

# Positron-annihilation lifetime spectroscopy with in-situ control of temperature, pressure and atmosphere to determine the free-volume of soft materials

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## ABSTRACT

We introduce a newly developed instrument for <sup>22</sup>Na-based positron-annihilation lifetime spectroscopy (PALS) with in-situ temperature, pressure and atmosphere control. The system is designed for PALS measurements of samples in changing atmospheric conditions, from vacuum ( $\sim 10^{-5}$  mbar) up to a gas pressure of 20 MPa. Furthermore, we can select the composition of the applied gas, such as N<sub>2</sub>, Ar, Ar/H<sub>2</sub>, CO<sub>2</sub> as well as CH<sub>4</sub> and adjust the sample temperature from room temperature to 200 °C. To test the measurement principle, we carried out PALS measurements on semi-crystalline polystyrene in (99.999 %) pure argon atmosphere varying the pressure and the temperature simultaneously, up to 4 MPa and T = 150 °C. Changing the sample environment in that way affects the free-volume of the polymer, which is reflected in the positron lifetime and intensity.

## 1. Introduction

During the last decades, the development of new polymer and membrane materials for various environmental, energy and medical applications has gained importance [1], e.g. gas-separation [2], carbon capture [3], water purification [4,5] and reverse osmosis [6]. An important property of these polymer materials is the free-volume ( $V_F$ ), i. e. the difference of the macroscopic volume ( $V$ ) and the temperature and pressure independent volume occupied by the polymer molecules ( $V_{occ}$ ). The  $V_F$  consists of free-volume elements (FVEs) that originate from irregular packing in the glassy state (*static* FVEs) or from segmental motion in the rubbery state (*dynamic* FVEs) [7]. Sometimes the fractional free-volume  $V_F/V$ , the ratio between free volume and macroscopic volume, is used to characterize the free-volume in polymers [8].

According to the free-volume theory [8,9], the  $V_F$  is responsible for the transport of atoms or molecules in and through the polymer matrix. Accordingly, the transport mechanisms are strongly governed by the FVEs size and distribution, the size of the penetrating atoms or molecules, as well as their interactions [2,10]. For example, the size of the FVEs in ion-exchange membranes determines the size of the molecules

that can be transported across the membrane [4]. The size of  $V_F$  depends mainly on the thermodynamic state of the system, i.e. temperature and pressure [10], but is also specific for each polymeric system. In the glassy state of polymers, the molecule chains are rigid and the effect of temperature on  $V_F$  is scarce. When reaching the glass transition temperature  $T_g$  the polymer chains begin to soften and the FVEs expansion accelerates with increasing temperature [11]. Softening of polymer chains may also be due to the presence of an atmosphere, e.g. humidity, gases or gas mixtures, and its pressure. The process of softening the polymer chains by a penetrant gas is known as plasticization and is a function of the gas solubility in the polymer and the pressure of the atmosphere [12]. In addition, varying ambient conditions can cause changes in the polymer structure, which leads to a change in the transport of molecules through the polymer matrix [10]. To obtain more insight on the size and abundance of the FVEs, positron-annihilation lifetime spectroscopy (PALS) has been used.

PALS is a reliable, nondestructive analytical method often used for the characterization of FVEs in the range of 1–30 Å [13,14]. With this technique, the lifetime of positrons in matter is determined by measuring the radiation caused by the annihilation of a positron with an

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electron. The positron lifetime is the elapsed time between the implantation of the positron into the material and the detection of at least one gamma emitted by the annihilation. It depends on the electron density at the location of annihilation. Thus, it is characteristic for different materials and their atomistic defects. Consequently, the lifetime of the positron increases when the local electron density decreases, which translates directly to the dimension of the defect.

In most polymers, a bound state of  $e^+$  and  $e^-$  can form, the Positronium (Ps). Positronium exists in two spin states, i.e. *para*-Positronium (p-Ps) with  $s = 0$  and *ortho*-Positronium (o-Ps) with  $s = 1$ , the latter most likely annihilates into three photons in vacuum. While the mean vacuum lifetime of p-Ps is 125 ps and will not change much in matter, the lifetime of o-Ps can be substantially shorter than its vacuum lifetime of 142 ns. In low electron density environments, e.g. polymer materials, o-Ps can annihilate with another surrounding electron that satisfies the selection rule of an  $s = 0$  state, resulting in a process called “pick-off” annihilation, which reduces the o-Ps lifetime to nanoseconds [15–17]. This reduced o-Ps lifetime yields information about size or size distribution of  $V_F$  in polymer materials.

It is well-established that the size of FVEs in polymers usually increases with temperature, which can be observed in the increase of o-Ps lifetime [18–22]. Measurements of various polymer materials show that, for specific gases, the lifetime of o-Ps increases with increasing pressure, but decreases after a certain point [23].

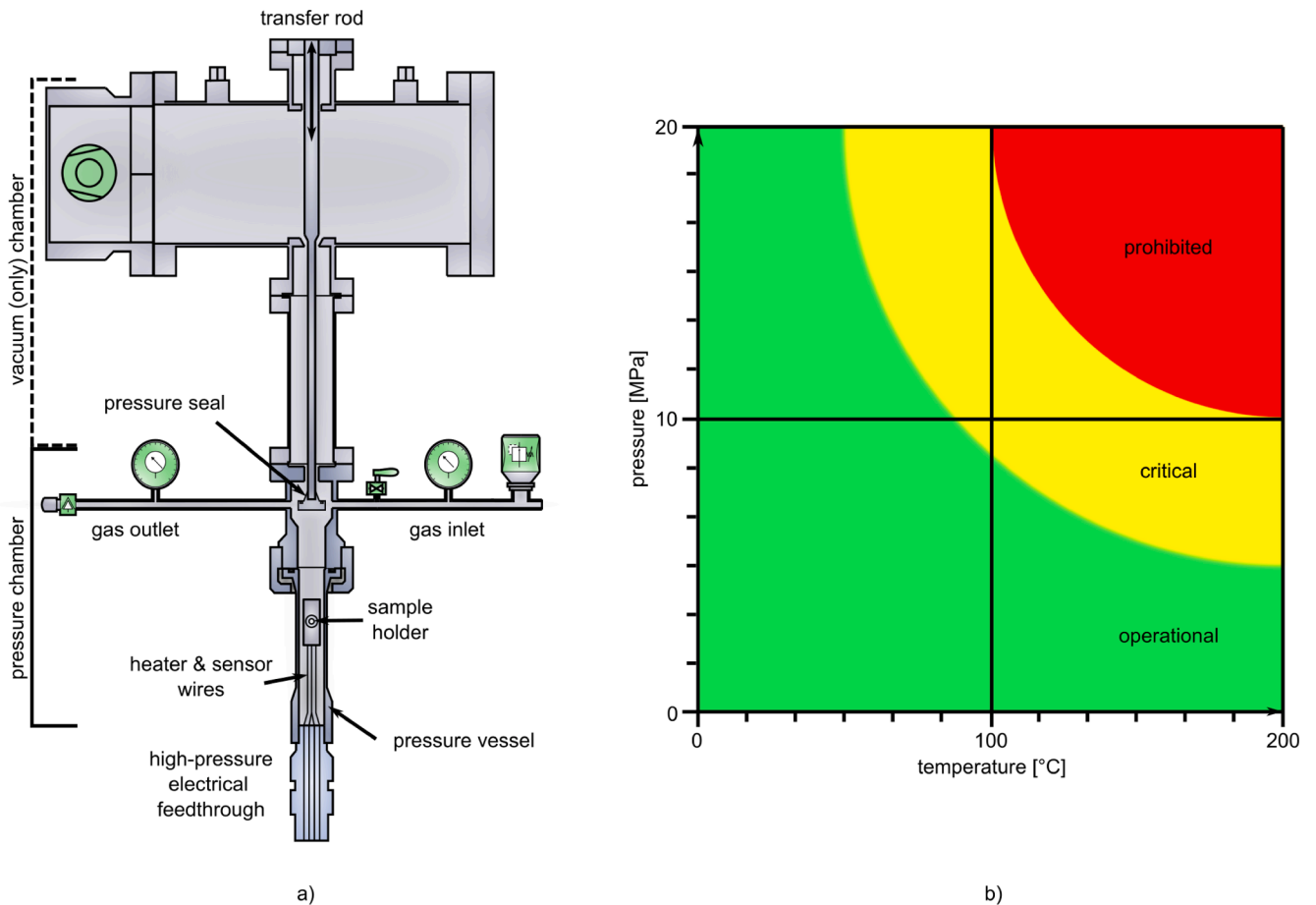
Usually only one of the two parameters (temperature, pressure) is changed during the measurement, while the other technically easy-to-set

conditions (air/vacuum, room temperature) are kept constant. For many polymers, however, these measurement conditions are insufficient to elucidate the material structure-performance relationship under actual operation, such as for pressure-driven membrane applications. Yet, very few studies show the influence of gas pressure or gas species while simultaneously varying temperature on the o-Ps lifetime in polymers and therefore, on the FVEs [23,24]. Here, we introduce a new instrument that is capable of measuring in-situ PALS with independent adjustment of ambient conditions, i.e. temperature, atmosphere and pressure. This instrument exposes the polymer directly to a defined atmosphere and provides information not only on the influence of pressure and temperature, but also on the influence of dissolved gas species on the free-volume of the polymer, resulting in a more realistic experimental environment for polymer materials used in various fields of science and engineering.

## 2. Apparatus

### 2.1. General design

A technical drawing of the instrument is shown in Fig. 1a. The apparatus consists of a vacuum section (top) and a high-pressure section (bottom), that can be mechanically separated from one another. The high-pressure unit can be evacuated and flooded with gas after separation from the vacuum unit. A scroll pump (Edwards nXDS10i) and a turbo pump (Edwards EXT70H) are installed at the vacuum section and the whole system is vacuum tight down to at least  $10^{-5}$  mbar. The



**Fig. 1.** (color, 2-column): a) A sketch of the basic design of the instrument with all important components. The instrument consists of a high-pressure chamber and a vacuum chamber, both can be mechanically separated by closing the pressure seal. The high-pressure chamber, which is also vacuum-tight, includes the gas circuit, the pressure vessel and the high-pressure electrical feedthrough for heating and temperature monitoring. b) Estimation, based on static thermo-mechanical simulations, of the application range of temperature and pressure for the pressure vessel. The green area shows the parameter space that is unproblematic to set. Parameter combinations in the yellow area should be applied with care and the red area is restricted.

vacuum is essentially limited by the components on the pressure side of the unit and the small turbo pump used, but is sufficient for degassing the samples environment.

In the gas control-circuit, the desired gas or gas mixture can be set and introduced to the pressure vessel. The pressure is monitored with two pressure gauges located near the pressure chamber at the gas inlet and outlet, respectively.

For pressure tightness, the pressure chamber must be isolated from the vacuum reservoir. This is realized by sealing the pressure chamber with a pressure seal. The pressure seal consists of a Viton® gasket on a metal disk which presses on a ring welded into the tube right beneath the undermost vacuum flange. It is operated with a transfer rod from the vacuum side of the instrument (see Fig. 1a). The seal is closed in direction of the pressure gradient from high to low pressure and is therefore self-sealing.

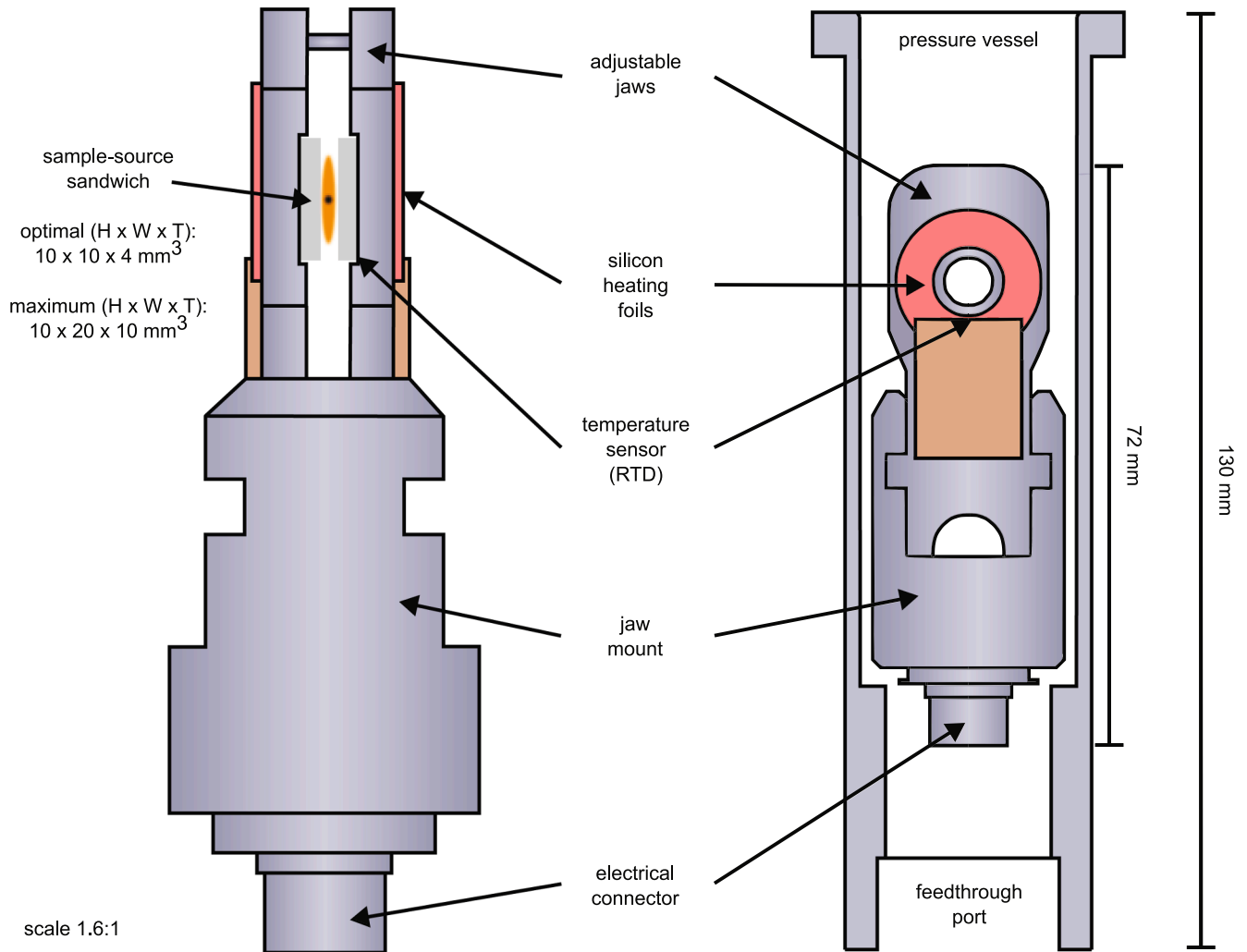
The pressure vessel is designed for up to 20 MPa of gas pressure and temperatures up to 200 °C. Fig. 1b shows a schematic p-T area of application for the instrument. This graph is an estimation based on simulation (Ansys [25], Solidworks [26]) and analytical calculations. The green area shows the pressure-temperature combination that has been extensively tested and is suitable for measurement operation. The yellow area is in principle accessible but has not been fully explored. For

pressure-temperature combinations in the red area, safe operation cannot be guaranteed. Calculations of the yield stress of the pressure vessel for the maximum design values of pressure and temperature yielded a maximum stress of 452 MPa before material failure. A thermo-mechanical simulation showed that the maximum stress in the vessel does not exceed 204 MPa under the conditions marked in green and yellow in Fig. 1b. It should be noted that these calculations are for the static case and do not account for any dynamic stress, which can occur during subsequent pressure-temperature cycles.

## 2.2. Positron source and sample holder

As a positron source, we use  $^{22}\text{Na}$  salt encapsulated in 7  $\mu\text{m}$  thick Kapton® foil with an activity of about 370 kBq (10  $\mu\text{Ci}$ ), which provides sufficient count rates (31 cps) while minimizing background due to false coincidence events. The positron source was provided by the Martin-Luther-University Halle-Wittenberg. When Kapton® is used for the confinement of the  $^{22}\text{Na}$  salt, the maximum allowable temperature must be below 200 °C. The positron source is placed between two identical samples, forming a so-called sample-source sandwich.

In Fig. 2, a detailed description of the sample holder is depicted. The sample holder generally consists of three main components, two jaws



**Fig. 2.** (color, 2-column): Detailed description of the sample holder. On the left side the sample-source sandwich can be seen placed between the two jaws and mounted onto the jaw mount. The jaws not only hold the sample-source sandwich at a defined position but also act as a thermal conductor between the heating foils and the sample. The heating procedure can be controlled by a resistance temperature detector integrated in one of the jaws. On the right side, the position of the sample holder in the pressure vessel is shown. This position is only obtained if the feedthrough is also installed, but for the sake of clarity the feedthrough was omitted.

and a jaw mount. The sample-source sandwich is placed between two jaws, which holds the sample-source sandwich in place and can be adjusted to fit samples with a maximum thickness of 5 mm per sample (10 mm for the sample-source sandwich). Moreover, the jaws serve as the thermal contact between two mounted silicon heating foils and the sample-source sandwich. Isolated from the heating foils a resistance temperature detector (RTD) is embedded in one of the jaws to control the sample temperature during in-situ heat treatment experiments. The two jaws can be attached via screws to each other and kept in place in guide rail to prevent movement of the sample during the experiment. The jaw mount is connected to a high-pressure feedthrough, which allows for electrical contacting from outside the pressure vessel.

### 2.3. Data acquisition

The data acquisition concept of the instrument can be seen in Fig. 3. The ambient parameters, i.e. temperature and pressure, can be monitored through the LabVIEW user interface. The annihilation radiation is detected by two detectors from SCIONIX. The detectors consist of two Hamamatsu R13089-100 photomultipliers (PMT) [27] each mounted with a 25 mm thick encapsulated CeBr<sub>3</sub> scintillator crystal. The detector signals are digitized by the DRS4 evaluation board, a digital oscilloscope developed by the Paul-Scherrer Institute in Switzerland [28], which is already used by other research groups for PALS [29,30]. To evaluate the annihilation events and extract the positron lifetime we use the DDRS4PALS, a software developed for the positron-annihilation lifetime spectroscopy with the DRS4 board that offers a wide variety of digital filters to optimize the quality of the acquired lifetime spectra, e.g. timing

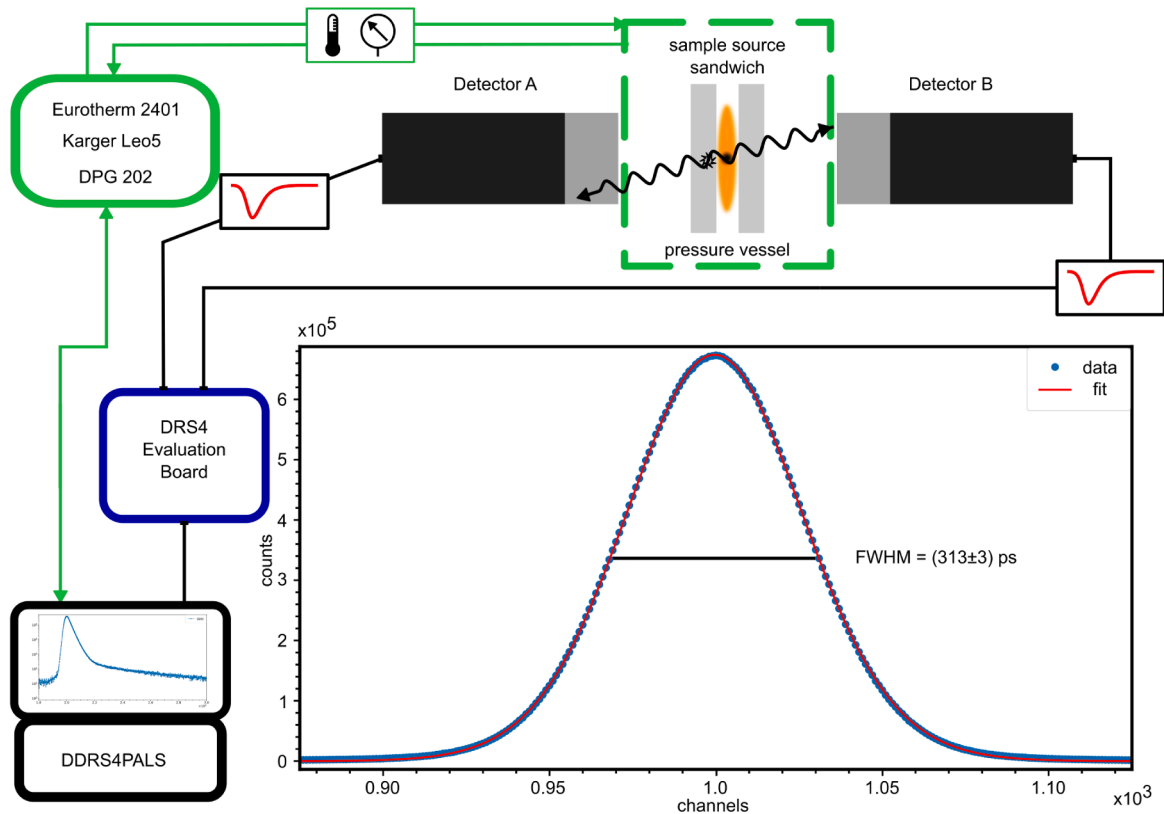
resolution and peak-to-background ratio [31]. For the analysis of positron annihilation lifetime measurements, the knowledge of the timing resolution of the data acquisition is critical. In the lower right corner of Fig. 3, the prompt spectrum for 511 keV gamma events can be seen. Since both 511 keV gamma quanta are measured and they are generated simultaneously, the time difference (width of the spectrum) is only due to the time inaccuracy of the electronics, detectors and scintillators. Fitting of the prompt spectrum yields the time resolution of the system and could be determined to be 313(3) ps (FWHM). Assuming identical characteristics of the photomultipliers, the single detector timing resolution can be approximated to be 221(2) ps (FWHM).

For proper data analysis, a minimum of  $2 \times 10^6$  events/spectrum (17 h) for polymer materials and  $4 \times 10^6$  events/spectrum for metals and semiconductors are required. These values are empirical values and have proven to be sufficient in numerous experiments in the past. To extract the instrument resolution function at each pressure level, a p-type Silicon reference sample with  $4 \times 10^6$  events/spectrum was measured before every measurement series.

Although not addressed in this work, it is generally possible to install different detector systems to measure different parameters of positron annihilation, e.g. the energy distribution of the annihilation radiation, which can be used to measure Doppler Broadening Spectroscopy (DBS) when measured separately, or Age Momentum Correlation (AMOC) when measured simultaneously with positron lifetime [32].

### 2.4. Positron-Lifetime Annihilation Spectroscopy (PALS)

PALS measurements are performed utilizing the positrons from the



**Fig. 3.** (color, 2-column): Schematic of the data acquisition unit. Both gamma events, i.e. start and stop events, are registered by the PMTs. The resulting anode signals (black circuit) are directly delivered to the analogue input of the DRS4 evaluation board [28] and processed by DDRS4PALS software [31]. The ambient parameters (green circuit) are monitored by a LabVIEW user interface. The graph in the lower right corner is a so-called prompt spectrum for 511 keV gamma events. By fitting a gaussian-like function to the data, we can analyse the width (FWHM) of the prompt spectrum, which corresponds to the instrument time resolution of the spectrometer for 511 keV gamma events.

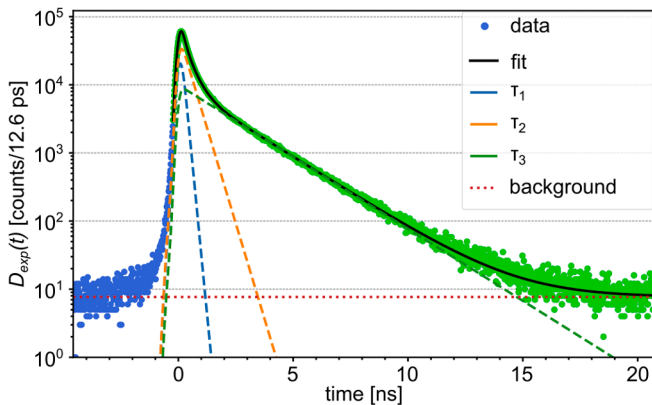
$\beta^+$ -decay of the  $^{22}\text{Na}$  source. The positron emission is directly followed by the emission of a gamma (1.27 MeV) of the daughter nuclei  $^{22}\text{Ne}$ , thus, the detection of this gamma serves as the start of the positron that is directly implanted into the material of interest. The electron-positron annihilation inside the material emits in most cases two 511 keV photons that are used to detect the end of the positron lifetime. Therefore, the lifetime of the positron is evaluated by the time difference of the 1.27 MeV and the 511 keV signals taken in coincidence for each annihilation event. A PALS-spectrum is obtained by collecting the number of annihilation events for each bin of positron lifetimes, resulting in a time-dependent spectrum  $D_{\text{exp}}(t)$  like the one depicted in Fig. 4. The measured distribution is well modelled by a function  $D_{\text{mod}}(t)$ , a sum of exponential functions convoluted with an instrument resolution function  $\text{IRF}(t)$  and superimposed on a background B:

$$D_{\text{mod}}(t) = \text{IRF}(t) * \left( \sum_{i=1}^k \frac{I_i}{\tau_i} \exp\left(-\frac{t}{\tau_i}\right) \right) + B \quad (1)$$

where  $k$  is the number of resolvable exponentials and  $I_i$  the relative intensity of the  $i$ -component in the spectrum.  $\tau_i$  represents the mean decay time that corresponds to the mean lifetime of a subpopulation  $i$  of the positrons that experience a similar electron density in the material.

### 3. Results and discussion

The thermoplastic polystyrene (PS) was the first polymer system for which simultaneous gas pressure and temperature-dependent PALS measurements were performed with the new instrument. The reason for this choice is that the glass transition temperature ( $T_g$ ) of PS is around 97 °C [33] and therefore, is significantly above room temperature and in the middle of the feasible temperature range of the instrument. This means that sufficient temperature points can be collected before and after the  $T_g$  without the necessity of sample cooling below room temperature. Compared to other thermoplasts, e.g. PMMA or PVC, with similar glass transition properties, PS possesses a higher gas diffusion constant  $D(30^\circ\text{C}) = 7.5 \times 10^{-8} \text{ cm}^2 \text{ s}^{-1}$  for the penetrant argon [34,35]. Diffusion in polymer materials is mainly governed by the atomic radius of the penetrating gas species [8,10,34]. Therefore, argon is a suitable penetrant due to its small atomic radius of  $d_{\text{Ar}} = 0.279 \text{ nm}$ , its inert chemical nature and accessibility [35,36]. The PS was purchased from Sigma-Aldrich as a semi-crystalline sheet with a dimension of  $300 \times 300 \text{ mm}^2$  and a thickness of 2 mm. Two  $10 \times 10 \text{ mm}^2$  pieces were cut out of the sheet and the positron source was placed in between the pieces (cfr.



**Fig. 4.** (color, 1-column): Fitted decay spectrum of polystyrene at room temperature and 0.1 MPa argon atmosphere. The raw data points are represented in blue and green: The data points that are included in the fitting process are printed in green, the ones in blue are not considered in the fitting process. Indicated in dashed lines are the exponential components attributed to the different positron lifetimes resulting from the least-square fit of the function from Eq. (1).

sample-source sandwich). The maximum energy of the positrons emitted by the  $^{22}\text{Na}$  source is 0.546 MeV. The implantation of the positron into the material can be described by a power law of the following form [32]:

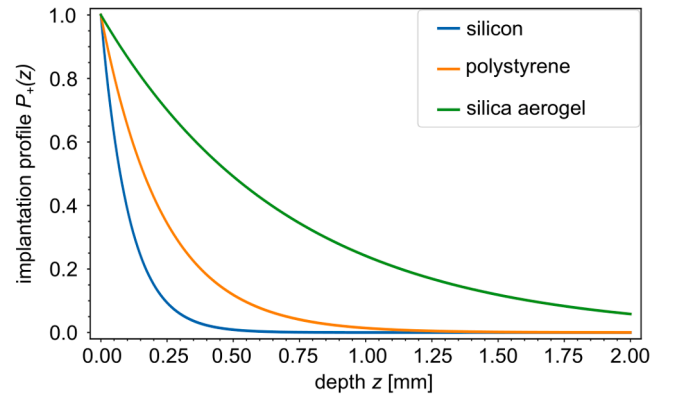
$$P_+(z) = \alpha \exp(-\alpha z), \alpha [\text{cm}^{-1}] = 17 \frac{\rho [\text{g/cm}^3]}{E_{\text{max}}^{1.43} [\text{MeV}]} \quad (2)$$

This implantation profile  $P_+(z)$  in the direction perpendicular to the sample surface is mainly dependent on the density  $\rho$  and the maximum positron energy  $E_{\text{max}}$ . In Fig. 5 the implantation profile from Eq. (2) is shown for silicon ( $\rho = 2.33 \text{ g/cm}^3$ ), PS ( $\rho = 1.05 \text{ g/cm}^3$ ) and silica aerogel ( $\rho = 0.35 \text{ g/cm}^3$ ) for a maximum sample thickness of 2 mm. The maximum penetration depth, i.e. when the implantation profile decreased to zero, changes with the density from 0.5 mm (silicon) to 4 mm (silica gel). The calculation of the implantation profile for PS with a density of  $1.05 \text{ g/cm}^3$  and a maximum positron energy of 0.546 MeV shows that a sample thickness of 2 mm is sufficient to avoid positrons escaping the sample material and annihilation elsewhere. For the pressure measurements, commercially available argon with a purity of more than 99.999 % was used as the penetrant gas.

#### 3.1. Room temperature measurements on polystyrene (PS)

Fig. 4 shows the spectrum of polystyrene at 0.1 MPa argon pressure and room temperature. The blue dots represent the raw data points that are not considered in the data analysis. The green dots show the data points which are used by the fit routine of Eq. (1) (black solid line). The red dotted horizontal line displays the mean background of the spectrum. The evaluated lifetime spectra contain three lifetime components,  $\tau_1 \approx 125$  (fixed) ps (blue dashed line) can be attributed to the annihilation of p-PS, while  $\tau_2 = 388(2)$  ps (orange dashed line) stems from free positrons annihilating directly in the polymer matrix, without forming positronium. The third component  $\tau_3 = 2056(3)$  ns (green dashed line) can be associated with the pick-off annihilation of o-PS close to the walls of the FVEs. All spectra analyzed showed the best results when 3 components were used for the model of Eq. (3). For small FVEs ( $r < 1 \text{ nm}$ ) the Tao-Eldrup model [37,38], based on the assumption of spherical or cylindric FVEs, was used as an approximation between the lifetime  $\tau_3$  and the mean radius of the FVEs:

$$\tau_3 = \frac{1}{2} \left[ 1 - \frac{r}{r + \Delta R} + \frac{1}{2\pi} \sin\left(\frac{2\pi r}{r + \Delta R}\right) \right]^{-1} \text{ ns} \quad (3)$$



**Fig. 5.** (color, 1-column): Calculations of the implantation profile  $P_+(z)$  with Eq. (2) for three different materials for a maximum sample thickness of 2 mm. It shows the dependence of the positron implantation on the density of the material. Silicon ( $\rho_{\text{Si}} = 2.33 \text{ g/cm}^3$ ) exhibits the least implantation distance of 0.5 mm, followed by polystyrene ( $\rho_{\text{PS}} = 1.05 \text{ g/cm}^3$ ) with 1.3 mm and silica gel ( $\rho_{\text{silicagel}} = 0.35 \text{ g/cm}^3$ ), where a sample thickness of 2 mm would not be sufficient. This must be considered to prevent positrons from escaping the sample and annihilating elsewhere.



The empirically determined parameter  $\Delta R$  approximates the reduction of the FVE radius due to interactions between o-Ps and electrons of the surrounding polymer chains. The value of  $\Delta R$  was determined to be 0.166 nm by calibration measurements on several molecular solids [14,37,38]. Although for larger FVEs ( $r > 1$  nm), the Tao-Eldrup model insufficiently correlates  $\tau_3$  with the radius of the FVEs, it is well applied for the measured positron lifetimes in PS, where the mean radii of the FVEs are below 1 nm. In any case, the model could be extended to account for the  $3\gamma$  annihilation, which becomes increasingly probable as the size of  $V_F$  increases and  $\tau_3$  approaches the vacuum lifetime of o-Ps [39]. The resulting mean positron lifetime of 2056(3) ns corresponds to a mean radius of the FVEs of the PS of  $r = 0.2899(3)$  nm at room temperature and 0.1 MPa argon pressure, meaning that it is well in the validity range of the Tao-Eldrup model (Eq. (3)).

### 3.2. Temperature dependent measurements on PS

During the first test for temperature dependent measurements, the thermal contact between the sample and the heating element was tested. Therefore, we heated the sample in air and measured the sample temperature at three different locations  $T_{s1}$ ,  $T_{s2}$  and  $T_C$ . Thermocouples were positioned on either side ( $T_{s1}$ ,  $T_{s2}$ ) and in the center ( $T_C$ ) of two  $10 \times 10 \times 2$  mm<sup>3</sup> polychlorotrifluoroethylene (PCTFE) sheets. The thermocouples on the sides of the PCTFE stack are thermally isolated from the jaws, to eliminate measurement distortion. We then calculated the mean temperature across the two PCTFE sheets. The slope of the linear fit of mean sample temperature and the set temperature was determined to be 0.98(0.01) over the range from 23(3) °C up to 200 °C. This shows sufficient thermal contact of the heating element to the sample and reveals a temperature difference of 2(1) % from the outside to the center of the polymer stack. It is important to mention that this difference can change for different materials. However, since the thermal conductivity coefficient of most polymers is rather low and in the same order of magnitude, the influence on the measurement are similar and negligible [40]. The samples were heated from room temperature 21(2) to 150(3) °C in increments of 25 °C and for every temperature a positron-annihilation lifetime spectrum was recorded.

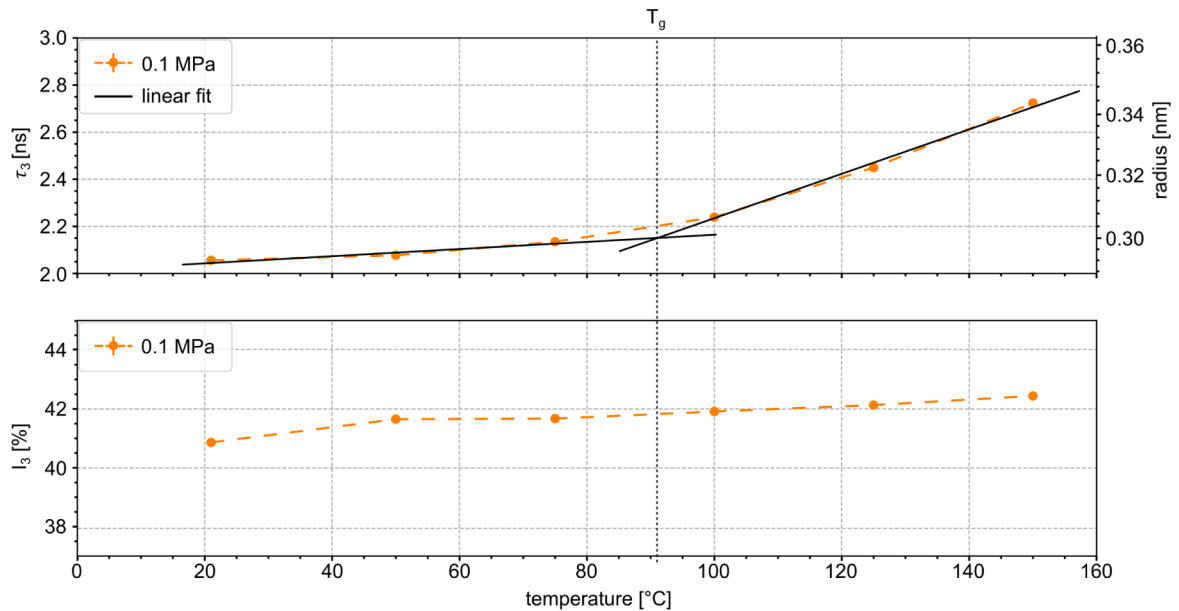
Fig. 6 shows the temperature dependence of  $\tau_3$  and  $I_3$  in 0.1 MPa argon atmosphere. For spatial reference, the FVE radius was calculated

with Eq. (3) and is shown on the right-hand y-axis. The glass transition temperature ( $T_g$ ) is depicted as a dashed vertical line. The lifetime analysis gives an o-Ps lifetime  $\tau_3$  of roughly 2 ns with an intensity  $I_3$  of 0.4 %. The lifetime  $\tau_3$  is an indicator for the dimension of the FVEs and  $I_3$  for the abundance of the FVEs. The results of the temperature dependence of  $\tau_3$  and  $I_3$  are shown in Table 1. At temperatures below the  $T_g$  the increase in  $\tau_3$  is less than 200 ps. Above the  $T_g$ , a steeper increase in  $\tau_3$  is noticeable ( $\approx 500$  ps/50 K), while the intensity  $I_3$  of this component increases only from 0.41 to 0.42 between 100 °C and 150 °C. Below the  $T_g$ , PS is in a non-equilibrium, glassy state, where the polymer chains minimal segmental mobility and the increase in  $\tau_3$  with increasing temperature is marginal. When the temperature reaches the  $T_g$ , i.e. upon the phase transition from glassy to rubbery, the polymer chains become more mobile and  $\tau_3$  increases more rapidly due to the increasing temperature. The negligible

**Table 1**

o-Ps lifetimes  $\tau_3$  and intensities  $I_3$  of PS as a function of temperature and 0.1, 2 and 4 MPa argon pressure. The statistical uncertainty of  $I_3$  from the fit is below 0.001 and is therefore omitted.

T [°C]	21(2)	50(1)	75(2)	100 (2)	125 (3)	*140 (3)** 146 (2) 150(3)	
p = 10 <sup>-9</sup> MPa	2021 (5) 36.3	2064 (5) 38.2	2122 (5) 38.4	2283 (5) 42.6	2475 (5) 43.6	**2731 (5) **43.7	$\tau_3$ [ps]  $I_3$ [%]
p = 0.1 MPa	2056 (3) 40.9	2077 (5) 41.5	2135 (5) 41.7	2239 (5) 42.0	2450 (5) 42.3	2724(6) 42.8	$\tau_3$ [ps]  $I_3$ [%]
p = 2 MPa	2099 (5) 39.4	2168 (6) 41.3	2228 (5) 41.7	2290 (5) 42.0	2448 (5) 43.0	2698(5) 43.1	$\tau_3$ [ps]  $I_3$ [%]
p = 4 MPa	2183 (6) 38.5	2260 (6) 41.0	2313 (6) 41.8	2400 (6) 41.9	2606 (6) 42.8	*2724(6) *43.4	$\tau_3$ [ps]  $I_3$ [%]



**Fig. 6.** (color, 2-column): Positron-annihilation lifetime results of the o-Ps lifetime  $\tau_3$  and the intensity  $I_3$  of PS at 0.1 MPa as a function of temperature. The corresponding free-volume element (FVE) radius, using Eq. (3), is plotted on the second axis as a geometric reference. There is a clear difference in FVE growth below and above  $T_g$ . By linear fitting of these two regions the  $T_g$  can be estimated to be 91(5) °C.

temperature dependence of  $I_3$  indicates that at temperatures above the  $T_g$ , the FVEs increase in size but not in abundance. Moreover, by linear fitting of the two data regions of  $\tau_3$  below and above the  $T_g$ , we can estimate the glass transition temperature of PS to be at 91(5) °C (see Fig. 6). The obtained results from the lifetime evaluation are consistent with previous publications [21,41]. In these publications the  $T_g$  was determined by means of differential scanning calorimetry (DSC) and positron annihilation lifetime spectroscopy.

### 3.3. Pressure dependence of $\tau_3$

In addition to temperature, the influence of the gas pressure on the FVEs of PS was simultaneously measured.

In a first step, we determined the pressure decrease in the pressure vessel at room temperature over a period of 9 days. In that period, the pressure dropped from 13.7(0.5) MPa to 13.5(0.5) MPa. Considering that a measurement with  $2 \times 10^6$  events/spectrum takes less than 2 days, the pressure loss of approximately 0.02 MPa/day is negligible and can be fully compensated by careful adjustments at the gas-inlet.

For our first test measurements, we investigated the influence of temperature and gas pressure on the  $V_F$  of PS. For this purpose, PALS measurements were taken on PS samples as a function of the temperature at vacuum ( $1 \times 10^{-9}$  MPa) and 3 different argon pressures: 0.1 MPa, 2 MPa and 4 MPa (see Table 1). Fig. 7 shows the o-Ps lifetime for the four different pressure states as a function of the temperature. On the right-hand y-axis, the FVE radius is displayed as a size reference. At room temperature,  $\tau_3$  increases with pressure. Upon heating, the  $\tau_3$  (T) curve shifts towards higher lifetimes with increasing pressure. In the glassy phase, there is a comparable increase in  $V_F$  concerning temperature in low-pressure (in vacuo, 0.1 MPa) and high-pressure measurements. In the rubbery phase, above the  $T_g$ , a steeper increase of  $\tau_3$  for lower pressures is apparent. Among all the pressure states measured, the vacuum measurement shows the lowest intensity  $I_3$  below the  $T_g$  with a transition to the highest intensity above the  $T_g$ . For the measurements in argon atmosphere, a pressure dependence of  $I_3$  below 75 °C is visible, until the intensities of the different pressure states converge at

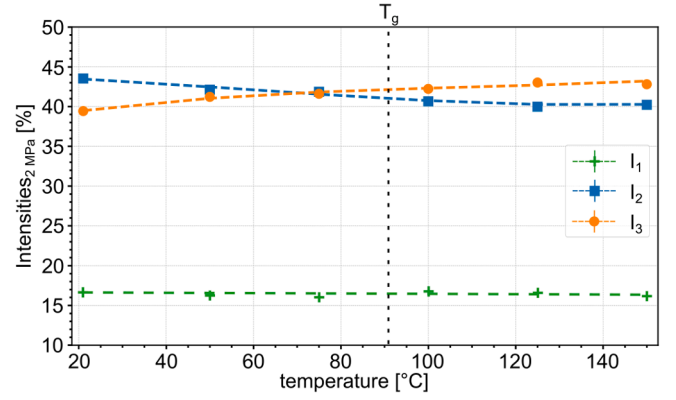


Fig. 8. (color, 1-column): Intensities as a function of temperature for 2 MPa argon pressure.  $I_1$  seems unchanged over the whole temperature range and independent of the phase change. For the intensities  $I_2$  and  $I_3$  an inverse correlation can be observed. The change in the glassy phase can either be explained by [44] or by employing the dual-mode sorption model. In the latter, a temperature dependent gas population can trap in the static FVEs present in the glassy phase. This results in a decrease in o-Ps annihilation and an increase in positron annihilation within the polymer matrix.

temperature above 75 °C and display an increase for higher gas pressures. The lowest  $I_3$  is reached for 4 MPa and 21(2) °C followed by the 2 MPa and 0.1 MPa measurement, respectively. In Fig. 8 the intensities ( $I_1$ ,  $I_2$ ,  $I_3$ ) for the 2 MPa measurement are shown as a function of temperature. Although  $I_1$  does not show any dependence on temperature or pressure,  $I_2$  and  $I_3$  display an inverse correlation. This inverse correlation holds true for 0.1 MPa and 4 MPa as well.

The increase in o-Ps lifetime with increasing argon pressure suggests the occurrence of polymer chain reorganization due to the interaction with the argon. Plasticization by argon has indeed been observed for polydimethyl siloxane and poly(ethyl methacrylate), even if argon has a low solubility [33,42,43]. The FVE expansion with increasing pressure is observed in both the glassy state and the rubbery state.

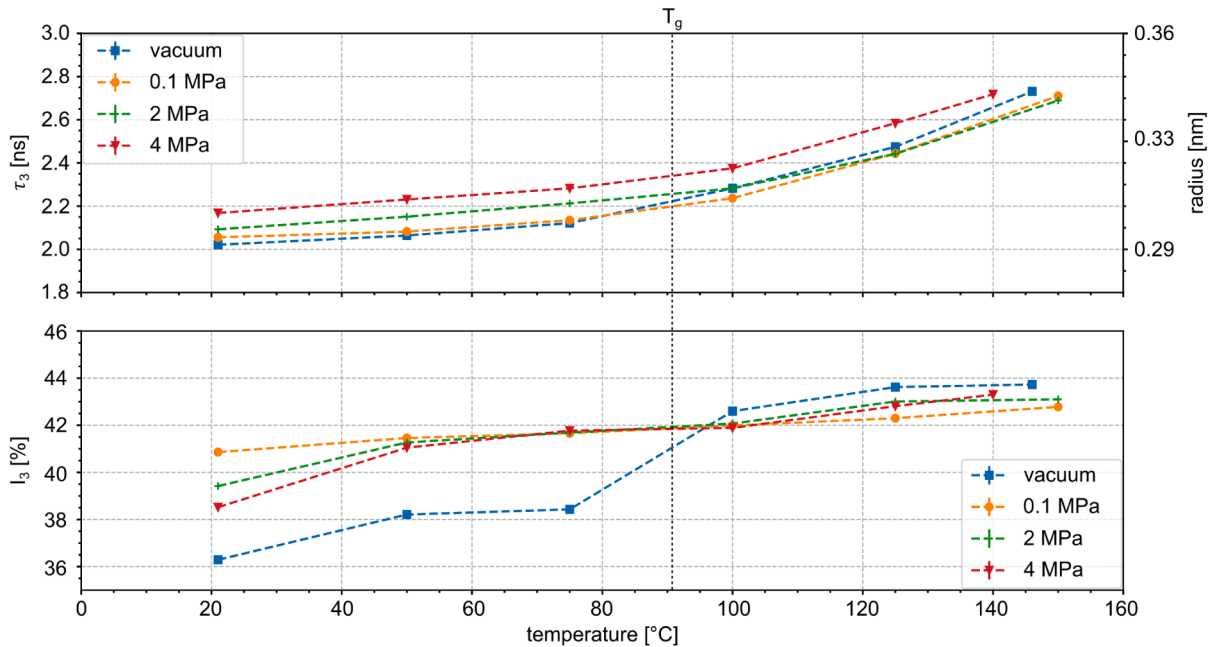


Fig. 7. (color, 2-column): o-Ps lifetime and intensity  $I_3$  of polystyrene at four different pressures. The  $T_g$  at 0.1 MPa is marked as a reference point of the phase transition. With increasing argon pressure an offset to higher o-Ps lifetimes is evident. At higher pressures the growth behaviour of the FVEs is similar to that at 0.1 MPa. An opposite trend in the intensity  $I_3$  is present for temperature close to room temperature, which however vanishes at higher temperatures. In vacuum condition the intensity is the lowest in the glassy state and the highest in the rubbery phase with an abrupt transition at the  $T_g$ .

In the rubbery phase, the steeper increase of  $\tau_3$  with temperature at lower pressures could be explained by the weaker compressive force of the argon on the polymer. In the rubbery phase with increasing gas pressure, the counter-effect of hydrostatic pressure appears to play a greater role and slows down the temperature-induced expansion of the FVEs [23]. To interpret the behavior of  $I_3$ , it is important to note that in the rubbery phase there exist only *dynamic* FVEs, whereas in the glassy phase also *static* FVEs can exist due to the non-equilibrium nature of that phase. The decrease in  $I_3$  and the simultaneous increase in  $I_2$  at lower temperatures (cfr. Fig. 8) was explained by the creation of additional smaller holes, which act as positron traps [44]. Another possible explanation of this phenomenon can be made by applying the dual-mode sorption model [12,45–47]. According to this model the gas transport in the glassy polymer is governed by two competing modes:

In the first mode the gas dissolves in the polymer matrix, while in the second mode the gas adsorbs in the *static* FVEs and can get immobilized there [12,47]. With increasing pressure, the number of gas atoms that can be trapped by the *static* FVEs also increases, obscuring more *static* FVEs for o-Ps pick-up annihilation. This is reflected in Fig. 7 for 0.1 MPa, 2 MPa and 4 MPa below 75 °C. The positrons that are not forming positronium, due to the decrease in vacant *static* FVEs, will eventually annihilate in the polymer matrix, contributing to  $I_2$ , which can be seen in Fig. 8. Furthermore, the second mode is temperature dependent and should diminish as the *static* FVEs and gas atoms become more mobile with temperature and convert to a more dynamic state. The temperature dependence can be seen in Figs. 7 and 8. Since the average size of the FVEs and the size of gas atoms are in the same order of magnitude, the occupation of the *static* FVEs seems to only have an effect on the amount ( $\sim I_3$ ) and not on the size of the FVEs ( $\sim \tau_3$ ). Under vacuum conditions, gas atoms are removed from the polymer, resulting in less plasticization. In the glassy phase, an overall reduction in  $V_F$  is visible, which is probably due to the rigid chains imploding and hence, closing some of the FVEs. Transitioning to the rubbery phase, the polymer matrix reaches an equilibrium state and the chains can relax, forming new *dynamic* FVEs. This is reflected in the rapid increase of  $I_3$  at the phase transition.

One possible reason why the intensity of the vacuum measurement is highest above the  $T_g$  may be that there are no argon atoms to occupy some of the *dynamic* FVEs, as is the case with the pressurized material. Please note that this is the first test measurement to show the potential of measuring PALS on soft matter materials with simultaneously controlling pressure, atmosphere composition and temperature, a more detailed investigation is needed to fully elucidate the occurring phenomena. Note that these effects can change for other gas species and polymers [23].

#### 4. Summary and conclusion

In this paper, we present proof of concept for an apparatus that allows us to measure positron lifetime spectra as a function of temperature, gas pressure, and atmospheric composition. The technical description of the system and the exact specifications have been defined. The samples can be heated up to 200 °C or be exposed to vacuum or a desired gas atmosphere of up to 20 MPa. Moreover, a combined treatment with temperature and pressure at slightly reduced values (see Fig. 1b) are also possible. The ability to control all three parameters simultaneously in this parameter range during the measurement is unique to date. The application of the instrument was demonstrated by using PS as an example. Here, the effect of temperature and argon atmosphere on the  $V_F$  of the polymer was investigated (see Table 1). It was shown that the size of the FVEs is a function of the argon pressure and sample temperature and can be explained by the plasticization of the polymer matrix. In addition, an alternative explanation of the temperature and pressure dependent reduction of  $I_3$  below the  $T_g$  was given. The results are compared to the results of investigations on polystyrene or other polymer systems where either atmosphere, pressure or temperature was varied but never simultaneously [21–24]. Overall, the test

measurements on Polystyrene show the capability of the in-situ multi-parameter control during PALS for the investigation of polymer material. A more detailed investigation of the evolution of the  $V_F$  of PS under different gas atmospheres will be performed in future experiments with the instrument introduced in this work. Also, in more applied fields of science, the instrument could be useful for in-situ measurements; e.g., to analyze the behavior of a gas separation membrane upon contact with gasses, to follow-up the vapor-induced crosslinking degree of a polymer, or to investigate the behavior of different adsorbents for air remediation.

#### CRediT authorship contribution statement

**R. Helm:** Writing – review & editing, Writing – original draft, Formal analysis. **J. Lehtonen:** Methodology, Investigation. **M. Mayerhofer:** Writing – review & editing, Validation. **J. Mitteneder:** Resources. **W. Egger:** Validation. **R. Verbeke:** Writing – review & editing, Writing – original draft. **P. Sperr:** Methodology, Conceptualization. **G. Dollinger:** Writing – original draft. **M. Dickmann:** Project administration, Conceptualization.

#### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

#### Data availability

Data will be made available on request.

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