



# The effect of radiation on the forward and reverse bias current–voltage ( $I$ – $V$ ) characteristics of $\text{Au}/(\text{Bi}_4\text{Ti}_3\text{O}_{12}/\text{SiO}_2)/n\text{-Si}$ (MFIS) structures

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## Abstract

Determining the radiation effects on the basic electrical parameters of the fabricated high-dielectric MFIS structures, they were exposed to the high-energy  $^{60}\text{Co}$   $\gamma$ -rays. For this purpose, the values of ideality factor ( $n$ ), barrier height ( $\Phi_B$ ) and series resistance ( $R_s$ ) were extracted from the forward bias  $I$ – $V$  data before and after irradiation by using various methods such as standard thermionic emission (TE) theory, Cheung's and Norde functions. Additionally, the energy-dependent profile of surface states  $N_{ss}$  was extracted by considering voltage dependence of  $n$ ,  $\Phi_B$  and  $R_s$  and compared each other. Experimental results show that the reverse saturation current ( $I_0$ ),  $n$  and  $R_s$  values increase with increasing radiation dose, but  $\Phi_B$  decreases. When the value of  $R_s$  is considered in the calculation of  $N_{ss}$ , they were found to be considerably decreased. The observed low discrepancies between  $N_{ss}$  after irradiation show that the use of a high-dielectric ferroelectric interlayer leads to an increase in the resistance of MS to radiation. It is more important to fabricate radiation-resisted electronic device, especially in the satellites due to hard radiation in space. As a result,  $N_{ss}$ ,  $R_s$  and the existence of interlayer are more effectual on the  $I$ – $V$  characteristics which must be considered in the electrical parameter calculation.

## 1 Introduction

The bismuth titanite ( $\text{Bi}_4\text{Ti}_3\text{O}_{12}$ ) is a high-dielectric ferroelectric materials such as barium oxide ( $\text{BaTiO}_3$ ) and strontium oxide ( $\text{SrTiO}_3$ ) and it has high-charge storage capacity/energy, wide bandgap ( $E_g$ ), high breakdown strength, low coercive field, high Curie temperature (675 °C) and peculiar switching behavior [1–5]. Therefore,  $\text{Bi}_4\text{Ti}_3\text{O}_{12}$  (BTO), which is belonging to Aurivillius family, has attracted

significant interest in the applications of devices such as optical and electro-optic devices, ferroelectric field-effect transistors (FeFETs), nonvolatile ferroelectric random-access memories (FeRAMs) and memory storage capacitors (MSCs) [6–8]. Among bismuth-layer-structure ferroelectrics,  $\text{Bi}_4\text{Ti}_3\text{O}_{12}$  films are the simplest, environment friendly and prominent compound. They are particularly attractive due to the high-speed transistor-based nonvolatile memories and nature of high densities [4–8]. FeRAMs have a wide operating temperature range, superior speed performance, high information density, the ability to serve in harsh environments and limitless write-to-read cycles [9, 10]. In addition, a metal-ferroelectric-metal (MFM)-type capacitor has been studied for many years to form FeRAMs.

In order to avoid interface diffusion between the semiconductor and ferroelectric layer, a thin insulator layer like  $\text{Si}_3\text{N}_4$ ,  $\text{SnO}_2$  and also  $\text{SiO}_2$  is inserted at the BTO/Si interlayer [11, 12]. In the light of the above-mentioned information, MFS type is evolved into a metal-ferroelectric-insulator-semiconductor (MFIS)-type structure. Thanks to this thin layer, the electric field reducing problem in the MFIS structure is decreased, while the reaction and interdiffusion between the ferroelectric layer and the semiconductor is prevented. The  $\text{SiO}_2$  is a stable and promising structure,

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especially with the ability to regulate load transitions, prevent internal diffusion and reduction in electric field, and precisely control the gate potential from the FET channel. Thanks to these features, in this study,  $\text{SiO}_2$  was preferred as an insulator layer in MFIS structures. However, the magnitude of the applied bias reduction caused by interlayer depends on the capacitance ratio of the BTO film and the interlayer.

In an MFIS structure, the metal and semiconductor are separated by an interlayer and the distribution of  $N_{ss}$  at the semiconductor/interlayer interface is continuous. For the electrical behavior of a metal–insulator/ferroelectric-semiconductor (MIS/MFS) and MFIS structures,  $R_s$  and  $N_{ss}$  are important parameters affecting these structures [13–31]. Although the main parameters of these structures have been studied under different conditions extensively, the irradiation effect on them has not been identified yet. For this reason, the identification of the irradiation effect on main electrical parameters at various irradiation doses is the goal of this study. Even though many methods have been developed for the determination of the after-irradiation behavior of interband radiation-induced of  $N_{ss}$  at the MIS type, Ma [32, 33], Winokur et al. [34], Da Silva et al. [35] and Tataroğlu et al. [36, 37] were among the pioneers who made systematic observations. Permanent and temporary effects of irradiation, which cause changes in crystal lattices, occur due to bombardment of the devices by irradiation and the generation of an electron–hole pair, respectively [38]. The radiation-generated holes which are less mobile than the electrons may diffuse in the interlayer, and also many stationary hole traps are existing.

In our previous studies [2, 8, 16, 18, 30, 31], both electrical and dielectric properties of the fabricated Al/p-Si and Au/n-Si (MS) SBDs with a thin high-dielectric  $\text{Bi}_4\text{Ti}_3\text{O}_{12}$  (BTO) interfacial layer have been investigated as function of frequency, temperature and voltage in detail. All these results have confirmed that the use of such high-dielectric interlayer leads to an increase in the performance of MS-type SBDs in respect of low series resistance ( $R_s$ ), low surface states ( $N_{ss}$ ), low leakage current, high capacitance, and hence can have more storage electrons or energy like an ultra-capacitor. Similarly, Yıldırım et al. for Au/ $\text{Bi}_3\text{Ti}_4\text{O}_{12}$ /n-Si [14] and Reddy et al. [5] for Au/ $\text{BaTiO}_3$ /n-GaN MIS-type structures show that MIS-type structure has a higher rectification rate with low reverse saturation current and surface states. Additionally, Çetinkaya et al. [2, 18] show that both the electrical and dielectric of these SBDs may be changed from one diode to another even at identically fabricated of them. Therefore, radiation dependence of electrical characteristics has been investigated in this study by using forward and reverse bias  $I$ – $V$  measurements before and after gamma radiation. Radiation-dependent capacitance–voltage ( $C$ – $V$ ) and conductance–voltage ( $G/\omega$ – $V$ ) characteristics of these

SBDs are also under our investigation and will be published soon, as the second part of this study.

The main purpose of this study is to achieve a better understanding of irradiation effect on main electrical parameters ( $I_0$ ,  $n$ ,  $\Phi_B$ ,  $R_s$ ) by measuring the forward bias  $I$ – $V$  measurements. Detailed analysis of the Au/( $\text{Bi}_4\text{Ti}_3\text{O}_{12}$ /SiO<sub>2</sub>)/n-Si structure, exposed to the maximum cumulative dose of 22 kGy at room temperature, was reported. Also, the  $N_{ss} - (E_c - E_{ss})$  profile of structure were extracted by considering voltage dependence of  $n$ ,  $\Phi_B$  and  $R_s$  and comparing each other. Experimental data indicate that the basic electrical parameters are extremely dependent on radiation dose.

## 2 Experimental procedures

Au/( $\text{Bi}_4\text{Ti}_3\text{O}_{12}$ /SiO<sub>2</sub>)/n-Si structures were performed on the phosphor-doped (n-Si) wafer with (100) direction, 0.7  $\Omega$  cm resistivity, 300  $\mu\text{m}$  thickness and 5.08 cm diameter. In the first stage, organic solvents ( $\text{CHCl}_3$ ,  $\text{CH}_3\text{COCH}$  and  $\text{CH}_3\text{OH}$ ) were used for degreasing of n-Si wafer. Later, n-Si wafer was etched in a sequence of  $\text{H}_2\text{SO}_4$ ,  $\text{H}_2\text{O}_2$ , 20% HF, a solution of  $6\text{HNO}_3$ :1HF:35 $\text{H}_2\text{O}$ , 20% HF. During surface cleaning of n-Si wafer, at each step, the wafer was rinsed in ultrapure deionized water (DW) having resistivity of 18  $\text{M}\Omega$  cm at about 10 min. In the second stage, n-Si wafer was transferred into high-vacuum thermal evaporation system. Here, it was deposited with 99.999% purity Au layer at 1  $\mu\text{Torr}$  and then annealed at 550  $^\circ\text{C}$  in nitrogen ambient with a flow rate of 2 l/min at for 20 min to get good ohmic contact. Thirdly, n-Si wafer was taken into RF magnetron sputtering device where it was deposited with  $\text{Bi}_4\text{Ti}_3\text{O}_{12}$  (BTO) ferroelectric film by using a hot compacting of BTO powder of a stoichiometric composition as a target material.

A Veeco Dektak 6 M thickness profilometer was utilized for measuring thickness of interfacial BTO layer as 2.4 nm [16, 30, 31]. Ar and O<sub>2</sub> gases' mixture was used as a working medium and the structure was kept at 700  $^\circ\text{C}$  for settling. The thin layer of SiO<sub>2</sub> at the BTO/Si interface was assumed to grow during annealing of the BTO films in air ambient. Finally, the ( $\text{Bi}_4\text{Ti}_3\text{O}_{12}$ /SiO<sub>2</sub>/n-Si/Au) sample was immediately transferred into thermal evaporation system and then Au rectifier contacts were thermally evaporated onto  $\text{Bi}_4\text{Ti}_3\text{O}_{12}$  film with the help of a mask with 1 mm diameter. Thus, the formation of the MFIS structure was completed and its schematic diagram is given in Fig. 1. The  $I$ – $V$  measurements of the MFIS structures were completed by using Keithley 2400  $I$ – $V$  source meter. The measurements were carried out before and after  $^{60}\text{Co}$  ( $\gamma$ -ray) source irradiation with the dose of 2.12 kGy/h and total dose range was 0–22 kGy.

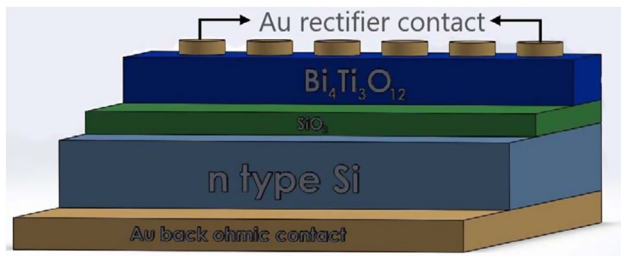


Fig. 1 The schematic presentation of the structure

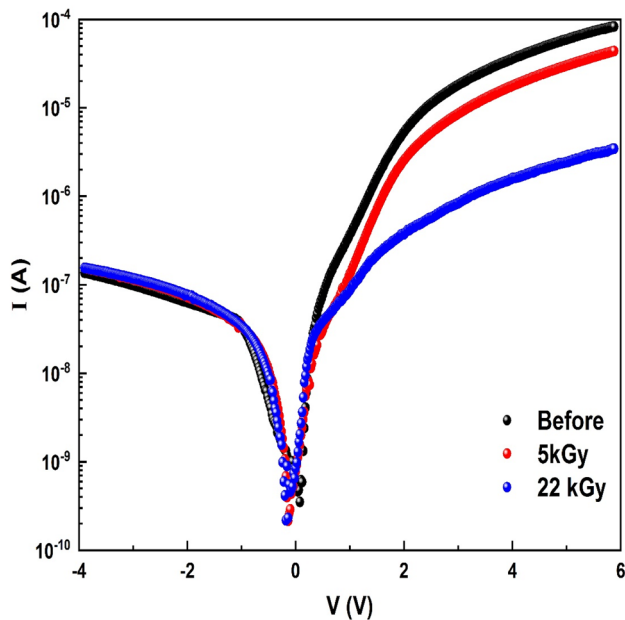


Fig. 2  $I$ – $V$  graphs of the structure

### 3 Results and discussion

It is generally known that radiation has two important effects on materials that we can classify permanently and temporarily [39]. If deterioration occurs due to radiation effects in crystal lattices, which have great importance, permanent effects can be seen in the structures. Also, temporary effects may occur due to the generation of an electron–hole pair. To understand these effects in detail, the radiation impact on the

$I$ – $V$  characteristics in MFIS structures has been investigated.  $I$ – $V$  measurements were performed before radiation and after various radiation doses which consist of 5 kGy, 22 kGy. Forward and reverse bias  $I$ – $V$  data of the structure, before and after  $\gamma$ -ray irradiation from  $^{60}\text{Co}$  gamma source, and measurements of which were carried out between  $-4/+6$  V, are presented in Fig. 2.  $I$  vs  $V$  plots of Au/ $\text{Bi}_4\text{Ti}_3\text{O}_{12}$ / $\text{SiO}_2$ / $n$ -Si (MFIS) structures have two distinct linear regions with different slopes as clearly seen from Fig. 2. The first linear region is expressed as Region I in the 0.12–0.38 V voltage range and the second linear region is expressed as Region II in the 0.40–0.80 V. Double parallel diode model can be utilized to explain such multi-linear regions. As tabulated in Table 1, related with irradiation, three main parameters ( $\Phi_{\text{Bo}}$ ,  $I_0$  and  $n$ ) of the structure for both Region I and Region II were acquired. Although the increase of the radiation dose to 22 kGy decreased the forward current value, it had no effect on the reverse bias current.

The correlation between current and applied forward biases can be written due to the thermionic emission (TE) as [40]

$$I = I_{o1} \left\{ \exp \left( \frac{q(V - IR_s)}{n_1 kT} \right) - 1 \right\} + I_{o2} \left\{ \exp \left( \frac{q(V - IR_s)}{n_2 kT} \right) - 1 \right\} + \frac{V - IR_s}{R_{sh}} \quad (1)$$

In the formula, reverse saturation currents, Region I and Region II ideality factors and series and shunt resistors are shown with  $I_{o1}$  and  $I_{o2}$ ,  $n_1$  and  $n_2$  and  $R_s$  and  $R_{sh}$ , respectively. Besides,  $IR_s$  corresponds to the voltage drop on the  $R_s$ . Moreover, the components of diffusion and recombination generation currents were depicted by the first and second terms in Eq. 1, respectively. In Eq. 1, the terms of  $I_{o1}$  and  $I_{o2}$  can be extracted from the straight-lines intercept of  $\ln(I)$ – $V$  plots at zero bias and can be expressed as:

$$I_{o1} = AA^* T^2 \exp \left( -\frac{q\Phi_{\text{Bo1}}}{kT} \right) \quad I_{o2} = AA^* T^2 \exp \left( -\frac{q\Phi_{\text{Bo2}}}{kT} \right), \quad (2)$$

where the quantities  $A^*$  and  $A$  are the effective Richardson constant ( $120 \text{ A/cm}^2 \text{ K}^2$  for  $n$ -type Si) and the rectifier contact area ( $7.85 \times 10^{-3} \text{ cm}^2$ ), respectively. Two linear regions

Table 1 The basic electrical parameters of the structure

	Region I			Region II			Ohm's law	
	$I_{o1}$ (A)	$n_1$	$\Phi_{\text{Bo1}}$ (eV)	$I_{o2}$ (A)	$n_2$	$\Phi_{\text{Bo2}}$ (eV)	$R_{sh}$ ( $\Omega$ )	$R_s$ ( $\Omega$ )
Before	$2.15 \times 10^{-10}$	2.63	0.839	$1.21 \times 10^{-8}$	10.89	0.738	$2.82 \times 10^7$	$7.20 \times 10^4$
5 kGy	$1.14 \times 10^{-9}$	5.04	0.797	$7.75 \times 10^{-9}$	14.25	0.749	$2.50 \times 10^7$	$1.30 \times 10^5$
22 kGy	$2.25 \times 10^{-9}$	5.32	0.780	$1.65 \times 10^{-8}$	23.73	0.730	$2.51 \times 10^7$	$1.66 \times 10^6$

slope at forward biases were utilized to determine the  $n$  values of MFIS structures as follows:

$$n_1 = \frac{q}{kT \tan \theta_1} \quad n_2 = \frac{q}{kT \tan \theta_2}. \quad (3)$$

Thus, the value of  $\Phi_{Bo}$  can be obtained from Eq. 4 by using  $A$  and  $I_o$ ,

$$\Phi_{Bo1} = \frac{kT}{q} \ln \left( \frac{AA^*T^2}{I_{o1}} \right) \quad \Phi_{Bo2} = \frac{kT}{q} \ln \left( \frac{AA^*T^2}{I_{o2}} \right). \quad (4)$$

In order to analyze radiation effects in more detail, it is of great importance to calculate some basic parameters such as  $n$  and  $\Phi_{Bo}$ . Thus, the basic diode parameters calculated in the light of the equations given above are shown in Table 1.

As clearly seen from Table 1,  $I_o$  values increase after exposure of the structure to the with increasing radiation dose.  $I_o$  values for Region I changed from  $2.15 \times 10^{-10}$  to  $2.25 \times 10^{-9}$  and Region II  $1.21 \times 10^{-8}$  A to  $1.65 \times 10^{-8}$  A. This radiation-induced change observed in  $I_o$  value could be attributed to the interfacial defect density increment [39]. There is an inverse proportion between the barrier height and reverse saturation current.

Depending on increasing irradiation dose, a decrease in  $\Phi_{Bo}$  was observed. According to some previous studies,  $\gamma$ -irradiation affects the free carrier concentration as it induces imperfections in the bandgap at the junction of the semiconductor [41, 42]. That is why radiation is an important factor for the barrier height in the structures and the barrier height value in Region I is close to the barrier height value in Region II and the value in Region I is higher than the value in Region II. According to recent studies in this field, X-ray photoelectron spectroscopy analysis points out defect generation which reduced the barrier height and enhanced tunneling effects, in Si dangling bonds [43].

While the values of ideality factor  $n$  in the first region were found to range from 2.63 at 0 kGy (before irradiation) to 5.32 at 22 kGy (after irradiation), values of ideality factor  $n$  in the first region were found to range from 10.89 at 0 kGy to 23.73 at 22 kGy. Obviously, the  $n$  values depend on the applied biases as Region I values are much lower than Region II values. The barrier homogeneity and high  $N_{ss}$  density localized at the interlayer effects are seen as the cause of high values in Region II [1, 11, 14]. Other possible mechanisms that can lead to  $n$  values greater than unity can be listed as image force effect, recombination production and tunneling [41, 42]. The ideality factor, which increases in parallel with the increase in applied radiation doses, is evidence of the deviation from the standard TE theory.

With the dose of radiation, defect and noise ratios occur that affect the performance of the structures. One of the important factors affecting this performance is resistance values. Utilizing from Ohm's law ( $R_i = V_i/I_i$ ), the resistance

( $R_i$ ) of the Au/Bi<sub>4</sub>Ti<sub>3</sub>O<sub>12</sub>/SiO<sub>2</sub>/n-Si (MFIS) structure was calculated between  $-4$  V/6 V.  $R_i$  values are extremely depending on biases as presented in Fig. 3.  $R_i$  values correspond to  $R_{sh}$  and  $R_s$  for high negative biases and high positive biases, respectively.

According to Table 1, it was observed that  $R_{sh}$  values remained almost constant, while  $R_s$  values increased in parallel with the increase in irradiation doses. This increase in  $R_s$  value indicates that free carrier density and mobility are reduced [44]. The reason for the decrease in mobility is the settlement of the defect centers that serve as a reunification center together with irradiation. The free carrier density will decrease when deep traps settle inside the material in relation to the displacement of the point defects. The intensity of irradiation-induced defect (trap) centers increases. Thus, the free carriers in the crystal lattice are captured by the defect (trap) centers and, consequently, a decrease in the carrier density is observed.

Another way used to determine  $n$ ,  $\Phi_{B(\text{Cheung})}$  and  $R_s$  values is a method which was carried out from the functions developed by Cheung method [45]. Cheung functions are defined using Eq. 1 as follows:

$$\frac{dV}{d \ln(I)} = n \frac{kT}{q} + R_s I, \quad (5)$$

$$H(I) = V - n \frac{kT}{q} \ln \left( \frac{I}{AA^*T^2} \right) = n \Phi_{B(\text{Cheung})} + R_s I, \quad (6)$$

where  $\Phi_{B(\text{Cheung})}$  is the barrier height obtained from the intercept of  $H(I)$  vs  $I$  plots and  $IR_s$  is the voltage drop across the series resistance of MFIS structure. The  $dV/d \ln(I)$  and  $H(I)-I$  curves obtained with the Cheung functions have linear lines and  $R_s$  values are obtained from the slope of these

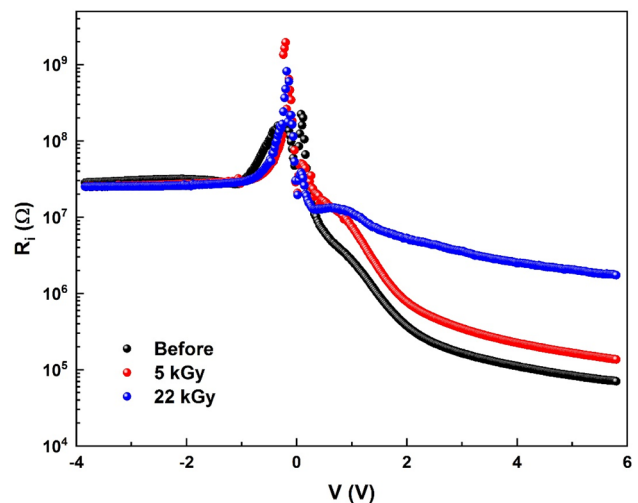


Fig. 3  $R_i$  characteristics of the structure

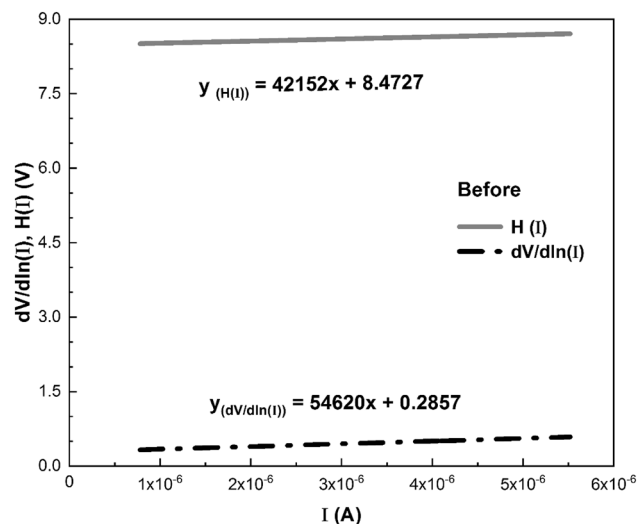


Fig. 4  $dV/d \ln(I)/H(I)-I$  plots of the structure for before radiation

lines before and after the irradiation of the structure. Cheung functions curves for MFIS structure are given in Fig. 4 for before radiation, Fig. 5 for 5 kGy and Fig. 6 for 22 kGy. All figures indicate that Cheung functions curves are linear lines.  $R_s$ ,  $n$  and  $\Phi_{B(\text{Cheung})}$  values curves are given in Table 2. As can be seen in Table 2, the obtained  $R_s$  values by Cheung functions are compatible with each other and increase with the increasing irradiation. The values of  $\Phi_{B(\text{Cheung})}$  were found to decrease, while the values of  $n$  increase with the increasing radiation dose ( $\Phi_{B(\text{Cheung})} = 0.740$  eV and  $n = 11.44$  at 0 kGy and  $\Phi_{B(\text{Cheung})} = 0.705$  eV and  $n = 26.80$  at 22 kGy).

On the other hand, as an alternative to the Cheung functions, another method can be also used presented by Norde to calculate some basic parameters [46]. Unlike Cheung

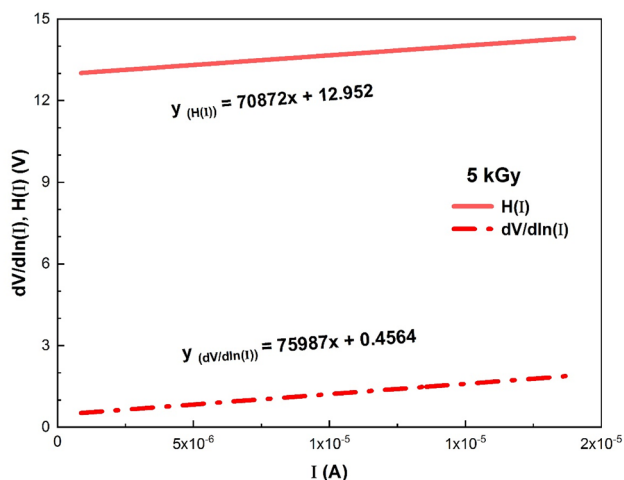


Fig. 5  $dV/d \ln(I)/H(I)-I$  plots of the structure for 5 kGy

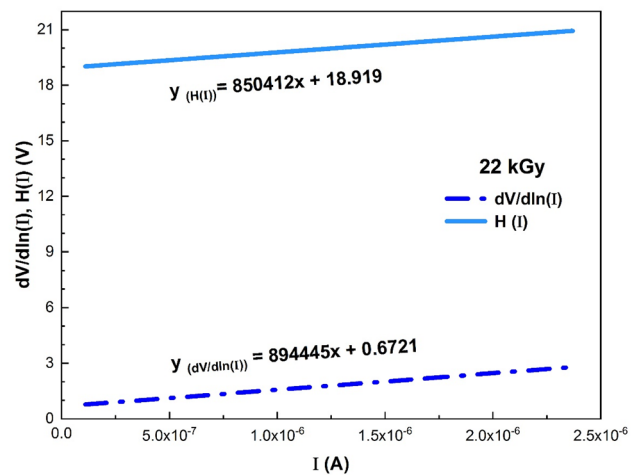


Fig. 6  $dV/d \ln(I)/H(I)-I$  plots of the structure for 22 kGy

functions, Norde function not only applied to the nonlinear region for the higher forward biases, but also applied to the full forward biases at  $I-V$  curve [47]. The modified Norde method is given as follows:

$$F(V) = \frac{V}{\gamma} - \frac{kT}{q} \ln \left( \frac{I}{AA^*T^2} \right), \quad (7)$$

where  $\gamma$  is the dimensionless value greater than the ideality factor which is extracted from the  $\ln(I)-V$  plots.  $\gamma$  values are 16.34 at before radiation, 19.96 at 5 kGy and 30.85 at 22 kGy. Using the minimum point of  $F(V)$  vs  $V$  plot,  $F(V_0)$ ,  $\Phi_{B(\text{Norde})}$  and  $R_s$  can be obtained from the following equations, respectively.

$$\Phi_{B(\text{Norde})} = F(V_0) + \frac{V_0}{\gamma} - \frac{kT}{q} \quad (8a)$$

$$R_s = \frac{(\gamma - n)kT}{qI_m}. \quad (8b)$$

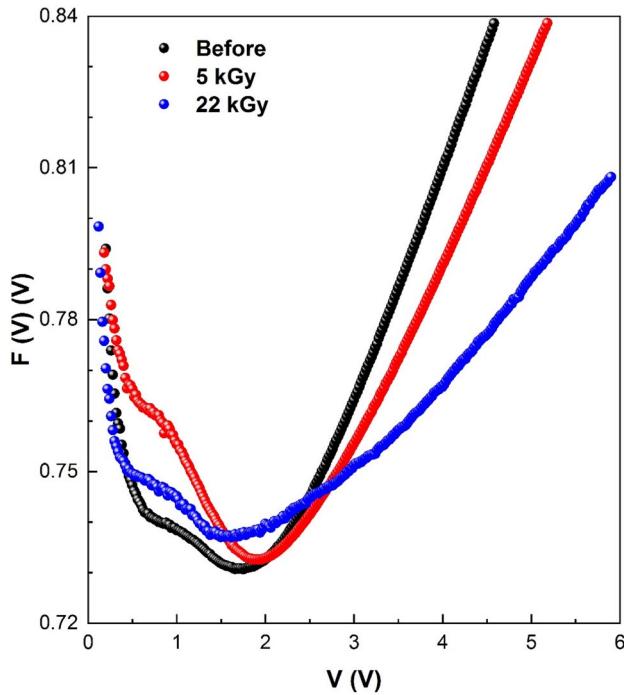
Figure 7 shows the  $F(V)$  vs  $V$  plots for the  $\text{Au/Bi}_4\text{Ti}_3\text{O}_{12}/\text{SiO}_2/n\text{-Si}$  (MFIS) structures. The values of  $\Phi_{B(\text{Norde})}$  and  $R_s$  acquired from Eqs. (8a) and (8b) under various irradiation conditions are presented in Table 2. The values of  $R_s$  calculated from Norde and Cheung methods are different from each other. As clearly seen in Table 2, the barrier height and series resistance values obtained from Norde theory are higher than those extracted from Cheung's functions. These variations in values acquired by using different methods may be result from the extraction in change regions of the  $I-V$  curves. Furthermore, as we mentioned above, there are differences in the basic parameters as the areas of application of the Norde and Cheung are different from each other.

Considering the voltage-dependent  $n(V)$  and effective barrier height ( $\Phi_e$ ),  $N_{ss}$  in equilibrium with the semiconductor



**Table 2** Basic electrical parameters of the structure obtained from Cheung and Norde functions

	$dV/d \ln(I) - I$		$H(I) - I$		Norde (Region I)		Norde (Region II)	
	$R_s (\Omega)$	$n$	$R_s (\Omega)$	$\Phi_{B(\text{Cheung})} (\text{eV})$	$R_s (\Omega)$	$\Phi_{B(\text{Norde})} (\text{eV})$	$R_s (\Omega)$	$\Phi_{B(\text{Norde})} (\text{eV})$
Before	$5.46 \times 10^4$	11.44	$4.22 \times 10^4$	0.740	$9.99 \times 10^5$	0.757	$4.65 \times 10^4$	0.813
5 kGy	$7.60 \times 10^4$	18.00	$7.09 \times 10^4$	0.722	$2.80 \times 10^6$	0.771	$7.03 \times 10^4$	0.803
22 kGy	$8.94 \times 10^5$	26.80	$8.50 \times 10^5$	0.705	$5.26 \times 10^6$	0.739	$5.26 \times 10^5$	0.765

**Fig. 7**  $F(V)$ - $V$  plots of the structure

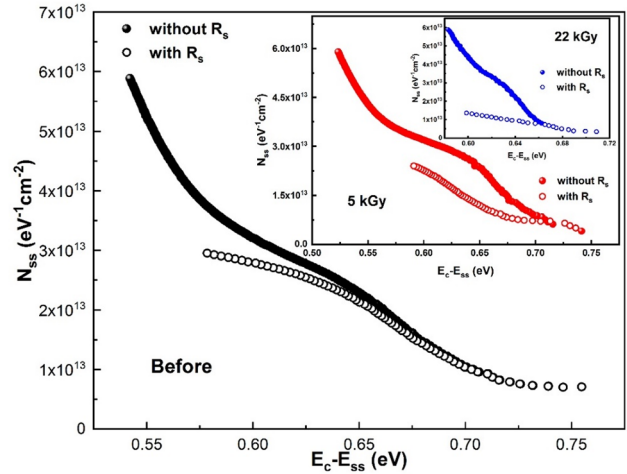
can be specified from the forward bias  $I$ - $V$  data [48]. Regardless of  $R_s$  values, the values of  $\Phi_e$  and  $n(V)$  can be calculated using Eqs. (9) and (10).  $\Phi_e$  is presumed to be voltage-dependent and derived by the following expression:

$$\Phi_e = \Phi_{Bo} + \beta(V - IR_s) = \Phi_{Bo} + \left(1 - \frac{1}{n(V)}\right)(V - IR_s). \quad (9)$$

Here the voltage coefficient of the  $\Phi_e$  is denoted by  $\beta$ . For MFIS structure, having the  $N_{ss}$  in equilibrium with semiconductor and voltage-dependent ideality factor is expressed as

$$n(V) = \frac{q}{kT} \left[ \frac{(V - IR_s)}{\ln(I/I_0)} \right] = 1 + \frac{\delta}{\epsilon_i} \left[ \frac{\epsilon_s}{W_D} + qN_{ss}(V) \right], \quad (10)$$

where the depletion layer width is denoted by  $W_D$  and the interlayer and semiconductor permittivities are denoted by  $\epsilon_i$  and  $\epsilon_s$ , respectively. This expression of  $n(V)$  is identical

**Fig. 8** The density of  $N_{ss}$  profiles as a function of  $(E_c - E_{ss})$ 

to Eq. 11 of Card and Rhoderick [49] and the expression for  $N_{ss}$  is converted to

$$N_{ss}(V) = \frac{1}{q} \left[ \frac{\epsilon_i}{\delta} (n(V) - 1) - \frac{\epsilon_s}{W_D} \right], \quad (11)$$

where  $\delta$  the interlayer thickness ( $\text{SiO}_2$ ) was obtained from the  $C$ - $V$  measured at 1 MHz in the strong accumulation region by using the  $C_{ox} = \epsilon_i \epsilon_0 A / \delta$  and found to be 41 Å in the previous study [16, 30, 31]. Then again, the interface states' energy,  $E_{ss}$ , to the conduction band's bottom,  $E_c$ , at the semiconductor's surface is derived by [50]

$$E_c - E_{ss} = q(\Phi_e - V). \quad (12)$$

The energy distribution profile of  $N_{ss}$  as a function of  $(E_c - E_{ss})$  was obtained from the forward bias  $I$ - $V$  characteristics by taking the bias dependence of the  $\Phi_e$  into account for each radiation dose. As seen in Fig. 8, the exponential growth of the  $N_{ss}$  from the with the semiconductor mid-gap toward the bottom of the conduction band is very apparent. The  $N_{ss}$  values extracted without considering the  $R_s$  are higher than those obtained taking into account the  $R_s$ . In addition, these decreases of interface states with increasing irradiation doses were attributed to the recombination of electron-hole pairs under the radiation and the existence

of an interlayer ( $\text{SiO}_2$ ) at MFIS interface. Hence,  $R_s$  must be considered in calculations of basic electrical parameters.

## 4 Conclusions

The forward and reverse bias  $I$ – $V$  characteristics of Au/ $\text{Bi}_4\text{Ti}_3\text{O}_{12}/\text{SiO}_2/n$ -Si (MFIS) structures exposed to  $^{60}\text{Co}$   $\gamma$ -irradiation of doses ranging from 0 to 22 kGy have been investigated at room temperature. While the forward current was detected to decrease with radiation dose increment, the irradiation effects on the reverse bias current were almost negligible. According to the experimental results, it was observed that the main electrical parameters such as  $I_0$ ,  $n$ ,  $\Phi_B$ ,  $R_s$  and  $R_{sh}$  values were strongly dependent on the irradiation effect. Among the main parameters which are exposed to increasing cumulative  $\gamma$ -ray doses, while the values of the ideality factor have an apparent increase, the values of zero-bias barrier height have a decrease. Growth in  $n$  values which increase with irradiation dose results from inhomogeneity of the interlayer and the presence of a thin insulating layer. On the other hand, another important parameter,  $R_s$ , was obtained by three different methods: Ohm's law, Cheung and Norde methods. Also, results obtained from these methods showed great compatibility with each other. The density of interface states ( $N_{ss}$ ) which was determined from the forward bias  $I$ – $V$  characteristics by considering the bias dependence of the  $\Phi_e$  and  $n$  decreases with radiation dose increment. Such a behavior of  $N_{ss}$  was attributed to the decrease in the recombination centers and because of the irradiation and reordering/restructuring of the bandgap surface states. In conclusion, the irradiation-dependent  $I$ – $V$  characteristics affirmed that  $R_s$  and  $N_{ss}$  are significant parameters that considerably affect the electrical qualifications of MFIS structures.

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