

EE 619

Radio Frequency Microelectronic Chip Design

Mid Semester Examination

27th Feb 2021, 1.00pm-4.00pm

1. Consider a system: $y(t) = \alpha_0 + \alpha_1 x(t) + \alpha_2 x^2(t)$
Where $x(t)$ is the input and $y(t)$ is the output
Say $x(t) = A_{in} \cos(\omega t)$
Suppose we plot the magnitude of the 2ω frequency component (in dB) at the output with respect to the magnitude of $x(t)$ (in dB). What will be the slope of this line be? (Express it in the form x:y i.e., for every x horizontal distance, the plot has a y vertical distance) **(1 mark)**

2. In an LNA choose all that are true: **(1 mark)**
 - a. The LNA decreases the signal noise as it passes through, thereby ensuring that SNR_{out} is slightly higher than SNR_{in}
 - b. The LNA adds very little noise to the input signal, thereby ensuring SNR_{out} is not much less than SNR_{in}
 - c. $Z_{s,opt}$ should be chosen close to 50Ω to ensure proper impedance matching.
 - d. Z_{in} should be equal to 50Ω so that $NF = NF_{min}$

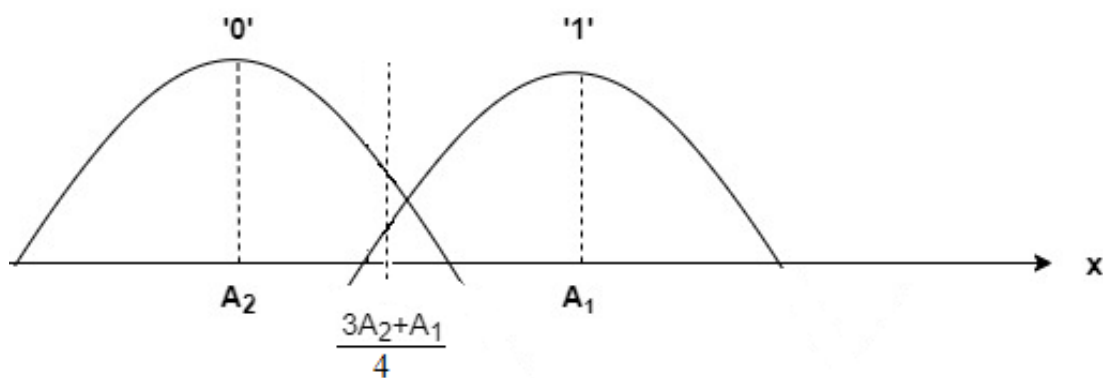
3. Choose all that are true. **(1 mark)**
While calculating SFDR,
 - a. $P_{in,min}$ is the value of P_{in} at which the SNR_{in} of the receiver is an acceptable value.
 - b. $P_{in,max} = P_{IIP3}$
 - c. $P_{in} = P_{in,max}$ when output intermodulation products are equal to the output noise floor.
 - d. $P_{in,min}$ is the value of P_{in} at which the receiver produces an output with an acceptable SNR_{out}

4. The number of frequency components of an FM modulated signal, when modulation index is 0 is **(0.5 mark)**
 - a. 1
 - b. 0
 - c. 2
 - d. 3

5. The bit energy (or power assuming $T_b = 1s$) for the bit '1' for ASK modulation is (write the answer) (assume A_c is the amplitude of the carrier) **(1 mark)**

Ans: _____

6. The figure below shows the probability of detection of '0' and '1'. The probability for bit '0' and bit '1' are given below:



$$p(\text{bit '0'}) = \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left[-\frac{(x-A_2)^2}{2\sigma^2}\right] \text{ and } p(\text{bit '1'}) = \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left[-\frac{(x-A_1)^2}{2\sigma^2}\right]$$

Suppose instead of $\frac{A_1+A_2}{2}$ we choose the threshold to be $\frac{3A_2+A_1}{4}$

- Find the probability of falsely detecting '0' **(2.5 mark)**
- Find the probability of falsely detecting '1' **(2.5 mark)**

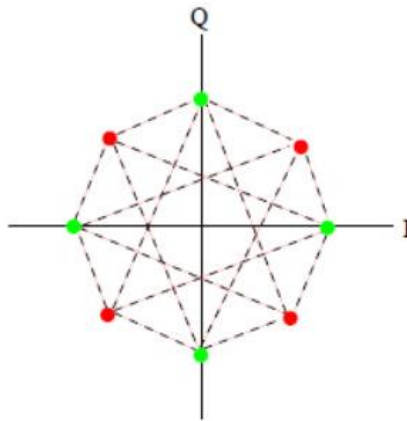
Express the answers in terms of the function $Q(\cdot)$, $A_1 - A_2$ and σ

7. **The** expression for $BER = Q\left(\frac{E_d}{2\sigma}\right)$ is applicable for all 3 ASK, PSK &FSK when threshold is $\frac{A_1+A_2}{2}$

- True or False? **(0.5 mark)**

8. In the figure shown OQPSK constellation is represented by the green dots or red dots?

(0.5 mark)



9. Power efficient modulation refers to (Choose all that are true)

(1 mark)

- a. A modulation scheme where resistive power loss in transmitter is less
- b. When spreading of spectrum due to non-linearities is less
- c. When the envelope of the modulated signal is constant
- d. When the inter-modulation distortion experienced by the transmitted signal is less

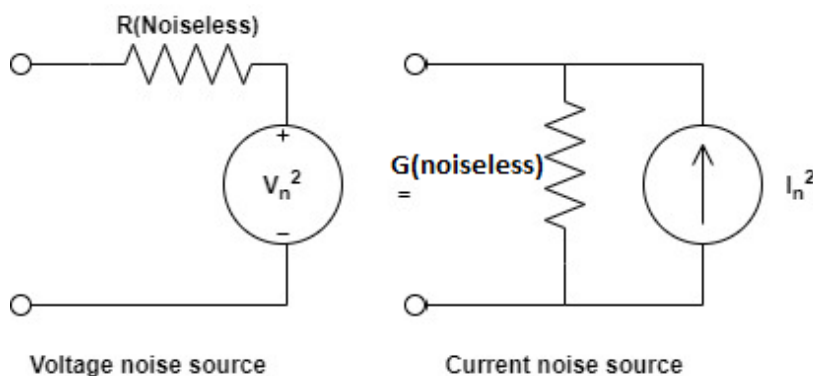
10. Which of the following modulation schemes can be detected non-coherently? (0.5 mark)

- a. OQPSK
- b. PSK
- c. FM
- d. DPSK

Choose all that are true.

11. Suppose the circuits shown in the figures below are equivalent

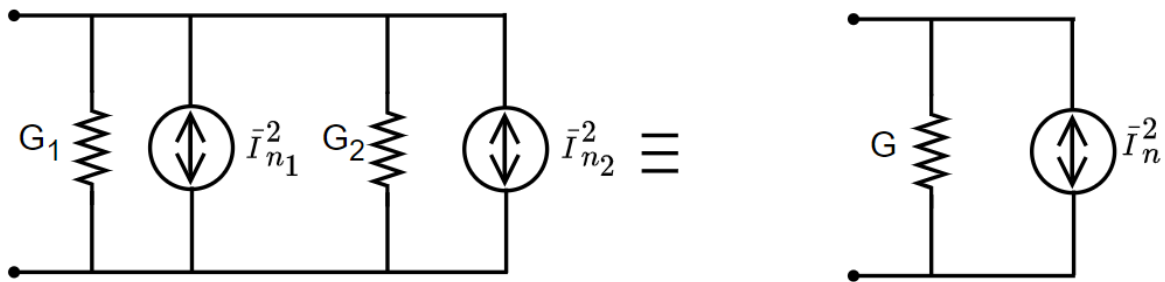
(1 mark)



- a. Express I_n^2 in terms of V_n^2 & R
- b. Express G in terms of R

12. Consider the following 2 equivalent circuits:

(1 mark)



\bar{I}_{n1}^2 and \bar{I}_{n2}^2 are the current noise sources of G_1 and G_2 . They are uncorrelated.

\bar{I}_n^2 is the current noise source of G .

G_1 , G_2 are noiseless conductances. G is a noiseless conductance.

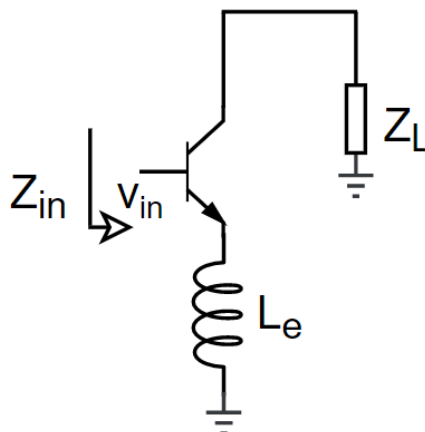
- Express G in terms of G_1 and G_2 .
- Express \bar{I}_n^2 in terms of \bar{I}_{n1}^2 and \bar{I}_{n2}^2

13. While expressing Noise Figure (NF) in dB, which of the following is the correct formula:

(0.5 mark)

- $20\log_{10}(\text{NF})$
- $10\log_{10}(\text{NF})$

14. Consider an Emitter degenerated CE amplifier as shown below:



The BJT small signal model parameters for the active region are as follows –

$$g_m = 40 \text{ mA/V}$$

$$r_b = 100 \, \Omega$$

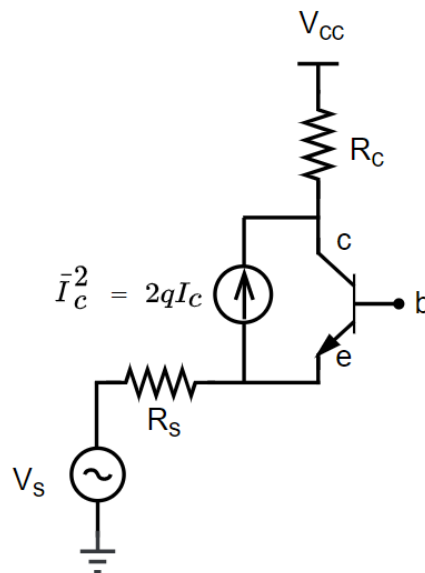
$$C_\pi = 1 \, \text{fF}$$

$$L_e = 6.33 \, \mu\text{H}$$

$$\text{Frequency, } f = 2 \, \text{GHz}$$

- Obtain an expression for $G_m = \frac{I_c}{V_{in}}$, ignoring r_b . Show that for sufficiently high values of L_e , G_m is independent of BJT parameters. **(2.5 mark)**
- Show that even if we include r_b , values of G_m will only be dependent on L_e (approximately) for the values given above. **(2.5 mark)**

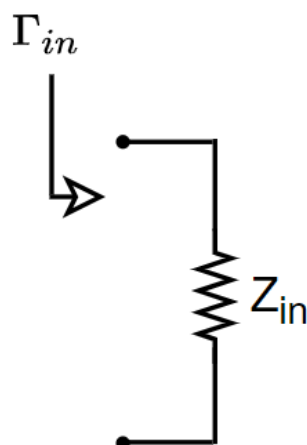
15. Consider a BJT in CB configuration:



Ignore all other sources of noise other than \bar{I}_c^2 and R_s :

- Find the expression for Noise Figure (NF) of this circuit. **(4 marks)**
- Show that when $g_m = G_s = 1/R_s$, $NF = 3/2$ **(1 mark)**

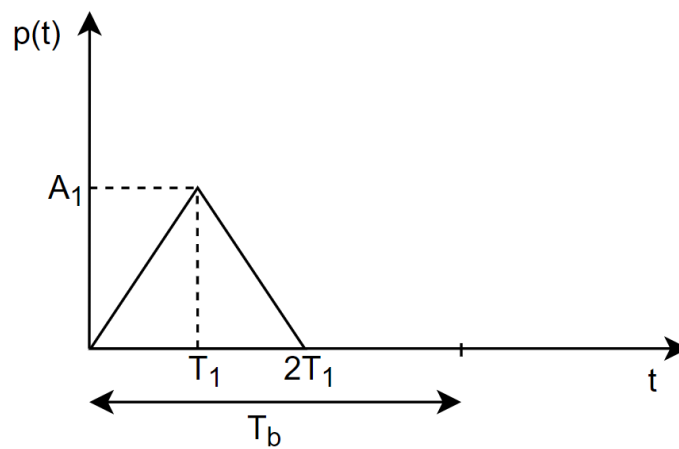
16. Consider the following circuit:



Γ_{in} is the reflection coefficient when characteristic impedance is Z_o .

- a. What is the value of Z_{in} in terms of Γ_{in} and Z_o ? **(2 marks)**
- b. What will the reflection coefficient be when the characteristic impedance is Z_o' (in terms of Γ_{in} , Z_o and Z_o') **(2 marks)**

17. Given:



Draw the waveform for $p(T_b - t)$ **(1.5 mark)**

[NOTE: Correctly label all amplitudes and points on 't' axis]