# Voltage dependence of equivalent circuit parameters of bilayer organic photovoltaics

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#### **ABSTRACT**

Despite the very different underlying physics of organic photovoltaics (OPVs), inorganic p-n junction's Shockley's diode equation is often applied to describe current density-voltage (JV) curves of OPVs. The model parameters, including the diode saturation current, diode ideality factor, series, and parallel resistances, are usually extracted and treated as constants in JV curve analyses. In this work, we develop a drift-diffusion bilayer interface (DD-BI) model for bilayer OPVs, which treats the donor-acceptor (D-A) heterojunction using the detailed balance between densities of polaron pairs, free electrons, and free holes. From the DD-BI model, we derive a diode equation, which is of Shockley's equation form, but each parameter is explicitly written in terms of the D-A interface properties. We call this model the self-consistent diode (SCD) model as it is consistent with the DD-BI results provided that the key parameters are from the simulation data. By studying the effects of light intensity and carrier mobility, we find that the Shockley SCD parameters are voltage dependent because of space charge accumulation around the D-A heterojunction. Our models are successful in explaining the common discrepancies in OPV JV curve analyses, such as the validity of fitting for series resistance, deviation of ideality factor from the theoretical values, and different resistance values under light and dark conditions. The results provide a better understanding of OPVs with a D-A heterojunction and how we can capture its physics using the SCD equation.

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## I. INTRODUCTION

The Shockley equation (SE), which was derived specifically for inorganic p-n junctions, <sup>1</sup> is often applied to describe current density-voltage (JV) curves of organic donor-acceptor (D-A) heterojunction (HJ) solar cells, <sup>2-6</sup> despite fundamental differences between the two systems. <sup>7</sup> Important characteristics of organic D-A HJ solar cells that are different from inorganic cells are lower carrier mobilities <sup>8,9</sup> and lower dielectric permittivity. Lower dielectric constant results in larger exciton binding energy and bound charge-pair states at D-A interfaces, which are usually referred to as charge transfer states or polaron pairs (PPs), while low mobilities enhance the importance of space charge effects. <sup>10</sup> The generalized Shockley equation with parasitic

resistances is usually written as

$$J = J_0 \left[ \exp \left( \frac{q(V_a - JR_s)}{n_{id}k_BT} \right) - 1 \right] - J_{ph} + \frac{V_a - JR_s}{R_p}, \tag{1}$$

where  $J_0$  is the diode saturation current density, q is the elementary charge,  $V_a$  is the applied or output voltage between the anode and the cathode,  $R_s$  is a series resistance,  $n_{id}$  is the ideality factor,  $J_{ph}$  is a constant photocurrent, and  $R_p$  is a parallel resistance.

There are debates among researchers whether the SE can be applied to organic solar cells (OSCs). On the one hand, Wurfel *et al.* disputed the overall applicability of the SE to OSCs on the

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grounds that the Shockley parameters,  $J_0$ ,  $n_{id}$ ,  $R_s$  and  $R_p$ , may have no physical meaning in OSCs. On the other hand, equivalent electrical circuit models similar to the SE are successful in describing electrical responses of OSCs in impedance spectroscopy measurements and providing insights into carrier dynamics. However, the Shockley parameters are not constants (i.e., they are functions of voltage, light intensity, and charge transport properties  $^{12-14}$ ), so accurate descriptions of the Shockley parameters' behavior are needed.

Giebink  $et~al.^{15}$  (GWWF) propose a model for organic D–A HJ equations that are in the same form as the SE, where each parameter is physically meaningful. Liraz  $et~al.^{16}$  (LSST) propose an extended interface rate model that includes more processes enabling comparison of different physical effects. However, both of these analytic models require assumptions to estimate implicit quantities, such as the voltage drop across the donor and acceptor regions and the electron and hole densities at the D–A interface ( $n_I$  and  $p_I$ ), which are affected by space charge accumulation in many OPV devices. A more comprehensive approach that treats space charge accumulation more accurately is to use self-consistent drift-diffusion simulations.  $^{17-19}$  Barker  $et~al.^{20}$  developed a drift-diffusion model for organic bilayer solar cells that takes the aforementioned organic properties into account.

Here, we adopt this system of equations to include the interface model of GWWF, and we show a precise connection with Shockley parameters in the self-consistent diode (SCD) model. The SCD equation provides a better understanding of the physical origins of the Shockley parameters including their dependence on applied voltage; and thus, answers questions about the validity of using the Shockley equation to describe JV curves of organic bilayer PV devices. In principle and qualitatively, we can apply this understanding to other photovoltaics with similar layer structures, such as interdiffusion bilayer OPV<sup>21</sup> and organic salt photovoltaics.<sup>22,23</sup>

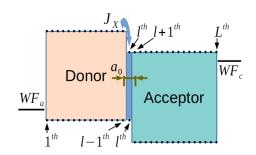
This paper focuses on introducing the SCD and DD-BI models, and showing how the voltage dependence of the SCD parameters reflect the fundamental physics of device models. We arrange the paper as follows. Section II is a theory section with two parts. The first part introduces the SCD equation and gives the relations of the SCD parameters to the quasi-Fermi energies for holes and electrons. The second part outlines the DD-BI device model and shows how the electron and hole quasi-Fermi energies are calculated from DD-BI calculations. Section III of the paper shows the voltage dependence of the equivalent circuit (SCD) parameters for a typical poly (3-hexylthiophene-2,5-diyl)/phenyl-C61-butyric acid ester (P3HT/PCBM) bilayer device. Note that interdiffusion heterojunctions with a donor-rich region near the anode and an acceptor-rich region near the cathode usually develop in this system even when using a sequential layer deposition method using orthogonal solvents. <sup>21,24,25</sup> However, instead of using the bulk heterojunction drift-diffusion model<sup>17</sup> which considers the blend of donor and acceptor molecules as a single active layer, we consider a donor-acceptor (D-A) heterojunction analogous to that of the inorganic p-n junction so we can gain physical insights into the diode properties of the D-A heterojunction in terms of D-A interface properties.

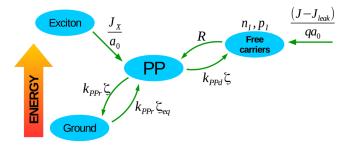
In the results section (Sec. III), we start from the effects of light intensity and voltage on the key D-A interface parameters. We then vary hole mobility to study the effects of space charge accumulation on the SCD parameters through the changes of carrier densities and quasi-Fermi levels. We explain why a constant resistance value is not sufficient to describe the diode characteristic. The correlations between series, parallel, and total solar cell resistances are explained later in the section. Section IV contains a discussion and summary of the key results of the paper. The supplementary material contains details of the implementation of the DD-BI model and some additional computational results that may be of interest to some readers.

In closing this introductory section, it is important to note that extensions of the GWWF model, such as the LSST model, and the inclusion of new physical effects are required for quantitative comparison with selected experimental systems over the full voltage range. However, the main purpose of this paper is to demonstrate precise relations between an important device model for bilayer OPVs and the self-consistent Shockley Diode equation. This analysis indicates that diode models of OPV IV response are consistent with bilayer OPV device simulations provided the Shockley parameters are voltage dependent. In the conclusion section, we argue that this voltage dependence is quite generic and persists in OPV device models that include a variety of additional physical effects. An important improvement of the DD-BI model used in the main text is to use a SRH recombination expression instead of the reduced form used in GWWF. In the supplementary material, we show that the voltage dependence of the Shockley parameters found in the simple recombination expression used by GWWF persists for a wide range of SRH model parameters, though with quantitative changes for some parameter values.

## II. THEORY

Figure 1 summarizes the modified GWWF interface model that is the basis for the DD-BI model and the SCD equation. Devices in this study consist of an anode, a donor layer, the D-A interface with a width  $a_0$ , an acceptor layer, and a cathode. We model the interface as a thin layer of mixed donor and acceptor molecules, having the energy levels at the highest occupied molecular orbital edge ( $E_{HOMO}$ ) and the lowest unoccupied molecular orbital edge ( $E_{LUMO}$ ) equal to  $E_{HOMO}$  of the donor and  $E_{LUMO}$  of the acceptor, respectively. As a result of photoexcitation, donor excitons diffuse to the interface with a current density  $J_X$ . Then, excited electrons transfer to acceptor molecules, forming interface polaron pairs (PPs) or charge transfer excitons. 10,26-28 The rate at which PPs reach the interface is  $J_X/a_0$ . Dissociations of PPs lead to free interface electrons and holes with densities  $n_I$  and  $p_I$ , respectively, at a rate of  $k_{PPd}\zeta$ , where  $k_{PPd}$  is PP dissociation coefficient and  $\zeta$  is PP density. PPs can also recombine to ground states at a rate of  $k_{PPr}\zeta$ , where  $k_{PPr}$  is PP recombination coefficient. PPs also come from recombination between interface free carriers (R) and thermal excitations of ground-state electrons ( $\zeta_{eq}$ ). Thermal equilibrium conditions, which are denoted by eq, are when  $J_X = 0$  and  $V_a = 0$ . R is general, and in the detailed calculations described in Sec. III, trap-assisted recombination is used for organic photovoltaic (OPV) examples. Summing all processes involving  $n_I$  and  $p_I$ 





**FIG. 1.** (Upper figure) An energy level diagram showing the device structure in this study. The dots represent the discretized spatial variable (x) or mesh points used in the DD-BI model. There are L mesh points, and the mesh separation length ( $\delta x$ ) between points is constant. We assume all processes involving PPs and interface free carriers (described in the lower figure) occur in the D–A interface region at the lth mesh point. (Lower figure) A diagram summarizing important rates at the D–A interface that affect interface PP density ( $\zeta$ ) and interface free carrier number densities ( $n_l$  and  $p_l$ ). Adapted from Ref. 15.

yields the total current density J. Note that we include a local leakage current density ( $J_{leak}$ ) to J, which we use to describe leakage current in the dark.

# A. The self-consistent diode (SCD) equation

The SCD equation is an analytical expression for OPV JV characteristics that is in the same form as the Shockley equation. It can accurately reproduce results from the drift-diffusion DD-BI device model, provided the SCD parameters are correctly extracted from the DD-BI model results. The SCD equation is an extension of the GWWF model, <sup>15</sup> which expresses the diode voltage and Shockley parameters in terms of quasi-Fermi energies and to include a leakage current in the dark.

Applying the detailed balance principle to  $\zeta$ ,  $n_I$ , and  $p_I$ , which are in steady states during solar cell operation, we obtain two interface rate equations,

$$\frac{J_X}{a_0} - k_{PPr}(\zeta - \zeta_{eq}) - k_{PPd}\zeta + R = 0,$$
 (2a)

$$k_{PPd}\zeta - R + \frac{(J - J_{leak})}{ga_0} = 0.$$
 (2b)

Solving Eq. (2) yields an expression for the current J as

$$J = qa_0(1 - \eta_{PPd})R_{eq}\left(\frac{R}{R_{eq}} - \frac{k_{PPd}}{k_{PPd,eq}}\right) - qJ_X\eta_{PPd} + J_{leak}, \quad (3)$$

where  $\eta_{PPd}$  is the PP dissociation probability expressed by  $\eta_{PPd} = k_{PPd}/(k_{PPd} + k_{PPr})$ ,  $^{29,30}$   $R_{eq}$  and  $k_{PPd,eq}$  are free carrier recombination rate and PP dissociation coefficient at equilibrium, and  $-qJ_X\eta_{PPd}$  is the voltage-dependent photocurrent.

The recombination rate R depends on the interface densities  $n_I$  and  $p_I$ . Generally, under illumination or bias, electrons and holes relax to achieve quasi-thermal equilibrium, where Fermi-Dirac statistics with separate quasi-Fermi energies ( $E_{fn}$  for electrons and  $E_{fp}$  for holes) can describe n and p,

$$n = N_{LUMO} \exp\left[\frac{-(E_{LUMO} - E_{fn})}{k_B T}\right], \tag{4a}$$

$$p = N_{HOMO} \exp\left[\frac{-(E_{fp} - E_{HOMO})}{k_B T}\right]. \tag{4b}$$

As a result, R usually contains an exponential function of  $E_{fn}$  and  $E_{fp}$  and a pre-factor term, which can be written in a general form as  $^{32}$ 

$$R = R_{eq} \exp\left(\frac{\Delta E_{fl}}{n_{id} k_B T}\right),\tag{5}$$

where

$$\Delta E_{fI} = E_{fn,I} - E_{fp,I} \tag{6}$$

is the difference in quasi-Fermi energies at the OPV interface.

We find that this form of R provides consistent numerical values of  $n_{id}$  with theories. For example, in the case of bimolecular recombination,  $^{33,34}$   $R = \beta n_I p_I$ , where  $\beta$  is a recombination coefficient. We obtain from Eq. (4) that

$$R = \beta N_{LUMO} N_{HOMO} \exp\left(\frac{-\Delta E_{HL}}{k_B T}\right) \exp\left(\frac{\Delta E_{fl}}{k_B T}\right),\tag{7}$$

where  $\Delta E_{HL}$  is the interface energy gap equal to acceptor  $E_{LUMO}$  minus donor  $E_{HOMO}$ . At equilibrium conditions where the quasi-Fermi levels do not split from the intrinsic Fermi level  $(E_f)$ , i.e.,  $\Delta E_{fl} = 0$ , we have

$$R_{eq} = \beta N_{LUMO} N_{HOMO} \exp(-\Delta E_{HL}/k_B T), \tag{8}$$

and hence Eq. (7) is in the same form as Eq. (5) with  $n_{id}=1$  as it must.

Substituting Eq. (5) for R in Eq. (3) yields our proposed general ideal diode equation for organic D-A PV with arbitrary

recombination processes,

$$J = qa_0(1 - \eta_{PPd})R_{eq}\left(\exp\left(\frac{\Delta E_{fl}}{n_{id}k_BT}\right) - \frac{k_{PPd}}{k_{PPd,eq}}\right)$$

$$- qJ_X\eta_{PPd} + J_{leak}.$$
(9)

With  $k_{PPd}/k_{PPd,eq} \approx 1$  as suggested by GWWF, <sup>15</sup> Eq. (9) is of a form similar to the Shockley form in Eq. (1), and it defines the diode saturation current as

$$J_0 = qa_0(1 - \eta_{PPd})R_{eq}. (10)$$

In order to make contact with device models, we need to relate the various terms in Eq. (9) to Eq. (1) by relating the equivalent circuit parameters to the quasi-Fermi energies and other quantities in the device models. These relations are as follows.

#### 1. Series resistance

According to Eqs. (1) and (9), the voltage across the Shockley diode, or photovoltaic voltage, is given by<sup>35</sup>

$$V_d = V_a - J(V_a)R_s = \frac{\Delta E_{fI}}{q},\tag{11}$$

which is the difference in quasi-Fermi energies in the middle of the interface region.

An obvious but important consequence of the equation is that the voltage at the D–A interface differs from the voltage across the electrodes  $(V_a)$  by  $JR_s$ . Hence, we have the definition of the voltage-dependent series resistance,  $R_s(V_a)$ , as

$$R_s(V_a) = \frac{V_a - \Delta E_{fI}/q}{I(V_a)}.$$
 (12)

The argument  $V_a$  will be dropped for simplicity. Because,  $V_a$  is the difference between anode and cathode Fermi energies ( $WF_a$  and  $WF_c$ ) under bias,

$$qV_a = WF_c(V_a) - WF_a(V_a). \tag{13}$$

Equation (12) defines  $R_s$  as the sum of the change of electron quasi-Fermi energy, in electronvolt, from the cathode to the interface plus the change in the hole quasi-Fermi energy from the anode to the interface, divided by the current density. In devices with multiple layers, changes of  $E_{fn}$  and  $E_{fp}$  arise from bulk transport and contact resistance <sup>12,36</sup> and can occur in any layers and interfaces so that the expression generalizes by taking a sum of all of the changes in quasi-Fermi energy. In this way, layers and contacts between layers can each be represented by its own value of R

The definition of  $R_s$  in Eq. (12) is valid even at open-circuit conditions where J=0 because quasi-Fermi levels align from the D-A interface to the electrodes, i.e.,  $V_{oc}=\Delta E_{fl}|_{V_a=V_{oc}}$ ,  $^{37,38}$  and, thus, both the numerator and the denominator approaches zero, making  $\lim_{V_a \to V_{oc}} R_s$  finite and solvable using L'Hospital's Rule.

#### 2. Ideality factor

According to Eq. (5), a general expression for  $n_{id}$  with arbitrary recombination types R is

$$n_{id} = \frac{\Delta E_{fI}}{k_B T ln(R/R_{eq})}.$$
 (14)

Hence,  $n_{id}$  measures the change in recombination rate ratio  $ln(R/R_{eq})$  at any  $V_a$  compared to the interface quasi-Fermi level splitting. We also note that Eq. (14) reduces to the expression proposed by Foertig *et al.*<sup>5</sup> [see e.g., Eq. (11) of their paper] at open-circuit voltage where  $\Delta E_{fl} = V_{oc}$ , which is derived differently.

#### 3. Parallel resistances

One of the simplest ways to extract parallel resistance  $(R_p)$  from a JV curve is to use  $R_p = [\partial J/\partial V_a]_{V_a=0}^{-1}$ , <sup>39</sup> i.e.,  $R_p$  governs the slope of a JV curve at  $V_a=0$  where higher slopes correspond to lower  $R_p$  values. However,  $R_p$  values measured under dark and illumination conditions usually differ by orders of magnitude. <sup>40</sup> Based on our simulations, which will be shown further in Sec. III E, the difference comes from the fact that leakage mechanisms under illumination are distinct from those in the dark.

By writing the voltage-dependent photocurrent term  $-qJ_X\eta_{PPd}$  as  $-qJ_X+qJ_X(1-\eta_{PPd})$ , the first term is the constant exciton current supplying the interface, and the second current is due to the total loss of excitons to ground states via PP recombination (i.e.,  $1-\eta_{PPd}$ ). The latter accounts for a finite slope of a light JV curve at  $V_a=0$  and can be considered as a leakage current. Let  $R_{p\_PP}$  be a recombination resistance of PP states that controls this leakage current  $qJ_X(1-\eta_{PPd})$ . We can write  $R_{p\_PP}$  from Eqs. (1) and (11) as

$$R_{p\_PP} = \frac{\Delta E_{fI}}{q^2 J_X (1 - \eta_{PPd})}.$$
 (15)

The local leakage current ( $J_{leak}$ ) is another leakage current in Eq. (9), which is necessary for device simulations in the dark (see Sec. III E). The actual mechanism behind the local leakage current is not fully understood, but trap-assisted tunneling processes <sup>41,42</sup> are sometimes important. For simplicity, we model  $J_{leak}$  similarly to the leakage current in Eq. (15) as

$$R_{p\_local} = \frac{\Delta E_{fl}}{q J_{leak}},\tag{16}$$

where  $R_{p\_local}$  is a fitting parameter.

Another process that causes a linear response of photocurrent at short-circuit conditions is photoconductivity. <sup>43,44</sup> We did not include this process because the device we used to validate our model with the optimal active layer thickness <sup>45</sup> shows high FF values and with no apparent linear slope of JV curves at short-circuit conditions. However, our model for  $J_{leak}$  in Eq. (16), which reads  $J_{leak} = R_{p,local}^{-1} \Delta E_{fl}/q$ , is in the same form as the photoconductivity current ( $J_{pc}$ ) model in the work by Renshaw *et al.*, <sup>43</sup> i.e.,  $J_{pc} = S_{pc}(V_a - JR_s - V_{bi})$ , where  $S_{pc}$  is the effective photoconductance (reciprocal of resistance). Our  $R_{p,local}$  value of  $2000\Omega m^2$  (see

Sec. III E) is consistent with their  $S_{pc}$  at zero illumination intensity  $(S_{pc,0})$  within an order of magnitude.

In the presence of light, both the recombination current  $qJ_X(1-\eta_{PPd})$  and the local leakage current  $J_{leak}$  occur, which can be modeled by two parallel resistances  $(R_{p\_PP}$  and  $R_{p\_local})^{46}$  (see Fig. 2). Accordingly, the total parallel resistance under illumination is

$$R_{p,\text{illumination}} = \left(\frac{1}{R_{p\_PP}} + \frac{1}{R_{p\_local}}\right)^{-1}.$$
 (17)

In most devices, the leakage current  $qJ_X(1-\eta_{PPd})$  is much larger than  $J_{leak}$  (i.e.,  $R_{p\_PP} \ll R_{p\_local}$ ), so  $R_{p,illumination} \approx R_{p\_PP}$ .

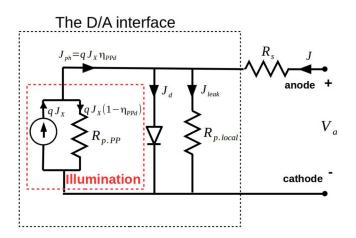
In the absence of light, the leakage current  $qJ_X(1-\eta_{PPd})$  vanishes, leaving  $J_{leak}$  as the only leakage pathway. Hence, total  $R_p$  in the dark is given by

$$R_{p,\text{dark}} = R_{p\_local}. \tag{18}$$

The difference between  $R_{p,\text{illumination}} \approx R_{p\_PP}$  and  $R_{p,\text{dark}} \approx R_{p\_\text{local}}$  leads to the discrepancy of measured  $R_p$  values under different conditions, <sup>11,40</sup> which will be discussed further in Sec. III E.

# 4. The SCD equation and its equivalent electrical circuit model

Putting together the results from above, we arrive at the SCD equation, which is a general JV relation in the Shockley equation



**FIG. 2.** An equivalent electrical circuit (EEC) model of the SCD equation [Eq. (19)] that has the total current (J) composed of the following component currents: the diode current  $J_d$ ; the total photocurrent  $J_{ph} = qJ_X\eta_{PPd}$ ; and the local leakage current  $J_{leak}$ .

form that can incorporate any recombination type,

$$J = J_0 \left[ \exp\left(\frac{q(V_a - JR_s)}{n_{id}k_BT}\right) - 1 \right] - qJ_X + (V_a - JR_s) \left(\frac{1}{R_{p,PP}} + \frac{1}{R_{p,local}}\right),$$
(19)

where the equivalent circuit parameters  $J_0$ ,  $R_s$ ,  $n_{id}$ ,  $R_{p\_PP}$ , and  $R_{p\_local}$  are defined in Eqs. (10), (12), (14), (15), and (16), respectively.

The equivalent electrical circuit (EEC) model corresponding to the SCD equation is given in Fig. 2, where each electrical component directly represents a real physical process in a bilayer OPV system. Thus, a single diode model where the EEC parameters are allowed to be voltage dependent gives a faithful representation of the true device physics. We now illustrate this correspondence and the typical dependence of EEC parameters on applied voltage by using device model calculations.

# B. The drift-diffusion for bilayer interface (DD-BI) model

The DD-BI model is a one-dimensional drift-diffusion model that implements the modified GWWF interface model in Fig. 1. The model solves the Poisson equation, current continuity equations, and drift-diffusion equations self-consistently as follows. The Poisson equation is given by

$$\frac{\partial^2}{\partial x^2} \psi = \frac{q}{\epsilon} [n + n_t - p - p_t], \tag{20}$$

where  $\psi$  is the electrostatic potential; n and p are free electron and hole concentrations, respectively;  $n_t$  and  $p_t$  are trapped electron and hole densities, respectively; and  $\epsilon$  is the permittivity. The current continuity equations are given by

$$\frac{\partial}{\partial x} J_n = qU,$$

$$\frac{\partial}{\partial x} J_p = -qU,$$
(21)

and the drift-diffusion constitutive equations are given by

$$J_{n} = -qn\mu_{n} \frac{\partial}{\partial x} \psi + q\mu_{n} V_{t} \frac{\partial}{\partial x} n,$$

$$J_{p} = -qp\mu_{p} \frac{\partial}{\partial x} \psi - q\mu_{p} V_{t} \frac{\partial}{\partial x} p.$$
(22)

Here,  $J_{n(p)}$  is the electron (hole) current density, U is the total free carrier generation rate equal to  $k_{PPd}\zeta-R$  (see Fig. 1),  $\mu_{n(p)}$  is the electron(hole) mobility, and  $V_t=k_bT/q$  is the thermal voltage. Here, we use the Einstein relation for the diffusion constant.<sup>47</sup> We neglect carrier generation in the bulk donor and acceptor layers because free carriers cannot be photo-generated from excitons without the D-A interface. Bulk carrier recombination is not included because electrons (holes) are the only majority carriers in

the acceptor (donor) [see the carrier densities in Fig. 6(a)]. We use Boltzmann statistics for free carriers' boundary conditions (see the supplementary material). Note that in order to include electrode's Fermi level pinning effects that cause induced bandgap narrowing and minority carrier recombination near the electrodes, image charge potential at the metal contact should be included as suggested by Magen and Tessler. However, as also suggested in the work, there are negligible minority carriers near the electrodes in the bilayer structure, so the effects are not detrimental.

The variables  $\psi$ , n,  $n_t$ , p,  $p_t$ ,  $J_n$ , and  $J_p$  depend on position x from the anode and are the key outputs from solving the above equations. The total current density J is the summation of  $J_n$  and  $J_n$ .

Solving Eqs. (20)–(22) numerically requires discretizations of all the variables into discrete values at mesh points as shown in Fig. 1. We use a constant mesh separation width  $(\delta x)$  of 1 nm, and the 1st and the Lth mesh points are donor and acceptor regions adjacent to the anode and the cathode, respectively. We assume the D–A interface is 1-nm thick from the l-1th to l+1th nodes, so the lth node, which is in the middle of the D–A interface, is the only node where carrier recombination and generation takes place.

We use an implicit Scharfetter–Gummel method<sup>49</sup> to solve the equations above, as has proven successful for bulk heterostructure devices;<sup>17</sup> however, the bilayer device model is more difficult to converge due to the sharp change in charge densities at the interface. Details of the computational methods are given in the supplementary material.

To make the connection to the interface model in Fig. 1, we calculate the electric field at the interface  $(F_I)$ , the PP density, and the rates  $k_{PPd}$  and  $k_{PPr}$ . The electric field  $F_I$  is positive when it points from the acceptor to the donor, i.e., the field promotes dissociation. In this case, the dissociation rate,  $k_{PPd}$ , is described by the Onsager–Bruan model, <sup>29</sup> which is given by

$$k_{PPd} = \frac{3}{4\pi a_0^3} k_{rec} \exp(-E_b/k_B T) \frac{J_1[2\sqrt{-2b}]}{\sqrt{-2b}},$$
 (23)

where  $k_{rec}=q(\mu_n+\mu_p)/\epsilon$  is the Langevin bimolecular recombination coefficient,  $E_b=q^2/(4\pi\epsilon a_0)$  is the PP binding energy,  $J_1$  is the first order of Bessel function of the first kind, and  $b=q^3F_I/(8\pi\epsilon k_B^2T^2)$ . If  $F_I$  is pointing from the donor to the acceptor, so the field aids recombination, the calculation procedure as suggested by GWWF is used, i.e., an additional barrier equal to  $-qF_Ir_ccos\theta$ , where  $r_c=q^2/(4\pi\epsilon k_BT)$  is the Onsager radius and  $\theta$  is the angle between PP separation length vector and D–A interface normal vector is added to the PP binding energy instead of using the Bessel function.  $k_{PPd}$  is averaged over the half-sphere using the following expression:

$$k_{PPd} = \frac{1}{\pi} \int_{-\pi/2}^{\pi/2} \frac{3}{4\pi a_0^3} k_{rec} \exp\left[\frac{-E_b + qF_I r_c \cos\theta}{k_B T}\right] d\theta.$$
 (24)

The PP recombination rate is described by

$$k_{PPr} = k_{PPr,0} \exp\left(\frac{-qF_I a_0}{k_B T}\right),\tag{25}$$

where  $k_{PPr,0}$  is the zero-field recombination rate.<sup>50</sup> Note that the sign of  $F_I$  is inverted from that of Ref. 50, so the definition of  $F_I$  is consistent with the  $k_{PPd}$  equations. The interface PP density is given by [Eq. (2)]

$$\zeta = \frac{J_X/a_0 + k_{PPr}\zeta_{eq} + R}{k_{PPr} + k_{PPd}}.$$
 (26)

Here, we use the recombination rate (R) for trap-assisted recombination in the same form as in GWWF,

$$R = \frac{q\mu_n}{\epsilon} n_I p_{It} + \frac{q\mu_p}{\epsilon} p_I n_{It}. \tag{27}$$

Each term in Eq. (27) is a reduced Shockley-Read-Hall (SRH) recombination <sup>51,52</sup> via donor HOMO tail states and acceptor LUMO tail states in the limit that the hole capture rate is much higher than electron capture rate in the donor and *vice versa* for the acceptor, so the SRH recombination can be considered as bimolecular recombination between localized trapped charges and mobile free carriers. <sup>53–55</sup> See Sec. SII in the supplementary material for the validity of using Eq. (27) to approximate the full SRH form including thermal emission from trap states.

We calculate trapped carrier densities in Eq. (27) using exponential trap distributions. <sup>56,57</sup> Acceptor trapped electron density at the interface ( $n_{lt}$ ) is approximated by the relation, <sup>15</sup>

$$n_{It} \approx H_A exp\left(\frac{E_{fn,I} - E_{LUMO,I}}{k_B T_{t,A}}\right),$$

$$n_{It} \approx H_A \left(\frac{n_I}{N_{LUMO}}\right)^{\frac{T}{T_{t,A}}},$$
(28)

where  $k_B T_{t,A} = E_{t,A}$  is the width of acceptor tail states and  $H_A$  is the total trap density at the acceptor LUMO band edge. A similar expression can be written for interface donor trapped hole density  $(p_{It})$  having the energetic width of  $E_{t,D} = k_B T_{t,D}$  and total trap density of  $H_D$  at the donor HOMO band edge,

$$p_{It} \approx H_D \exp\left(\frac{E_{HOMO,I} - E_{fp,I}}{k_B T_{t,D}}\right),$$

$$p_{It} \approx H_D \left(\frac{p_I}{N_{HOMO}}\right)^{\frac{T}{I_{t,D}}}.$$
(29)

Once the electron and hole densities are found at each position in the device, we use the definitions in Eq. (4) to find the electron quasi-Fermi level  $E_{fn}$ ,

$$E_{fn} = E_{LUMO} + k_B T ln(n/N_{LUMO}), \tag{30}$$

and the hole quasi-Fermi level  $E_{fp}$ ,

$$E_{fp} = E_{HOMO} - k_B T ln(p/N_{HOMO}). \tag{31}$$

The Shockley parameters in the SCD equation can then be evaluated using the expressions in Eqs. (10), (12), and (14)–(16). From

this construction, it is clear that if the equivalent circuit parameters are calculated in this way, the EEC provides a precise representation of the device model.

#### III. RESULTS

In this section, results for a typical bilayer OPV system are presented to illustrate the voltage dependence of the equivalent circuit parameters. Then, we apply our models to the dependence of these equivalent circuit parameters on donor hole mobility.

The devices studied are based on a P3HT/PCBM system that has the thicknesses of the donor and the acceptor layers of 50 nm and 22 nm. Definitions and values of simulation parameters are summarized in Table I. The parameters result in a JV curve under illumination having  $V_{oc} = 0.67 \text{ V}$ ,  $J_{sc} = -70 \text{ Am}^{-2}$ , and FF = 67%, which are close to the values quoted in Ref. 45; i.e.,  $V_{oc} = 0.66 \text{ V}$ ,  $J_{sc} = -69 \text{Am}^{-2}$ , and FF = 68%. We did not attempt a high resolution fit to the experimental data as we intend to use values typical of organic PVs not to fit a specific system. Unless stated otherwise,

**TABLE I.** Summary of definitions and values of important parameters used in simulations of P3HT/PCBM bilayer solar cells.

Parameter	Definition	Values
$\mu_p$	Hole mobility in the donor and acceptor layers	$2.0 \times 10^{-8} \text{ m}^2$ $V^{-1} \text{ s}^{-1} 58$
$\mu_n$	Electron mobility in the donor and acceptor layers	$2.0 \times 10^{-7} \text{ m}^2$ $V^{-1} \text{ s}^{-1} 59$
$\phi_a, \phi_c$	Injection barriers at the anode	0.2 eV 60, 0.1
<i>  u                                   </i>	and the cathode $\phi_a = WF_{anode} -$	eV
	$E_{HOMO,D}$ and $\phi_c = E_{LOMO,A} - WF_{anode}$ , where WF denotes work	
	function.	
$\epsilon$	Dielectric permittivity of the	$3.8\epsilon_0$ 61 and
	donor and acceptor layers	62
$E_{t,A}$ , $E_{t,D}$	Characteristic Urbach tail	$E_{t,A} = 40 \text{ meV},$
	energies of exponential trapped	$E_{t,D}$ 60 meV 62
	electron and trapped hole	
	distributions	
$k_{PPr,0}$	The zero-field polaron pair recombination rate	$(30 \mu\text{s})^{-1}$
$E_{LUMO,D}$ ,	The LUMO and the HOMO	-3.0  eV, -4.9
$E_{HOMO,D}$	energy levels of the donor	eV 63 and 64
$E_{LUMO,A}$ ,	The LUMO and the HOMO	-3.7  eV, -6.1
$E_{HOMO,A}$	energy levels of the acceptor	eV 63 and 64
$N_{HOMO}$ ,	Densities of states at the HOMO	$1.0 \times 10^{27} \mathrm{m}^{-3}$
$N_{LUMO}$	and the LUMO band edges of	
	both the donor and the acceptor	
$H_D$ , $H_A$	Total trap densities at the band	$1.0 \times 10^{24} \mathrm{m}^{-3}$
	edges of the donor and the	
	acceptor	20 -
$J_X$	Exciton current density reaching	$4.4 \times 10^{20} \mathrm{m}^{-2}$
	the D–A interface	$s^{-1}$
$a_0$	The D-A interface width	1.0 nm

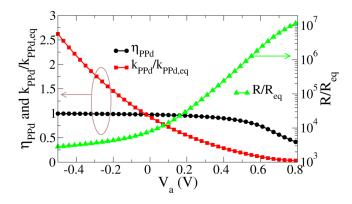
parameter values in Table I are used throughout this study as control variables.

In the following, we first show how the SCD Shockley parameters vary with applied voltage. Then, we vary donor hole mobility to illustrate how the voltage-dependent Shockley parameters change as the device physics changes. First, Fig. 3 presents the voltage dependence of dissociation and recombination quantities for the materials data in Table I. The figure shows that the approximation  $k_{PPd}/k_{PPd,eq} \sim 1$ , as used in Eq. (19), is a good approximation over most of the applied voltage range as the quantity  $R/R_{eq}$  is quite large over the voltage range considered.

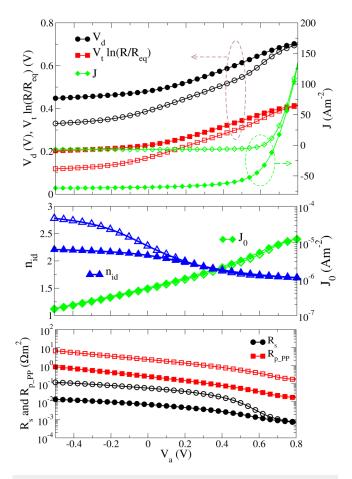
#### A. Applied voltage dependence of SCD parameters

The way that the SCD Shockley parameters vary with the applied voltage at two intensities (1 sun and 0.1 suns), using the material's values of Table I, are presented in the bottom two panels of Fig. 4. These results are calculated from DD-BI device simulations using Eqs. (10), (12), (14), and (15) to find the Shockley parameters. Key quantities in these equations are presented in the top panel of the figure. Clearly, the SCD Shockley parameters are both voltage and intensity-dependent, and the origin of these behaviors is easy to trace to the device physics through the voltage dependences of the key device properties, as presented in the top panel of the figure.

In this particular case (see Table S4), the SCD Shockley parameters vary by an order of magnitude or more in going from the short-circuit to open-circuit conditions. The primary reason is the increase in charge density from the electrode injections, which reduces the series resistance. The increased carrier density also results in increased interface trapped carrier density,  $n_{It}$  and  $p_{It}$ , and changes the nature of trap-assisted recombination as indicated by the ideality factor, e.g., at one sun intensity,  $n_{id} = 2.10$  at short circuit while at open circuit, it is 1.72. These changes cause the variations of the key quantities in Fig. 3, which directly affect the diode saturation current and parallel resistance. The strong dependence of the Shockley parameters on applied voltage leads to questions about the validity of extracting the correct physics insights



**FIG. 3.** Plots of  $\eta_{PPd}$ ,  $k_{PPd}/k_{PPd,eq}$ , and  $R/R_{eq}$  as a function of  $V_a$  of a device with parameters in Table I.



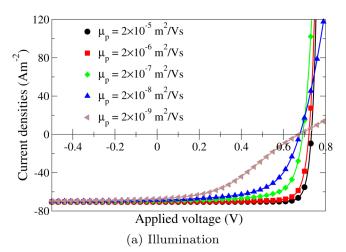
**FIG. 4.** Voltage dependences of key properties and the SCD Shockley parameters in the SCD model: (upper panel)  $V_d$ ,  $V_t ln(R/R_{eq})$ , and J; (middle panel)  $n_{id}$  and  $J_0$ ; and (bottom panel)  $R_s$  and  $R_{p\_PP}$ , derived from DD-BI results under 1—sun intensity (opaque symbols) and 0.1—sun intensity (open symbols).

when using constant Shockely parameters, as is typical in experimental studies of  $\mathsf{OPVs.}^{11}$ 

## B. Effects of changing the hole mobility

In many new OPV materials developing methods to increase the hole mobility is a challenge, and it is, thus, important to understand the effects of hole mobility on device physics. In this section, devices with hole mobilities  $(\mu_p)$  in the range of  $10^{-5}$  to  $10^{-9}\,\mathrm{m}^2/\mathrm{Vs}$  are studied, and how the device physics changes the voltage dependence of the SCD Shockley parameter is discussed. The other materials values used in this section are taken from Table I.

Figure 5 shows JV curves calculated using the DD-BI (symbols) and the SCD (solid lines) models under illumination and dark conditions for the five different hole mobility values. Values of  $J_{sc}$ ,  $V_{oc}$ , FF, and relative power conversion efficiency (PCE) of the devices under illumination are summarized in Table S5 and



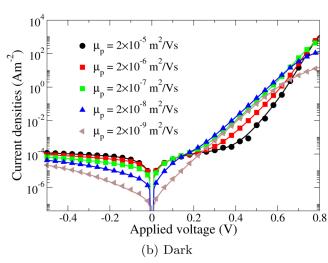


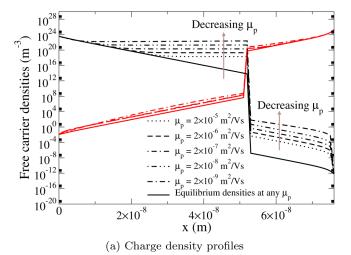
FIG. 5. Simulated JV curves under (a) illumination and (b) dark conditions of P3HT/PCBM bilayer devices with different hole mobilities.

Fig. S5. Short-circuit current does not change noticeably as the hole mobilities reduce. The reduction of FF is the primary reason for losing PCE, and the trend agrees well with other works in the literature. <sup>11,65,66</sup> The s-shaped JV behavior is noticeable in the device with  $\mu_p = 2 \times 10^{-9} \, \mathrm{m^2 V^{-1} \, s^{-1}}$  because of charge accumulation in the active layer (see the discussion below)

Reductions of the dark current in the high  $V_a$  limit and the slopes around  $V_{oc}$  under illumination indicate an increment in  $R_s$  as a result of decreasing the hole mobility. Series resistance is usually related to carrier mobilities via the electrical conductivities,  $^{11}$   $\sigma_n = q\mu_n n$  and  $\sigma_p = q\mu_p p$ , where n and p are free electron and hole densities, respectively. However, due to the fact that the charge densities are not constant in space [see Fig. 6(a)] because of space charge accumulation, the relationship between  $R_s$  and the electrical conductivity (or resistivity) has to be obtained via an

integral over the active layers' thicknesses. Here, we use the expression for  $R_s$  in terms of quasi-Fermi energies [see Eq. (12)], which is valid under any circumstances and fully treats space charge effects.

Figure 6 shows free hole density, free electron density (top figure), the quasi-Fermi energies, and band diagrams (bottom figure) as a function of position at short-circuit conditions ( $V_a = 0V$ ). The density and potential profile are used to calculate energy level diagrams using Eq. (4) in Fig. 6(b). At thermal equilibrium, where  $J_X = 0$  and  $V_a = 0$ , electron and hole density profiles decay exponentially from the electrodes and are almost invariant with changing  $\mu_p$ . The reason for this behavior is that at equilibrium, the density of



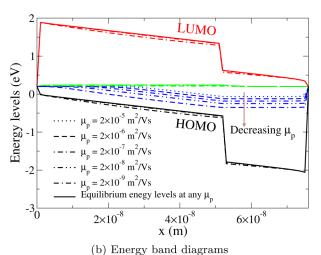


FIG. 6. Calculation results at short-circuit conditions ( $V_a = 0 \text{ V}$  and  $J_X = 4.4 \times 10^{22} \,\mathrm{m}^{-2} \,\mathrm{s}^{-1}$ ) and at thermal equilibrium ( $V_a = 0V$  and  $J_X = 0$ ) of (a) hole densities (black lines) and electron densities (red lines) as a function of position—charge density profiles—of the devices with different  $\mu_{\scriptscriptstyle D}$  values. (b) Energy band diagrams showing  $E_{fp}$  (blue lines),  $E_{fn}$  (green lines), HOMO (black lines), and LUMO (red lines) levels as a function of position calculated from the density profiles using Eq. (4).

free carriers is small, so the applied coulomb potential from the electrodes is not screened. The LUMO and the HOMO bands then appear almost linear due to the linear potential dropped across the active layers, except near the electrodes where charges accumulate. Because total electron  $(J_n)$  and hole  $(J_p)$  currents have to be zero at equilibrium, i.e.,  $J_n(x) = \mu_n(x)n(x)\nabla E_{fn,eq}(x) = 0$  and  $J_p(x) = \mu_p(x)p(x)\nabla E_{fp,eq}(x) = 0$ , <sup>31</sup> equilibrium quasi-Fermi energies  $(E_{fn,eq}$  and  $E_{fp,eq})$  have to be spatially invariant and do not split from each other. Hence, based on these conditions and Eq. (4),  $n_{eq}$  and  $p_{eq}$  distribute exponentially from the electrodes to the D-A interface and are not affected by carrier mobilities.

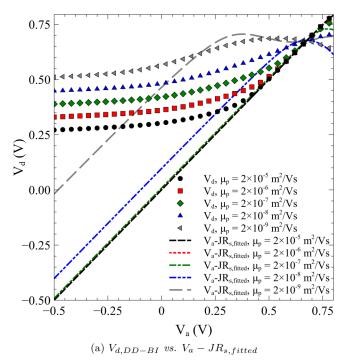
Under illumination, photo-generation processes at the D-A interface produce a considerable number of carriers, resulting in higher majority charge densities around the D-A interface that screen the applied coulomb potential. Near the interface, the screened electric field leads to reduced drift currents and spatial invariance of majority interface charge accumulation. This process can be considered as space charge accumulation, and the degree of the accumulation depends on the mobilities, as shown in Fig. 6(a), i.e., there is more space charge accumulation when charge mobility is lower. In the device with  $\mu_p = 2 \times 10^{-9} \,\mathrm{m}^2 \,\mathrm{V}^{-1} \,\mathrm{s}^{-1}$ , the level of donor space charge accumulation is high, which significantly increases interface recombination and reduces charge extraction, giving rise to the s-shaped curve in Fig. 5. This high level of space charge accumulation is similar to the work by Wang et al.,67 which introduces a thick exciton blocking layer to induce the s-shape effects.

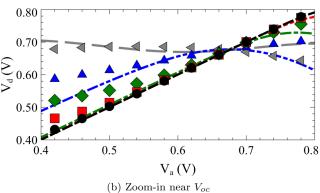
According to Eq. (4),  $E_{fp}$  near the donor interface has to be parallel to  $E_{HOMO}$  because of the constant majority carrier density and vice versa for  $E_{fn}$  and  $E_{LUMO}$  in the acceptor. This process gives rise to a split of interface quasi-Fermi levels;  $\Delta E_{fI} = E_{fn,I} - E_{fp,I}$ , where  $\Delta E_{fI}/q$  is the actual voltage driving the D-A interface—the diode voltage  $(V_d)$ . Higher degrees of space charge accumulation from lower  $\mu_p$  values bring  $E_{fp}$  closer to  $E_{HOMO}$ , resulting in the broader space charge region and a higher diode voltage.

## C. Space charge effect on diode voltage

Diode voltages of the devices having different  $\mu_p$  values from two different methods: (1)  $qV_d = E_{fn,I} - E_{fp,I}$  and (2)  $V_d = V_a - J(V_a)R_s$ , where  $R_s$  is a constant from fitting, but  $J(V_a)$  is from the simulations, are plotted in Fig. 7. Note that our  $V_d$  results agree with the internal voltage  $(V_{int})$  in Ref. 11. The results indicate that a constant  $R_s$  cannot reproduce the actual diode voltage except in the voltage range near  $V_{oc}$  in high-mobility devices, which are not typical for OPVs. The lack of treatment of space charge effects near the interface when assuming a constant R<sub>s</sub> causes the problems evident in this figure, while  $qV_d = E_{fn,I} - E_{fp,I}$  already includes the space charge effects in the quasi-Fermi levels. The results here agree with those by Würfel et al.11 with the following

First, for  $V_a < V_{oc}$ ,  $V_d$  is always higher than  $V_a$  because of space charge accumulation near the D-A interface that splits the interface quasi-Fermi levels. This accumulation of  $n_I$  and  $p_I$ causes an increase in Gibbs free energy density,  $n_I E_{fn,I} - p_I E_{fp,I}$ , in interface donor and acceptor molecules.<sup>68</sup> The change in the Gibbs free energy creates an electromotive force (emf), which is  $V_d$  in this case. The emf voltage must be larger than the external voltage  $(V_a)$ 





**FIG. 7.** Plots of (a) the diode voltages:  $V_d = (E_{fn,l} - E_{fp,l})/q$ , compared with  $V_d$  plots using the conventional equation:  $V_d = V_a - JR_s$ , where  $R_s$  is a constant fitting parameter and (b) a zoom-in area of the plot near open-circuit voltage.

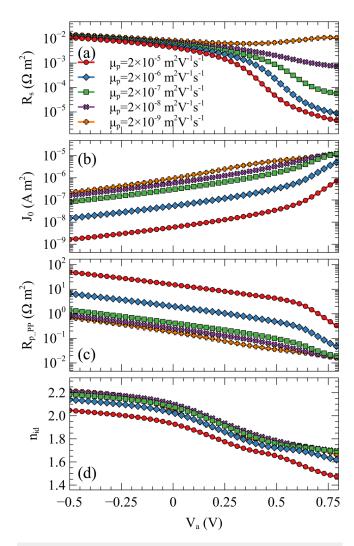
during solar cell operation so that the internal voltage drives free carriers out of the cell. Using the expression  $V_a - JR_s$ , where  $R_s$  is a constant, results in an incorrect description of  $V_d$ , including prediction of negative values at low bias.

Second, the conventional relation  $V_d = V_a - JR_s$ , where  $R_s$  is a constant, found by fitting to experimental data describes  $V_d$  under illumination surprisingly well around  $V_{oc}$  [see Fig. 7(b)].  $R_s$  around  $V_{oc}$  is relevant as the diode current that mainly depends on  $V_d$  becomes dominant there and determines the open-circuit JV slope and FF.  $V_a - JR_s$  with constant  $R_s$  completely fails to predict  $V_d$  at low and reverse bias regimes, as these regimes are dominated by the

voltage-dependent photocurrent  $(-qJ_X\eta_{PPd})$ . For these reasons, the Shockley equation with constant parameters usually fits experimental OPV JV curves under illumination. However, well-fitted parameters may not be able to provide physical insights because they do not include the voltage and illumination dependencies properly. Significant errors may arise in interpreting the physical meaning derived from using constant values of the fitting parameters.

# D. Effects of carrier mobility on the voltage-dependent SCD parameters

Figure 8 shows the voltage-dependent SCD parameters in the devices having different  $\mu_p$  values. It is known that carrier mobility



**FIG. 8.** The SCD parameters: (a)  $R_{s}$ , (b)  $J_{0}$ , (c)  $R_{p\_PP}$ , and (d)  $n_{id}$ , as a function of  $V_{a}$  of the devices having different donor hole mobility values ranging from  $2 \times 10^{-9} \, \mathrm{m^2 \, V^{-1} \, s^{-1}}$  to  $2 \times 10^{-5} \, \mathrm{m^2 \, V^{-1} \, s^{-1}}$  calculated using Eqs. (10), (12), (14), and (15) with the DD-BI simulation results.

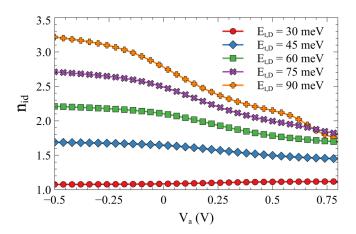
directly relates to the series resistance. However, carrier mobility also affects parallel resistance, diode saturation current, and the ideality factor due to space charge accumulation and recombination. Note that our  $R_s$  results are consistent with transport resistances measured using impedance spectroscopy by Guerrero *et al.*<sup>12</sup> The details about the voltage dependences of each SCD parameter are as follows.

According to the series resistance curves in the top panel of Fig. 8,  $R_s$  values of the devices having different  $\mu_p$  values have greater difference at higher applied voltages than at the short-circuit conditions. At  $V_a \approx 0$ , the built-in potential extracts almost all the current  $J_X$  out of the cell as the photocurrent, making  $\eta_{ppd} \approx 1$  and  $J \approx -qJ_X$ . This process is illustrated in Fig. 1 the rate  $J_X/a_0$  on the left flowing through the PP states flows into the outgoing rate  $J/qa_0$  on the right. In this situation, the densities  $\zeta$ ,  $n_I$ , and  $p_I$  are almost constant and balanced by the interface recombination and dissociation rates (see Fig. S6 in the supplementary material, for example). As a result, the interface electron-hole product  $(n_I p_I)$  is almost constant, as well as the split of quasi-Fermi levels because  $E_{fn,I} - E_{fp,I} \propto k_B T \ln(n_I p_I)$  [see Eq. (4)]. These results explain the small variations of  $V_d$  trends in the negative and low  $V_a$  regimes in Fig. 7(a) and accordingly explain the convergence of the  $R_s$  functions in Fig. 8. At high voltages, devices having higher mobilities can be injected with carriers from the electrodes more easily as  $V_a$ increases, resulting in a higher degree of interface charge accumulation and quasi-Fermi level splitting. Hence,  $\Delta E_{fI}/q$  of high-mobility devices will be closer to the external voltage, resulting in lower  $R_s$ values according to Eq. (12).

Moreover, in the high  $V_a$  limit, for injection barriers lower than  $0.3 \, {\rm eV},^{69}$  charge transport is dominated by injected charges from the electrodes. Space charge limited current (SCLC) limit  $^{39,59,70,71}$  explains the current J following the relations  $J \propto \mu V_a^p$  (i.e., Mott–Gurney law ) or  $J \propto \mu V_a^{m+1}$  if traps are present where  $m = E_t/k_BT$  and  $E_t$  is the characteristic Urbach tail energy.  $^{56,72}$  In this limit,  $R_s$  can be approximated by  $[\partial J/\partial V_a]^{-1}$ , so  $R_s \propto \mu^{-1} V_a^{-m}$ , which agrees with our results in Fig. 8, i.e.,  $R_s$  at  $V_a = 0.8V$  approximately varies with  $V_a^{-m}$ , where m = 2.3, and increases by about an order of magnitude when  $\mu_p$  is lowered by an order of magnitude.

The second panel in Fig. 8 shows plots of  $J_0$  of the devices. As described in Eq. (10),  $J_0$  primarily depends on  $\eta_{PPd}$ , which varies from unity to zero as  $V_a$  increases. Plots of  $\eta_{PPd}(V_a)$  functions are shown in Fig. S7 in the supplementary material. At high reverse bias,  $\eta_{PPd} \to 1$  as PPs are efficiently dissociated by the built-in and applied voltages, so  $J_0$  values are minimal due to the term  $1 - \eta_{PPd}$ . At the high  $V_a$  limit,  $\eta_{PPd} \to 0$  as the applied voltage significantly suppresses PP dissociation.  $J_0$  converges to  $qa_0R_{eq}$ . Interestingly,  $R_{eq}$  is not significantly affected by the mobility, so  $J_0$  functions with different  $\mu_p$  values approximately converge to the same value at high  $V_a$ , as seen in the figure.

The third panel of Fig. 8 shows the  $R_{p\_PP}$  functions of the devices having different  $\mu_p$  values. JV curves with higher slopes at low  $V_a$ , for example, the device with  $\mu_p = 2 \times 10^{-9} \,\mathrm{m^2 \, V^{-1} \, s^{-1}}$ , have higher magnitudes of the leakage current  $qJ_X(1-\eta_{PPd})$  and, thus, lower  $R_{p\_PP}$  values.  $R_{p\_PP}$  does not have a specific origin but it is associated with poor dissociation of PPs, i.e.,  $\eta_{PPd}$ . Similarly to the conventional  $R_p$ , higher  $R_{p\_PP}$  values are desirable.



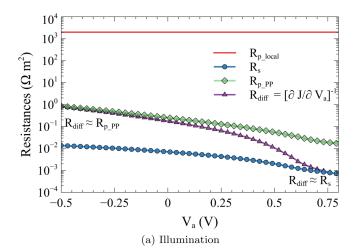
**FIG. 9.** Voltage-dependent ideality factor values calculated using Eq. (14) of the device with  $\mu_p=2\times 10^{-8}\,\mathrm{m^2\,V^{-1}\,s^{-1}}$  but varying the width of donor tail states ( $E_{l,D}$ ) from 30 to 90 meV.

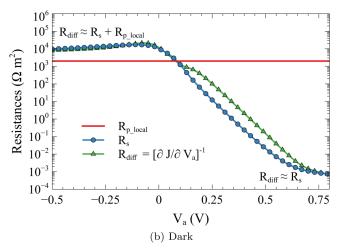
To understand the  $n_{id}$  results in the bottom panel of Fig. 8, we first look into the correlations between  $n_{id}$  and trap characteristics. In Fig. 9, we plot voltage-dependent  $n_{id}$  values of the device with  $\mu_p = 2 \times 10^{-8} \,\mathrm{m}^2 \,\mathrm{V}^{-1} \,\mathrm{s}^{-1}$  but different characteristic widths of donor tail states  $(E_{t,D})$  from 30 meV to 90 meV from the donor HOMO. The graphs confirm that deeper trap states result in higher  $n_{id}$  values. In devices with shallow traps, higher trapping and de-trapping rates between trap states and delocalized states result in interface trapped carrier densities ( $n_{It}$  and  $p_{It}$ ) closer to free carrier densities ( $n_I$  and  $p_I$ ). In this case, trap-assisted recombination in Eq. (27) will be similar to bimolecular recombination<sup>53</sup> and  $n_{id}$ approaches one. Moreover, the shift of recombination processes from trap-assisted recombination at low  $V_a$  to bimolecular recombination at higher  $V_a$  causes the voltage-dependent characteristics of  $n_{id}$ . Hence, we can understand from the  $n_{id}$  results in Fig. 8 that lower carrier mobility results in higher densities of trapped carriers and higher degrees of trap-assisted recombination.

# E. Contributions of $R_s$ , $R_{p\_PP}$ , and $R_{p\_local}$ to the measurement of resistance

We compare  $R_s$ ,  $R_{p\_PP}$ , and  $R_{p\_local}$  with the total differential resistance,  $R_{\rm diff} = [\partial J/\partial V_a]^{-1}$ , of the device with  $\mu_p = 2 \times 10^{-8} \, {\rm m}^2 \, {\rm V}^{-1} \, {\rm s}^{-1}$  as a function of  $V_a$  in Fig. 10 in order to show that each resistance actually contributes to the measurable total cell resistance. In devices with non-ohmic JV behaviors, such as diodes and solar cells, the differential (or dynamic) resistance is often measured for analysis purposes. Note that we use  $R_{p\_local} = 2000 \, \Omega {\rm m}^2$  for both under dark and illumination conditions, and note also that the leakage current  $qJ_X(1-\eta_{PPd})$  is zero in the dark, so  $R_{p\_PP}$  is infinitely high (i.e., does not play a role).

Under illumination, at low and negative  $V_a$ , the diode current is irrelevant as recombination of free carriers is very low, so recombination current is conducted by  $J_{leak}$  and  $qJ_X(1-\eta_{PPd})$ . The two leakage currents are under the same bias of  $V_d$ , but  $R_{p\_local} \gg R_{p\_PP}$ , so total leakage current in this regime is





**FIG. 10.** Plots of  $R_{\rm S}$ ,  $R_{\rm p\_PP}$ , and  $R_{\rm p\_local}$  as a function of applied voltage compared to the total differential resistance  $(R_{\rm diff} = [\partial J/\partial V_a]^{-1})$  of the device with  $\mu_p = 2 \times 10^{-8} \, {\rm m^2 \, V^{-1} \, s^{-1}}$  under (a) illumination and (b) dark conditions. Note that constant  $R_{\rm p\_local} = 2000 \, \Omega {\rm m^2}$  is used in both cases.

dominated by  $qJ_X(1-\eta_{PPd})$ , and thus only  $R_{p\_PP}$  contributes to the total device resistance [see Eq. (17)]. This prediction excellently agrees with  $R_{\rm diff}$  in Fig. 10(a). As  $V_a$  increases, the diode current increases, resulting in reducing  $R_{\rm diff}$  values. Once the diode current dominates,  $R_s$ , which primarily governs the diode term through the diode voltage, becomes the dominant resistance, and  $R_{\rm diff} \rightarrow R_s$ , which is clearly exhibited in the plot.

In the dark, only  $R_s$  and  $R_{p\_local}$  contribute to the total resistance. At negative  $V_a$  where the diode current is negligible,  $R_s$  and  $R_{p\_local}$  are connected in series (see Fig. 2 for an illustration). Consequently,  $R_{\rm diff} \approx R_s + R_{p\_local}$ , which agrees with Fig. 10(b). At low positive  $V_a$ ,  $R_s$  reduces from the higher numbers of injected carriers. However, both  $R_s$  and  $R_{p\_local}$  still play a role and result in  $R_{\rm diff}$  being an interpolation between the two resistances. Above a threshold voltage that activates the diode, the majority of the total

dark current is the diode current, so  $R_s$  dominates the resistances and  $R_{\rm diff} \to R_s$ .

As we can see from the results,  $R_s$ ,  $R_{p\_PP}$ , and  $R_{p\_local}$  are associated with well defined physical properties and contribute in different ways to the measured differential resistance. This result is another example of the validity and utility of the SCD equation in describing the correct physics of OPVs.

#### IV. CONCLUSIONS

We presented the SCD equation, which is equivalent to the Shockley equation but with voltage-dependent parameters, based on the DD-BI device model that solves the charge transport equations self-consistently. The two models provide physical definitions of Shockley parameters that are self-consistent and physically meaningful.

First, the diode saturation current, which is given by  $J_0 = qa_0(1-\eta_{PPd})R_{eq}$ , is a modified equilibrium recombination current under bias. It can vary many orders of magnitude under bias as it depends on the term  $1-\eta_{PPd}$  but it can roughly predict the equilibrium recombination rate as  $J_0 \approx qa_0R_{eq}$  in the high  $V_a$  limit.

For  $R_s$ , the relation  $V_d = V_a - JR_s = \Delta E_{fI}/q$ , where  $V_a$  is the difference between the electrode Fermi energies in electronvolt under bias, defines  $R_s$  as a resistance that spatially changes  $E_{fn}$  and  $E_{fp}$ , in eV, from the electrodes to the D–A interface. At solar cell operation voltages,  $\Delta E_{fI}/q$  is higher than  $V_a$ , so there is an electromotive force driving photo-generated charges to the external circuit. A constant fitted  $R_s$  cannot reproduce the nature of  $V_d$  because space charge effects are not included. Constant  $R_s$  can only result in reasonable  $\Delta E_{fI}/q$  values around  $V_{oc}$  in high-mobility devices and should be used for comparison purposes.

For  $R_p$ , we find that two sources of  $R_p$  with very different values are needed to simulate a device both under illumination and dark conditions correctly. The first one is  $R_{p\_local}$  from actual leakage pathways, such as pinholes. The other is the recombination resistance  $R_{p\_PP}$  from overall recombined PPs that causes a virtual leakage current of  $qJ_X(1-\eta_{PPd})$ . Total parallel resistance is  $R_p = (1/R_{p\_local} + 1/R_{p\_PP})^{-1}$ , where only  $R_{p\_local}$  dominates in the dark and only  $R_{p\_PP}$  typically dominates under illumination.

An ideality factor measures the change of free carrier recombination rate relative to the equilibrium value under the influence of the diode voltage,  $n_{id} = \Delta E_{fl}/V_t ln(R/R_{eq})$ . We show that this form of  $n_{id}$  yields valid  $n_{id}$  values that correlate to the trap characteristics and recombination processes.

This paper points out the importance of the voltage dependence of Shockley diode equation parameters for a complete description of OPV device physics when space charge effects are important. Though obtaining the true voltage-dependent functions is challenging experimentally, a combined experimental/device model approach is likely to be productive in many cases using the methodology presented here. Though the analysis here concentrates on the DD-BI model using the GWWF model, the voltage dependence of the associated Shockley parameters is expected to be robust for devices where space charge effects are important, as demonstrated in the supplementary material for the case of SRH recombination kinetics. Key to the analysis described here are the

explicit relations between DD-BI results and Shockley equation parameters. It is important to extend this work to include additional physical processes to enable fully quantitative extraction of voltage dependent parameters for a wide range of OPV devices.

#### SUPPLEMENTARY MATERIAL

See the supplementary material for the details of implementing the DD-BI model, the validity conditions of the reduce form of the SRH recombination via tail states, values of the SCD parameters:  $R_{p\_PP}$ ,  $R_s$ ,  $J_0$ , and  $n_{id}$ , at short-circuit and open-circuit conditions under 0.1—sun and 1—sun illumination intensities, efficiency parameters, interface densities, and polaron pair dissociation probability of the devices with different hole mobility values.

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#### **DATA AVAILABILITY**

The data that support the findings of this study are available from the corresponding authors upon reasonable request.

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