

# Degradation and Recovery of *n*-Type Multi-Crystalline Silicon Under Illuminated and Dark Annealing Conditions at Moderate Temperatures

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**Abstract**—Recently, an *n*-type multi-crystalline silicon (mc-Si) was observed to be susceptible to degradation under illumination at elevated temperatures with similarities to carrier-induced degradation in *p*-type mc-Si. In this study, we demonstrate degradation and regeneration of the effective lifetime of non-diffused *n*-type mc-Si wafers using illuminated and dark annealing conditions at moderate temperatures. Under illuminated annealing conditions, the degradation and regeneration rates of the *n*-type mc-Si are observed to be slower than those of the *p*-type mc-Si; however, the opposite trend was observed under dark annealing conditions. The carrier-induced degradation kinetics of the *n*-type wafers can be described by degradation and regeneration that occur simultaneously, and the activation energies have been identified to be  $1.23 \pm 0.16$  eV for the degradation process and  $1.34 \pm 0.08$  eV for the regeneration. Surprisingly, no degradation was observed in *n*-type mc-Si under dark annealing above 160 °C. Rather, at these conditions, a two-stage improvement in the lifetime was observed. Although degradation occurs after a subsequent laser treatment, the stable lifetime at the end of the degradation is still slightly higher than its initial value.

**Index Terms**—Degradation, multi-crystalline silicon (mc-Si), *n*-type, silicon solar cells.

## I. INTRODUCTION

MULTI-CRYSTALLINE silicon (mc-Si) wafers are known to degrade under illumination at elevated temperature [1]–[8] and under dark annealing [9]–[12]. This degradation is often named light and elevated temperature induced degradation (LeTID) [2], [3], [5], [13], [14]; however, as it has been reported that light is not required for its formation, is also called carrier-induced degradation (CID) [2], [5], as it seems that

excess carriers are the main requirement for this degradation. Other forms of light-induced degradation, such as the formation of the boron–oxygen (B–O) complex or iron–boron (Fe–B) pair dissociation, cannot explain this degradation of carrier lifetime, as CID has been observed also in gallium-doped mc-Si wafers, and its time scales are significantly slower compared with B–O degradation [1]. Under standard field operation conditions, the degradation and recovery cycle of CID in *p*-type mc-Si solar cells has an extremely long timescale from 5 to 20 years, depending on the location of the photovoltaic (PV) system [2], and would result in a significant energy yield loss over this period (because of a drop in efficiency of up to 16% relative) [15]. The shift of the silicon (Si) PV industry toward passivated emitter rear cells (PERC) fabricated using *p*-type mc-Si substrates [16] is being challenged by this degradation. To date, the root cause of CID has not been clarified and, therefore, remains a key area of research focus.

Krauss *et al.* suggested that the rear surface passivation plays a role in the formation of CID [6]. However, the evidence presented by Nakayashiki *et al.* [4] demonstrated that CID is caused by a bulk defect, as a reduction of the bulk lifetime ( $\tau_{\text{bulk}}$ ) was observed after light soaking at elevated temperature. This conclusion was later confirmed by Vargas *et al.* [17] who reported no degradation of the surface passivation quality provided by different silicon nitride ( $\text{SiN}_x$ ) layers when degrading wafers using the laser-accelerated process proposed of Payne *et al.* [3]. Padmanabhan *et al.* [18] supported the hypothesis of a bulk defect being the root cause of CID as they observed degradation and regeneration of both PERC and aluminum back surface field cells. Based on these reports, several studies have been focused on extracting the Shockley–Read–Hall parameters of the CID-related bulk defect using the injection-dependent lifetime spectroscopy [19] technique [4], [7], [20], [21]. Tungsten (W), titanium (Ti), and molybdenum (Mo) were suggested as possible defect candidates; however, later studies suggested that these should be ruled out because of their low diffusivity being inconsistent with observed results [22], [23].

Generally, the CID defect in mc-Si is activated by illumination at elevated temperature [2], [24]. However, Chan *et al.* [9] demonstrated that CID can also be activated by dark annealing at moderate temperatures. Later reports by Chen *et al.* [10] and Fung *et al.* [11] demonstrated that degradation caused by dark annealing alone is similar to that caused by illumination at

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elevated temperature. Fung *et al.* [11] suggested that dark annealing processes allow defect precursors to move into mc-Si bulk and then to gradually deplete. Recently, Vargas *et al.* [12] studied the degradation and regeneration of *p*-type mc-Si in the dark; they found that higher temperatures lead to faster degradation and regeneration rates, as well as a smaller degradation extent. Based on the extracted rates, they reported activation energies of  $1.08 \pm 0.05$  eV and  $1.11 \pm 0.04$  eV for the degradation and regeneration processes, respectively.

The CID kinetics is of particular importance as it can provide insight into the nature of the defect. Bredemeier *et al.* [25] studied the CID kinetics by using two exponential functions associated with the fast and slow defects. However, they only considered the degradation part of the degradation/regeneration curve. A single exponential function and an improved double exponential function were then used by Kwapił *et al.* [26] to extract the CID kinetics. They found that the degradation rate is almost linearly proportional to the excess minority carrier concentration  $\Delta n$ . Vargas *et al.* [12] then used a modified two exponents model to describe the CID kinetics by considering that the degradation and regeneration happen simultaneously [26]. A good agreement was achieved between the model and the experimental data.

It is important to note that almost all the studies agree that a high-temperature firing process is required to trigger the CID [5], [7], [8], [27]. Several recent studies have suggested that hydrogen, introduced during firing step, plays a role in CID of mc-Si wafers [4], [9], [10], [17], [23], [27]–[29]. It can either form a part of the CID defect complex [27], [29] or passivate the recombination active defect [29], [30]. Kersten *et al.* demonstrated that the CID was only observed on fired samples with a hydrogen-containing dielectric layer, such as hydrogenated-SiN<sub>x</sub> [31]. Vargas *et al.* modulated the extent of CID degradation by varying the hydrogen fraction in SiN<sub>x</sub> layers [17]; an increasing extent of degradation was observed by increasing the hydrogen released from the dielectric layer during the firing. Additionally, a thicker SiN<sub>x</sub> layer was shown to cause a more severe CID [32]. Recently, Jensen *et al.* [33] reported that they were able to separate the effects of the thermal process (firing) from the introduction of hydrogen into the wafer. They found that the firing process itself is not required for CID to occur; the introduction of hydrogen via a plasma source is able to trigger degradation.

Currently, little is known regarding CID mechanism in *n*-type wafers. Sio *et al.* [34] reported a degradation and regeneration in *n*-type mc-Si wafers with phosphorous diffusion under illumination at elevated temperatures using samples fired at a peak temperature of 700 °C. They observed a smaller degradation extent and slower degradation and regeneration rates compared with *p*-type mc-Si wafers that were treated under similar conditions. In that study, degradation was only observed in the *n*-type wafers that were fired. This particular behavior is similar to CID of *p*-type mc-Si wafers, which as discussed has a strong dependence on the firing conditions and has not been observed for non-fired samples [5], [7], unless hydrogen is introduced into the Si in another manner [33]. Although not using mc-Si, Chen *et al.* [35] studied CID on *n*-type Czochralski (Cz)

grown wafers. They observed bulk degradation on a fired sample with a diffused layer (either boron or phosphorus) and surface degradation on fired non-diffused samples. Since CID in mc-Si *n*-type wafers was only studied under illumination in [34], in this contribution, both accelerated laser-based process [3] and dark annealing are used to study the degradation and regeneration of non-diffused *n*-type mc-Si wafers. A direct comparison is done with *p*-type mc-Si wafers treated under similar conditions. A detailed investigation of the temperature dependence of degradation and recovery under dark annealing is presented. We also determine the kinetics of the different processes using our modified double-exponential model [12].

## II. MATERIAL AND METHOD

Six sister 6-in phosphorus-doped *n*-type (thickness:  $207 \pm 4$  μm; doping density  $N_D$ :  $(1.0 \pm 0.1) \times 10^{15}$  cm<sup>-3</sup>) and six boron-doped *p*-type (thickness:  $184 \pm 5$  μm; doping density  $N_A$ :  $(8.5 \pm 0.4) \times 10^{15}$  cm<sup>-3</sup>) commercially available high-performance mc-Si wafers were used in this study. All wafers underwent saw damage etching (3 μm per side) using hydrofluoric acid, acetic acid, and nitric acid at room temperature. After receiving a Radio Corporation of America cleaning, SiN<sub>x</sub> layers with refractive index of 2.08 (at 632 nm) and thickness of 75 nm were deposited on all wafers by an industrial plasma-enhanced chemical vapor deposition system (MAiA, Meyer Burger) [36] to form symmetrical lifetime test structures. Five wafers (from each polarity) were then fired at a set peak temperature of 855 °C (actual wafer peak temperature of  $774 \pm 9$  °C), followed by a laser cleaving into square tokens with dimension 3.9 cm × 3.9 cm. Sets of six sister tokens (*p*- and *n*-type) were selected to be used in this study.

One set from each polarity (five fired tokens and one non-fired token) went to laser-accelerated degradation at a wafer temperature of 140 °C and light intensity of 45 kW/m<sup>2</sup> [3] in progressive treatment time steps until a completed degradation and regeneration cycle was achieved. The evolution of the effective lifetime  $\tau_{\text{eff}}$  was monitored after each treatment step using PL images (BTi LIS-R1) [37] and a photoconductance-based lifetime tester (WCT-120, Sinton instruments) [38]. The  $\tau_{\text{eff}}$  measurements were done at a sample temperature of 30 °C and were analyzed using the generalized method [39].

The effect of dark annealing at moderate temperatures was investigated using another set of six *n*-type tokens (five fired and one non-fired) and *in situ* lifetime measurements using a WTC-120TS lifetime tester (Sinton instruments). The following actual wafer temperatures (as measured by a *k*-type thermocouple in direct contact with a similar sample) were investigated: 100, 120, 140 (fired and un-fired tokens), 150, and 160 °C. An additional token from a neighboring location to this set was dark annealed at 175 °C. One set of *p*-type tokens (three fired and one non-fired) received the same dark annealing process at 140, 150, and 175 °C.

In this study, the Kane–Swanson [40] method, as implemented in the Sinton Instrument spreadsheet, was used to monitor changes in the surface saturation current density ( $J_{0s}$ ) and the high-injection  $\tau_{\text{bulk}}$  at  $\Delta n = 1 \times 10^{16}$  cm<sup>-3</sup> (for *n*-type) and

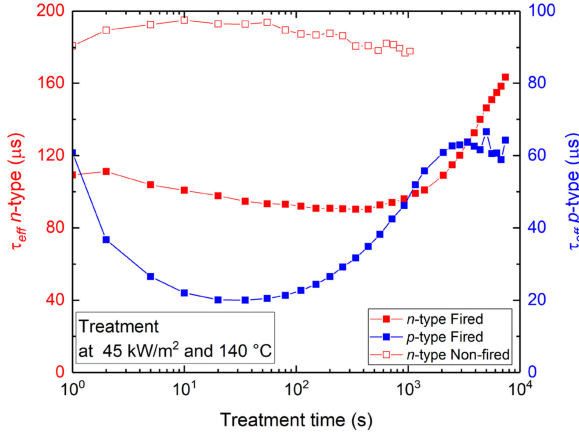


Fig. 1. Evolution of the effective lifetime as a function of the laser processing time. The lines are an aid for the reader and the state before treatment corresponds to a time of 1 s.

$\Delta n = 3 \times 10^{16} \text{ cm}^{-3}$  (for *p*-type). Quokka 2 [41] based one-dimensional modeling was used to confirm the obtained values by varying  $J_{0s}$  and  $\tau_{\text{bulk}}$  to fit the measured  $\tau_{\text{eff}}$ . As Auger lifetime seems to be almost constant between room temperature and 200 °C [42], the Auger model of Richter *et al.* [43] was used in this study for all the analysis. The normalized defect density (NDD) was calculated using the following equation, based on the high injection  $\tau_{\text{bulk}}$  ( $\tau_{\text{bulk}}$  is used here to avoid impacts by changes in the surface passivation quality):

$$\text{NDD}(t) = \left[ \frac{1}{\tau_{\text{bulk}}(t)} - \frac{1}{\tau_{\text{bulk}}(t=0)} \right]. \quad (1)$$

In this study, the CID kinetics was obtained using the following equation [12]:

$$\text{NDD}(t) = \text{NDD}_{\text{max}} [1 - \exp(-r_{\text{deg}}t)] - \text{NDD}_{\text{max}} (1 + A) [1 - \exp(-r_{\text{reg}}t)] \quad (2)$$

where  $\text{NDD}_{\text{max}}$  is the maximum value of the NDD,  $r_{\text{deg}}$  ( $r_{\text{reg}}$ ) is the degradation (regeneration) rate, and  $A$  is a correction factor to account for additional improvements of  $\tau_{\text{bulk}}$  at the end of the process. The fitting was made using the 95% confidence bounds method, as implemented in MATLAB [44].

### III. RESULTS AND DISCUSSION

#### A. Accelerated Laser Degradation and Mitigation of the Degradation of *n*-Type mc-Si

The evolution of the  $\tau_{\text{eff}}$  (extracted at  $\Delta n = 1 \times 10^{15} \text{ cm}^{-3}$ ) of representative *n*-type and *p*-type wafers after firing is presented in Fig. 1 as a function of the cumulated laser treatment duration. The initial lifetimes of the fired samples were  $110 \pm 6 \mu\text{s}$  and  $60 \pm 3 \mu\text{s}$  for the *n*-type and *p*-type wafers, respectively. Both types of wafers demonstrated degradation and recovery of  $\tau_{\text{eff}}$ . Fig. 1 also shows the normalized lifetime of the non-fired *n*-type wafer (initial lifetime of  $180 \pm 9 \mu\text{s}$ ). No degradation and recovery can be identified for this wafer ( $\tau_{\text{eff}}$  variations below 8.5%), pointing toward a CID behavior, similar to a previous

study [24]. However, there are clear differences between the wafers. 1) The degradation rate of the *n*-type wafers during illuminated annealing is much slower than that of the *p*-type wafers. The maximum degradation is obtained after 35 s for the *p*-type wafers, while it takes 150 s of laser treatment to reach maximum degradation of the *n*-type wafers. 2) The extent of the degradation is much smaller ( $\sim 17\%$ ) for the *n*-type wafers compared with the *p*-type wafers ( $\sim 77\%$ ). 3)  $\tau_{\text{eff}}$  of the *n*-type wafers improves considerably ( $>50\%$  and still improving) at the end of the laser treatment carried out here, in contrast to the *p*-type wafers that demonstrate a moderate improvement in the range of 5%–10%.

To further illustrate the degradation and recovery in the *n*-type wafers, Fig. 2(a) presents the injection-dependent  $\tau_{\text{eff}}$  after different laser treatment time durations. The change in the low injection region indicates a strong bulk-related degradation. In order to confirm this hypothesis,  $J_{0s}$  and the high-injection  $\tau_{\text{bulk}}$  were extracted using two methods: 1) the slope-based method of Kane–Swanson [40] at  $\Delta n = 1 \times 10^{16} \text{ cm}^{-3}$ ; and 2) fitting of the measured  $\tau_{\text{eff}}$  using Quokka 2 (in  $\Delta n$  range of  $5.4 \times 10^{15} \text{ cm}^{-3}$  to  $1.7 \times 10^{16} \text{ cm}^{-3}$ ) [41]. Both methods show similar trends, as illustrated in Fig. 2(b): 1) a clear bulk degradation, followed by a significant improvement after a long laser-based treatment; and 2) improvement in surface passivation quality (as indicated by about 14% reduction of  $J_{0s}$ ). The absolute difference between the obtained  $J_{0s}$  is probably because of the non-uniform  $\Delta n$  profile across the wafer's depth, as discussed in [45]. Both trends confirm that the observed degradation is within the bulk. The increase of  $\tau_{\text{bulk}}$  at the end of the process is likely because of hydrogen passivation of preexisting bulk defects or a reduction of the firing-induced CID-related defect [46]. Note that contrary to [47] and [48], we observe improvement of the surface passivation quality during light and moderate temperature treatments, probably because of the different light sources (laser used in this study) and different  $\text{SiN}_x$  layers used in this study.

Fig. 3 presents PL images of both *n*- and *p*-type wafers at different laser treatment stages. All the images were taken with an exposure time of 0.3 s using an 810 nm laser and photon flux of  $2.55 \times 10^{17} \text{ cm}^{-2}\text{s}^{-1}$ . The images were processed using the recently developed software described in [49]. The relative change in PL intensity of the images was calculated by  $(I - I_0)/I_0 \times 100\%$ , where  $I_0$  and  $I$  are the PL images before the treatment and at the most degraded or final state. As shown in Fig. 3, degradation and regeneration occurs across the entire wafer, but not uniformly. While it seems that grain boundaries and other crystal defects degrade less than the intra-grain regions in the *p*-type wafers [50], we have not identified a correlation between the degradation extent and particular locations in the *n*-type wafers. This will be investigated more deeply in the near future.

#### B. Degradation and Recovery of *n*-Type mc-Si Under Dark Annealing

The evolution of the normalized  $\tau_{\text{bulk}}$  extracted at  $\Delta n = 1 \times 10^{16} \text{ cm}^{-3}$  following the Kane–Swanson method [40] for the *n*-type wafers under dark annealing at different temperatures is



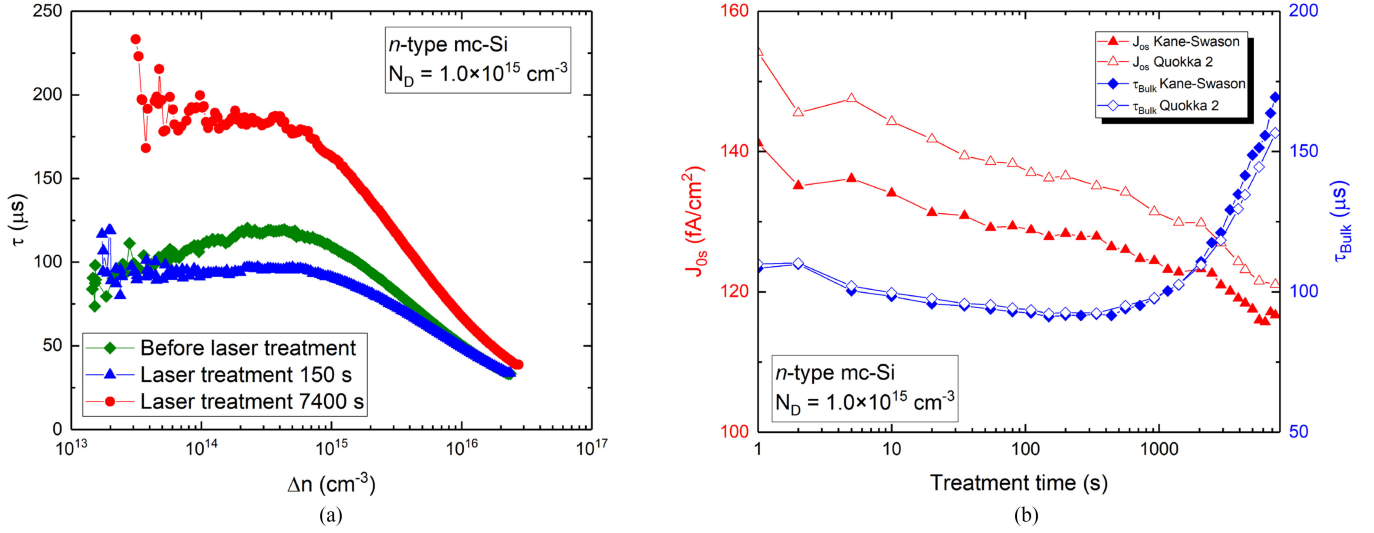


Fig. 2. (a) Injection-dependent effective lifetime of an *n*-type wafer as a function of the laser treatment time duration. (b) Surface saturation current density and high injection bulk lifetime as extracted using the Kane–Swanson [40] method and Quokka 2 [41] modeling.

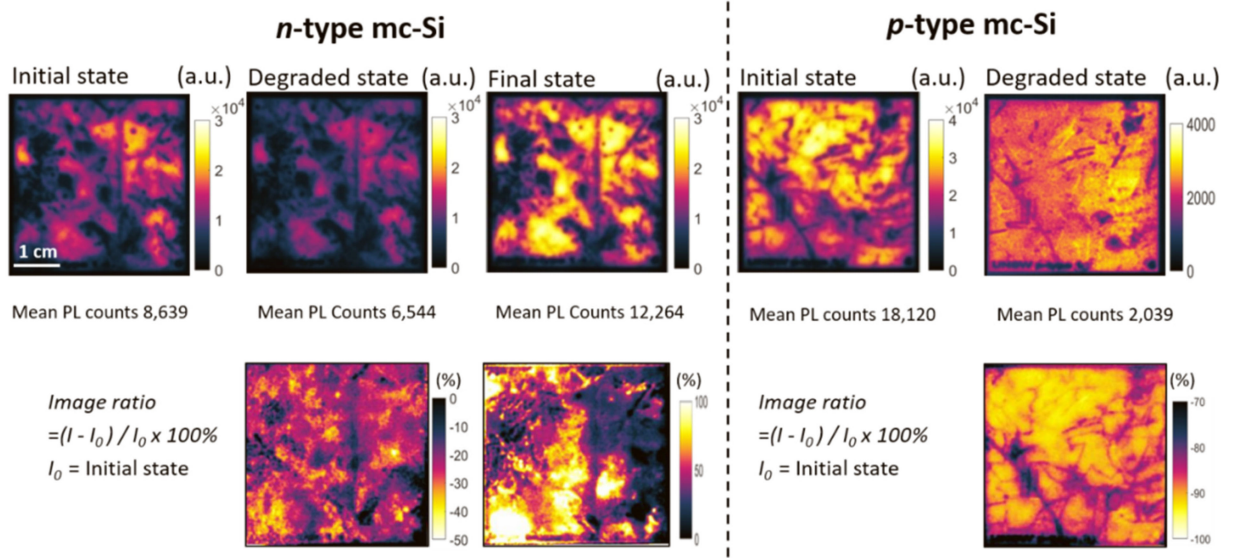


Fig. 3. PL images for the *n*- and *p*-type mc-Si samples at different stages along with the image ratio compared with the state before the laser process. Note the different scales between the images.

shown in Fig. 4(a). A slight change in the  $J_{0s}$  was observed ( $<5\%$ ) during the process.  $\tau_{\text{bulk}}$  measured at room temperature is in the range  $102 \pm 16 \mu\text{s}$  for the fired *n*-type wafers and  $201 \pm 10 \mu\text{s}$  for the non-fired wafer. The  $\tau_{\text{bulk}}$  of the *n*-type wafer reduced 49% after firing (the surface passivation is not degraded after firing) in contrast to the *p*-type wafer where lifetime improvement was observed after the firing process. This can be explained by competing processes happening during firing: improvement of bulk due to hydrogenation and degradation due to CID. However, at this stage, we cannot separate these possible processes. The time evolution of the normalized  $\tau_{\text{bulk}}$  at  $\Delta n = 3 \times 10^{16} \text{ cm}^{-3}$  of the *p*-type samples (initial lifetime  $131 \pm 6 \mu\text{s}$  for the fired wafers; and  $72 \pm 4 \mu\text{s}$  for the non-fired one) is displayed in Fig. 4(b). Since the degradation and regeneration

of these samples are very slow at temperatures below  $175^\circ\text{C}$  [12], only partial regeneration was observed in the time frame of this experiment. Note that the Kane–Swanson method [40] was used to extract  $\tau_{\text{bulk}}$  for the dark annealed wafers as Quokka 2 [41] cannot be used for fitting lifetime measurements at higher temperatures. Based on the comparison between the two methods at room temperature, we assume that the obtained trend is a good representation, despite the fact that the *p*-type wafers were not measured at high injection.

For the *n*-type wafers [see Fig. 4(a)], degradation and regeneration of  $\tau_{\text{bulk}}$  can be appreciated, except for annealing at 160 and  $175^\circ\text{C}$ , where only an improvement is observed. Higher degradation extent is obtained for *n*-type wafers treated at lower temperatures. The degradation extent is decreasing with

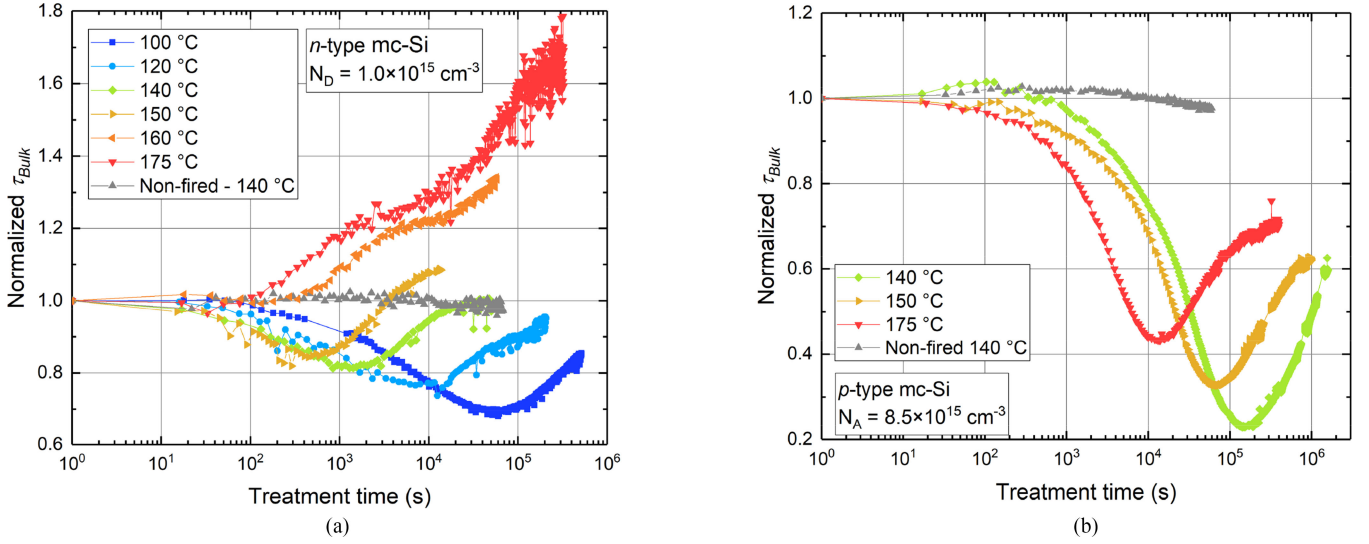


Fig. 4. Evolution of the high injection bulk lifetime for wafers under dark annealing at different temperatures. (a) *n*-type wafers. (b) *p*-type wafers.

increasing annealing temperature. The degradation rate has also a strong dependence on the temperature; at higher temperatures, the degradation rate is much faster. No degradation and regeneration of  $\tau_{bulk}$  can be seen for the non-fired wafer. A similar behavior is observed for the *p*-type wafers (see Fig. 4(b) and [12]), however, with slower degradation and regeneration rates compared with the *n*-type wafers and with a larger degradation extent. Interestingly, the  $\tau_{bulk}$  values of *n*-type wafers are higher at the end of the annealing process above 150 °C compared with their initial values. A similar observation was reported for *p*-type samples [12]. We assume that it is due to passivation of preexisting bulk defects or preformed CID defects during firing. Further studies are required to prove this hypothesis. To our knowledge, this is the first time that degradation of the *n*-type mc-Si wafers using dark annealing is reported. The similarities between the *n*- and *p*-type wafers (temperature dependence of the degradation extend and rates) may indicate that the defect responsible for the degradation is the same in both materials.

Surprisingly, the  $\tau_{bulk}$  of *n*-type wafer keeps improving under dark annealing at 175 °C. In order to test the stability of this improvement, a wafer was processed using the accelerated laser process at 45 kW/m<sup>2</sup> and 140 °C for almost 2 h at the end of 90 h dark annealing treatment at 175 °C (this laser condition is roughly equivalent to 20 years in the field which is similar to the lifespan of PV modules). Despite the fact that  $\tau_{bulk}$  was degraded to about 50% of its post dark annealing value (see Fig. 5), the stable  $\tau_{bulk}$  at the end of the degradation (105  $\mu$ s) is still slightly higher than the lifetime before dark annealing (92  $\mu$ s). This indicates that dark annealing at 175 °C (or higher temperature) can suppress the lifetime degradation (from its initial value after firing) because of CID in the *n*-type mc-Si wafers. It is interesting to note the higher degradation extent and very slow rates observed during this laser treatment, compared with the wafers with no pre-dark annealing (see Fig. 1). This difference could be an indication of modulation of the degradation kinetics due to initial dark annealing as suggested by Chan *et al.* [10] for the *p*-type mc-Si.

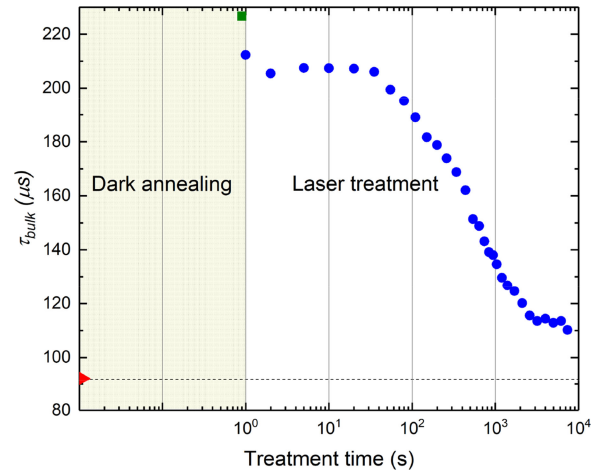


Fig. 5. Evolution of the high injection  $\tau_{bulk}$  under laser treatment for the wafer that initially received dark annealing at 175 °C.

### C. Kinetics and Activation Energies of the Illuminated and Dark Annealing Degradation and Recovery Reactions

The evolution of the NDD is analyzed using the proposed kinetic model [see (2)] for the wafers under the laser-accelerated degradation process (see Fig. 1) and the wafers under dark annealing (except for 160 and 175 °C), where the degradation and regeneration are assumed to occur simultaneously. Good agreement between the measurements and the model was obtained for the wafers under laser treatment [see Fig. 6(a)]. In the case of dark annealing, excellent fits are obtained for all temperatures, except for the wafer annealed at 100 °C [see Fig. 6(b)].

Table I presents the degradation and regeneration rates of wafers treated by laser illumination (45 kW/m<sup>2</sup> and 140 °C) and dark annealing at 140 °C, based on the fit to the proposed model [see (2)]. The data for *p*-type (treated by dark annealing) is obtained from [12], as the degradation and regeneration are too slow to observe in the time frame of this experiment. For laser-based treatments, the rates of the *p*-type wafers are

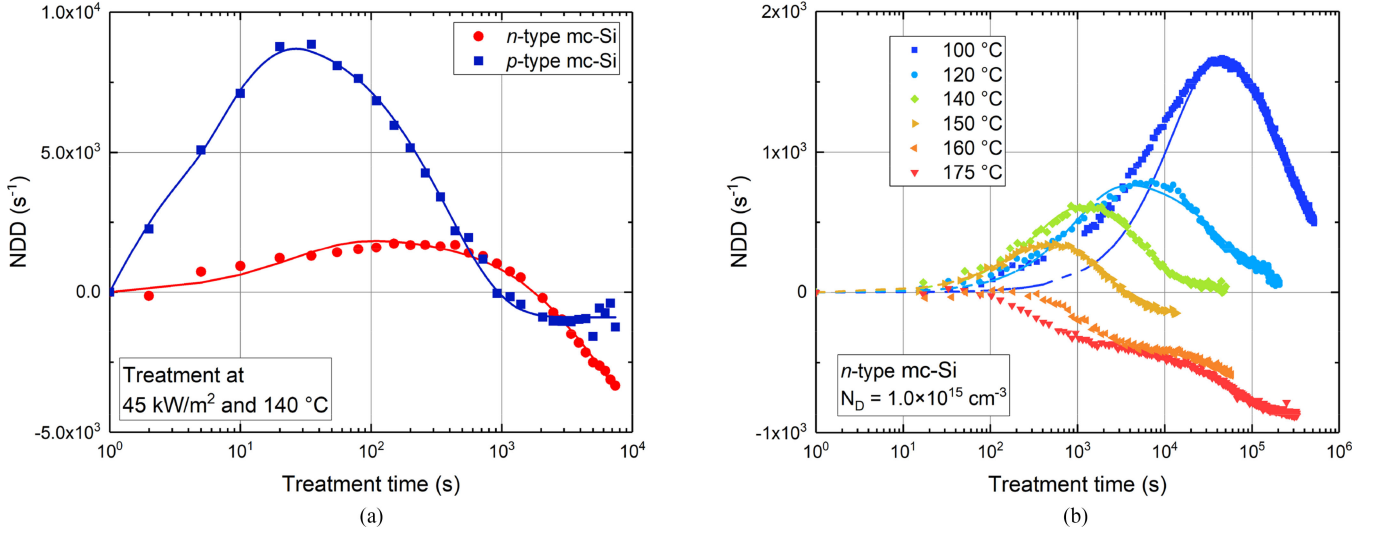


Fig. 6. Measured (symbols) and modeled (solid lines) NDD. (a)  $n$ - and  $p$ -type wafers under laser-based treatment. (b)  $n$ -type wafers under dark annealing (NDD of the sample under the dark annealing at 160 and  $175^\circ\text{C}$  was also included without fit).

TABLE I  
DEGRADATION AND REGENERATION RATES OF SOME SAMPLES BASED ON THE PROPOSED FITTING MODEL (FIT AT  $140^\circ\text{C}$ )

Sample	$\text{NDD}_{\max} (\text{s}^{-1})$	$A$	$r_{\text{deg}} (\text{s}^{-1})$	$r_{\text{reg}} (\text{s}^{-1})$
$p$ -type mc-Si – Laser treatment	$(9.55 \pm 0.38) \times 10^3$	$0.093 \pm 0.018$	$0.153 \pm 0.020$	$(2.61 \pm 0.24) \times 10^{-3}$
$p$ -type mc-Si – Dark annealing at $138^\circ\text{C}$ [12]	$(3.85 \pm 0.16) \times 10^4$	$-0.059 \pm 0.021$	$(5.52 \pm 0.43) \times 10^{-6}$	$(4.54 \pm 0.46) \times 10^{-7}$
$n$ -type mc-Si – Laser treatment	$(2.01 \pm 0.23) \times 10^3$	$2.7 \pm 1.1$	$0.038 \pm 0.018$	$(1.81 \pm 0.75) \times 10^{-4}$
$n$ -type mc-Si – Dark annealing at $140^\circ\text{C}$	$(7.81 \pm 0.29) \times 10^2$	$-0.047 \pm 0.010$	$(2.56 \pm 0.20) \times 10^{-3}$	$(1.67 \pm 0.12) \times 10^{-4}$

faster than those of the  $n$ -type wafers (five times faster degradation rate, more than ten times faster regeneration rate). This observed behavior parallels that observed by Sio *et al.* [34] on mc-Si  $p$ -type and  $n$ -type wafers under illumination. However, an opposite trend is obtained under dark annealing, with the rates of degradation and regeneration for  $n$ -type wafers being faster than those of the  $p$ -type wafers. A plausible reason is one that was explored earlier in [35] suggesting that the recovery of CID may be related to the out-diffusion of a hydrogen species toward the surface of the wafer. It is also plausible that if hydrogen is involved in the formation of the recombination active defect, then the diffusion of hydrogen to the defect precursor may also play a role in determining the degradation rate.

At  $150^\circ\text{C}$ , the reported diffusivity of  $\text{H}^-$  is approximately 2.5 orders of magnitude higher than that of  $\text{H}^+$ . Furthermore, the reported diffusivity of  $\text{H}^0$  is approximately 1.5 orders of magnitude higher than that of  $\text{H}^-$  [51]. Under dark annealing conditions in  $n$ -type Si at  $140^\circ\text{C}$ , the fractional charge state concentrations of  $\text{H}^+$ ,  $\text{H}^0$ , and  $\text{H}^-$  are  $6.4 \times 10^{-2}$ ,  $7.8 \times 10^{-4}$ , and  $9.4 \times 10^{-1}$ , respectively, with a clear dominance of  $\text{H}^-$  [52]. In contrast, in  $p$ -type Si, the corresponding fractional charge state concentrations are  $1 \times 10^0$ ,  $6.8 \times 10^{-8}$  and  $1.5 \times 10^{-10}$ , respectively. This gives a domination of  $\text{H}^-$  in  $n$ -type Si and domination of  $\text{H}^+$  in  $p$ -type Si. Furthermore, the fractional concentration of  $\text{H}^-$  is 9.5 orders of magnitude higher in  $n$ -type Si than that in  $p$ -type Si. Similarly, the fractional concentration of

$\text{H}^0$  is approximately four orders of magnitude higher in  $n$ -type Si than that in  $p$ -type Si. Under these conditions, one would then expect both the degradation and regeneration rates in  $n$ -type to be several orders of magnitude greater than in  $p$ -type in the dark.

Under illumination, the expected  $\Delta n$  of the  $n$ -type and  $p$ -type samples from the initial state to the most degraded state are approximately  $5.4 \times 10^{16}$  to  $5.2 \times 10^{16} \text{ cm}^{-3}$  and  $8.0 \times 10^{16}$  to  $5.8 \times 10^{16} \text{ cm}^{-3}$ , respectively. For these carrier concentrations, the expected fractional hydrogen charge state concentrations in the  $n$ -type for  $\text{H}^+$ ,  $\text{H}^0$ , and  $\text{H}^-$  are  $7.1 \times 10^{-1}$ ,  $2.7 \times 10^{-1}$ , and  $1.4 \times 10^{-2}$ , respectively. Since the change of  $\Delta n$  during the laser treatment is small (4%), the fractional concentrations remain the same. For  $p$ -type, the corresponding concentrations at initial state are  $6.8 \times 10^{-1}$  ( $\text{H}^+$ ),  $3.1 \times 10^{-1}$  ( $\text{H}^0$ ), and  $1.4 \times 10^{-2}$  ( $\text{H}^-$ ). Then, the concentration for  $\text{H}^0$  and  $\text{H}^-$  decreases by 12% and 15%, respectively, during treatment, while the fractional concentration for  $\text{H}^+$  increases by 6%. For both  $n$ -type and  $p$ -type under laser treatment,  $\text{H}^+$  (with the lowest diffusivity among three) is dominant for both  $n$ -type and  $p$ -type. We cannot confidently pinpoint the relationship between hydrogen diffusion and fast degradation and regeneration rates of the  $p$ -type wafer under illumination.

For both  $n$ -type and  $p$ -type wafers, the degradation rate under illumination is faster than that obtained using dark annealing. For  $n$ -type, the degradation rate increased by a factor of

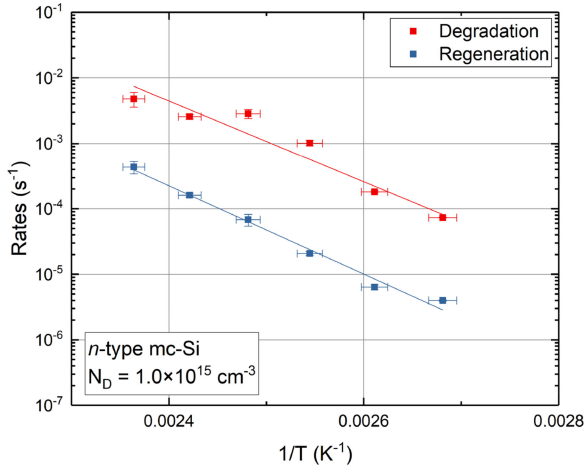


Fig. 7. Arrhenius plot of the samples under dark annealing with the best linear fit.

15 under illumination compared with dark annealing. This closely correlates with the expected increase in the total electron concentration of the sample under illumination compared with that during dark annealing. For *p*-type, the degradation rate increased by a factor of  $2.7 \times 10^4$  under illumination. This also closely correlates with the expected increase in the total electron concentration. The acceleration of both degradation and regeneration rates with illumination on *p*-type wafers has been explored in various works [10], [23], [26]. CID has been understood to be dependent on the carrier concentration and possibly even thermally generated carriers. Thus, an increase in illumination may drive forward both the degradation and regeneration reactions.

Interestingly, we find the regeneration rates of *n*-type wafers treated by laser and dark annealing to be comparable, with no significant increase in the regeneration rate with illumination. This unexpected result cannot yet be explained and requires further investigation and modeling, and could potentially provide more clues in determining the mechanism for regeneration, such as a reducing concentration of  $H^-$  with carrier injection. It is also interesting to note that the ratios from *n*-type to *p*-type for the degradation or regeneration rate under the dark treatment are both around 400. Regarding the laser treatment, the ratios from *n*-type to *p*-type are 0.25 for the degradation rate and 0.07 for the regeneration rate. This indicates that the CID mechanisms are different between *n*-type and *p*-type under illumination. The large value of the factor  $A$  for the *n*-type wafer under the laser treatment indicating that the improvement of  $\tau_{\text{eff}}$  at the end of the process is significant.

Based on the extracted rates for the samples under dark annealing [see Fig. 6(b)], the activation energies were extracted using an Arrhenius analysis, as illustrated in Fig. 7. The Arrhenius function was defined as

$$r_{\text{deg/reg}} = C \times \exp \left[ -\frac{E_{\text{deg/reg}}}{k_B T} \right] \quad (3)$$

where  $C$  is a constant,  $k_B$  is the Boltzmann constant,  $T$  is the temperature, and  $E_{\text{deg/reg}}$  are the degradation and regeneration

activation energies, respectively. The activation energies are found to be  $1.23 \pm 0.16$  eV for the degradation process and  $1.34 \pm 0.08$  eV for the regeneration process. These energies are similar to those determined for *p*-type mc-Si wafers ( $1.04 \pm 0.06$  eV for the degradation process and  $1.05 \pm 0.04$  eV for the regeneration process [12]). The small difference (in the range of 20%) could be explained by the smaller temperature range used in this paper (100–150 °C, limited by the temperatures at which degradation is observed in the *n*-type mc-Si) compared with the wider range (140–300 °C) used in [12] for *p*-type wafers, which can lead to an additional uncertainty in the confidence intervals for the *n*-type samples. The fact that the degradation kinetics under the laser and dark annealing of *n*- and *p*-type wafers can be modeled using the same equation could be an indication of a similar degradation mechanism.

#### IV. CONCLUSION

In this study, the presence of a minority-carrier-lifetime degradation and regeneration cycle in non-diffused and fired *n*-type mc-Si wafers was demonstrated by using accelerated laser-based illuminated and dark annealing at moderate temperatures. The degradation rate and degradation extent are found to be lower than those of *p*-type mc-Si wafers when the illuminated annealing is used, similar to previously reported results. Surprisingly, the *n*-type mc-Si treated by dark annealing has a faster degradation and regeneration rate than the *p*-type mc-Si under same treatment; however, the extent is smaller, and the degradation cannot be observed at annealing temperatures of 160 °C or above. Significant lifetime improvement of the *n*-type wafers is observed under higher temperature (above 160 °C) dark annealing; however, the improved lifetime is not stable under a subsequent accelerated laser degradation process. Instead, a pronounced and slower degradation was found on that wafer, indicating a possible modulation of the degradation kinetics due to dark annealing. Based on a model that considers degradation and regeneration happening simultaneously, the evolution of those processes in *n*-type mc-Si can be described, and based on the extracted rates, activation energies are  $1.23 \pm 0.16$  eV for the degradation process and  $1.34 \pm 0.08$  eV for the regeneration process. Considering the similitudes found for the *n*-type and *p*-type mc-Si samples processed under similar conditions (firing, laser-accelerated process, dark annealing, and kinetics), it is very likely that both have similar nature; therefore, the *n*-type mc-Si also suffers from the same CID that occurs in *p*-type mc-Si. These findings could help guide further studies to determine the root causes of degradation of mc-Si as well as possible mitigation solutions.

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