	$Gx_1 + 2Gx_3$	$Gx_2$	$-2Gx_3$	$10^{-2}$	1	1	1.01	1.08	3.57
7	$Gx_1 + 2.75Gx_3$	$Gx_2$	$-2Gx_3$	$10^{-2}$	1	1	1.02	1.05	2.98
8	$Gx_1 + 1.25Gx_3$	$Gx_2$	$-2Gx_3$	$10^{-2}$	1	1.02	1	1.12	3.85
9	$-Gx_1 + 10Gx_3$	$Gx_2$	0	$10^{-2}$	1	1.03	1	1.03	1.65
10	$-Gx_1 + Gx_3$	$Gx_2$	0	$10^{-2}$	1	1.01	1	1.04	2.29
11	$2Gx_1 + 3Gx_3$	$-Gx_2$	$-Gx_3$	$10^{-2}$	1	1.04	1.04	1	2.52
12	$-Gx_1 + 3.75Gx_2$	$Gx_2$	$2Gx_3$	$10^{-2}$	1	1	1.03	1.06	2.03
13	$-Gx_1 + 1.5Gx_2$	$-Gx_2$	$2Gx_3$	$10^{-2}$	1	1.00	1	1.01	2.34
14a	$Gx_3$	0	0	$10^{-2}$	0.99	1	1.00	1.03	4.14
14b	$Gx_3$	0	0	$10^{-2}$	1	1	1.00	1.02	3.90

Table 1: Flows used, and the resulting error computation in computing the second-order orientation tensor  $A$ .

Closure	CPU Time	Normalized Time
Hybrid - Original	25	1
Hybrid - Optimized	6.9	0.3
ORT - Original	770	31
ORT - Optimized	21	0.8
FEC	26	1.0

Table 2: Normalized Computational Times

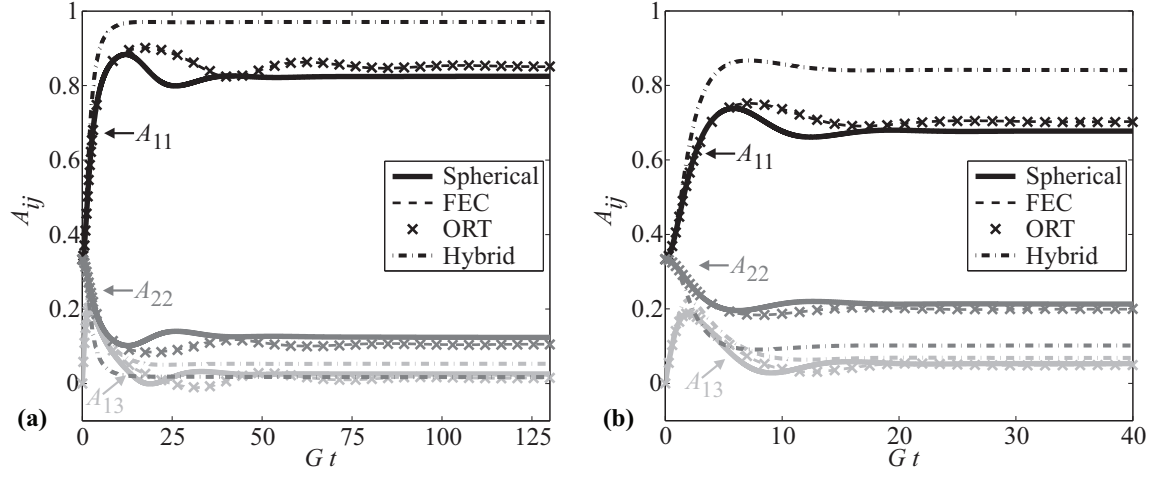


Figure 1: Transient Solution for selected components of  $A$  for simple shear flow under isotropic diffusion (a)  $C_I = 10^{-3}$  and  $\lambda = 0.99$  and (b)  $C_I = 10^{-2}$  and  $\lambda = 0.95$ .

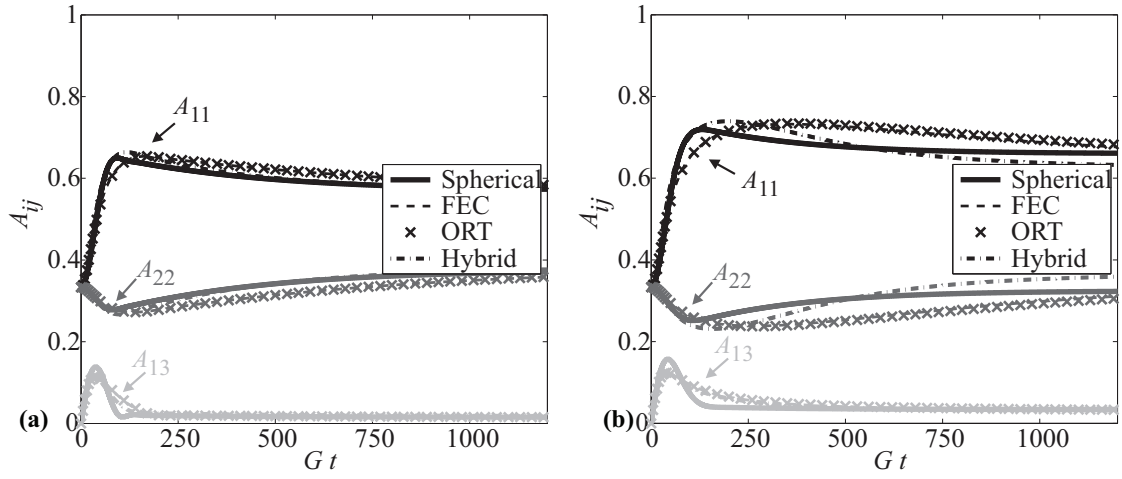


Figure 2: Transient Solution for selected components of  $A$  for simple shear flow under anisotropic rotary diffusion (ARD-RSC) (a)  $\kappa = 1/30$  and  $\lambda = 0.95$  and (b)  $\kappa = 1/30$  and  $\lambda = 1.0$ .

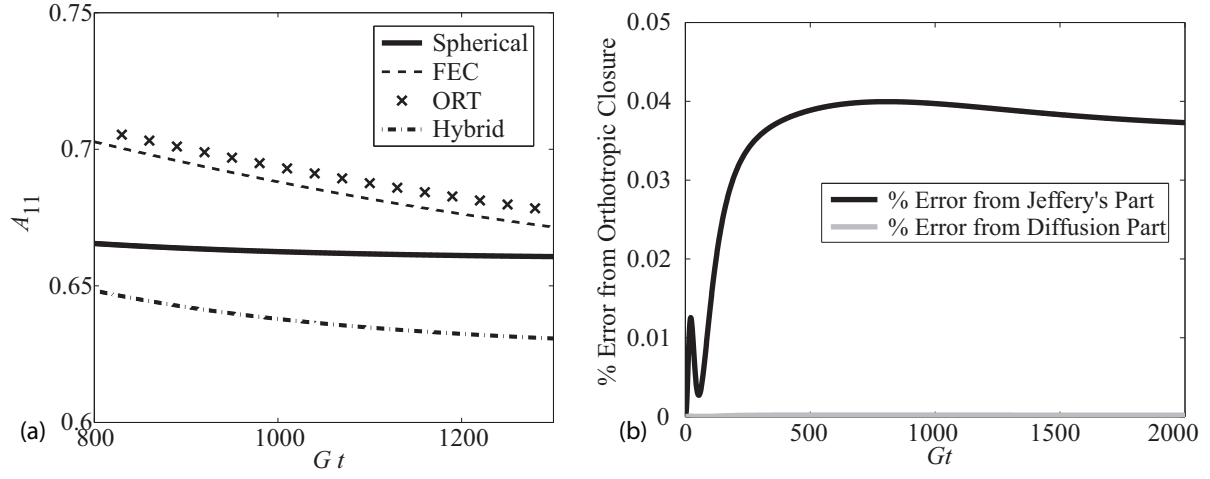


Figure 3: Anisotropic rotary diffusion results, simple shear  $\kappa = 1/30$  and  $\lambda = 1.0$  (a) Selected time range of for  $A_{11}$  (b) Transient error in derivative computation for the fitted orthotropic closure ORT compared to FEC.

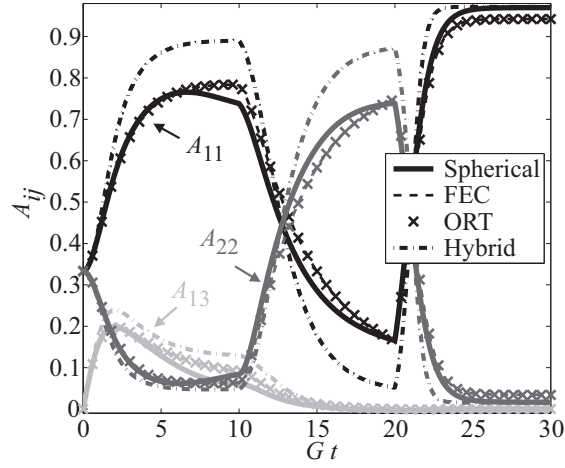


Figure 4: Transient solution for selected components of  $A$  for mixed flow from the Folgar-Tucker model with  $C_I = 10^{-2}$  and  $\lambda = 1.0$ .



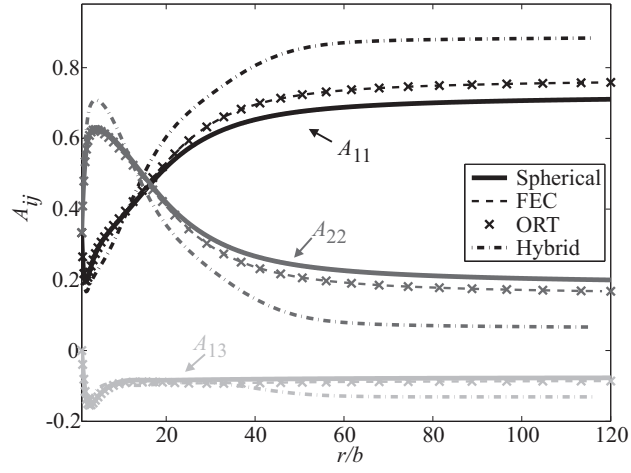


Figure 5: Transient solution for selected components of  $A$  for center-gated disk flow from the Folgar-Tucker model with  $C_I = 10^{-2}$  and  $\lambda = 1.0$  for  $r/b = 4/10$ .