Example

A 3-phase, 415V, 50Hz, 4-pole, star-connected induction motor has the following per-phase equivalent circuit parameters: stator impedance Z_1 =(0+j0.8) Ω , referred rotor impedance Z'_2 =(0.2+j0.8) Ω and magnetising impedance Z_m =(0+j40) Ω .

- (a) Using the exact equivalent circuit, calculate the torque when the slip is 0.05;
- (b) Calculate the torque for the same slip using the approximate equivalent circuit where the magnetising branch is transferred to the supply terminals. Compare this value with the one calculated in (a).

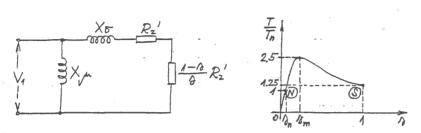
(a)
$$\int_{0.8[\pi]} \int_{0.8[\pi]} \int_{0.8[\pi]} \int_{0.2[\pi]} \int_{0.05} \int_{0.05$$

(b)
$$X_{61}=0.852$$
 $X_{62}=0.8$ $\frac{R_2}{\delta}=0.2$ $\frac{1}{\delta}$ $\frac{1}{2}=\frac{V_{ph}}{V_{R_2}^{-1/2}+X_6^2}=\frac{V_{ph}}{V_{R_2}^{-1/2}+X_6^2}=\frac{V_{ph}}{V_{R_2}^{-1/2}+(6X_6)^2}$ $T=\frac{3I_2^{1/2}R_2^{1/2}}{I_2^2}=\frac{3V_{ph}}{I_2^2}\times\frac{0.05\times0.2}{I_2^2+(0.05\times1.6)^2}=1097\times\frac{1}{4.64}=236.4 [Nm]$ The percentage difference: $I_{60}-I_{60}I_{60}=1097$ $I_{60}I_{60}=1097$ $I_{60}I_{60}$

Example

A 3-phase, 50 Hz, 4-pole induction motor can be represented by simplified equivalent circuit where the stator and mechanical losses are neglected, and the magnetizing reactance is transferred to the supply terminals. The motor has the maximum / rated torque ratio $T_m/T_n = 2.5$ and the starting / rated torque ratio $T_{st}/T_n = 1.25$.

Calculate the slip in the steady-state operation when the motor is loaded with rated torque.



Based on approximate equivalent circuit, Kloss' equations applied at points N and S of torque/speed curve, respectively, are

$$\frac{T_m}{T_n} = \frac{\frac{A_m}{A_m} + \frac{A_m}{A_m}}{2} \qquad (N)$$

$$\frac{T_m}{T_{S\delta}} = \frac{\frac{\delta m}{1} + \frac{1}{\delta m}}{2} \qquad (S)$$

Im is given, and knowing Tse the ratio In Im can be found as

$$\frac{T_m}{T_{st}} = \frac{\frac{T_m}{T_n}}{\frac{T_{st}}{T_{st}}} = \frac{2.5}{1.25} = 2$$

Hence

$$\frac{\delta_m + \delta_n}{\delta_n} = 2.5 \implies \frac{\delta_m + \delta_n}{\delta_n} = 5 \qquad (1)$$

$$\frac{\partial_m + \frac{1}{\partial_m}}{2} = 2 \implies \partial_m + \frac{1}{\partial_m} = 4 \qquad (2)$$

From (2) $\partial_m^2 - 4 \partial_m + 1 = 0 \Rightarrow (\partial_m)_{1,2} = 2 \pm \sqrt{4-1}$ $\partial_m = 0.267$ (The value $\partial_m = 3.73$ is not acceptable, since machine operates as a motor.)

Substituing this value for 8m into (1) gives

$$\frac{0.267}{A_n} + \frac{A_n}{0.267} = 5$$

i.e. $\Delta_n^2 - 1.335 N_n + 0.0713 = 0 \implies \Delta_n = \frac{4.335 \pm \sqrt{1.335^2 + 4 \times 0.0713}}{2}$

 $A_n = 0.0557$ (The value $A_n = 1.279$ is not acceptable as the machine operates as motor and hence $0 < A_n < A_n$)

Example

A 3-phase, 415V, 50Hz, 4-pole delta-connected cage induction motor has the rated speed of 1425rev/min at full (rated) load. The starting current is six times larger than the rated current.

(Assume that the motor can be represented by an approximate per-phase equivalent circuit in which the magnetising branch is transferred to the supply terminals and the only significant loss is in the rotor cage.)

Determine:

- (a) the starting torque developed by the motor as percentage of the full (rated) load torque;
- (b) the per unit slip and speed in rev/min at which the motor develops max (stall) torque;
- (c) the motor maximum (stall) torque as percentage of the full (rated) load torque.

a) The synchronous speed is

$$N_0 = \frac{601}{H} = \frac{60.50}{4/2} = 1500 \left[\frac{res}{main}\right]$$

The full local slip is

$$A_n = \frac{1500 - 1425}{1500} = 0.05$$

The relationship between targue, rator current and slip

$$T = \frac{P_0}{L_0} = \frac{P_0 u_2}{L_0} \left[\frac{3 L_0^2 R_0}{R_0} - \frac{R_0}{R_0} \right]$$

At starting: $A_{st} = 1$ and $A_{st} = \frac{3 L_0 l_0}{R_0} R_0$.

At starting: $A_{st} = 1$ and $A_{st} = \frac{3 L_0 l_0}{R_0} R_0$.

Hence,
$$\frac{I_{st}}{I_n} = \left(\frac{I_{2(st)}}{I_{2(n)}}\right)^2 0.05$$

$$T_{st} = 6^2 0.05 \cdot T_n = 1.8 T_n$$

b) From kloss' equation

$$\frac{T_{st}}{T_m} = \frac{2}{\frac{R_m}{I_0} + \frac{1}{R_m}} \qquad \text{where } I_m \text{ is mex targue and } I_m \text{ the corresponding (critical) slip}}$$

and
$$\frac{T_n}{I_m} = \frac{2}{\frac{R_m}{I_m} + \frac{1}{R_m}} \qquad \text{where } I_m \text{ is mex targue and } I_m \text{ the corresponding } I_m \text{ the } I_$$