



# Statistical analysis of current–voltage characteristics in Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN Schottky barrier heterojunction using different methods

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## Abstract

We report on the influence of incorporation of Ta<sub>2</sub>O<sub>5</sub> thin film at the interface of Au/GaN by means of e-beam evaporation technique. The fabricated Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junctions have been analysed using *I*–*V* measurements and were extended to a voltage range of  $\pm 20$  V. The Schottky diode parameters for instance  $\Phi_{bo}$ , *n* and *R<sub>S</sub>* values are evaluated using *I*–*V* curves at room temperature. The statistical distribution analysis provides the mean ' $\Phi_{bo}$ ' value of 0.85 eV with deviation of 0.00181 eV and mean value from '*n*' is 1.36 with a normal deviation of 0.00562. Two important electrical parameters such as *R<sub>S</sub>* and *R<sub>sh</sub>* values are also extracted from *I*–*V* characteristics. Furthermore, Cheung, Norde, modified Norde, Hernandez and Chattopadhyay methods are used to evaluate the Schottky barrier parameters from *I*–*V* data. The comparison is made between the extracted electrical parameters such as *n*,  $\Phi_{bo}$  and *R<sub>S</sub>* from *I*–*V* characteristics of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junctions and are in well agreement with each other. Under forward-bias, the fabricated Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction conduction mechanisms such as ohmic and SCL were found to be dominant at lower and higher voltage regimes, respectively. By fitting reverse-bias region of *I*–*V* curves, PF conduction mechanism was found to be dominant at the interfaces of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN. In conclusion, the obtained superior rectification ratio of  $6.06 \times 10^4$  and higher SBH of 0.87 eV was ascribed to the purposefully deposited undoped GaN buffer layer between epitaxial GaN and sapphire substrate.

**Keywords** Ideality factor · Ta<sub>2</sub>O<sub>5</sub> interfacial layer · Series/shunt resistance · Gallium nitride · Schottky barrier height

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## 1 Introduction

Presently, wide-bandgap semiconductors (WBGs) such as AlN, InN and GaN are broadly used in device fabrication which includes applications of short wavelength range optoelectronic, high-frequency/power electronic devices. This was accomplished due to their higher intrinsic material properties of WBGs compared to conventional semiconductors such as Si and GaAs as indicated in Table 1 [1–3]. Among these WBG materials, gallium nitride (GaN) has the potential in terms of good optical/electrical properties, high carrier mobility, strong ultraviolet absorption, high chemical resistivity, direct bandgap, good thermal conductivity and high melting points [1–7]. These aforesaid properties cause GaN to be used in diverse important applications such as sensors, light-emitting diodes, metal–semiconductor field effect transistors (MSFETs), high electron mobility transistors (HEMTs), heterostructure field effect transistors (HFETs) and photocatalysts [8–15]. As GaN-based metal/semiconductor junction (MSJ)-based Schottky barrier diodes (SBDs) are vital in almost all electronic devices, analysis of electronic properties/current transport at the MSJ interfaces requires further analysis on reliable and stable ohmic/Schottky contacts. Current–voltage ( $I$ – $V$ ) features of MSJs give an enormous information on electrical and physical assets of a bulk material of semiconductor and its interface. The MSJ-based devices may be affected by low breakdown voltage and high leakage current, which bounds the device performance, stability and reliability. One can overcome this limitation by retaining a thin high- $k$  dielectric oxide layer at the interface of MSJ. This deliberately deposited high- $k$  interlayer has remarkable advantages such as greater rectification ratio, lower leakage current, lower ideality factor ( $n$ ), higher Schottky barrier height (SBH:  $\Phi_{bo}$ ) and good thermal stability. Also, the MIS junction characteristic depends on the interface states, interlayer homogeneity and series resistance ( $R_s$ ). The vital limitations of existing conventional gate dielectric materials such as silicon dioxide ( $\text{SiO}_2$ ) are prone

to higher gate leakage currents, thus, the search for materials with advanced high- $k$  dielectric constant to permit further reduction in the gate leakage currents in the real time device applications.

Developments in shrinking the size of integrated circuits (ICs) to improve the logical density and performance of chips necessitates the substitution of copper (Cu) for aluminium (Al) as interconnections in silicon-based ICs. This is due to the fact that Cu offers lower resistivity, superior electromigration and stress-voiding resistance compared to Al and its alloys [16]. Still, Cu limits its usage owing to its high mobility/reactivity and poor adhesiveness, which should be elucidated first prior to its practical usage in ICs. Novel materials that act as effective diffusion barrier and adhesion promoters between Cu and underlying substrate are essential. Materials such as tantalum (Ta), tantalum nitride (Ta<sub>N</sub>) and tantalum carbide (TaC) thin films are already proven as the utmost capable diffusion barriers and were used to prevent diffusion/reaction of Cu with the underlying silicon and adjoining  $\text{SiO}_2$  dielectrics [17–19]. Thus, the above-said superior electrical, structural and thermal stability characteristics of Ta, TaC, Ta<sub>N</sub> found applications as renowned diffusion barriers in electronic devices [20] and X-ray lithography [21–23]. On the other hand, tantalum pentoxide ( $\text{Ta}_2\text{O}_5$ ) became an attractive material due to its high- $k$  dielectric property and found applications in anti-reflective coatings, photocatalysts and resistance-change random access memory (ReRAM) [24–26]. Many other research groups have explored the fabrication of  $\text{Ta}_2\text{O}_5$  as an interfacial oxide layer at the MS interface and tested their electrical characteristics by diverse deposition methods [27–32]. For example, Yu et al. [27] and Joo et al. [28] reported that Pt/ $\text{Ta}_2\text{O}_5$ /SiC and Pd/ $\text{Ta}_2\text{O}_5$ /SiC MIS type SBD structures could be used in hydrogen gas sensing applications. Lakshmi et al. [29] investigated Au/ $\text{Ta}_2\text{O}_5$ /n-GaN MIS structure and studied its electrical properties at different annealing temperatures. They concluded that the annealed samples exhibited betterment in electrical properties due to the reduction of interface states density. Alimardani et al. [30] fabricated  $\text{Nb}_2\text{O}_5$ - and  $\text{Ta}_2\text{O}_5$ -based MIS structures by means of atomic layer deposition technique and they reported that the dominant conduction mechanism at smaller biases was Schottky emission whereas at higher biases it was Frenkel–Poole (PF) emission. Reddy et al. [31] investigated Al/ $\text{Ta}_2\text{O}_5$ /p-Si MIS SBD with  $\text{Ta}_2\text{O}_5$  as the insulating layer and reported higher SBH for the prepared devices compared to Al/p-Si MS SBD. Kumar et al. [32] fabricated Ni/n-GaN SBDs and reported current transport properties using different methods.

In MIS junction, the traditional thermionic emission (TE) theory is not sufficient to describe the charge or carrier transport mechanism through the intentionally deposited interfacial interlayer [33, 34]. As the SBH is often influencing the current transport at the interfaces of MIS structure, we

**Table 1** Material properties of Si, GaAs, 4H-SiC and GaN for comparison

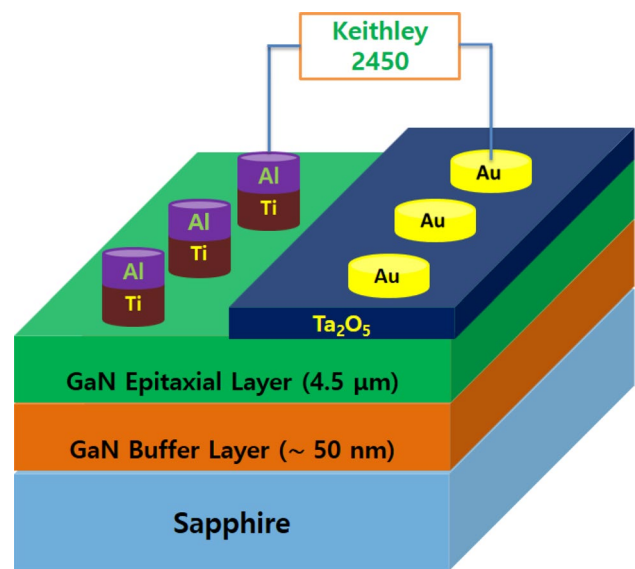
Parameter	Si	GaAs	4H-SiC	GaN
$E_g$ (eV)	1.12	1.42	3.25	3.40
$E_C$ (MV/cm)	0.3	0.4	3.0	4.0
$\mu_n$ ( $\text{cm}^2\text{V}^{-1}\text{S}^{-1}$ )	1500	8500	1000	1250
$\epsilon$	11.8	12.8	9.7	9.0
$V_{sat}$ ( $10^7$ cm/s)	1	2	2	2.5
$\lambda$ ( $\text{W}\cdot\text{cm}^{-1}\cdot\text{K}^{-1}$ )	1.5	0.5	4.9	2.3

$E_g$  bandgap;  $E_C$  critical electric field;  $\mu_n$  electron mobility;  $\epsilon$  dielectric constant;  $V_{sat}$  saturation electron velocity;  $\lambda$  thermal conductivity

extended our analysis of electrical parameters by TE theory with different methods. This can allow one to understand better about the SBH ( $\Phi_{bo}$ ),  $n$ ,  $R_S$  and current conduction mechanisms, which are highly crucial for the technology of advanced device fabrication. The key significance of the present manuscript is to describe the electronic parameters using different fitting methods using experimentally measured  $I$ – $V$  data of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD in the  $\pm 20$  V range at room temperature. As high work function metal gold (Au) is used as a Schottky contact and Al/Ti is used as ohmic contact, we have obtained a very good rectification. Also, we have used UV–Visible, AFM and XRD techniques to check the Ta<sub>2</sub>O<sub>5</sub> oxide layer bandgap, surface morphology and crystallinity of Al/Ti/GaN structure, respectively.

## 2 Materials and methods

Si-doped n-type GaN epitaxial layer with 4.5  $\mu\text{m}$  thickness was grown on undoped GaN buffer layer of thickness  $\sim 50$  nm, which confined on sapphire (0001) substrate using metal organic chemical vapour deposition (MOCVD). Estimated carrier concentration of the n-type GaN epitaxial layer was found to be  $1\text{--}3 \times 10^{17} \text{ cm}^{-3}$ . Prior to the deposition of metals and oxide, n-GaN sample was undergone with cleaning procedure steps reported in our previous work [35]. By an electron beam (e-beam) evaporation system, Ti/Al (30 nm/60 nm) was deposited onto half portion of 5 mm size of n-GaN with dots of 0.003 cm diameter. Then samples were annealed at 650  $^{\circ}\text{C}$  for 60 s in N<sub>2</sub> gas to yield better adhesive ohmic contact to n-GaN. Subsequently, the Ta<sub>2</sub>O<sub>5</sub> of purity 99.9% ( $\sim 35$  nm thick) material which is in pellet form was deposited on other half portion (2.5 mm) of the n-GaN substrate. Then Au (70 nm) metal of purity 99.99% was deposited on Ta<sub>2</sub>O<sub>5</sub> film using e-beam evaporation system using 0.03 mm diameter stainless steel mask. The schematic of the fabricated Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD heterojunction is shown in Fig. 1. Deposited Au and Ta<sub>2</sub>O<sub>5</sub> film thickness was evaluated by quartz crystal microbalance at a pressure of  $3\text{--}5 \times 10^{-5}$  mbar. UV–Vis technique (Shimadzu, UV-1800, Japan) was employed to evaluate the direct optical bandgap of the Ta<sub>2</sub>O<sub>5</sub> material. Atomic force microscopy (AFM: A.P.E. Research, Italy) analysis was employed to distinguish the surface morphology/contact quality of Ta<sub>2</sub>O<sub>5</sub> on to GaN. X-ray diffraction (Panalytical XPRD Pro) technique was used to check the interfacial reaction between Ti/Al and GaN. The  $I$ – $V$  characteristic properties of the prepared Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction were studied by 2450 model Keithley source. Finally, using different methods, the Schottky diode parameters were interpreted with the help of the conduction mechanisms such as ohmic, space charge limited (SCL), Schottky emission (SE) and Poole–Frenkel (PF) at 300 K, respectively.



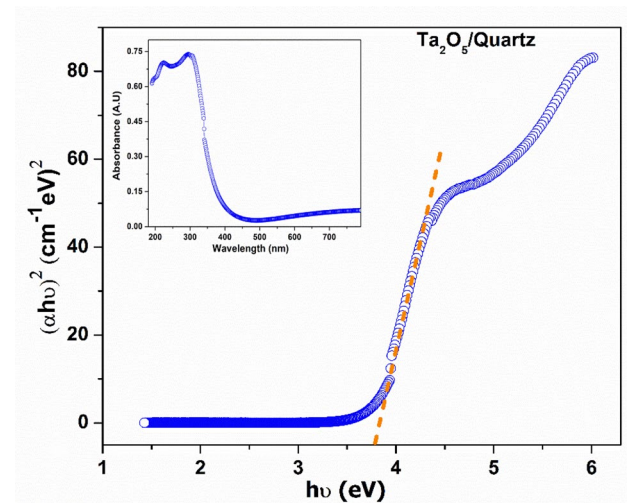
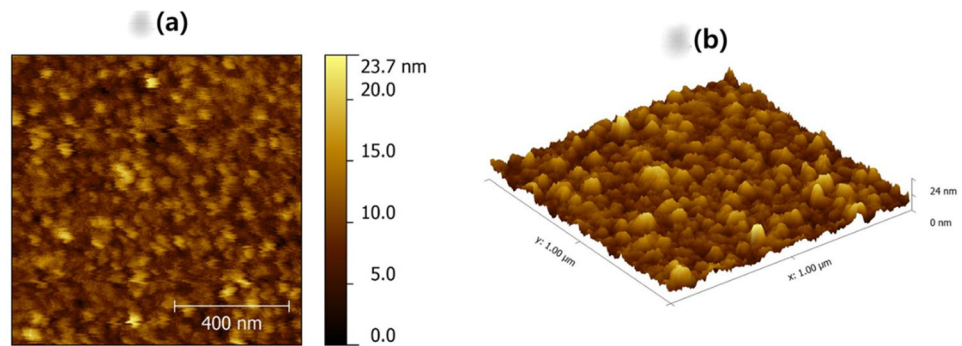
**Fig. 1** Schematic diagram of the fabricated Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD

## 3 Results and discussion

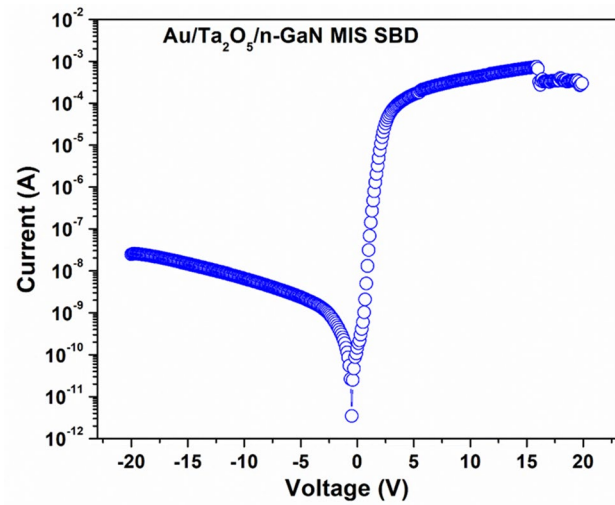
As thin film growth mechanism is influencing the electrical, optical and structural properties of the fabricated device performance or functionality, surface topography has been employed to analyse the Ta<sub>2</sub>O<sub>5</sub> films. Generally, topographical information is acquired using AFM in non-contact mode which is being the utmost preferred compared to the other techniques due to its versatility. Figure 2a, b displays the two and three-dimensional surface morphologies of Ta<sub>2</sub>O<sub>5</sub> films made on n-type GaN using non-contact mode AFM with scan area of 1  $\mu\text{m}^2$ . It indicates the formation of smooth and continuous surface morphology with root-mean square roughness of 2.80 nm. As shown in Fig. 2b, the formed Ta<sub>2</sub>O<sub>5</sub> films deposited by means of e-beam evaporation revealed gathering of atomic clusters or island. Similar surface morphology was observed for Ta<sub>2</sub>O<sub>5</sub> films in the case of ion-assisted e-beam evaporation [36] and e-beam evaporation [37] techniques.

To understand the electronic structure with the help of optical bandgap of Ta<sub>2</sub>O<sub>5</sub> films, UV–Vis absorption spectral study was employed. In general, the absorption arises as of electronic transitions related within the Ta<sub>2</sub>O<sub>5</sub> material. The UV–Vis spectrum for the as-deposited Ta<sub>2</sub>O<sub>5</sub> films on quartz is shown in the inset of Fig. 3. As can be seen from the inset of Fig. 3, the maximum absorption for Ta<sub>2</sub>O<sub>5</sub> film was observed to take place below 400 nm with a sharp absorbance peak noticed at 295 nm. Direct optical bandgap of the as-deposited Ta<sub>2</sub>O<sub>5</sub> thin films was evaluated using Tauc's plot. As shown in Fig. 3, the consequent Tauc's plot is used for the estimation of the direct optical

**Fig. 2** The top view of **a** 2D **b** 3D AFM surface morphology of the as-prepared Ta<sub>2</sub>O<sub>5</sub> film on n-GaN



**Fig. 3** UV–Vis absorption spectra of as-prepared Ta<sub>2</sub>O<sub>5</sub> films (shown in inset) and Tauc's plot of  $(\alpha h\nu)^2$  versus  $h\nu$



**Fig. 4** Forward and reverse  $\ln(I)$ – $V$  characteristics of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction measured at room temperature in the voltage range  $\pm 20$  V

bandgap energy ' $E_g$ ' by extrapolation of the  $(\alpha h\nu)^2$  versus ' $h\nu$ ' curve to zero absorption and can be written as [38]

$$\alpha h\nu = E_D(h\nu - E_g)^{1/2}, \quad (1)$$

where  $\alpha$  is absorption coefficient,  $E_D$  is constant and ' $h\nu$ ' is photon energy.

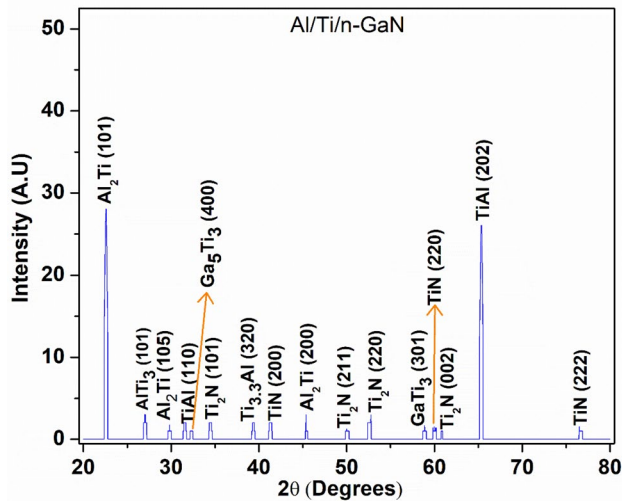
The evaluated direct optical bandgap energy of 3.85 eV estimated for the as-deposited Ta<sub>2</sub>O<sub>5</sub> film in the present work is in well accordance with the earlier reported value of 3.9 eV in the case of e-beam evaporated as-deposited Ta<sub>2</sub>O<sub>5</sub> films [37].

The Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction showed a good rectification as shown in Fig. 4 with a reverse leakage current of  $6.4 \times 10^{-10}$  A at  $-2$  V. This result designates the reduction of leakage current due to the intentionally introduced Ta<sub>2</sub>O<sub>5</sub> interlayer at the interface of Au and n-GaN. The basic electrical parameters of the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD can be derived using TE theory. The forward bias  $I$ – $V$  relation can be written according to TE theory [39, 40].

$$I = AA^*T^2 \exp\left(-\frac{q\Phi_{bo}}{kT}\right) \left[ \exp\left(\frac{q(V - IR_s)}{nkT}\right) - 1 \right]. \quad (2)$$

In Eq. (2),  $I_0$  is the reverse-saturation current determined from  $\ln(I)$ – $V$  plot at  $V=0$  and  $A^*$  is the Richardson constant [35] ( $26.4 \text{ A cm}^{-2} \text{ K}^{-2}$  for n-type GaN). As can be seen in Fig. 4, the  $\ln(I)$ – $V$  plot for Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD in the voltage range of  $\pm 20$  V displayed a good rectification ratio. The rectification ratio (RR), i.e. the ratio of forward current ( $4 \times 10^{-4}$  A) to reverse current ( $6.59 \times 10^{-9}$  A) at 10 V bias was found to be  $6.06 \times 10^4$ . This ensures that the fabricated MIS junction is exhibiting superior RR due to the formations of good Schottky (Au) and ohmic (Ti/Al) contacts. To check the quality of the fabricated Al/Ti ohmic contact to GaN, we have employed X-ray diffraction study with a  $2\theta$  scan in the range of  $20$ – $80^\circ$ . Figure 5 illustrates the grazing-incidence X-ray diffraction (GIXRD) scan of the Al/Ti/GaN sample annealed at  $650^\circ \text{C}$  in  $\text{N}_2$  atmosphere for a period of one minute. The peaks found at  $2\theta = 22.6, 26.4, 29.05, 31.5, 39.1, 45.5$  and  $65.4^\circ$  correspond to Ti–Al





**Fig. 5** XRD plot of Al/Ti/n-GaN structure annealed at 650 °C for 1 min in N<sub>2</sub> ambient

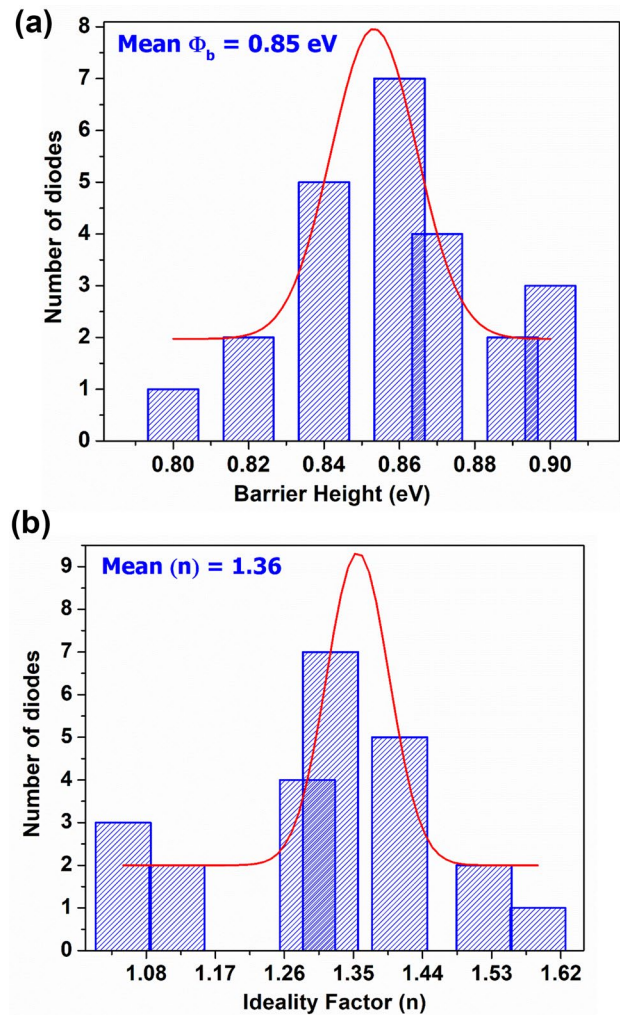
alloys of Al<sub>2</sub>Ti (101), AlTi<sub>3</sub> (101), Al<sub>2</sub>Ti (105), TiAl (110), Ti<sub>3</sub>Al (320), Al<sub>2</sub>Ti (200) and TiAl (202), respectively. The two peaks originated at  $2\theta = 32^\circ$  and  $59.1^\circ$  corresponds to Ga–Ti phases of Ga<sub>5</sub>Ti<sub>3</sub> (400) and GaTi<sub>3</sub> (301), respectively. Furthermore, Ti–N phases of Ti<sub>2</sub>N (101), TiN (200), Ti<sub>2</sub>N (211), Ti<sub>2</sub>N (220), TiN (220), Ti<sub>2</sub>N (002) and TiN (222) found at  $2\theta = 34.5, 41, 50.2, 52.3, 60.2, 61$  and  $76.3^\circ$ , respectively. Most of the above-said Ti–N and Ti–Al phases were already reported in previous works [41–44]. The presence of Ti–N and Ti–Al phases in the X-ray diffractogram of Al/Ti metallization point out the development of good quality ohmic contacts to n-GaN. Thus, the formation of these desired Ti–N compound and low resistance inter-metallic Ti–Al phases are crucial in obtaining the superior quality ohmic contact, confirming the creation of N vacancies at the MS interface which intern enhances the tunnelling current ensuring the formation of good ohmic contact to n-GaN [45–47].

The SBH ( $\Phi_{bo}$ ) is calculated by means of Eq. (3) and the slope of the  $\ln(I)$ – $V$  characteristics yields the ideality factor ( $n$ ) value that are attained from the following equation:

$$\Phi_{bo} = \frac{kT}{q} \ln \left( \frac{AA^*T^2}{I_0} \right), \quad (3)$$

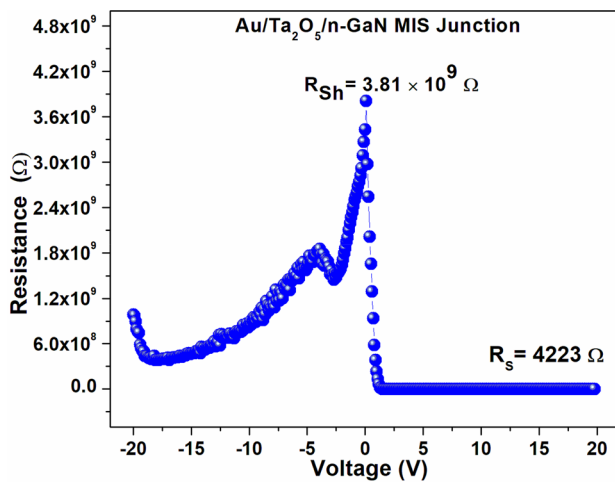
$$n = \frac{q}{kT} \frac{dV}{d(\ln I)}. \quad (4)$$

We fabricated the sixteen number of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD heterojunction dots/devices on the same GaN semiconductor. The ' $\Phi_{bo}$ ' and ' $n$ ' values are calculated from the distinct  $I$ – $V$  plots ( $\pm 20$  V). The diodes SBH ( $\Phi_{bo}$ ) values varied from 0.80 to 0.90 eV and the ' $n$ ' values



**Fig. 6** **a** Gaussian distribution of Schottky barrier heights and **b** ideality factors calculated from the forward bias  $I$ – $V$  characteristics for Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction

ranged from 1.05 to 1.59. From the results, it is clear that the identically prepared MIS junction ' $\Phi_{bo}$ ' and ' $n$ ' values slightly varied from diode to diode. These results indicated that the potential barriers at the interfaces of MIS SBD strongly depend on the Ta<sub>2</sub>O<sub>5</sub> interlayer between metal and semiconductor as well as applied voltage that is expected by the image-force effect. Figure 6a, b shows the statistical distribution analysis of the ' $\Phi_{bo}$ ' and ' $n$ ' values for the sixteen Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junctions from  $I$ – $V$  plot with the voltage range of  $\pm 20$  V, at room temperature. The calculated ' $\Phi_{bo}$ ' and ' $n$ ' values are experimentally fitted by Gaussian distribution functions. The statistical analysis yields an average ' $\Phi_{bo}$ ' value of 0.85 eV with normal deviation of 0.00181 eV and average ' $n$ ' of 1.36 with a normal deviation of 0.00562 for the Ta<sub>2</sub>O<sub>5</sub>-based MIS SBD. The calculated ' $n$ ' is larger than unity and the reason for this can be ascribed to the facts such as the distribution



**Fig. 7** Junction resistance versus voltage for the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction at room temperature

of the interface states, recombination-generation/tunneling process and image-force effects [48].

The shunt resistance ( $R_{sh}$ ) and series resistance ( $R_s$ ) are the other two important electrical parameters to be evaluated for the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD. These values are extracted using the expression  $R_j = \partial V / \partial I$  from  $I$ - $V$  analysis at room temperature and is shown in Fig. 7. Generally, in the case of ideal device, the  $R_s$  and  $R_{sh}$  should be close to zero and infinity, respectively [49]. From Fig. 7, the  $R_s$  and  $R_{sh}$  values are evaluated as 4.2 kΩ and 3.81 GΩ, respectively. These higher values of  $R_s$  and  $R_{sh}$  may be due to the deliberately deposited Ta<sub>2</sub>O<sub>5</sub> interlayer/interface states density ( $N_{ss}$ ) at the MS interface. Also, the  $R_s$  and  $N_{ss}$  are essential parameters in MIS SBDs, which affect the linearity of the  $I$ - $V$  characteristics, when the applied voltage is effectively high as shown in Fig. 4. The  $R_s$  is significant in the non-linear curve region at the high applied voltage in the forward bias  $I$ - $V$  characteristics. The main parameters such as ' $n$ ' and  $R_s$  can also be evaluated by Cheung and Cheung method [50]. The Cheung's function can be written as

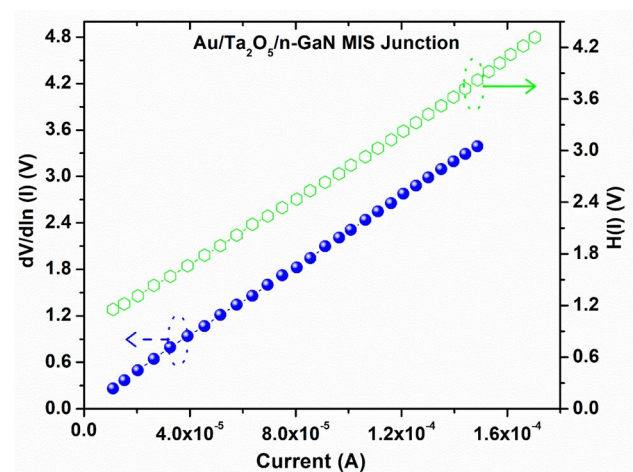
$$\frac{dV}{d(\ln I)} = IR_s + n \left( \frac{kT}{q} \right), \quad (5)$$

$$H(I) = V - \left( \frac{nkT}{q} \right) \ln \left( \frac{I}{AA^*T^2} \right), \quad (6)$$

and  $H(I)$  is represented as

$$H(I) = n\Phi_{bo} + IR_s. \quad (7)$$

The  $dV/d(\ln I)$  versus  $I$  curve for Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD is illustrated in Fig. 8. The plot should produce a



**Fig. 8** Plot of  $dV/d\ln(I)$  and  $H(I)$  versus  $I$  for the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction

straight line for the non-linear section of forward bias  $I$ - $V$  characteristics. The ' $R_s$ ' and ' $n$ ' values are calculated from slope and intercept of the plot as shown in Fig. 8. The extracted  $R_s$  and ' $n$ ' values for Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD are 22.6 kΩ and 1.30, respectively. The  $H(I)$  versus  $I$  plot for Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD at 300 K is also shown in Fig. 8. According to Eq. (7), Fig. 8 also be a straight line with intercept (y-axis) equal to  $\Phi_b$  results. The calculated  $\Phi_b$  and  $R_s$  values were 0.88 eV and 19.7 kΩ, respectively. The  $R_s$  values acquired from  $H(I)$  versus  $I$  plot are consistent with the  $dV/d(\ln I)$  plot which signifies the reliability of the Cheung's methodology.

To calculate consistent  $\Phi_{bo}$  and  $R_s$  values of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD, an alternate method was developed by Norde and Bohlin [51, 52]. Usually, the  $n$  values lie between 1 and 2; the function  $F(V)$  can be expressed as

$$F(V) = \frac{V}{2} - \frac{KT}{q} \ln \left( \frac{I(V)}{AA^*T^2} \right). \quad (8)$$

The current ( $I_0$ ) corresponds to minimum of  $F(V)$  versus  $V$  plot and  $R_s$  can be extracted using [39]

$$R_s = \frac{kT}{qI_0}, \quad (9)$$

and  $\Phi_{bo}$  can be extracted using

$$\Phi_{bo} = F(V_{\min}) + \frac{V_{\min}}{2} - \frac{KT}{q}, \quad (10)$$

where  $F(V_{\min})$  and  $V_{\min}$  are the values of  $F(V)$  and  $V$  conforming to the least current ( $I_0$ ) values. The modified Norde function can be written as [39]

$$F(V) = \frac{V}{\gamma} - \frac{KT}{q} \ln \left( \frac{I(V)}{AA^*T^2} \right). \quad (11)$$

Meanwhile, the ‘ $n$ ’ value lies between 1 and 2; therefore,  $\gamma=2$  ( $>1$ ). Then the  $\Phi_b$  and  $R_s$  values are calculated using the following equations [39]:

$$R_s = \frac{kT(\gamma - n)}{qI_{\min}}, \quad (12)$$

$$\Phi_{bo} = F(V_{\min}) + \frac{V_{\min}}{\gamma} - \frac{kT}{q}. \quad (13)$$

The  $F(V)$  versus  $V$  plot for the fabricated Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD is shown in Fig. 9. The estimated  $\Phi_{bo}$  and  $R_s$  values are 0.85 eV and 96 M $\Omega$ . The calculated  $\Phi_{bo}$  values from the Norde method demonstrate good agreement with the  $\Phi_{bo}$  value calculated using  $I$ – $V$  method. But the calculated  $R_s$  values from Norde method are higher compared to the Cheung’s function. This is owing to the fact that the Cheung’s method is applied only to the non-linear region of  $I$ – $V$  characteristics whereas in Norde method, the fitting is made to the entire forward bias region of the  $I$ – $V$  curves of the fabricated MIS SBD.

To calculate ‘ $n$ ’ and ‘ $\Phi_{bo}$ ’ values, a new method was developed by Hernandez et al. [53] from the homogeneous non-ideal  $I$ – $V$  plot. Voltage-dependent properties of the ‘ $n$ ’ and  $\Phi_b$  can be conveyed with a voltage-dependent function as [39]

$$Z(V, T)_i = \frac{kT}{q} \left[ \ln \left( \frac{I_i}{AA^*T^2 [1 - \exp(-qV_d/kT)]} \right) \right] \quad (14)$$

$$\text{and } Z(V, T)_i = -\Phi_{bo}(V, T)_i + \frac{V_d}{n_o(V, T)_i}. \quad (15)$$

Using Fig. 10, the voltage-dependent ‘ $n$ ’ and  $\Phi_b$  values were calculated as 1.32 and 0.89 eV, respectively.

For huge values of  $R_s$  and interface state densities ( $N_{ss}$ ), the logarithmic  $I$ – $V$  plot becomes non-linear as shown in Fig. 4. This factor limits the evaluation of saturation current ( $I_0$ ) from fitting; hence, the calculated values of  $\Phi_{bo}$  using  $I_0$  are not reliable. To avoid this limitation, Chattopadhyay [54] developed a model to evaluate the surface potential ( $\Psi_s$ ) and it can be expressed as

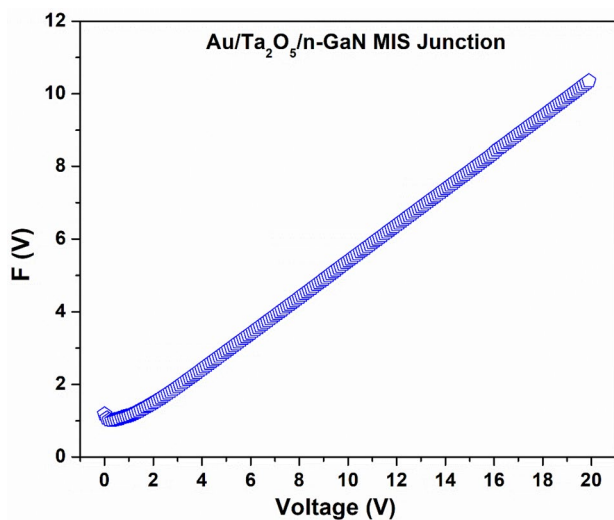
$$\Psi_s = \frac{kT}{q} \ln \left( \frac{AA^*T^2}{I} \right) - V_n. \quad (16)$$

Using this method,  $\Phi_{bo}$  and  $n$  values can be evaluated from [29, 55]

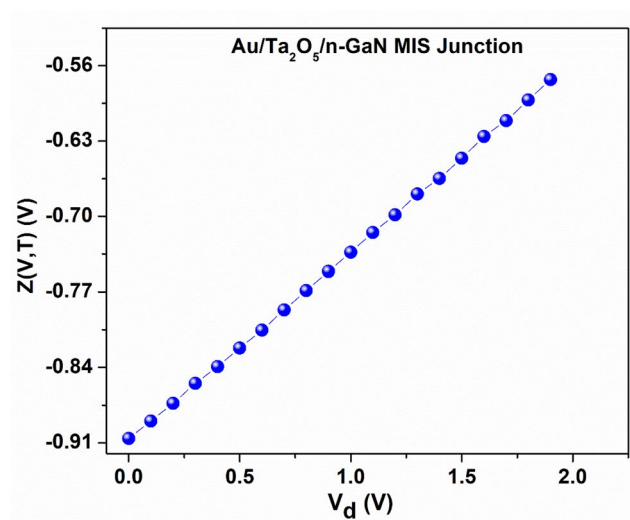
$$\Phi_{bo} = \Psi_s(I_C, V_C) + C_2 V_C + V_n. \quad (17)$$

$$C_2 = \frac{1}{n} = - \left( \frac{d\Psi_s}{dV} \right)_{I_C, V_C}. \quad (18)$$

Using Eqs. (17) and (18), the ‘ $\Phi_{bo}$ ’, ‘ $n$ ’ values of the MIS SBD were found to be 0.82 eV and 1.28, respectively. ‘ $\Phi_{bo}$ ’ and ‘ $n$ ’ values attained from the  $\Psi_s$  versus  $V$  plot (Fig. 11) were consistent with those calculated from the forward-bias ( $I$ – $V$ ) and  $Z(V, T)_i$  versus  $V$  plots of the prepared Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD. Thus, consequently, the methods employed here have shown effective and good consistence with each other. The reason for this can be ascribed to the insertion of Ta<sub>2</sub>O<sub>5</sub> oxide layer at the MS



**Fig. 9** Modified  $F(V)$  versus  $V$  plot for the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction



**Fig. 10** The plot of  $Z(V, T)_i$  versus  $V_d$  for the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction

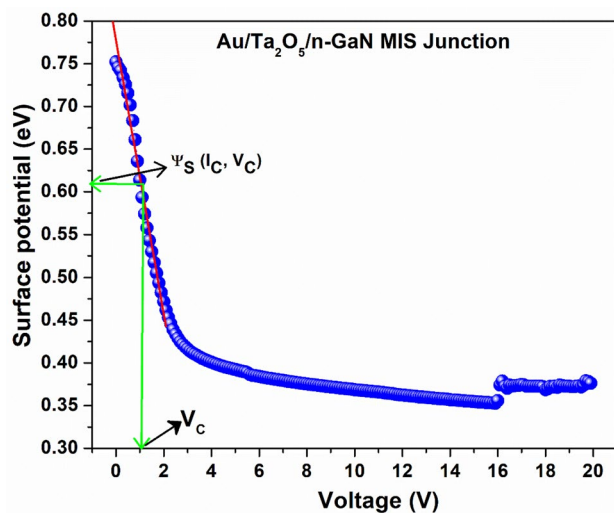


Fig. 11 Surface potential versus forward bias voltage characteristics of the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction

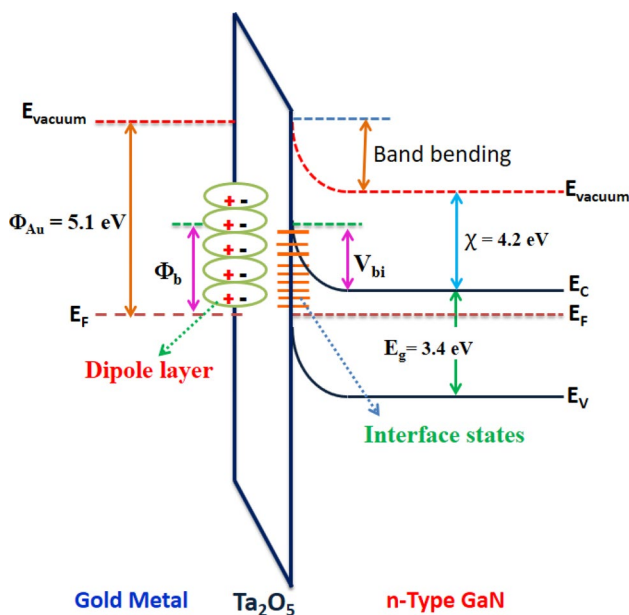


Fig. 12 Energy band diagram of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction

interface. Figure 12 elucidates the energy level band diagram of the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junctions with interfacial layer indicating work function of Au metal, electron affinity/energy gap of GaN and the resulting band bending after the contact has been made. As can be seen from Fig. 12, the SBH ( $\Phi_{b0}$ ) is defined as the potential difference between the Fermi level and the conduction band edge of GaN. However, the effective  $\Phi_{b0}$  is influenced by some non-idealities such as image-force effect and surface states related to native oxide interface which can affect the semiconductors surface potential [33, 34].

Figure 13 denotes the current transport mechanism (CTM) in the forward-bias Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction. The  $\log(I)$  versus  $\log(V)$  shows different linear regions (I, II, and III) yielding three different slopes. In Region-I, the calculated slope value is 1.68 which is close to unity indicating ohmic behaviour. The reason for this may be due to silicon doping to GaN and/or carriers which were created thermally [56]. The slope value estimated in the region-II was 5.63 which is higher than 2 may be attributable to the space-charge-limited current (SCLC) by way of presence of isolated trapping levels in GaN layer as well as in high- $k$  Ta<sub>2</sub>O<sub>5</sub> layer. When fitting was made in region-III, the value of slope decreases to 2.57 indicating that the prepared MIS SBD reaching the trap-filling limit [57, 58]. This analysis leads to the conclusion that there is clear transition in the carrier transport mechanism at the interfaces of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN as a function of applied voltage.

To know the current conduction mechanisms that are taking place in the extracted reverse-bias  $I$ - $V$  characteristics of the fabricated Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction,  $\ln(I_R)$  versus  $V_R^{1/2}$  plot was made and is shown in Fig. 14. This plot allows one to know whether Poole-Frenkel emission (PFE) or Schottky emission (SE) conduction mechanisms is taking place in the extracted reverse-bias  $I$ - $V$  curves of the fabricated device. In the reverse bias, if the current is dominated by PFE mechanism which can be expressed as [59]

$$I_R = I_0 \exp\left(\frac{\beta_{PF} V^{1/2}}{kTd^{1/2}}\right), \quad (19)$$

and the SE mechanism is defined as

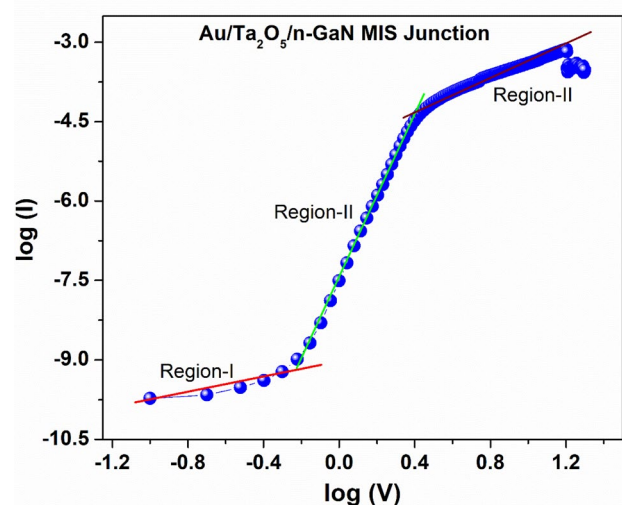
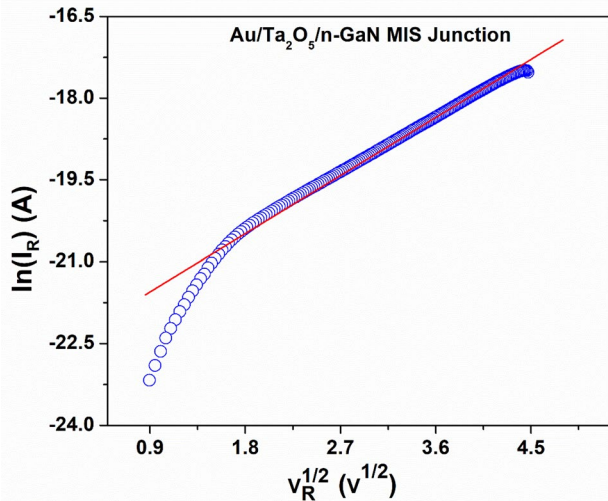


Fig. 13 The forward bias  $\log(I)$  versus  $\log(V)$  plot for the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction





**Fig. 14** Plot of  $\ln(I_R)$  versus  $V_R^{1/2}$  for the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction

$$I_R = AA^*T^2 \exp\left(\frac{-\Phi_{bo}}{kT}\right) \exp\left(\frac{\beta_{SC} V_R^{1/2}}{kTd^{1/2}}\right), \quad (20)$$

where ‘ $d$ ’ is the thickness of the film,  $\beta_{PF}$  is PFE and  $\beta_{SC}$  is SE field lowering coefficients, respectively. Further, the theoretical values for  $\beta_{PF}$  and  $\beta_{SC}$  can be written as

$$2\beta_{SC} = \beta_{PF} = \left(\frac{q^3}{\pi\epsilon_0\epsilon_r}\right)^{1/2}, \quad (21)$$

where  $q$ ,  $\epsilon_0$  and  $\epsilon_r$  are the electric charge, relative permittivity of free space and semiconductor, respectively. Usually, the value of  $\beta_{PF}$  is twice the value of  $\beta_{SC}$ . The estimated theoretical values of  $\beta_{PF}$  and  $\beta_{SC}$  are  $1.51 \times 10^{-5}$  and  $7.58 \times 10^{-6}$  eVm<sup>1/2</sup> V<sup>-1/2</sup>, respectively, for the Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBDs. As shown in Fig. 14, the linear fitting in the plot of  $\ln(I_R)$  versus  $(V_R)^{1/2}$  confirms a linear relationship which demonstrate that the reverse current being dominated by PFE. The linear fitting to the  $\ln(I_R)$  versus  $(V_R)^{1/2}$  curve yielded the slope value of  $4.54 \times 10^{-5}$  eVm<sup>1/2</sup> V<sup>-1/2</sup> for the prepared MIS SBD. The experimentally calculated  $\beta_{PF}$  value of  $4.54 \times 10^{-5}$  eVm<sup>1/2</sup> V<sup>-1/2</sup> from the slope is approximately closer to the theoretical value calculated for PFE mechanism, i.e.  $1.51 \times 10^{-5}$  eVm<sup>1/2</sup> V<sup>-1/2</sup>. Consequently, these results suggest that the PFE transport mechanism is governing the reverse leakage current in the prepared MIS SBD device. In the case of the PFE conduction mechanism, the theoretical

and experimentally calculated values are not in very close agreements and this is due to the facts such as the existence of trap states in the bandgap of Ta<sub>2</sub>O<sub>5</sub> insulating layer and structural defects with high density which enhances the trap levels/charge carriers de-trapping at the interfaces of the prepared MIS SBD devices [60, 61]. All the extracted Schottky barrier parameters using different methods from Figs. 4–14 were compared with the previously reported values in the literature [62–69] and tabulated in Table 2.

## 4 Conclusions

In summary, the Ta<sub>2</sub>O<sub>5</sub> interlayer was deposited using e-beam evaporation technique onto n-type GaN. Electrical parameters of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junctions have been discussed using  $I$ – $V$  measurements with voltage range  $\pm 20$  V. Statistical distribution study was used to evaluate the average  $n$  and SBH values by fitting the Gaussian distribution function and the corresponding resulted values are 0.85 eV with a normal deviation of 0.00181 eV and 1.36 with normal deviation of 0.00562, respectively, for the MIS SBD heterojunction. The  $R_s$  and  $R_{sh}$  values are also determined from  $I$ – $V$  curves and the values are 4.2 k $\Omega$  and 3.81 G $\Omega$ , respectively. The electrical properties have been evaluated with diverse methods such as Rhoderick’s, Cheung’s, Modified Norde’s, Hernandez’s and Chattopadhyay’s. The ‘ $n$ ’ values are extracted using Cheung’s and Chattopadhyay’s method is close to unity (1), while this value is nearly  $> 2$  by Rhoderick’s and Hernandez’s methods. The results revealed that the calculated SBH values obtained from forward bias  $I$ – $V$  curves through different methods are almost consistent with each other. From the forward-bias  $I$ – $V$  curves of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS junction, conduction mechanisms such as ohmic is found to be active in the low-voltage regime whereas SCLC at high voltage regimes, respectively. Furthermore, reverse  $I$ – $V$  characteristics interpreted that PFE conduction mechanism is dominant in the fabricated Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS heterojunction. To conclude, the betterment in rectification ratio, SBHs and good fitting of experimental data to equations of different methods were ascribed to the facts of deliberately deposited Ta<sub>2</sub>O<sub>5</sub> and undoped GaN buffer layers in the fabricated Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD heterojunction.

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**Table 2.** Different Schottky barrier parameters acquired from the  $I$ – $V$  characteristics of Au/Ta<sub>2</sub>O<sub>5</sub>/n-GaN MIS SBD in the present work and comparison with the previously reported MIS SBD structures in the literature

Barrier parameters	$I$ – $V$ measurements	statistical analysis average values	Cheung’s functions $dV/d(\ln I)$ versus $I$	$H(I)$ versus $I$	Norde plot	$\Psi_S$ – $V$ plot	$Z(V, T)_i$ – $V$ plot					
Leakage current	$1.467 \times 10^{-10}$		–	–	–	–	–					
Barrier height (eV)	$0.87 \pm 0.01$	$0.85 \pm 0.01$	–	$0.88 \pm 2.0E-16$	$0.85 \pm 0.01$	$0.82 \pm 6E-17$	$0.89 \pm 6E-4$					
Ideality factor ( $n$ )	$1.29 \pm 0.01$	$1.35 \pm 0.01$	1.30	–	–	1.28	$1.32 \pm 0.02$					
Series resistance ( $\Omega$ )	4.2E3	–	$22.6E3 \pm 2.2E-12$	$19.7E3 \pm 1.9E-12$	96.2E6	–	–					
Shunt resistance ( $\Omega$ )	3.81E9	–	–	–	–	–	–					
Comparison with the literature												
Ref. no.	From $I$ – $V$		Cheung’s functions				Norde		$\Psi_S$ – $V$ plot		$Z(V, T)_i$ – $V$ plot	
			$dV/d(\ln I)$ – $I$		$H(I)$ – $I$							
	$\Phi_{bo}$ (eV)	$n$	$R_S$	$n$	$\Phi_{bo}$ (eV)	$R_S$	$\Phi_{bo}$ (eV)	$R_S$	$\Phi_{bo}$ (eV)	$n$	$\Phi_{bo}$ (eV)	$n$
[62]	0.63	1.3	–	–	–	–	–	–	–	–	–	–
[63]	–	3.12	27.9 k $\Omega$	3.19	0.76	–	0.85	–	–	–	–	–
[64]	0.85	1.03	–	–	–	–	0.93	–	0.89	1.83	0.89	1.96
[65]	0.71	1.22	1.58 k $\Omega$	1.31	0.30	1.41 k $\Omega$	0.75	0.94 k $\Omega$	0.71	1.22	0.76	1.24
[66]	0.36	3.86	42.9 $\Omega$	4	0.41	4	0.44	42 $\Omega$	0.40	3.65	0.39	4.5
[67]	0.80	1.39	436.8 k $\Omega$	2.70	0.76	454 k $\Omega$	0.79	14.2 M $\Omega$	0.79	1.37	0.79	1.66
[68]	0.65	3.44	21.49 $\Omega$	–	–	32.56 $\Omega$	–	–	–	–	–	–
[69]	0.73	1.65	974.6 $\Omega$	1.91	0.62	911 $\Omega$	–	–	–	–	–	–

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