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The role of 60 Co γ -ray irradiation on the interface states and series resistance in MIS structures

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ABSTRACT

The effect of γ -ray exposure on the metal-insulator-semiconductor (MIS) structures has been investigated using the electrical characteristics at room temperature. The MIS structures are irradiated with 60 Co γ -ray source. The energy distribution of interface states was determined from the forward bias I–V characteristics by taking into account the bias dependence of the effective barrier height and ideality factor. The value of series resistance decreases with increasing dose. Experimental results confirmed that γ -ray irradiation have a significant effect on electrical characteristics of MIS structures. © 2009 Elsevier Ltd. All rights reserved.

1. Introduction

Metal-insulator-semiconductor (MIS) structures consist of a semiconductor substrate covered by an oxide layer upon which a metal electrode gate is deposited. The MIS structures have been intensively investigated due to their technological applications (Rhoderick and Williams, 1988; Nicollian and Brews, 1982; Quennoughı, 1997; Depas et al., 1992; Konofaos et al., 1997; Haddara and El-Sayed, 1988; Singh, 1985; Tataroğlu et al., 2006; Cova and Singh, 1997; Sands et al., 1992; Card and Rhoderick, 1971). In the presence of an insulator layer, the density of interface states ($N_{\rm ss}$) and series resistance ($R_{\rm s}$), the I-V, C-V and $G/\omega-V$ characteristics deviate from those expected for ideal behavior of Schottky diodes (Tataroğlu et al., 2006; Cova and Singh, 1997; Sands et al., 1992; Card and Rhoderick, 1971; Tataroğlu and Altındal, 2006; Türüt and Sağlam, 1992; Gökçen et al., 2008; Szatkowski and Sieranski, 1992).

Recently, the radiation response of these devices has been found to change significantly when these devices are exposed to irradiation stress treatments (Winokur et al., 1976, 1984; Hughes, 1977; Chin and Ma, 1983; Da Silva et al., 1987, 2000; Schwank et al., 1986; Ma, 1989). Winokur et al. (1976) and Ma (1989) were among the first to make a systematic observation of the after irradiation behavior of $N_{\rm ss}$ in MIS devices.

There are two effects of radiation: a transient effect due to the electron-hole pair generation and a permanent effect to the bombardment of devices with radiation which causes changes in the crystal lattice. Radiation generates electron–hole pairs in the insulator that subsequently interact with trapping sites with the insulating film. The radiation generated electrons either recombine with the holes or move out of insulator. The radiation generated holes may diffuse in the insulator, but are less mobile than the electrons; many stationary hole traps are also present. There are some methods to determine values of R_s and N_{ss} (Nicollian and Brews, 1982; Norde, 1979; Sato and Yasamura, 1985; Cheung and Cheung, 1986).

The main aim of this study is to investigate the effects of surface charge states on MIS structures by I-V, C-V and $G/\omega-V$ characteristics as a function of the irradiation doses (0–5 kGy) at room temperature. In addition, we investigated the effects of R_s and N_{ss} on these characteristics.

2. Experimental detail

The Al/SiO₂/p-Si (MIS) structures were fabricated on, 2″ diameter float zone $\langle 100 \rangle$ boron-doped (p-type) single crystals Si wafer having thickness of 280 µm and resistivity of 8 Ω cm. The Si wafer was degreased for 5 min in organic solvent of trichloroethylene (CHclCcl₂), acetone (CH₃COCH₃) and methyl alcohol (CH₃OH) and then etched in a sequence of sulfuric acid (H₂SO₄) and hydrogen peroxide (H₂O₂), 20% hydrofluoric acid (HF, a solution of nitric acid (6HNO₃): 1 HF:35 H₂O, 20% HF and finally quenched in de-ionised water for a prolonged time. Preceding each cleaning step, the wafer was rinsed thoroughly in de-ionized water of resistivity of 18 M Ω cm. After surface cleaning of Si, high purity Al metal (99,999%) with a thickness of \sim 2000 Å was thermally evaporated from the tungsten filament onto the whole back surface of the Si wafer in

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the pressure of $\sim 1 \times 10^{-6}\, \rm Torr$ in oil vacuum pump system. The ohmic contact was formed by sintering the evaporated Al back contact at 650 °C for 60 min in flowing dry nitrogen ambient at a rate of 2 l/min. This process served both to sinter the Al and to form the required thin insulator layer (SiO₂) on the upper surface of wafer. To form the Schottky contacts, the circular dots of $\sim 1\,\rm mm$ diameter and $\sim 2000\,\rm \mathring{A}$ thick Al are deposited onto the oxidized surface of the wafer through a metal shadow mask in a liquid nitrogen trapped vacuum system in a vacuum of $\sim 2 \times 10^{-6}\,\rm Torr$. The interfacial insulator layer thickness was estimated to be about 40 $\rm \mathring{A}$ from high frequency (1 MHz) measurement of the interface insulator capacitance in the strong accumulation region for MIS Schottky diode (Szatkowski and Sieranski, 1992).

The C-V and $G/\omega-V$ measurements were carried out using an HP 4192A LF impedance analyzer (5–13 MHz). The ac signal was generated by a low-distortion oscillator with the amplitude attenuated to 50 mV_{rms} to meet the small signal requirement for thin oxide capacitors. Also, the I-V measurements were carried out using a Keithly 220 programmable constant-current source and a Keithly 614 electrometer. The C-V, $G/\omega-V$ and I-V measurements were performed before and after 60 Co γ -ray source irradiation with the dose rate of 2.12 kGy/h at room temperature. All measurements were carried out with the help of a microcomputer through an IEEE-488 ac/dc converter card.

3. Results and discussion

When the MIS structures have R_s , according to thermionic emission (TE) model, the relation between the V and I can be written as (Rhoderick and Williams, 1988)

$$I = I_0 \exp\left(\frac{q(V - IR_s)}{nkT}\right) \left[1 - \exp\left(\frac{-q(V - IR_s)}{kT}\right)\right]$$
 (1)

where I_o in the reverse saturation current and expressed as

$$I_o = AA^*T^2 \exp\left(-\frac{q\Phi_{bo}}{kT}\right) \tag{2}$$

where n is an ideality factor, Φ_{bo} the effective barrier height at zero bias, A the diode area, A^* the effective Richardson constant and equals to $32\,\mathrm{A/cm^2\,K^2}$ for p-type Si. Fig. 1 shows $\mathrm{Ln}\,I-V$ characteristics of MIS structures before and after $^{60}\mathrm{Co}$ γ -ray irradiation. The n is calculated from the slope of the linear region of the forward bias $\mathrm{Ln}\,I-V$ plot and can be written from Eq. (1) as

$$n = \frac{q}{kT} \frac{dV}{d \ln I} \tag{3a}$$

and also the dependence of n from V can be written as

$$n(V) = \frac{qV}{kT \operatorname{Ln}(I/I_0)}$$
 (3b)

The value of Φ_{bo} is calculated from the I_o at zero bias and is given by

$$\Phi_{bo} = \frac{kT}{q} \operatorname{Ln} \left(\frac{AA^{**}T^2}{I_0} \right) \tag{4}$$

The value of n and Φ_{bo} were determined from Eq. (3b) and (4), respectively, before and after irradiation. As can be seen in Fig. 1, an interesting feature of the forward bias semi-logarithmic I-V curves is the intersection at a certain bias (1.28 V). As can be seen in Figs 3 and 4, similar results have been observed in the C-V and G/ω -V characteristics. The reason of this behavior can be attributed to the inhomogeneties of Schottky barrier at metal-semiconductor (M-S) interface (Chand, 2004; Osvald, 2006; Dökme and Altındal, 2006; Pakma et al., 2008). Also, the value of R_S is significant in the downward curvature (at high bias voltages) of the forward bias I-V characteristics and it depends on

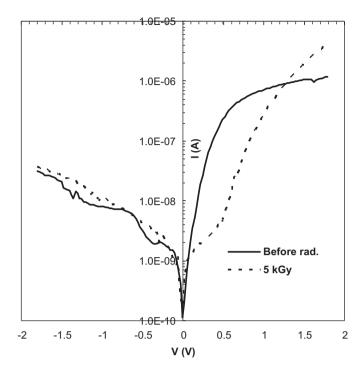


Fig. 1. Forward and reverse bias I–V characteristics of MIS structure before and after γ -ray irradiation.

the magnitude of the R_s . Chand (2004) and Osvald (2006) show that the value of R_s plays a subtle role in keeping this intersection hidden. Under γ -radiation, the value of R_s decreases due to the reduction in carrier density in the depletion region of diode through the introduction of traps and recombination centers associated with radiation effect. Therefore, intersection behavior in the forward bias I-V plot will be inevitable.

However, the role of radiation-induced interface traps is not fully understood, especially at the microscopic level, as well as the connection with processing sequences. We think that the study on these questions will undoubtedly continue.

It was found that presence of series resistance in diode causes bending due to current saturation and plays subtle role in keeping this crossing hidden. For our sample, the R_s is shown to play a crucial role in effecting forward bias I-V, C-V and $G/\omega-V$ curves of MIS structures. The values of n and Φ_{bo} were found to have a stronger dose rate and range from 3.49 and 0.76 eV at 0 kGy (before irradiation) to 4.61 and 0.83 eV at 5 kGy, respectively.

The effective barrier height Φ_e is assumed to be bias voltage dependent due to the presence of an interfacial insulator layer and the interface states located at Si/SiO₂ interface, which can be expressed as (Cova and Singh, 1997)

$$\Phi_e = \Phi_{bo} + \beta(V - IR_s) = \Phi_{bo} + \left(1 - \frac{1}{n(V)}\right)(V - IR_s)$$
(5)

by considering the applied voltage dependence of the barrier height (BH), where β is the voltage coefficient of the effective BH (Φ_e) used in place of the BH (Φ_{bo}) and it is a parameter that combines the effects of N_{ss} which is in equilibrium with the semiconductor (Winokur et al., 1976; Hughes, 1977; Cheung and Cheung, 1986).

Furthermore, in a p-type semiconductor, to evaluate the distribution of the interface states $N_{ss} - (E_{ss} - E_V)$ having energy of N_{ss} , E_{ss} with respect to top of the valance band at the surface of the semiconductor is given by (Rhoderick and Williams, 1988; Card and Rhoderick, 1971)

$$E_{\rm ss} - E_{\rm V} = q(\Phi_{\rm e} - {\rm V}) \tag{6}$$

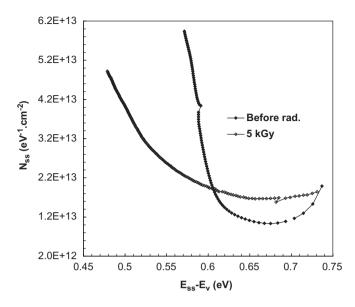


Fig. 2. The density of interface states (N_{ss}) distribution profiles as a function $E_{ss}-E_v$ obtained from the forward bias I-V characteristics.

where E_{ss} is the energy of interface states N_{ss} and E_V is the valance bend edge.

Assuming the voltage dependent n values, ε_s = 11.8 ε_o , ε_i =3.8 ε_o , δ =40 Å and W_D =5 μm in Eq. (5), the energy distribution profile of N_{ss} was obtained before and after irradiation and is given in Fig. 2.

$$N_{ss}(V) = \frac{1}{q} \left[\frac{\varepsilon_i}{\delta} (n(V) - 1) - \frac{\varepsilon_s}{W_D} \right]$$
 (7)

where ε_i and ε_s are the permittivity of the insulator layer (SiO₂) and the semiconductor, respectively; W_D width of the depletion region and δ the thickness of the interfacial insulator layer.

As shown in Fig. 2, the increase in the N_{ss} from mid gap towards the bottom of E_V is very apparent. The mean value of N_{ss} was found about 3×10^{13} cm⁻² eV⁻¹.

The C-V and G/ω characteristics were measured before and after irradiation at 1 MHz and are given in Figs 3 and 4. As the forward bias I-V curves, both the C-V and $G/\omega-V$ curves show an intersection behavior at a certain bias voltage. These behaviors may be attributed to the lack of free charges under irradiation. By the inspection of Figs 3 and 4, C and G/ω increase at high forward and reverse voltages (Candelori et al., 1999; De Vasconcelos and Da Silva, 1997), but decreases in the range of low forward and reverse biases. The increase in C and G/ω with radiation especially at forward bias is a result of the decreasing in the semiconductor depletion width. Also, the C-V measurements at high frequency are relatively easily and rapidly carried out, and these measurements can yield interesting and meaningful results to show the negligibility of excess capacitance. This makes the contribution of interface state capacitance to the total capacitance negligibly small (Hung and Cheng, 1987; Akkal et al., 2000). Since the presence of N_{ss} , the device behavior is different than ideal case of C-V and G/ω -V characteristics. These N_{ss} can easily follow the ac signal especially at low frequencies and yield excess capacitance, which depends on their relaxation time and cause a bias shift of the C-V and $G/\omega-V$ curves. Therefore, the C-V and G/ω -V measurements are carried out at sufficiently high frequency of 1 MHz.

We believe that the trap charges have enough energy to escape from the traps localized at $\mathrm{Si/SiO_2}$ interface. These interface states usually cause a bias shift, and the frequency and capacitance dispersion of the C-V and $G/\omega-V$ curves. In addition, the series

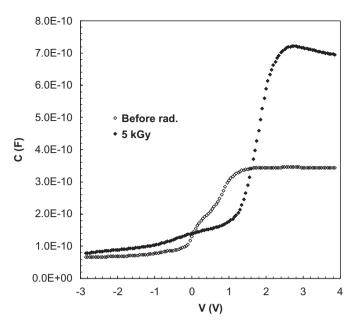


Fig. 3. The C-V characteristics of the MIS structure before and after γ -ray irradiation obtained at 1 MHz and room temperature.

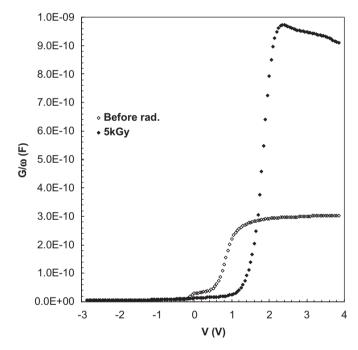


Fig. 4. The G/ω –V characteristics of the MIS structure before and after γ -ray irradiation obtained at 1 MHz and room temperature.

resistance is an important parameter, which causes changes in the electrical characteristics for Schottky structures (Nicollian and Brews, 1982).

There are several methods to extract the series resistance of MIS structure in literature (Norde, 1979; Sato and Yasamura, 1985). In this study we have used the conductance method developed by Nicollian and Goetzberger (Nicollian and Goetzberger, 1965; Nicollian and Goetzberger, 1967). The real series resistance of MIS structures can be subtracted from the measured capacitance (C_m) and conductance (G_m) in strong accumulation region at high frequency $(f \ge 500 \, \text{kHz})$ (Hung and Cheng, 1987; Nicollian and Goetzberger, 1965, 1967). In addition, the voltage

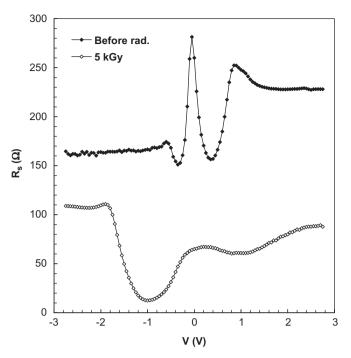


Fig. 5. Series resistance (R_s) vs gate bias under irradiation dose at 1 MHz.

and frequency dependence of the series resistance profile can be obtained from the C–V and G/ω –V curves. To determine series resistance R_s , the MIS structure is biased into strong accumulation at sufficiently high frequency. The measured impedance (Z_m) at strong accumulation of MIS structure using the parallel RC circuit (Nicollian and Brews, 1982) is equivalent to the total circuit impedance as

$$Z_m = \frac{1}{G_m + j\omega C_m} \tag{8}$$

Comparing the real and imaginary part of the impedance, the series resistance is given by (Nicollian and Brews, 1982; Norde, 1979; Nicollian and Goetzberger, 1967)

$$R_s = \frac{G_m}{G_m^2 + (\omega C_m)^2} \tag{9}$$

where C_m and G_m represent the measured capacitance and conductance in strong accumulation region.

The series resistance is an important parameter to designate the noise ratio of device as dependent on radiation dose. Therefore, both the real values and voltage dependence of the series resistance $R_{\rm s}$ were calculated from Eq. (9) according to Ref. Nicollian and Goetzberger (1965) and are given in Fig. 5. As can be seen in Fig. 5, the value of the series resistance decreased with increasing dose for each voltage.

4. Conclusion

The effect of γ -ray on MIS structure has been investigated using the I-V, C-V and $G/\omega-V$ characteristics at room temperature. The MIS structures are irradiated with 60 Co γ -ray source in the dose range of 0–5 kGy. The values of n increase with irradiation dose due to an increase of induced by radiation. The density of N_{ss} distribution profiles as a function $E_{ss}-E_{v}$ was extracted from the forward bias I-V characteristics before and after irradiation by taking into account the bias dependence of the Φ_{e} and n. The values of N_{ss} showed an experimental decrease with bias from the top of the valance band towards the mid gap. The measured C-V

and $G/\omega - V$ characteristics of MIS structures show fairly large radiation dispersion. The R_s profile of sample was extracted from the measured C_m and C_m/ω measurements according to admittance method and its value decreases with increasing dose rate. In addition, the experimental I-V, C-V and $G/\omega - V$ curves exhibit intersection behavior at a certain bias voltage. These behaviors may be attributed to the lack of free charges under irradiation. Experimental results show that γ -ray irradiation have a significant effect on MIS structures.

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