

Sizing of d.c. traction circuit

Goals and constraints

Calculation of voltage drops

Thermal calculation

Selectivity of the protections

Electrical standards

Sizing of d.c. traction circuit

Goals and constraints

Calculation of voltage drops

Thermal calculation

Selectivity of the protections

Electrical standards

Goals

- **Number and Positioning of TPSSs;**
- **Number and Size of Transformer Rectifier Groups;**
- **Wire Section of traction line;**
- **Number and pk of parallel points.**

Design constraints and verifications

Design constraints

1. **Maximum voltage drops,**
2. **Maximum current density**
3. **Transformer overload limit.**

Other Verifications

- **Selectivity of protections**
- constraints 1), 2) and 3) also in case of out of order of a single TPSS.

Design Constraints: Voltage Drop Limits

- IEC 850: measured voltage on pantograph

Type of traction	V_{\min}	V_n	V_{\max}
D.C.	500	750	900
D.C.	1000	1500	1800
D.C.	2000	3000	3600
A.C. 16 2/3 HZ	12000	15000	17250
A.C. 50 HZ	19000	25000	27500

Total Voltage Drop: Grid + TPSS + contact line + return circuit line

Design Constraints: Current Density

- **Current Density: $J < 4 \text{ A/mm}^2$**
- Electrical limit for copper wire: **$T_{\text{max}} = 85^\circ \text{ C}$**

$T_{\text{max}} = 45^\circ \text{ C}$ (environmental conditions) + **40° C** (maximum increase of temperature because of electric load)

Design Constraints: TPSS Power

Transformer Overload:

- **Overload for 2 hours**
- **Overload for 5 minutes**

Other verifications: selectivity of protections

$$I_{SC}^{MIN} > I_{LOAD}^{MAX}$$

- I_{SC}^{MIN} minimum short circuit current
- I_{LOAD}^{MAX} maximum load current

Sizing of d.c. traction circuit

Goals and constraints

Calculation of voltage drops

Thermal calculation

Selectivity of the protections

Electrical standards

Calculation of TPSS Voltage Drops



Open-Circuit: $V_u = 3.400 \text{ V}$

On load: total voltage drops = transformer voltage drops ($>$) + rectifier voltage drops ($<$)

- Silicon rectifiers 3.600 kW:

$$V_{sc}^{\text{trasf}} = 0.07 \text{ pu} \rightarrow \text{Voltage drop}_{\text{tot}} < 8\%$$

Calculation of voltage drops on contact line – simplified hypotheses

- Constant voltage at the exit of the TPSS
- Absorbed current from train: constant and independent from the voltage value

Contact line resistance

$$R_l = \frac{18,8}{s} \times l(\text{Ohm})$$

18,8 Ω mm² / km (copper resistivity)

Rail resistance

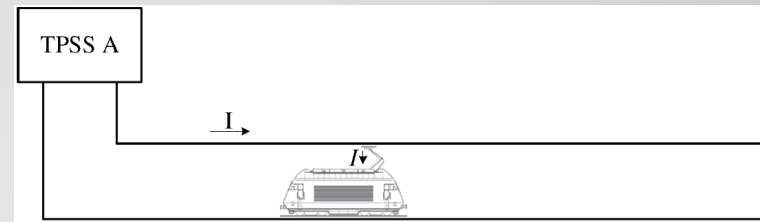
$$R_b = \frac{1}{2p} \times L(\text{Ohm})$$

p = mass per linear meter of rail

Calculation of voltage drops on contact line – case study

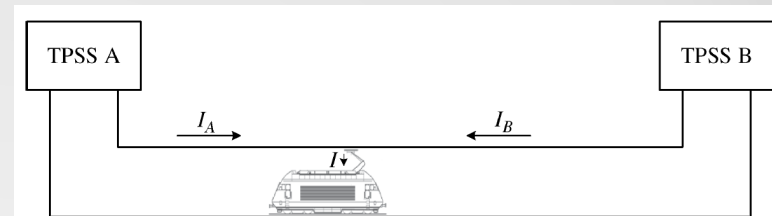
- UNILATERAL POWER SUPPLY

- 1 TRAIN
- 2 TRAINS
- Uniformly Distributed Load

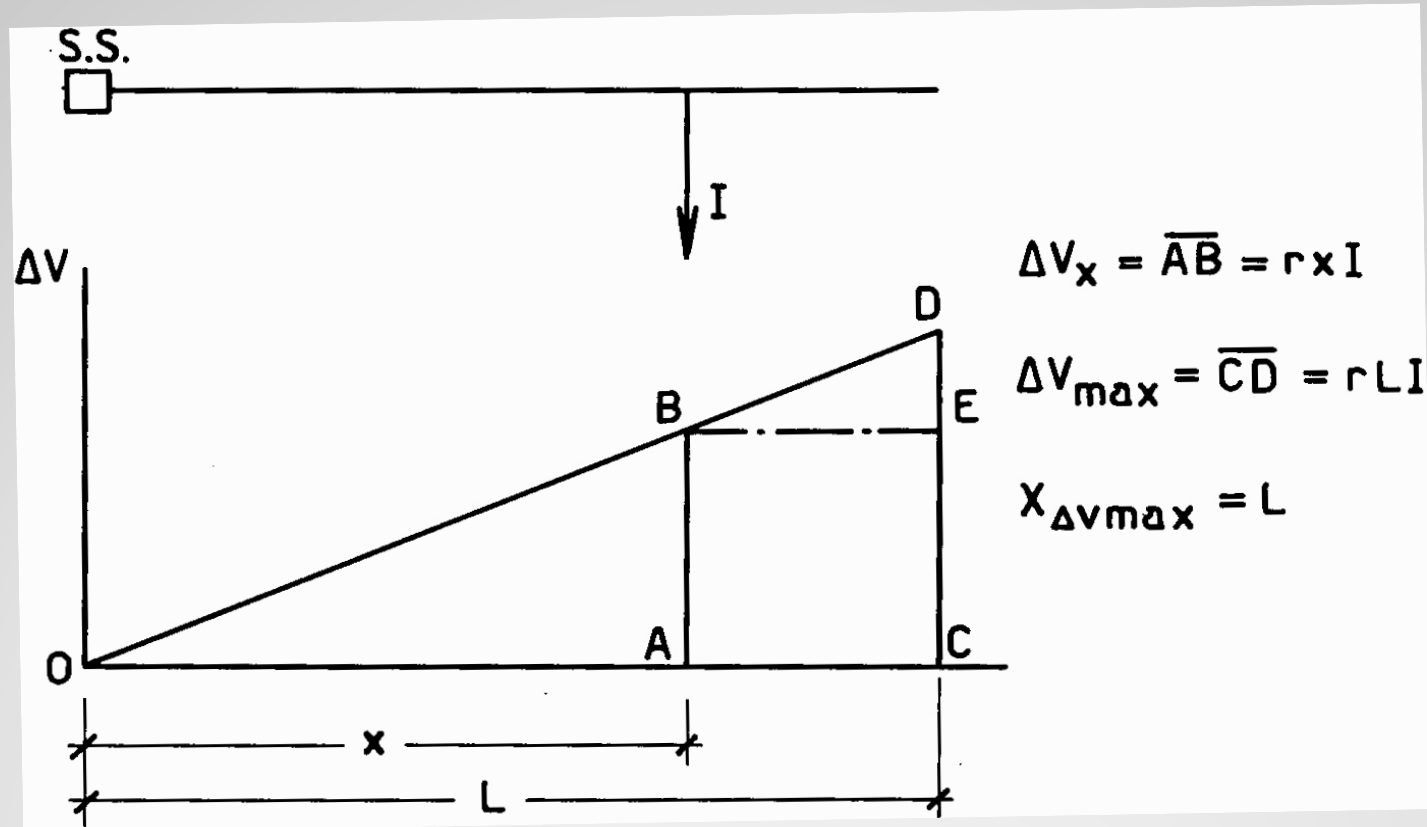


- BILATERAL POWER SUPPLY

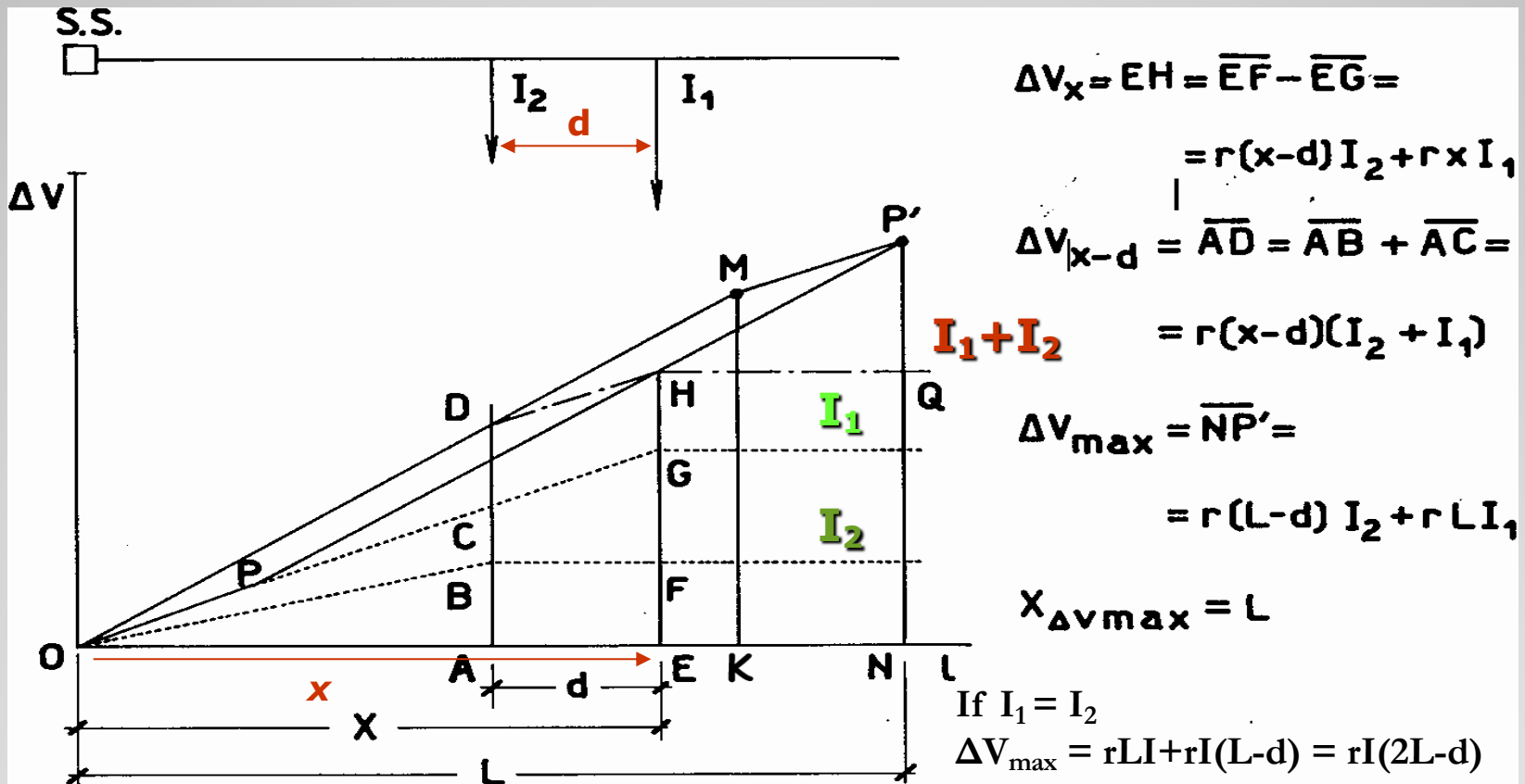
- 1 TRAIN
- 2 TRAINS
- Uniformly Distributed Load



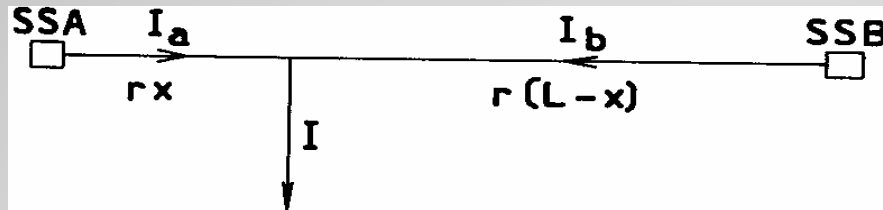
Calculation of voltage drops on contact line : unilateral power supply



Calculation of voltage drops on contact line : unilateral power supply

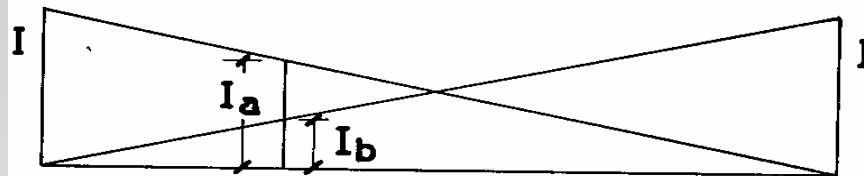


Calculation of voltage drops on contact line : bilateral power supply



$$I_a + I_b = I$$

$$rx I_a = r(L-x) I_b$$



$$I_a = \frac{L-x}{L} I$$

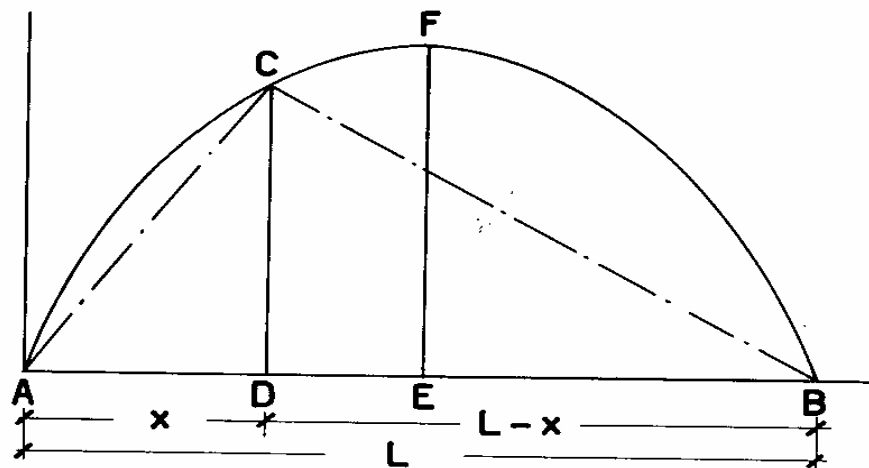
$$I_b = \frac{x}{L} I$$

$$\Delta V_x = \overline{CD} = rx I_a = r(L-x) I_b =$$

$$= r \frac{x(L-x)}{L} I$$

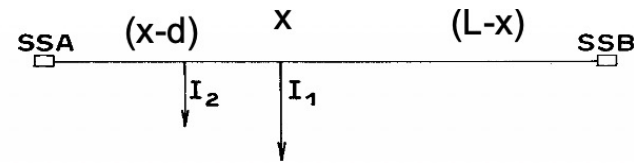
$$\Delta V_{\max} = \overline{EF} = \frac{r L I}{4}$$

$$x_{\Delta v \max} = \frac{1}{2} L$$



Maximum voltage drop of 25% of bilateral power supply

Calculation of voltage drops on contact line : bilateral power supply



$$I_1 = I_{1a} + I_{1b} ; \quad r x I_{1a} = r(L-x) I_{1b}$$

$$I_{1a} = [(L-x) / L] I_1 \rightarrow I_{1a} = I_1 \text{ se } x = 0 \\ = 0 \text{ se } x = L$$

$$I_{1b} = (x / L) I_1 \rightarrow I_{1b} = I_1 \text{ se } x = L \\ = 0 \text{ se } x = 0$$

$$\Delta V_x = r x I_{1a} = r x (L-x) / L I_1$$

$$\Delta V_{x-d} = r(x-d) I_{1a} = r(x-d) [(L-x)/L] I_1$$

$$I_2 = I_{2a} + I_{2b} ; \quad r(x-d) I_{2a} = r(L-x+d) I_{2b}$$

$$I_{2a} = [(L-x+d) / L] I_2$$

$$I_{2b} = (x-d) / L I_2$$

$$\Delta V_{x-d} = r(x-d) I_{2a} = r(x-d) (L-x+d)/L I_2$$

$$\Delta V_x = r(L-x) I_{2b} = r(L-x) [(x-d)/L] I_2$$

$$\Delta V_x = r x (L-x) / L I_1 + r (L-x) [(x-d)/L] I_2 = \frac{r(L-x)}{L} [x I_1 + (x-d) I_2]$$

$$\Delta V_{x-d} = r(x-d) [(L-x)/L] I_1 + r(x-d) (L-x+d)/L I_2 = \frac{r(x-d)}{L} [(L-x) I_1 + (L-x+d) I_2]$$

Calculation of voltage drops : parameters

- **Voltage level:** 3 kV o 1.5 kV (in Italy)
- **Wire section:** equivalent section= (contact line number* contact line section*0,7) + (messenger wire number * messenger wire section) + (reinforcement feeder number * reinforcement feeder section)
- **Distance between TPSSs**

Sizing of d.c. traction circuit

Goals and constraints

Calculation of voltage drops

Thermal calculation

Selectivity of the protections

Electrical standards

Thermal Calculation - limits

Current density: $J < 4 \text{ A/mm}^2$



For copper wire: $T_{\text{max}} = 85^\circ \text{ C}$

Thermal Calculation - limits

- Time constant of about 10' with a density current of 4 A/mm² , increase of temperature of 40° C in 30 '
- Time constant of about 7' with interruption of current, temperature lowering of 40° C in 20 '

Sizing of d.c. traction circuit

Goals and constraints

Calculation of voltage drops

Thermal calculation

Selectivity of the protections

Electrical standards

Selectivity of the protections

The following condition needs to be verified on each feeder:

$$I_{SC}^{MIN} > I_{LOAD}^{MAX}$$

$$I_{SC}^{MIN} = V_{do_{min}} / (R_{PTSS} + (r * L) + R_g)$$

$V_{do_{min}}$ open-circuit minimum voltage;

r kilometric resistance of the line at maximum temperature;

L distance between PTSSs;

R_{sse} maximum internal resistance of TPSSs;

R_g fault resistance;

Selectivity of the protections

Other protections: relays conditioned to the gradient, Minimum Voltage relays or Maximum Nondirectional Line Current relays, pilot wire

If distance between PTSSs is 40 km:

$R = 40 \times 0.08 \, \Omega/\text{km} = 3,2 \, \Omega/\text{km} \Rightarrow I = V/R = 3400/3,2 \approx 1000 \, \text{A} \approx \text{operating current}$

$$\frac{\Delta V'}{V} = \frac{r' L' I'_{max}}{4V} = 0,2$$

$$I'_{sc} = \frac{V}{r' L'}$$

$$\frac{\Delta V''}{V} = \frac{r'' L'' I''}{4V} = 0,1$$

$$I''_{sc} = \frac{V}{r'' L''}$$

$$\frac{I'_{max}}{I'_{sc}} = 0,8$$

$$\frac{I''_{max}}{I''_{sc}} = 0,4$$

Sizing of d.c. traction circuit

Goals and constraints

Calculation of voltage drops

Thermal calculation

Selectivity of the protections

Electrical standards

RFI Electrical standard- contact line

Traction Circuit

Catenary of 540mm² per direction

- 2 Messenger wires of 120 mm²
- 2 Contact lines of 150 mm²

- **Reinforcement feeder (1 conductor or 2):** **100 mm²**
150 mm²

RFI Electrical standard– TPSS

5.4 MVA Group:

- Nominal Power 5,4 MVA
- Open-circuit Voltage 3,6 kV
- Internal resistance 0,13 Ω
- Overload 100% for 2h - 133% for 5 min

RFI Electrical standard

- **Standard:**
- $L = 16 \text{ km}$
- $S = 540 \text{ mm}^2 (2 \times 150 \text{ mm}^2 + 2 \times 120 \text{ mm}^2)$
- $P_{\text{TPSS}} = 2 \times 5.400 \text{ kW}$ (overload: 100 % for 2h – 133 % for 5')