Someone, Signals and Systems

#### 1 Modulation Sinusoidal Amplitude Modulation

Synchronous Demodulation:

 $y(t) = \cos(\omega_c t) x(t)$ 

 $c'(t) = cos(\omega_c t + \Delta \omega t + \phi)$  (local carrier)

Have Fun!

 $x_r(t) = x(t)\cos(\Delta\omega t + \phi)$ Asynchronous Demodulation:

 $y(t) = cos(\omega_c t)[x(t) + A]$ , A + x(t) > 0

no DC component 
$$\rightarrow \eta = \frac{E(x^2(t))}{E(x^2(t)) + A^2}$$
  
 $\frac{1}{1 + PAPR_x}$ 

# Quadrature Modulation

$$y(t) = x_I(t)cos(\omega_c t) - x_Q(t)sin(\omega_c t)$$

$$y(t)cos(\omega_c t + \phi) \rightarrow LPF(Gain = 2) \rightarrow$$

$$x_I(t)cos(\phi) + x_Q(t)sin(\phi)$$

$$-y(t)sin(\omega_c t) \rightarrow LPF \rightarrow x_Q(t)$$

#### Single-Sideband Modulation

$$x(t) = x_I(t)$$

$$H_h(j\omega) = \begin{cases} -j, & \omega > 0\\ j, & \omega < 0 \end{cases}$$

 $y_{USB}(t) \rightarrow X_O(j\omega) = X(j\omega)H_h(j\omega)$ , note the  $\omega_{c0}$  of LPF  $y_{SSB}(t) \rightarrow X_Q(j\omega) = -X(j\omega)H_h(j\omega)$ 

spectrum efficiency:  $SSB = QM = 2 \times AM$ Pulse-Amplitude Modulated Signals

 $y(t) = \sum x(nT)p(t-nT), p(t) = Sa(\frac{\pi t}{T}) + p_1(t)$ 

$$P_1(j\omega)$$
 is real,  $\omega_M=\pm \frac{2\pi}{T}$ , even, odd around  $\frac{\pi}{T}(\text{ISI-free})$   
Frequency Modulation

$$y(t) = cos(\omega_c t + \theta_c(t))$$

$$\frac{\mathrm{d}\theta_c(t)}{\mathrm{d}t} = k_f x(t), x(t) = A\cos(\omega_m t)$$

$$m_f = \frac{k_f A}{\omega_m}, y(t) = cos(\omega_c t + m_f sin(\omega_m t))$$
NB:  $m_f << \frac{\pi}{2}$ 

$$y(t) \approx \cos(\omega_c t) - m_f (\sin(\omega_m t))(\sin(\omega_c t))$$

$$= \cos(\omega_c t) + 0.5 m_f \cos(\omega_c t + \omega_m t) - 0.5 m_f \cos(\omega_c t + \omega_m t)$$

$$0.5m_f cos(\omega_c t - \omega_m t)$$
 WM:

### Multiplexing and Multiple Access

## 2 Laplace Transform

 $X(s) = \int_{-\infty}^{\infty} x(t)e^{-st} dt$ 

## Unilateral: ∫₀∞

### Properties

Reduced rational fraction  $X(s) = \frac{N(s)}{D(s)}$  (When

 $s = \infty$  is zero or pole) ROC

# Right sided: $(\sigma \in ROC) \rightarrow (\Re \varepsilon s > \sigma \subseteq ROC)$

Left sided:  $(\sigma \in ROC) \rightarrow (\Re s < \sigma \subseteq ROC)$ Two sided:  $\sigma_1 < \Re s < \sigma_2$ 

Bounded by poles or  $\infty$ , no poles contained in

$$X(s) = \mathcal{F}\{x(t)e^{-\sigma t}\} \to x(t) = \frac{1}{2\pi i} \int_{\sigma - j\infty}^{\sigma + j\infty} X(s)e^{st} dt$$

$$\frac{2\pi i}{2\pi i} \int_{\sigma - j\infty}^{\sigma - j\infty} X(s)e^{st} dt$$

$$= \frac{e^{\sigma t}}{2\pi} \int_{-\infty}^{+\infty} X(\sigma + j\omega)e^{j\omega t} d\omega \text{ (when } \Re s = \sigma \text{ in }$$

ROC)
$$\mathcal{L}^{-1}\{s^n\} = u_n(t), all \ s$$

$$\mathcal{L}^{-1}\left\{\frac{1}{(s+a)^n}\right\} = \begin{cases} \frac{-t^{n-1}}{(n-1)!}e^{-at}u(-t), & \Re\varepsilon s < -a\\ \frac{t^{n-1}}{(n-1)!}e^{-at}u(t), & \Re\varepsilon s > -a \end{cases}$$
Properties(ROC)

## $X_1(s) = \mathcal{L}\{x_1(t)\}, ROC = R_1$

$$X_{2}(s) = \mathcal{L}\{x_{2}(t)\}, \text{ROC} = R_{2}$$

$$aX_{1}(s) + bX_{2}(s) = \mathcal{L}\{ax_{1}(t) + bx_{2}(t)\}, \text{ROC} \supseteq$$

$$R_{1} \cap R_{2} (R_{1} \cap R_{2} = \emptyset \rightarrow \text{ROC} = \emptyset)$$

$$X_{1}^{*}(s^{*}) = \mathcal{L}\{x_{1}^{*}(t)\}, \text{ROC} = R_{1}$$

$$e^{-s\tau}X_{1}(s) = \mathcal{L}\{x_{1}(t-\tau)\}, \text{ROC} = R_{1}$$

$$X_1(s) = \mathcal{L}\{x_1(t)e^{\tau t}\}, \text{ROC} = R_1 + \Re c \tau$$

$$\frac{1}{|a|}X_1(\frac{s}{a}) = \mathcal{L}\{x_1(at)\}, \text{ROC} = aR_1 = \{s|\frac{s}{a} \in R_1\}$$

$$X_1(s)X_2(s) = \mathcal{L}\{x_1(t) * x_2(t)\}, \text{ROC} \supseteq R_1 \cap R_2$$
(This equality may not hold if  $R_1 \cap R_2 = \emptyset$ )
$$sX(s) = \mathcal{L}\{x'(t)\}, \text{ROC} \supseteq R_1, X'(s) = \emptyset$$

 $\mathcal{L}\{-tx(t)\}, ROC = R_1$ 

$$\mathcal{L}\{\cos(\omega_0 t)u(t)\} = \frac{s}{s^2 + \omega_0^2}, \mathcal{L}\{\sin(\omega_0 t)u(t)\} = \frac{\omega_0}{s^2 + \omega_0^2}$$

 $\frac{1}{s}X(s) = \mathcal{L}\{\int_{-\infty}^{t} x(\tau)d\tau\}, ROC \supseteq (R \cap (\Re\varepsilon s > 0))$ 

#### **Analysis**

Casual  $\rightarrow$  ROC = right-half plane  $Casual(Rational) \leftrightarrow ROC = right-half plane$ LTI Stability  $\leftrightarrow j\omega$  – axis  $\subseteq$  ROC Casual Stability  $\leftrightarrow$  all poles have negative real part

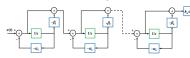
#### **Block Diagram**

Direct: 
$$H(s) = \frac{\sum b_i s^i}{\sum a_i s^i}$$
, 
$$b_s \qquad b_{s_1} \qquad b_{s_2} \qquad b_1 \qquad b_1$$

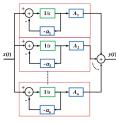
$$a_{s_1} \qquad b_{s_2} \qquad b_1 \qquad b_2$$

$$a_{s_1} \qquad a_{s_2} \qquad a_1 \qquad a_0$$

Parrallel: 
$$H(s) = A \frac{\prod s - \alpha_i}{\prod s - \beta_i}$$



Cascade:  $H(s) = \sum_{s=a}^{A_i} \frac{A_i}{s-a}$ 



#### **Unilateral Laplace**

#### 3 z Transform $X(z) = \sum_{n=-\infty}^{+\infty} x[n]z^{-n}, z = e^s$ : $\Re \varepsilon s = \sigma \to |z| =$

#### Examples

$$\mathcal{Z}\{\cos(\omega_0 n)u[n]\} = \frac{1 - z^{-1}cos\omega_0}{1 - 2z^{-1}cos\omega_0 + z^{-2}}$$
$$\mathcal{Z}\{\sin(\omega_0 n)u[n]\} = \frac{z^{-1}sin\omega_0}{1 - 2z^{-1}cos\omega_0 + z^{-2}}$$

## inverse z-Transform

## $x[n] = \frac{1}{2\pi i} \oint X(z) z^{n-1} dz$

#### 4 PID **Linear Feedback**

Forward H(s), Feedback G(s) (z when dis-

$$Q(s) = \frac{Y(s)}{X(s)} = \frac{H(s)}{1 + H(s)G(s)}$$

Open loop transfer:  $\frac{R(s)}{E(s)} = H(s)G(s)$ 

Error transfer:  $\frac{E(s)}{X(s)} = \frac{1}{1+H(s)G(s)}$ 

Compensation: (forward  $H(j\omega)$ , backward K),

 $Q(s) \approx \frac{1}{K}$ , (approx irrelevant to H)  $Gain \times BW \equiv Constant$ 

#### **PID Control**

$$x(t) \xrightarrow{+} \underbrace{+}_{O} \underbrace{+}_{O} \underbrace{+}_{O} \underbrace{+}_{H_{c}(s)} \underbrace{+}_{U} \underbrace{+}_{U} \underbrace{+}_{H_{p}(s)} \underbrace{+}_{U} \underbrace{+}$$

$$E(s) = \frac{X(s)}{1+H_0(s)} - \frac{H_p(s)}{1+H_0(s)}I(s) - \frac{H_0(s)}{1+H_0(s)}D(s)$$

$$Y(s) = \frac{H_0X(s)}{1+H_0(s)} + \frac{H_p(s)}{1+H_0(s)}I(s) + \frac{H_0(s)}{1+H_0(s)}D(s)$$

Error transfer: $H_{e}(s) = \frac{1}{1+H_{e}(s)}$ , close loop:

$$H(s) = \frac{H_o(s)}{1 + H_o(s)}, H(s) + H_e(s) = 1$$

## Steady State Error

Assume the system to be stable system.

$$f(+\infty) = \lim_{s \to 0} sF(s)$$
  
 $x(t) = \frac{t^k}{k!} u(t), X(s) = s^{-(k+1)}$ 

$$e_{ss} = \lim_{s \to 0} sE(s) = \lim_{s \to 0} \frac{s^{-k}}{(1 + H_c(s)H_p(s))}$$
  
type-k system: limited non-zero  $e_{ss}$  for k

type-k system. Inflited flot-zero 
$$\varepsilon_{ss}$$
 for  $k$   $H_p(s) = s^{-m} \hat{H}_p(s), H_c(s) = s^{-n} \hat{H}_c(s), 0 < |\hat{H}_p(s)|, |\hat{H}_c(s)| < \infty$ 

 $e_{SS} = \frac{1}{s^{n+m} + \hat{H}_n(s)\hat{H}_c(s)s^{k-(n+m)}}$ , type- m + n sys tem for tracking x

## Similar analysis for interference suppression I(s), type- n

$$\mathbf{1.}H_c(s) = k_P$$

$$x(t) = u(t)$$

$$H_p(s) = \frac{A}{s+a}, H(s) = \frac{Ak_p}{s+a+Ak_p}, e_{ss} = \frac{a}{a+k_pA}$$

 $k_P$  increase  $\Rightarrow$  faster response, less error  $H_p(s) = \frac{A}{s^2 + a_1 s + a_2}, H(s) = \frac{Akp}{s^2 + a_1 s + a_2} =$ 

$$\frac{Ak_P}{Ak_P + a_2} \frac{\omega^2}{s^2 + 2\zeta_{ws} + \omega^2}, \text{ damped oscillation}$$

$$e_{ss} = \frac{a_2}{a_2 + k_P A} k_P \text{ increase} \Rightarrow \text{damp decrease,}$$

enhance oscillation, less error

$$2.H_c(s) = \frac{k_I}{s}$$

$$H_p(s) = \frac{A}{s+a}, H(s) = \frac{k_I A}{s^2 + as + k_I A}, H_e(s) = \frac{s(s+a)}{s^2 + as + k_I A}$$
  $k_I$  increase  $\Rightarrow$  damping factor decrease to zero  $x(t) = u(t) \rightarrow e_{ss} = 0, x(t) = tu(t) \rightarrow e_{ss} = \frac{a}{k_I A}$ 

$$3.H_c(s) = k_D s$$

Inverse system: 
$$Q(s) = \frac{1}{\frac{1}{H(s)} + G(s)} \approx \frac{1}{G(s)}$$
 (when  $H_p(s) = \frac{A}{s+a}, H(s) = \frac{k_D A s}{(k_D A + 1) s + a}, H(s) = \frac{H_p(s)}{(k_D A + 1) s + a}$ 

$$x(t) = u(t), y(\infty) = 0$$
 (can't track constant error)

$$\mathbf{4.}H_c(s) = k_P + k_D s$$

$$\begin{split} H_p(s) &= \frac{A}{s+a}, H(s) = \frac{(k_P + k_D s)A}{(Ak_D + 1)s + Ak_P + a} \\ x(t) &= u(t), y(\infty) = H(0) = \frac{k_P A}{a + k_P A}, y(0+) = \frac{k_D A}{1 + k_D A} \end{split}$$

5.
$$H_c(s) = k_P + \frac{k_I}{s}$$
 (lower ss error)

$$x(t)=u(t)\rightarrow e(\infty)=0; x(t)=tu(t)\rightarrow e(\infty)=\frac{a}{K_IA}$$

## PLL 5 State-Space Analysis

## CT

$$[q_1(t),...,q_L(t)]^T = q(t)$$

$$\frac{dq(t)}{dt} = Aq(t) + bx(t)$$

$$y(t) = c^T q(t) + dx(t)$$

# Stability

for LTI: Asymptotic Stable(about  $\lambda_i$ )=BIBO

# Modal Coordinates(CT for example)

$$[v_1,...,v_L] = V$$
,  $A$ 's eigenvectors  $q(t) = V r(t)$  evolution:  $b = V \beta$ 

$$\frac{dr_i(t)}{dt} = \lambda_i r_i(t) + \beta_i x(t)$$
output:

$$\xi = V^T c$$
  
 
$$y(t) = \xi^T r(t) + dx(t)$$

Reachability i – th mode is reachable:  $\beta_i \neq 0$ 

Matrix:  $R_L = [A^{L-1}b, ..., b]$  is full rank

## Observability

i-th mode is observable:  $\xi_i \neq 0$ 

Matrix: 
$$O_L = \begin{bmatrix} c^T A \\ c^T A \end{bmatrix}$$
 L re