Finite Volume Methods for Hydrodynamics

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Finite Volume Methods for hydrodynamics

Overview

- Linear hyperbolic systems and nonlinear scalar equations: Riemann problem, Burgers equation, shocks and rarefactions. Explicit time integration, CFL condition, TVD concept and TVDLF method.
- Finite Volume discretization: integral versus differential form, from 1D to multi-D.
- Euler equations: gas dynamics in 1D, solution of the Riemann problem. TVDLF simulations.
- Roe solver for Euler equations: characteristic based shock-capturing schemes.
 Comparison with TVDLF.

Linear Hyperbolic Systems

constant coefficient linear system

$$\vec{q_t} + A\vec{q_x} = 0$$

- \Rightarrow with $\vec{q}(x,t) \in \Re^m$ and matrix $A \in \Re^{m \times m}$
- hyperbolic when A is diagonalizable with real eigenvalues
 - ⇒ **strictly hyperbolic** when distinct
 - $\Rightarrow m$ right eigenvectors + m real eigenvalues

$$A\vec{r}_p = \lambda_p \vec{r}_p$$
 with $p:1,\ldots,m$

write as

$$[A] \left[\vec{r}_1 \mid \vec{r}_2 \mid \dots \mid \vec{r}_m \right] = \left[\vec{r}_1 \mid \vec{r}_2 \mid \dots \mid \vec{r}_m \right] \left[\begin{array}{c} \lambda_1 \\ \lambda_2 \\ & \dots \\ \lambda_m \end{array} \right]$$

- \Rightarrow or shorthand $AR = R\Lambda$ with diagonal matrix Λ
- \Rightarrow matrix R with right eigenvectors as columns
- The solution to system $\vec{q_t} + A\vec{q_x} = 0$ is equivalent to:
 - \Rightarrow pre-multiply with R^{-1} or:

$$(R^{-1}\vec{q})_t + R^{-1}(R \Lambda R^{-1})\vec{q}_x = 0$$

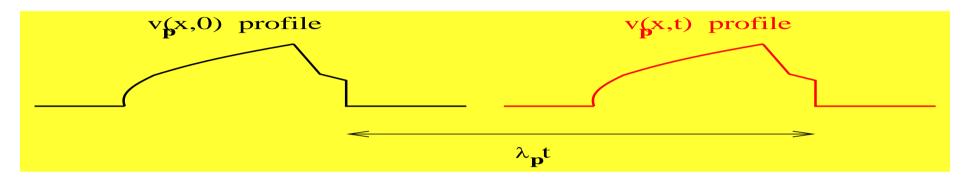
 \Rightarrow redefine $\vec{v} \equiv R^{-1}\vec{q}$ to get

$$\vec{v}_t + \Lambda \vec{v}_x = 0$$

 $\Rightarrow m$ independent constant coefficient linear advection equations!

Each advection equation has trivial analytic solution:

$$v_p(x,t) = v_p(x - \lambda_p t, 0)$$



⇒ analytic solution to the full linear hyperbolic system is

$$\Rightarrow \vec{q}(x,t) = \sum_{p=1}^{m} v_p(x - \lambda_p t, 0) \vec{r_p}$$

- \Rightarrow depends on initial data at m discrete points
- \Rightarrow superposition of m waves, advected independently without distortion
- nomenclature: \vec{v} are 'characteristic variables'
 - \Rightarrow curves $x = x_o + \lambda_p t$ are "p-characteristics"

The Riemann problem for a linear hyperbolic system

- Riemann Problem for linear hyperbolic system:
 - \Rightarrow initial data $\vec{q}(x,0) = \left\{ \begin{array}{ll} \vec{q_l} & x < 0 \\ \vec{q_r} & x > 0 \end{array} \right.$
 - ⇒ decompose initial data in terms of right eigenvectors as

$$\vec{q_l} = \sum_{p=1}^m \alpha_p \vec{r_p}$$

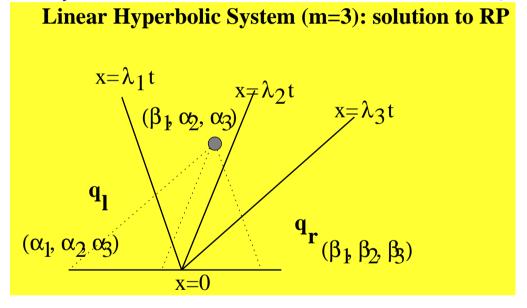
$$\vec{q}_r = \sum_{p=1}^m \beta_p \vec{r}_p$$

- then at t=0, characteristic variables are $v_p(x,0)=\left\{ egin{array}{ll} \alpha_p & x<0 \\ \beta_p & x>0 \end{array} \right.$
 - $\Rightarrow \text{ hence } v_p(x,t) = \left\{ \begin{array}{ll} \alpha_p & \text{if } x \lambda_p t < 0 \\ \beta_p & \text{if } x \lambda_p t > 0 \end{array} \right.$

the solution to the Riemann problem for linear hyperbolic system is then:

$$\vec{q}(x,t) = \sum_{\text{all p where } x - \lambda_p t < 0} \alpha_p \vec{r}_p + \sum_{\text{all p where } x - \lambda_p t > 0} \beta_p \vec{r}_p$$

 \Rightarrow graphically illustrated for m=3 with $\lambda_1<\lambda_2<\lambda_3$



- constant states separated by discontinuities
 - ⇒ traveling at characteristic speeds
 - \Rightarrow Note: jumps are eigenvectors of matrix A

Scalar nonlinear conservation law

• nonlinear scalar conservation law for u(x,t) written as

$$u_t + (f(u))_x = 0$$

- inviscid Burgers equation for $f(u) = u^2/2$
 - ⇒ quasi-linear form (assuming differentiability):

$$u_t + u u_x = 0$$

- \Rightarrow characteristic speed from Jacobian, i.e. derivative, $f_u = u \equiv f'(u)$
- \Rightarrow similar to linear advection equation $u_t + v \, u_x = 0$ (fixed v), which has trivial solution: u(x,0) advected with speed v

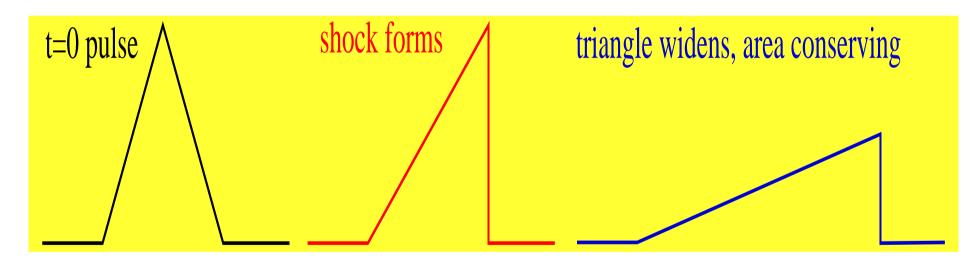
- Nonlinearity in inviscid Burgers $u_t + u u_x = 0$
 - \Rightarrow advection with local speed u
- Consider t=0 triangular pulse (width $2x_0$, height h_0) given by

$$u(x,0) = \begin{cases} u_0 & x \le -x_0 \\ u_0 + h_0 \frac{x_0 + x}{x_0} & -x_0 < x \le 0 \\ u_0 + h_0 \frac{x_0 - x}{x_0} & 0 < x \le x_0 \\ u_0 & x > x_0 \end{cases}$$

- ⇒ wave steepening and shock formation expected!
- tip of triangle experiences fastest rightward advection
 - ⇒ conserving total area underneath triangle, front edge steepens.
- discontinuity forms at time $t_s = x_0/h_0$
 - ⇒ tip of triangle catches up rightmost point of front edge
 - ⇒ discrete equivalent of conservation law across discontinuity
 - \Rightarrow Rankine-Hugoniot relation for left u_l and right u_r values

$$f(u_l) - f(u_r) = s\left(u_l - u_r\right)$$

- for inviscid Burgers case, find shock speed $s = (u_l + u_r)/2$
- fully analytic solution to triangular pulse problem
 - \Rightarrow after shock forms, base of triangle widens due to the speed difference between left edge traveling with u_0 , and shocked right edge traveling at speed s(t). In accord with conservation, the height of the triangle must therefore decrease in time.



⇒ Assignment: try different numerical schemes to simulate this evolution

The Riemann problem for Burgers

- specific initial condition separating 2 constant states
- Riemann problem for scalar conservation law

$$u = u_l$$
 for $x \le 0$

$$u = u_r$$
 for $x > 0$

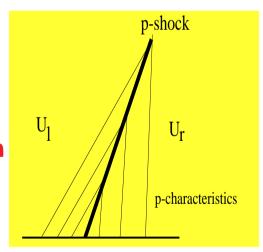
Rankine-Hugoniot states

$$f(u_l) - f(u_r) = s(u_l - u_r)$$

- \Rightarrow symmetric in arguments u_l and u_r
- For inviscid Burgers: only shock expected for $u_l > u_r$
 - ⇒ extra condition for admissable shock: Lax entropy condition

$$f'(u_l) > s > f'(u_r)$$

- ⇒ shock speed between characteristic speeds of 2 states
- ⇒ characteristics 'go into the shock'



- Rarefaction waves for Burgers equation
 - \Rightarrow when $u_l < u_r$ expect right state 'runs away' from left
 - \Rightarrow try 'centered simple wave' $u(\xi) = u(x/t)$
 - ⇒ conservation law translates into

$$f'(u)\frac{du}{d\xi} = \xi \frac{du}{d\xi}$$

⇒ rarefaction wave: for Burgers:

$$u(x,t) = u(x/t) = \begin{cases} u_l & x < u_l t \\ x/t & u_l t < x < u_r t \\ u_r & x > u_r t \end{cases}$$

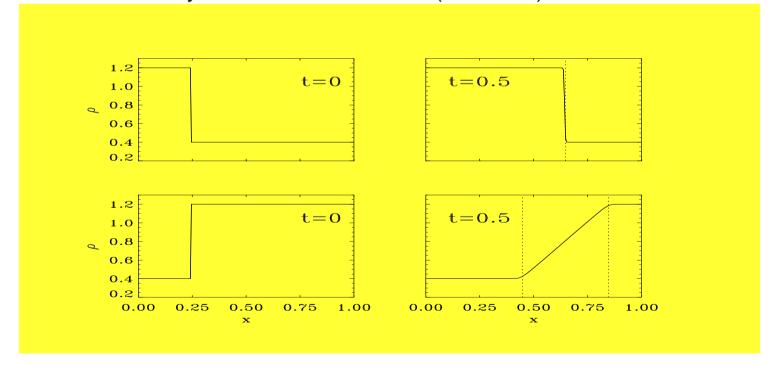
 $\Rightarrow u$ decreases (density: medium gets rarefied) when signal passes

Riemann problem for inviscid Burgers has two cases:

$$\Rightarrow \rho_l > \rho_r$$
: shock traveling at speed $s = \frac{\rho_l + \rho_r}{2}$

$$\Rightarrow \rho_l < \rho_r \text{: } \underline{\text{rarefaction wave}} \ \rho(x,t) = \rho(x/t) = \begin{cases} \rho_l & x < \rho_l t \\ x/t & \rho_l t < x < \rho_r t \\ \rho_r & x > \rho_r t \end{cases}$$

⇒ Numerically with TVDLF scheme (see later):



Numerical methods for nonlinear conservation law

- introduce spatial $x_i = i\Delta x$ and temporal $t^n = n\Delta t$ steps
 - \Rightarrow try **explicit** scheme on Burgers, directly discretize $u_t + u u_x = 0$ to

$$u_i^{n+1} - u_i^n + \frac{\Delta t}{\Delta x} u_i^n \left(u_i^n - u_{i-1}^n \right) = 0$$

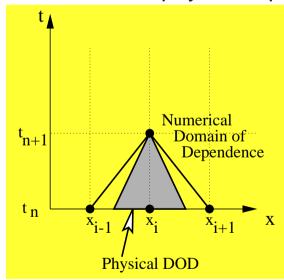
- \Rightarrow initial data [1,1,1,0,0,0] remains solution to this scheme
- \Rightarrow **WRONG!!!!** should be traveling shock at speed s=0.5
- reason: above scheme non-conservative (but ok for continuous data!)
 - ⇒ conservative scheme is of form

$$\mathbf{U}_{i}^{n+1} = \mathbf{U}_{i}^{n} - \frac{\Delta t}{\Delta x} \left[\mathbf{F}_{i+1/2} - \mathbf{F}_{i-1/2} \right]$$

 \Rightarrow numerical fluxes $\mathbf{F}_{i+1/2}$: time-average fluxes over cell edges $x_i + \frac{1}{2}\Delta x \equiv x_{i+\frac{1}{2}}$

Explicit time integration

- calculate fluxes (and sources) from known time level t^n
- ullet Explicit: Δt restricted by Courant, Friedrichs, Lewy condition domain of dependence of discretization must include PDE domain of dependence
 - $\Rightarrow \Delta t \leq$ crossing time of cells by fastest wave
 - $\Rightarrow \Delta t \leq \Delta x/c^{\max}$ with maximal physical speed c^{\max}



Lax-Friedrichs and Max-Cormack methods

Better explicit discretization: first order Lax-Friedrichs

$$u_i^{n+1} = \frac{u_{i+1}^n + u_{i-1}^n}{2} - \frac{\Delta t}{2\Delta x} \left(f_{i+1}^n - f_{i-1}^n \right)$$

⇒ scheme is **conditionally stable**: restriction by CFL condition

$$\left| \frac{\Delta t}{\Delta x} f'(u_i) \right| \le 1$$

⇒ conservative scheme, identify numerical flux as

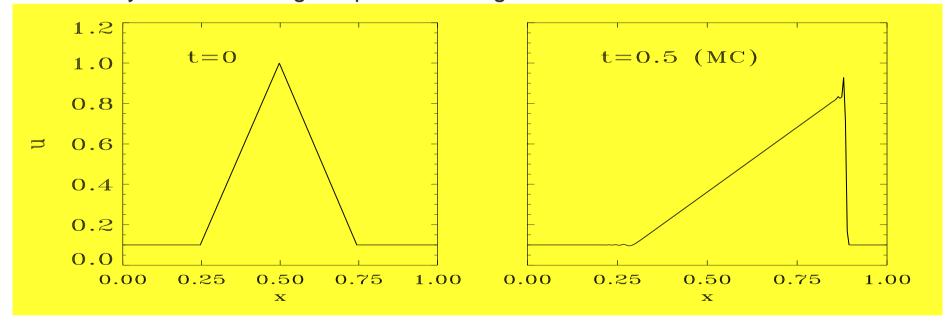
$$F_{i+1/2}^{LF} = \frac{1}{2} \left\{ f_{i+1} + f_i - \frac{\Delta x}{\Delta t} \left[u_{i+1} - u_i \right] \right\}$$

ullet first order accuracy: local truncation error $\propto \Delta t$

another, multilevel method: two-step MacCormack method:

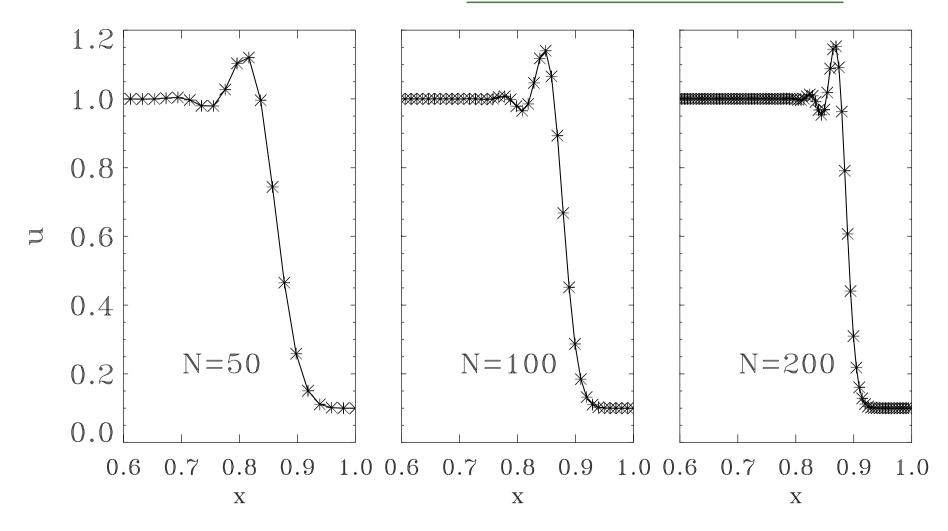
'predictor':
$$u_i^* = u_i^n - \frac{\Delta t}{\Delta x} \left(f_{i+1}^n - f_i^n \right)$$
 'corrector':
$$u_i^{n+1} = \frac{1}{2} (u_i^n + u_i^*) - \frac{1}{2} \frac{\Delta t}{\Delta x} \left(f_i^* - f_{i-1}^* \right)$$

- \Rightarrow step size in predictor now Δt
- \Rightarrow second order accurate: local truncation error $\propto \Delta t^2$
- Numerically simulate triangular pulse for Burgers



⇒ in agreement with theory, except for the 'wiggles'

- MacCormack method: dispersive
 - ⇒ manifests Gibbs phenomenon: for linear advection of discontinuity



 \Rightarrow non-monotonicity preserving: monotone u(x,0) develops extrema

Total Variation Diminishing concept

• total variation of function u(x) on domain [0,1] defined as

$$TV(u) \equiv \int_0^1 \left| \frac{du}{dx} \right| \, \mathrm{d}x$$

 \Rightarrow total variation of numerical approximation of u

$$TV(u^n) = \sum_{i=0}^{N} |u_{i+1}^n - u_i^n|$$

scheme is total variation diminishing (TVD) in time if

$$TV(u^{n+1}) \le TV(u^n) \quad \forall n$$

 \Rightarrow solution scalar conservation law has TVD property $\forall t_2 > t_1$

$$TV(u(x,t_2)) \leq TV(u(x,t_1))$$

- a TVD scheme is clearly monotonicity preserving!
 - ⇒ a new local extremum would raise TV
- Harten: any scheme written in general form

$$u_i^{n+1} = u_i^n + A_{i+1/2} \underbrace{\left(u_{i+1}^n - u_i^n\right)}_{\Delta u_{i+1/2}^n} - B_{i-1/2} \underbrace{\left(u_i^n - u_{i-1}^n\right)}_{\Delta u_{i-1/2}^n}$$

 \Rightarrow is TVD when coefficients $A_{i+1/2}$ and $B_{i-1/2}$ obey

$$A_{i+1/2} \ge 0$$

$$B_{i-1/2} \ge 0$$

$$0 \le A_{i+1/2} + B_{i+1/2} \le 1$$

first order Lax-Friedrichs scheme is TVD, since rewrites as

$$u_i^{n+1} = u_i^n + \frac{1}{2} \left(1 - \frac{\Delta t}{\Delta x} \frac{f_{i+1}^n - f_i^n}{\Delta u_{i+\frac{1}{2}}} \right) \Delta u_{i+\frac{1}{2}} - \frac{1}{2} \left(1 + \frac{\Delta t}{\Delta x} \frac{f_i^n - f_{i-1}^n}{\Delta u_{i-\frac{1}{2}}} \right) \Delta u_{i-\frac{1}{2}}$$

⇒ TVD requirements translate to CFL condition

$$\left| \frac{\Delta t}{\Delta x} \frac{f_{i+1}^n - f_i^n}{u_{i+1}^n - u_i^n} \right| \le 1$$

⇒ generalize Lax-Friedrichs scheme to second order, keep TVD property

TVDLF scheme

Recall: numerical flux for first-order Lax-Friedrichs is

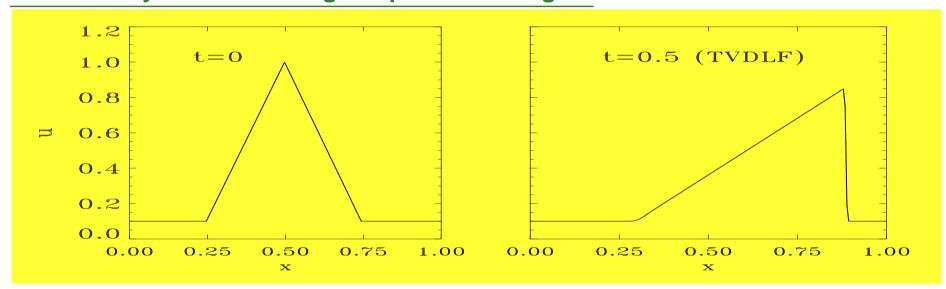
$$F_{i+1/2}^{LF} = \frac{1}{2} \left\{ f_{i+1} + f_i - \frac{\Delta x}{\Delta t} \left[u_{i+1} - u_i \right] \right\}$$

⇒ can improve scheme by changing to Local Lax-Friedrichs flux

$$F_{i+1/2}^{\text{LLF}} = \frac{1}{2} \left\{ f_{i+1} + f_i - |\alpha_{i+\frac{1}{2}}| \left[u_{i+1} - u_i \right] \right\}$$

- $\Rightarrow \alpha_{i+1/2} = \frac{f_{i+1}^n f_i^n}{u_{i+1}^n u_i^n}$, proxy for local characteristic speed f'(u)
- ⇒ still in accord with TVD, if CFL condition satisfied

- turn into second order accurate TVDLF scheme by
 - ⇒ use predictor-corrector approach (raise temporal accuracy)
 - ⇒ use some form of linear interpolation in space (but keep TVD!)
- Numerically simulate triangular pulse for Burgers



- \Rightarrow Riemann problem for $u_l > u_r$
- \Rightarrow Riemann problem for $u_l < u_r$

TVDLF scheme

- Robust, general scheme to ANY hyperbolic system, ensures TVD (for scalar)
 - ⇒ Predictor-corrector approach for temporal advance

$$\mathbf{U}^{n+1/2} = \mathbf{U}^n + \frac{\Delta t}{2} \left[-\nabla \cdot \mathbf{F}(\mathbf{U}^n) + \mathbf{S}(\mathbf{U}^n) \right]$$

$$\mathbf{U}^{n+1} = \mathbf{U}^n + \Delta t \left[-\nabla \cdot \mathbf{F}(\mathbf{U}^{n+1/2}) + \mathbf{S}(\mathbf{U}^{n+1/2}) \right]$$

- \Rightarrow CFL condition links Δt with Δx (explicit scheme)
- slope limited linear reconstruction and flux expression

$$\mathbf{F}_{i+\frac{1}{2}} = \frac{1}{2} \left\{ \mathbf{F}(\mathbf{U}_{i+\frac{1}{2}}^{L}) + \mathbf{F}(\mathbf{U}_{i+\frac{1}{2}}^{R}) - |c^{\max}(\frac{\mathbf{U}_{i+\frac{1}{2}}^{L} + \mathbf{U}_{i+\frac{1}{2}}^{R}}{2}) | \left[\mathbf{U}_{i+\frac{1}{2}}^{R} - \mathbf{U}_{i+\frac{1}{2}}^{L} \right] \right\}$$

- \Rightarrow scalar c^{\max} denotes maximal physical propagation speed
- \Rightarrow for 1D HD c^{\max} is $|v_x|$ plus sound speed, for MHD $c^{\max} = |v_x| + c_f$

Integral form of conservation law

- consider cell $[x_1, x_2]$ and quantity u(x, t) within cell
 - \Rightarrow flux over cell edge f(u) changes total mass from t_1 to t_2 by

$$\int_{x_1}^{x_2} u(x, t_2) dx = \int_{x_1}^{x_2} u(x, t_1) dx + \int_{t_1}^{t_2} f(x_1, t) dt - \int_{t_1}^{t_2} f(x_2, t) dt$$

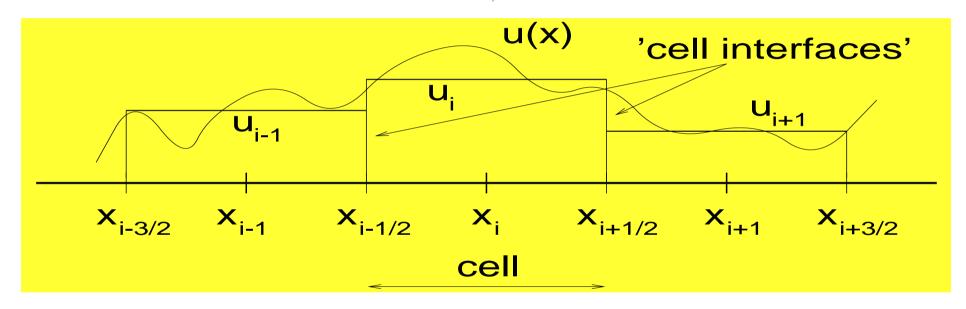
⇒ integral form of scalar conservation law

$$u_t + (f(u))_x = 0$$

- integral form more general: allows for discontinuous solutions
 - ⇒ differential form assumes differentiable functions

- Finite Volume method in 1D for system of conservation laws
 - \Rightarrow interpret U_i as average value of U(x,t) in $[x_{i-1/2},x_{i+1/2}]$:

$$\mathbf{U}_i(t) \equiv \frac{1}{\Delta x_i} \int_{x_{i-1/2}}^{x_{i+1/2}} \mathbf{U}(x,t) \, \mathrm{d}x \,,$$



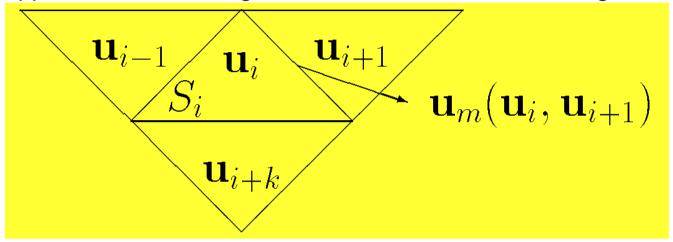
⇒ update volume averages by

$$\frac{d\mathbf{U}_i}{dt} + \frac{1}{\Delta x_i} \left(\mathbf{F}_{i+1/2} - \mathbf{F}_{i-1/2} \right) = 0.$$

⇒ discretized equation is integral law, weak solutions obey conservation

Finite Volume on unstructured grids

Finite volume approach: natural on general 2D and 3D unstructured grids



multidimensional set of conservation laws

$$\frac{\partial \mathbf{U}}{\partial t} + \nabla \cdot \mathbf{F} = 0$$

 \Rightarrow in 3D, the $\nabla \cdot \mathbf{F}$ with three Cartesian coordinate axes

$$\nabla \cdot \mathbf{F} = \frac{\partial \mathbf{F}_x}{\partial x} + \frac{\partial \mathbf{F}_y}{\partial y} + \frac{\partial \mathbf{F}_z}{\partial z}$$

- discretize space in control volumes V_i
 - \Rightarrow bounding surfaces ∂V_i , unit normal $\mathbf{n}=(n_x,\ n_y,\ n_z)$

$$\frac{d \int_{V_i} \mathbf{U}(\mathbf{x}, t) d\mathbf{x}}{dt} = -\int_{\partial V_i} \mathbf{F} \cdot \mathbf{n} dS$$

$$= -\int_{\partial V_i} (\mathbf{F}_x n_x + \mathbf{F}_y n_y + \mathbf{F}_z n_z) dS$$

 \Rightarrow introduce (8 \times 8 for MHD) matrix $T(\mathbf{n})$ which rotates vector quantities to local orthogonal coordinate system \mathbf{n} , \mathbf{t} , $\mathbf{s} \equiv \mathbf{n} \times \mathbf{t}$, where latter are tangential unit vectors within ∂V_i

$$\begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & \sin\theta & \cos\varphi & \sin\theta & \sin\varphi & \cos\theta & 0 & 0 & 0 & 0 \\ 0 & \cos\theta & \cos\varphi & \cos\theta & \sin\varphi & -\sin\theta & 0 & 0 & 0 & 0 \\ 0 & -\sin\varphi & \cos\varphi & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \sin\theta & \cos\varphi & \sin\theta & \sin\varphi & \cos\theta \\ 0 & 0 & 0 & 0 & \cos\theta & \cos\varphi & \cos\theta & \sin\varphi & -\sin\theta \\ 0 & 0 & 0 & 0 & -\sin\varphi & \cos\varphi & 0 \end{pmatrix}.$$

HD and MHD equations must be unchanged under rotation

$$\mathbf{F}_x n_x + \mathbf{F}_y n_y + \mathbf{F}_z n_z = T^{-1}(\mathbf{n}) \mathbf{F}_x \left(T(\mathbf{n}) \mathbf{U} \right)$$

⇒ obtain essentially 1D problem in direction normal to volume boundary

$$\frac{d\int_{V_i} \mathbf{U}(\mathbf{x}, t) d\mathbf{x}}{dt} = -\int_{\partial V_i} T^{-1}(\mathbf{n}) \mathbf{F}_x (T(\mathbf{n}) \mathbf{U}) dS$$

- control volumes with multiple, flat surface segments
 - ⇒ integral over boundary into discrete sum over its sides
 - \Rightarrow only information of grid: volumes V_i , and geometry of cells: number of bounding surface segments, their surface area and their normal directions.

The Euler equations

conservation laws for 1D dynamics of compressible gas

$$\begin{cases} \rho_t + (\rho v)_x = 0 \\ m_t + (m v + p)_x = 0 \\ e_t + (e v + p v)_x = 0 \end{cases}$$

- vector of conserved quantities $U = \left(egin{array}{c}
 ho \\ m \\ e \end{array} \right)$
 - ⇒ total energy density related to pressure by

$$e = \underbrace{\frac{\rho v^2}{2}}_{\text{kinetic}} + \underbrace{\frac{p}{\gamma - 1}}_{\text{thermal energy}}$$

 \Rightarrow ratio of specific heats γ

- internal energy considerations
 - \Rightarrow specific (\equiv per unit mass) internal energy e_i^s

$$\Rightarrow \rho e_i^s = p/(\gamma - 1)$$

• for ideal gas: temperature defined as $p = \mathcal{R}\rho T$ with gas constant \mathcal{R}

$$\Rightarrow e_i^s(T) = \frac{\mathcal{R}T}{\gamma - 1} = \frac{(c_p - c_v)T}{\frac{c_p}{c_v} - 1} = c_v T$$

- $\Rightarrow c_v$ specific heat at constant volume
- generally $\gamma=\frac{\alpha+2}{\alpha}$, where α is the total number of degrees of freedom over which internal energy can be distributed
 - ⇒ for molecules: translational, rotational, vibrational
 - \Rightarrow monoatomic gas: only 3 translational DOF $\rightarrow \gamma = 5/3$

• deduce equation for 'entropy' $s = p\rho^{-\gamma}$

$$\frac{\partial s}{\partial t} + v \frac{\partial s}{\partial x} = 0$$

- \Rightarrow since v(x,t): Not in conservation form!
- ⇒ like advection equation
- $\Rightarrow s$ constant along characteristics $\frac{dx}{dt} = v$: Riemann Invariant
- equivalent to the 'characteristic' equation

$$\Rightarrow$$
 along $\frac{dx}{dt} = v$, find

$$dp - c_s^2 d\rho = 0$$

$$\Rightarrow$$
 with $dp = p_t dt + p_x dx$ and $c_s^2 = \gamma p/\rho$

• write system as $U_t + (F(U))_x = 0$ with flux vector

$$F = \begin{pmatrix} m \\ \frac{m^2 3 - \gamma}{\rho} + (\gamma - 1)e \\ \frac{em}{\rho} \gamma - \frac{\gamma - 1}{2} \frac{m^3}{\rho^2} \end{pmatrix}$$

⇒ Flux Jacobian becomes

$$\frac{\partial F}{\partial U} = \begin{pmatrix} 0 & 1 & 0\\ \frac{m^2 \gamma - 3}{\rho^2 2} & \frac{m}{\rho} (3 - \gamma) & \gamma - 1\\ -\gamma \frac{em}{\rho^2} + (\gamma - 1) \frac{m^3}{\rho^3} \frac{e\gamma}{\rho} + (1 - \gamma) \frac{3}{2} \frac{m^2}{\rho^2} & \frac{m\gamma}{\rho} \end{pmatrix}$$

⇒ 3 eigenvalues/right eigenvectors

- eigenvalue $\lambda_1 = \frac{m}{\rho} \sqrt{\frac{\gamma p}{\rho}} = v c_s$
 - \Rightarrow eigenvector $ec{r_1}=\left(egin{array}{c} 1 \ v-c_s \ rac{v^2}{2}-vc_s+rac{c_s^2}{\gamma-1} \end{array}
 ight)$
- eigenvalue $\lambda_2 = \frac{m}{\rho} = v$
 - \Rightarrow eigenvector $\vec{r_2} = \begin{pmatrix} 1 \\ v \\ \frac{v^2}{2} \end{pmatrix}$
- eigenvalue $\lambda_3 = \frac{m}{\rho} + \sqrt{\frac{\gamma p}{\rho}} = v + c_s$
 - $\Rightarrow \text{ eigenvector } \vec{r_3} = \begin{pmatrix} 1 \\ v + c_s \\ \frac{v^2}{2} + vc_s + \frac{c_s^2}{\gamma 1} \end{pmatrix}$

Rankine-Hugoniot relations for Euler system

$$F(U_{l}) - F(U_{r}) = s (U_{l} - U_{r})$$

$$\Rightarrow \begin{cases} m_{l} - m_{r} = s(\rho_{l} - \rho_{r}) \\ \left[\frac{m_{l}^{2} 3 - \gamma}{\rho_{l}} + (\gamma - 1)e_{l}\right] - \left[\frac{m_{r}^{2} 3 - \gamma}{\rho_{r}} + (\gamma - 1)e_{r}\right] = s(m_{l} - m_{r}) \\ \left[\frac{e_{l} m_{l}}{\rho_{l}} \gamma - \frac{\gamma - 1}{2} \frac{m_{l}^{3}}{\rho_{l}^{2}}\right] - \left[\frac{e_{r} m_{r}}{\rho_{r}} \gamma - \frac{\gamma - 1}{2} \frac{m_{r}^{3}}{\rho_{r}^{2}}\right] = s(e_{l} - e_{r}) \end{cases}$$

- \Rightarrow for given right state: 3 equations for 4 unknowns s, U_l
- verify that Contact Discontinuity obeys RH

$$\Rightarrow s = v$$
, $v_l = v_r = v$, $p_l = p_r = p$ while $\rho_l \neq \rho_r$

 \Rightarrow '2-wave' for eigenvalue $\lambda_2=v$ has (generalized Riemann) invariants v and p

general solution to Riemann Problem:

- \Rightarrow given two states U_l and U_r
- \Rightarrow find intermediate state U_{mr} connected to U_r by a '3-wave'
- ⇒ which is such that its velocity and pressure

$$U_{mr} = \begin{pmatrix} \rho_{mr} \\ m_{mr} \\ e_{mr} \end{pmatrix} \equiv \begin{pmatrix} \rho_{mr} \\ v_* \\ p_* \end{pmatrix}$$
 conservative primitive

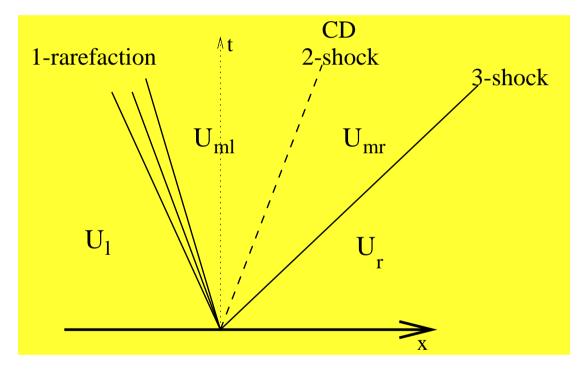
match the velocity and pressure of intermediate state

$$U_{ml} = \begin{pmatrix} \rho_{ml} \\ v_* \\ p_* \end{pmatrix}$$

connected to U_l by a '1-wave'

 \Rightarrow the states U_{ml} and U_{mr} can be connected by a '2-shock' (contact discontinuity)

- note: counts ok:
 - \Rightarrow 6 equations for 6 unknowns $(s_1, \rho_{ml}, v_*, p_*)$ and $(s_3, \rho_{mr}, v_*, p_*)$



- ⇒ again only entropy-satisfying shocks allowed
- ingredients to solve RP: L R_1 or $S_1 M_l \text{CD} M_r R_3$ or $S_3 \text{R}$

Euler system in terms of primitive variables

$$\begin{pmatrix} \rho \\ v \\ p \end{pmatrix}_{t} + \begin{pmatrix} v & \rho & 0 \\ 0 & v & \frac{1}{\rho} \\ 0 & \gamma p & v \end{pmatrix} \begin{pmatrix} \rho \\ v \\ p \end{pmatrix}_{x} = 0$$

 \Rightarrow possible to deduce

$$v_t + (v \pm c) v_x \pm \frac{1}{\sqrt{\gamma p \rho}} (p_t + (v \pm c)p_x) = 0$$

- since $\frac{2c}{\gamma-1} = \frac{2}{\gamma-1} \sqrt{\frac{\gamma p}{\rho}}$ and under constant $s = p \rho^{-\gamma}$
 - \Rightarrow can be rewritten to

$$\left(v \pm \frac{2c}{\gamma - 1}\right)_t + \left(v \pm c\right)\left(v \pm \frac{2c}{\gamma - 1}\right)_x = 0$$

- found (generalized) Riemann Invariants
 - \Rightarrow for '1-wave' v-c: invariants are s and $v+\frac{2c}{\gamma-1}$
 - \Rightarrow for '2-wave' v: invariants are v and p
 - \Rightarrow for '3-wave' v+c: invariants are s and $v-\frac{2c}{\gamma-1}$

can be written as 'characteristic' equations

$$\Rightarrow dp - \rho c dv = 0 \text{ along } \frac{dx}{dt} = v - c$$

$$\Rightarrow dp - c^2 d\rho = 0$$
 along $\frac{dx}{dt} = v$

$$\Rightarrow dp + \rho c dv = 0 \text{ along } \frac{dx}{dt} = v + c$$

 \Rightarrow could be used to solve IVP in (x,t) space

back to Rankine-Hugoniot relations for Euler system

$$F(U_l) - F(U_r) = s \left(U_l - U_r \right)$$

- \Rightarrow consider again stationary shock $s=0 \rightarrow m_l=m_r$
- ⇒ two remaining equations result in

$$\frac{v_l^2}{2} + \frac{c_l^2}{\gamma - 1} = \frac{v_r^2}{2} + \frac{c_r^2}{\gamma - 1} = \frac{\gamma + 1}{2(\gamma - 1)}c_*^2$$

- \Rightarrow last equality for sonic point where $v_* = c_*$
- \Rightarrow again leads to $c_*^2 = v_l v_r$ **Prandtl Meyer relation**
- \Rightarrow stationary shock separates super- from subsonic state (w.r.t. c_*)!

ullet further analysis of stationary shock introduces $M_l=rac{v_l}{c_l}$

$$\frac{v_l}{v_r} = \frac{(\gamma + 1)M_l^2}{(\gamma - 1)M_l^2 + 2}$$

 \Rightarrow and since $m_l = m_r$ we get for the density ratio

$$\frac{\rho_l}{\rho_r} = \frac{(\gamma - 1)M_l^2 + 2}{(\gamma + 1)M_l^2}$$

⇒ pressure ratio can be shown to obey

$$\frac{p_l}{p_r} = \frac{\gamma + 1}{1 - \gamma + 2\gamma M_l^2}$$

 \Rightarrow for stationary shock: all jumps depend on γ and M_l only

- moving shock: Galilean transformation
 - ⇒ leaves all thermodynamic quantities unchanged
 - \Rightarrow change to parameters $lpha=rac{\gamma+1}{\gamma-1}$ and $P=rac{p_l}{p_r}$
 - ⇒ stationary shock obeys

$$\frac{v_l}{v_r} = \frac{\alpha + P}{\alpha P + 1} = \frac{\rho_r}{\rho_l}$$

 \Rightarrow three parameters for a moving shock: α , P, shock speed s give

$$\frac{v_l - s}{v_r - s} = \frac{\alpha + P}{\alpha P + 1} = \frac{\rho_r}{\rho_l}$$

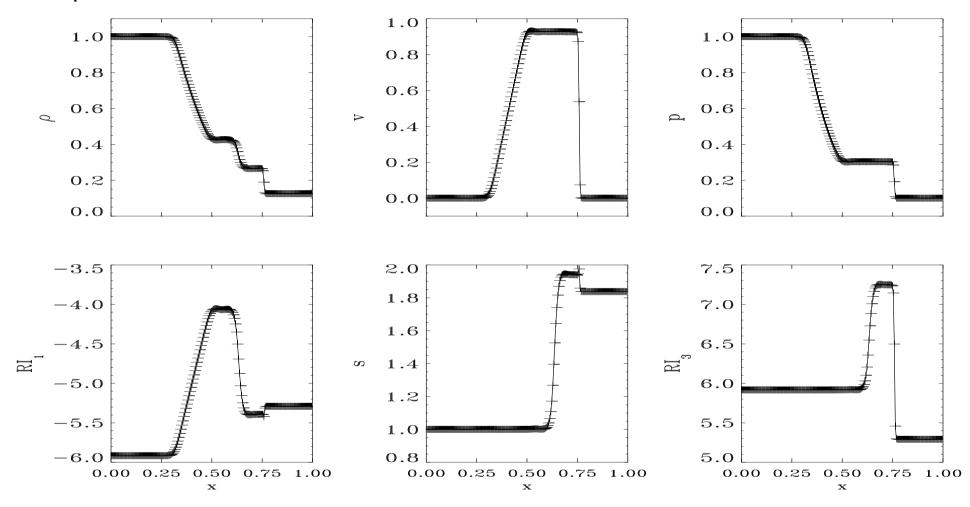
 \Rightarrow while also

$$(s - v_l)^2 = c_l^2 \left[1 + \frac{\gamma + 1}{2\gamma} \left(\frac{p_r}{p_l} - 1 \right) \right]$$

Numerical tests

- Perform series of Riemann Problem calculations for 1D Euler
 - ⇒ always use 2nd order accurate, conservative, TVDLF discretization
 - ⇒ TVDLF is 'Total Variation Diminishing Lax-Friedrichs' scheme
 - ⇒ monotonicity preserving, but diffusive especially at CD
 - \Rightarrow 200 grid points on [0,1], $\gamma=1.4$
 - \Rightarrow BCs: $\partial x = 0$
- Start with classical 'Sod' problem
 - $\Rightarrow U_l = (\rho_l, v_l, p_l) = (1, 0, 1) \text{ and } U_r = (0.125, 0, 0.1)$
 - ⇒ 'shock tube problem': diaphragm separates 2 gases at rest

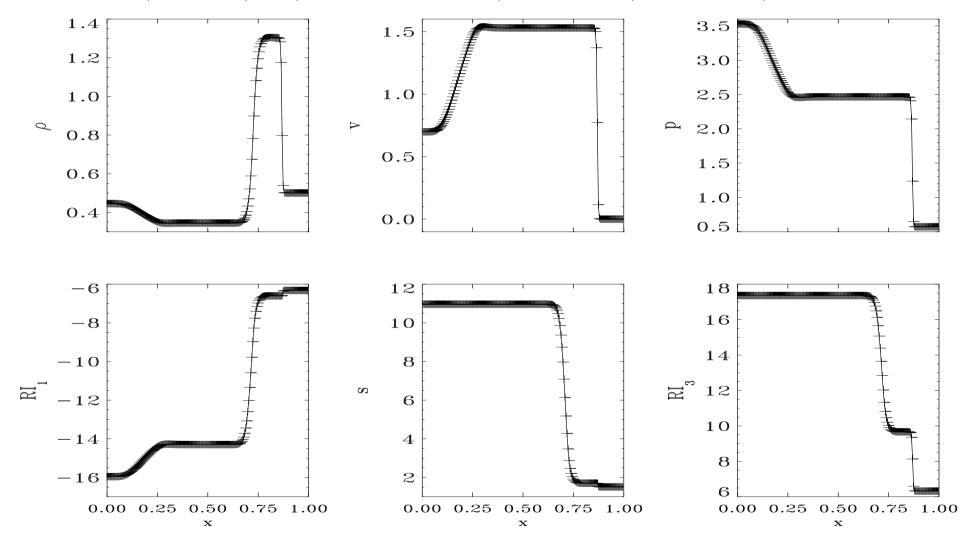
• Sod problem at t = 0.15



- \Rightarrow note R_1 where Riemann Invariants s and $v + 2c/(\gamma 1)$ are constant
- \Rightarrow CD spread over many cells

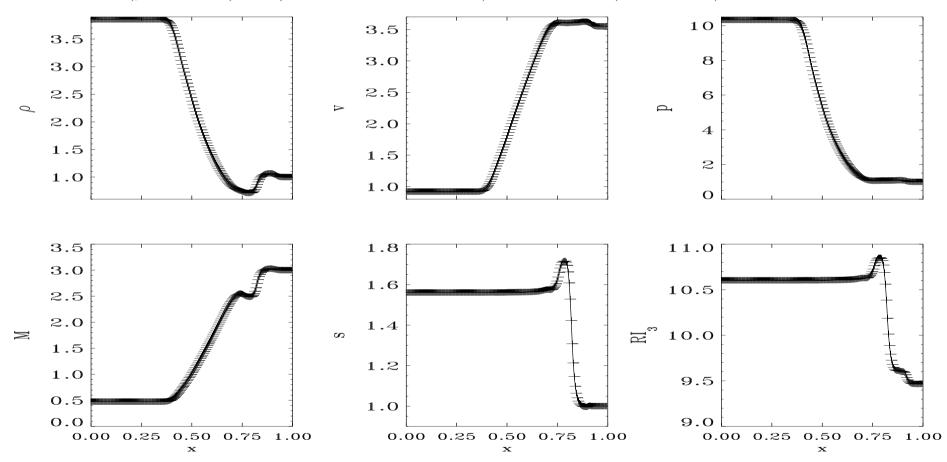
• test case from Lax: initial rightwardly moving left state, till t=0.15

$$\Rightarrow U_l = (\rho_l, v_l, p_l) = (0.445, 0.698, 3.528)$$
 and $U_r = (0.5, 0, 0.571)$



- Sod and Lax test case: remain subsonic $M=v/c_s<1$
 - ⇒ Arora & Roe Mach 3 test case considers

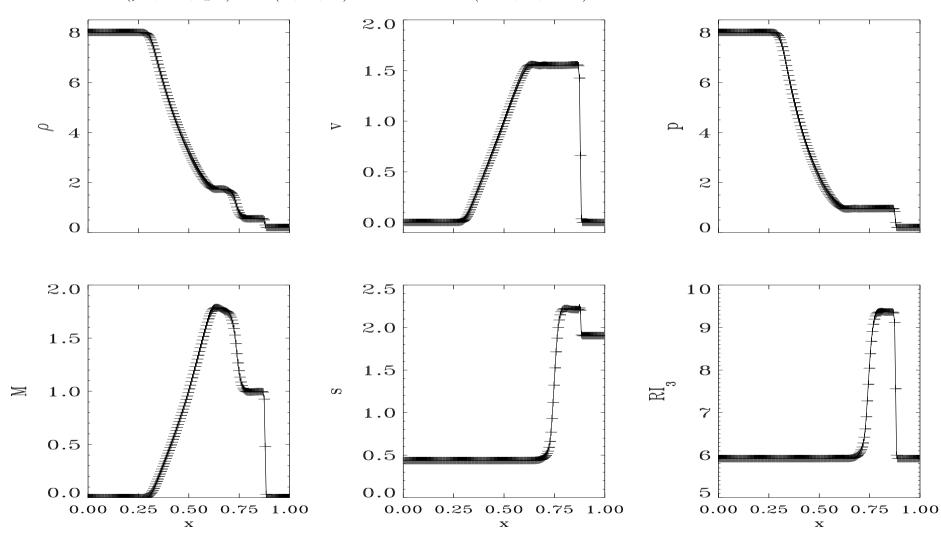
$$\Rightarrow U_l = (\rho_l, v_l, p_l) = (3.857, 0.92, 10.333) \text{ and } U_r = (1, 3.55, 1)$$



 \Rightarrow solution at t = 0.09

• supersonic shock tube problem at time t=0.1562

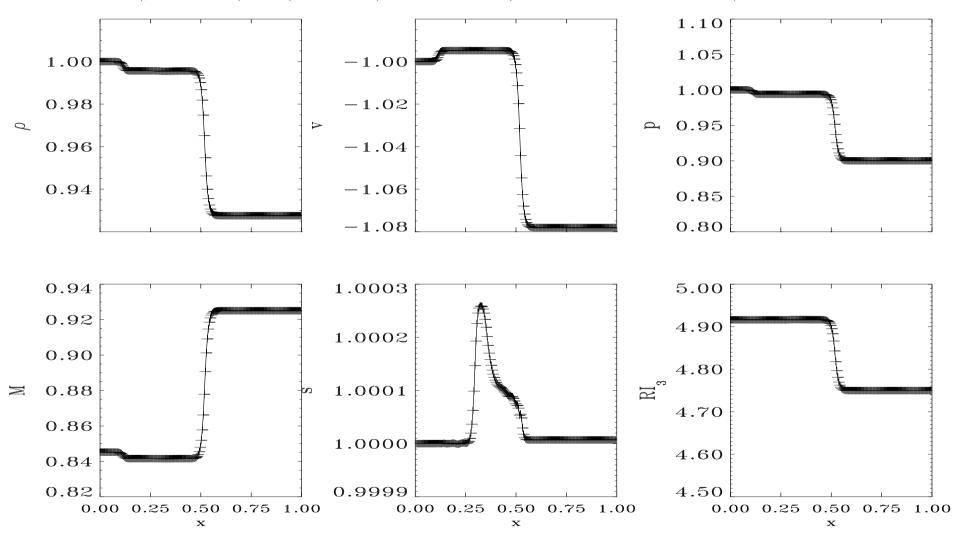
$$\Rightarrow U_l = (\rho_l, v_l, p_l) = (8, 0, 8) \text{ and } U_r = (0.2, 0, 0.2)$$



⇒ better behaviour at contact than in Mach 3 case

• case of a slowly moving very weak shock, show t=0.175

$$\Rightarrow U_l = (\rho_l, v_l, p_l) = (1, -1, 1) \text{ and } U_r = (0.9275, -1.0781, 0.9)$$

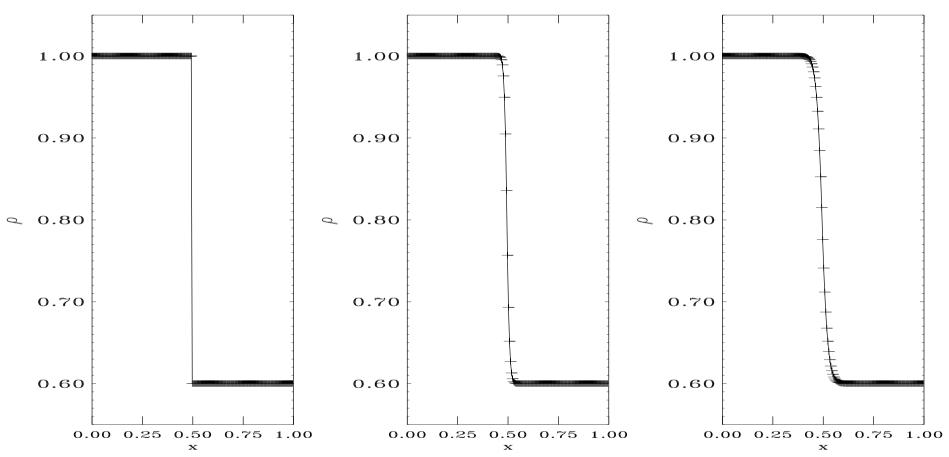


⇒ leftward rarefaction and rightward shock: (too) many cells in shock!

stationary contact discontinuity

$$\Rightarrow U_l = (\rho_l, v_l, p_l) = (1, 0, 0.5) \text{ and } U_r = (0.6, 0, 0.5)$$

 $\Rightarrow t = 0$ and t = 0.1 and t = 1 solution



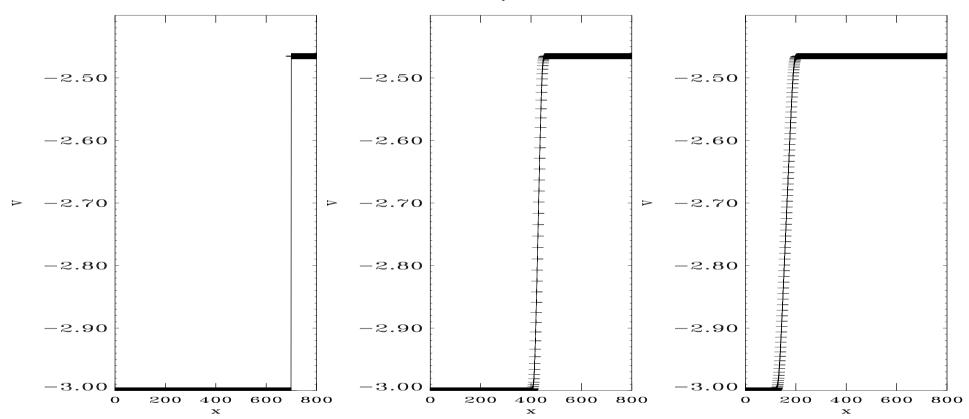
⇒ diffusion obvious: increasingly (too) many cells in CD!

recognizing a rarefaction wave

 \Rightarrow 800 cells from [0,800] with $\gamma=5/3$

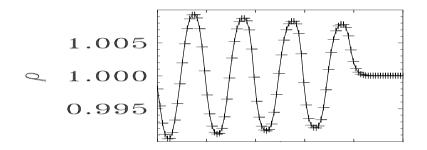
$$\Rightarrow U_l = (\rho_l, v_l, p_l) = (1, -3, 10) \text{ and } U_r = (0.87469, -2.46537, 8)$$

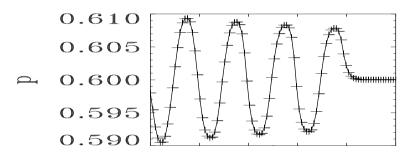
 $\Rightarrow t = 0$ and t = 40 and t = 80 solution, plot v

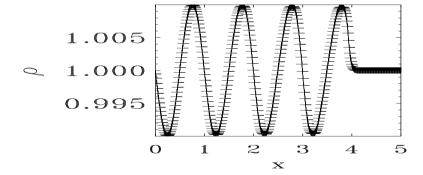


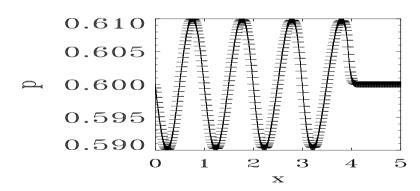
⇒ two states with same entropy: rarefaction emerges

- Linear sound waves: time dependent driver $v = A \sin(2\pi t/P)$ at x = 0
 - \Rightarrow density $\rho(t=0)=1$, v(t=0)=0, p(t=0)=0.6 with $\gamma=5/3$
 - $\Rightarrow A = 0.02$ with P = 1 generates sound waves (amplitude 0.01)
 - \Rightarrow compare TVDLF for 100 versus 400 cells at t=4



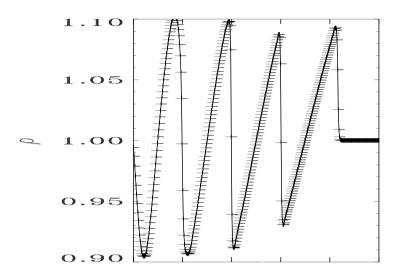


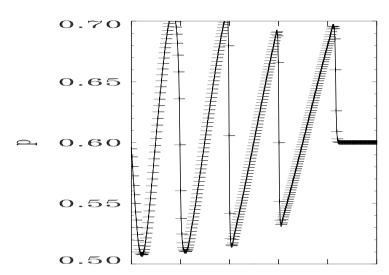




⇒ to follow linear dynamics: need high resolution to battle diffusion!

• sound wave steepening and shock formation: take amplitude A=0.2





- ⇒ nonlinear shock formation well captured
- Caution to use these methods for pure linear wave processes
 - ⇒ high resolution prerequisite
 - ⇒ seperate true physical diffusion from numerical effects
 - ⇒ note that 10 % variations already imply nonlinear effects!

Approximate Riemann solver based methods

- modern high resolution, shock-capturing schemes for Euler
 - ⇒ capitalize on known solution of the Riemann problem
 - ⇒ originally developed by Godunov
- always use conservative scheme of form

$$\frac{dU_i}{dt} + \frac{1}{\Delta x} \left(F_{i+1/2} - F_{i-1/2} \right) = 0$$

- \Rightarrow cell values U_i change through fluxes across cell edges
- \Rightarrow edge-centered numerical flux $F_{i+1/2}(U_{i-p},U_{i-p+1},\ldots,U_{i+q})$

The Godunov scheme

- values U_i^n for time $t = t_n$
 - ⇒ consider piecewise constant values in cells
 - \Rightarrow serve as initial condition to solve $U_t + (F(U))_x = 0$ for $t > t_n$
 - \Rightarrow restrict timestep to $\Delta t_{n+1} < \frac{\Delta x}{2 \max|\lambda|}$
 - \Rightarrow with λ eigenvalue of flux Jacobian F_U
 - ⇒ then exact solution given by solving RP at cell interfaces
 - \Rightarrow restriction on timestep ensures no wave interaction within Δt_{n+1}
- Godunov scheme
 - \Rightarrow denote exact RP solution for state U_i^n and U_{i+1}^n as $\hat{U}\left(\frac{x-x_{i+1/2}}{t},U_i^n,U_{i+1}^n\right)$
 - ⇒ numerical flux

$$F_{i+1/2}(U_i, U_{i+1}) = F(\hat{U}(0, U_i^n, U_{i+1}^n))$$

⇒ need an exact Riemann solver

The Roe solver

- due to piecewise constant representation
 - ⇒ Godunov scheme 1st order accurate
- exact solution to RP is complicated
 - ⇒ scheme is not exact due to piecewise constant representation
 - ⇒ might as well solve RP in approximate fashion
- schemes exploiting approximate Riemann solver
 - \Rightarrow use linearization of the nonlinear problem
 - ⇒ recall: exact solution for linear hyperbolic system known

Roe-type approximate Riemann solver

- general procedure to solve system $\mathbf{U}_t + (\mathbf{F}(\mathbf{U}))_x = 0$
 - \Rightarrow local Riemann problem from left and right interface values \mathbf{U}_l and \mathbf{U}_r .
 - ⇒ instead of exact nonlinear solution, solve a linear Riemann problem

$$\mathbf{U}_t + (\mathbf{G}(\mathbf{U}))_x = 0$$

- \Rightarrow $\mathbf{G}(\mathbf{U}) = \mathbf{F}(\mathbf{U}_r) + A(\mathbf{U} \mathbf{U}_r)$ includes constant matrix $A = A(\mathbf{U}_l, \mathbf{U}_r)$
- ⇒ matrix must satisfy conditions
 - 1. $\mathbf{F}(\mathbf{U}_l) \mathbf{F}(\mathbf{U}_r) = A(\mathbf{U}_l, \mathbf{U}_r) (\mathbf{U}_l \mathbf{U}_r),$
 - 2. $A(\mathbf{U}_l, \mathbf{U}_r) \to \mathbf{F}_{\mathbf{U}}(\mathbf{U}_r)$ as $\mathbf{U}_l \to \mathbf{U}_r$,
 - 3. $A(\mathbf{U}_l, \mathbf{U}_r)$ has only real eigenvalues,
 - 4. $A(\mathbf{U}_l, \mathbf{U}_r)$ has a complete system of eigenvectors.
- ⇒ exact solution obtained when initial states obey Rankine-Hugoniot relations
- ⇒ consistency and solvability of the linear Riemann problem.

• if Roe matrix A found, Roe scheme uses the numerical flux

$$\mathbf{F}_{i+1/2}\left(\mathbf{U}_{i},\mathbf{U}_{i+1}\right) = \mathbf{F}(\mathbf{U}_{i}) + A_{i+1/2}\left(\hat{\mathbf{U}} - \mathbf{U}_{i}\right)$$

 $\Rightarrow \hat{\mathbf{U}} = \hat{\mathbf{U}}(0, \mathbf{U}_i, \mathbf{U}_{i+1})$ is exact solution of linear Riemann problem

• Latter solution easy: when $A_{i+1/2}\vec{r}^p = \lambda_p \vec{r}^p$ write

$$\mathbf{U}_{i+1} - \mathbf{U}_i = \sum \alpha_p \vec{r}^p$$

 \Rightarrow can show that the solution along the (x,t) ray $(x-x_{i+\frac{1}{2}})/t=0$

$$\hat{\mathbf{U}} = \frac{\mathbf{U}_i + \mathbf{U}_{i+1}}{2} + \frac{1}{2} \left[\sum_{\lambda_p < 0} - \sum_{\lambda_p > 0} \right] \alpha_p \vec{r}^p$$

fill in for Roe flux, use first Roe condition to get

$$\mathbf{F}_{i+1/2} = \frac{1}{2} \left(\mathbf{F}(\mathbf{U}_i) + \mathbf{F}(\mathbf{U}_{i+1}) \right) - \frac{1}{2} \sum |\lambda_p| \alpha_p \vec{r}^p$$

- Needed: Roe matrix A, its eigenvalues λ_p , its right eigenvectors \vec{r}^p , and the wave strengths α_p
 - \Rightarrow when left eigenvectors $ec{l}^p$ given, wave strengths

$$\alpha_p = \vec{l}^p \cdot (\mathbf{U}_{i+1} - \mathbf{U}_i)$$

- In practice: use for A the Flux Jacobian ${\bf F_U}$, evaluated in average state, e.g. arithmetic average of ${\bf U}_l$ and ${\bf U}_r$
 - ⇒ then not all Roe conditions fullfilled though
 - \Rightarrow all ingredients known: eigenvalues (characteristic speeds), eigenvectors from R, left eigenvectors from R^{-1}
- Note: wave strengths can also be computed from primitive jumps

$$\alpha_p = \vec{\mathbf{l}}^p \cdot (\mathbf{V}_{i+1} - \mathbf{V}_i)$$

 \Rightarrow left eigenvectors $ec{\mathbf{l}}^p$ are found from rows of

$$\mathbf{R}^{-1} = R^{-1} \mathbf{U}_{\mathbf{V}}$$

⇒ where transformation matrix relates primitive with conservative formulation

$$d\mathbf{U} = \mathbf{U}_{\mathbf{V}}d\mathbf{V}$$

• solver completely determined once matrix $A_{i+1/2}$ that satisfies the Roe conditions is constructed

$$\Rightarrow \text{ recall that } U = \left(\begin{array}{c} \rho \\ m \\ e \end{array} \right) \text{ and } F = \left(\begin{array}{c} m \\ \frac{m^2 3 - \gamma}{\rho} + (\gamma - 1)e \\ \frac{em}{\rho} \gamma - \frac{\gamma - 1}{2} \frac{m^3}{\rho^2} \end{array} \right) = \left(\begin{array}{c} \rho v \\ \rho v^2 + p \\ v(e + p) \end{array} \right)$$

$$\Rightarrow$$
 introduce vector $Z = \begin{pmatrix} \sqrt{\rho} \\ \sqrt{\rho}v \\ (e+p)/\sqrt{\rho} \end{pmatrix}$

 \Rightarrow find that

$$U = \begin{pmatrix} z_1 z_1 \\ z_1 z_2 \\ \frac{1}{\gamma} z_1 z_3 + \frac{\gamma - 1}{2\gamma} z_2 z_2 \end{pmatrix}$$

 \Rightarrow and similarly

$$F = \begin{pmatrix} z_1 z_2 \\ \frac{\gamma + 1}{2\gamma} z_2 z_2 + \frac{\gamma - 1}{\gamma} z_1 z_3 \\ z_2 z_3 \end{pmatrix}$$

 \Rightarrow both U and F are quadratic functions of elements of Z

- define difference $\delta a = a_{i+1} a_i$
 - \Rightarrow verify existence of matrices B and C such that
 - $\Rightarrow \delta U = B\delta Z$ and $\delta F = C\delta Z$
 - \Rightarrow matrices B and C have elements linear in $\bar{z} = \frac{1}{2} \left(z_i + z_{i+1} \right)$
- matrix $A_{i+1/2} \equiv C B^{-1}$ then satisfies

$$\Rightarrow A_{i+1/2}\delta U = \delta F$$

⇒ first Roe condition

define so-called Roe-averages as

$$\bar{v} \equiv \frac{\sqrt{\rho_i}v_i + \sqrt{\rho_{i+1}}v_{i+1}}{\sqrt{\rho_i} + \sqrt{\rho_{i+1}}}$$
$$\bar{h} \equiv \frac{\sqrt{\rho_i}h_i + \sqrt{\rho_{i+1}}h_{i+1}}{\sqrt{\rho_i} + \sqrt{\rho_{i+1}}}$$

- \Rightarrow latter uses the total specific enthalpy $h=rac{e+p}{
 ho}$
- \Rightarrow can write matrix $A_{i+1/2}$ as

$$A_{i+1/2} = \begin{pmatrix} 0 & 1 & 0 \\ \frac{\gamma - 3}{2} \bar{v}^2 & (3 - \gamma) \bar{v} & \gamma - 1 \\ \frac{\gamma - 1}{2} \bar{v}^3 - \bar{v} \bar{h} & \bar{h} - (\gamma - 1) \bar{v}^2 & \gamma \bar{v} \end{pmatrix}$$

- \Rightarrow by inspection, this is equal to $F_U(\bar{U})$
- \Rightarrow flux Jacobian evaluated at Roe averaged state \bar{U}
- ⇒ thus satisfies all other Roe conditions
- can be shown that matrix satisfying all Roe conditions is unique

- all ingredients for Roe flux now known
 - \Rightarrow eigenvalues $\lambda_1 = \bar{v} \bar{c}$, $\lambda_2 = \bar{v}$, $\lambda_3 = \bar{v} + \bar{c}$
 - \Rightarrow uses sound speed from $\bar{c}^2 = (\gamma 1) \left(\bar{h} \frac{\bar{v}^2}{2} \right)$
 - $\Rightarrow \text{ recall eigenvectors } \vec{r_1} = \begin{pmatrix} 1 \\ \bar{v} \bar{c} \\ \bar{h} \bar{v}\bar{c} \end{pmatrix} \vec{r_2} = \begin{pmatrix} 1 \\ \bar{v} \\ \frac{\bar{v}^2}{2} \end{pmatrix} \vec{r_3} = \begin{pmatrix} 1 \\ \bar{v} + \bar{c} \\ \bar{h} + \bar{v}\bar{c} \end{pmatrix}$
 - \Rightarrow coefficients $\alpha_p = \vec{r}^p \cdot (U_{i+1} U_i)$
 - \Rightarrow with orthogonal left eigenvectors $ec{l}^p$ from $ec{l}^p \cdot ec{r}_q = \delta^p_q$ given by

$$\vec{l}^{1} = \left(\frac{\bar{v}}{4\bar{c}}(2 + (\gamma - 1)\frac{\bar{v}}{\bar{c}}), -\frac{1}{2\bar{c}}(1 + (\gamma - 1)\frac{\bar{v}}{\bar{c}}), \frac{\gamma - 1}{2}\frac{1}{\bar{c}^{2}}\right)$$

$$\vec{l}^2 = \left(1 - \frac{\gamma - 1}{2} \frac{\vec{v}^2}{\vec{c}^2}, \ (\gamma - 1) \frac{\vec{v}}{\vec{c}^2}, \ -(\gamma - 1) \frac{1}{\vec{c}^2}\right)$$

$$\vec{l}^3 = \left(-\frac{\bar{v}}{4\bar{c}} (2 - (\gamma - 1)\frac{\bar{v}}{\bar{c}}), \ \frac{1}{2\bar{c}} (1 - (\gamma - 1)\frac{\bar{v}}{\bar{c}}), \ \frac{\gamma - 1}{2}\frac{1}{\bar{c}^2} \right)$$

• coefficients α_p expressed in primitive variable differences

$$\alpha_1 = \frac{1}{2\bar{c}^2} \left(\Delta p - \bar{c}\bar{\rho}\Delta v \right)$$

$$\alpha_2 = \Delta \rho - \frac{1}{\bar{c}^2} \Delta p$$

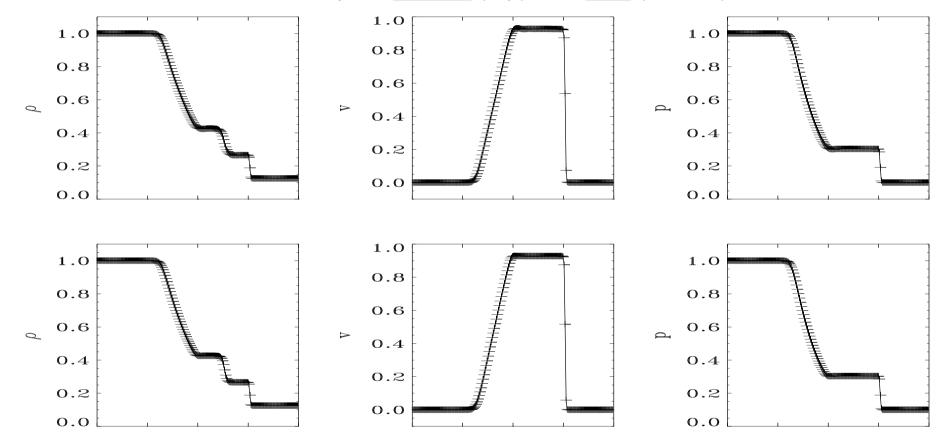
$$\alpha_3 = \frac{1}{2\bar{c}^2} \left(\Delta p + \bar{c}\bar{\rho}\Delta v \right)$$

- \Rightarrow with $\bar{
 ho} = \sqrt{\rho_i \rho_{i+1}}$
- ⇒ correspondence with characteristic equations

Numerical tests

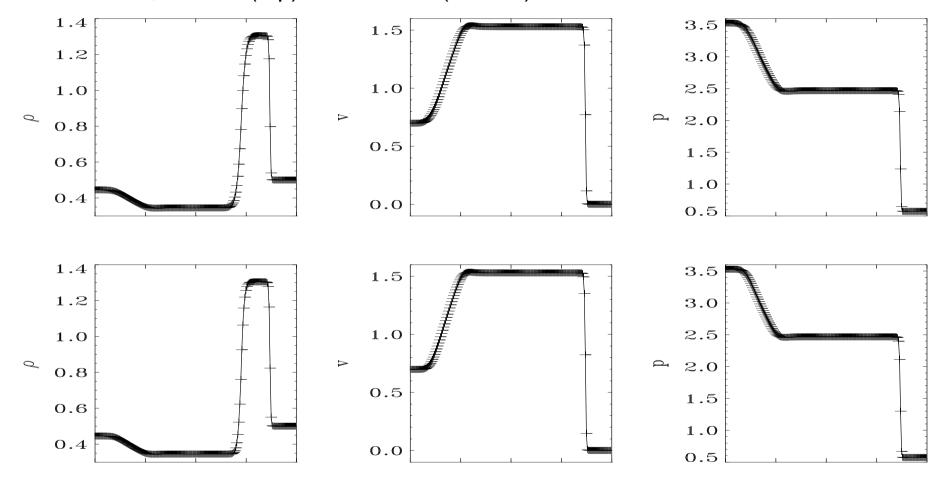
- Perform series of Riemann Problem calculations for 1D Euler
 - ⇒ compare 2nd order conservative TVDLF with Roe-based TVD
 - \Rightarrow 200 grid points on [0,1], $\gamma=1.4$ and BCs: $\partial x=0$
- Start with classical 'Sod' problem
 - $\Rightarrow U_l = (\rho_l, v_l, p_l) = (1, 0, 1) \text{ and } U_r = (0.125, 0, 0.1)$
 - ⇒ 'shock tube problem': diaphragm separates 2 gases at rest

• Sod shock tube t = 0.15: compare <u>TVDLF</u> (top) with <u>Roe</u> (bottom)



⇒ Roe: slight improvement for CD

Lax test case, TVDLF (top) versus TVD (bottom)

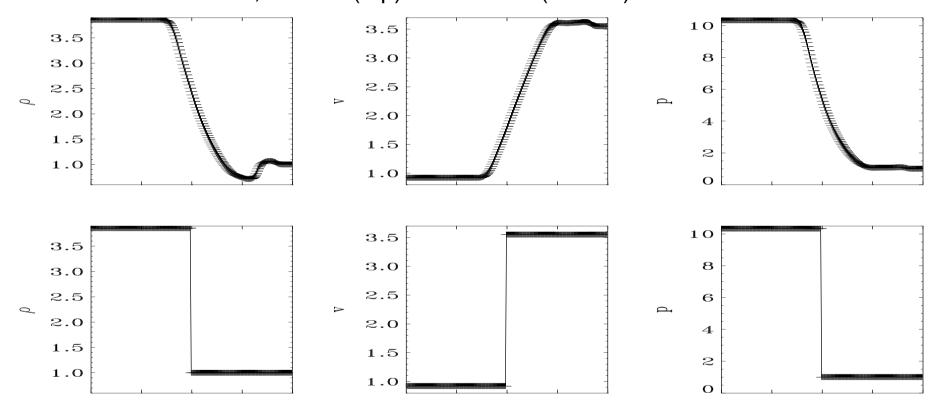


 \Rightarrow slight improvement for CD

Arora & Roe Mach 3 test case considers

$$\Rightarrow U_l = (\rho_l, v_l, p_l) = (3.857, 0.92, 10.333) \text{ and } U_r = (1, 3.55, 1)$$

• Mach 3 test at t = 0.09, TVDLF (top) versus Roe (bottom)



⇒ Roe gives completely wrong solution!!!!

- Erroneous Mach 3 result due to presence of M=1 point
 - $\Rightarrow R_1$ -rarefaction (expansion fan) goes transonic
 - \Rightarrow eigenvalue $\lambda_1 = \bar{v} \bar{c} = 0$ at sonic point
 - \Rightarrow what if simultaneously $\alpha_2 = \alpha_3 = 0$?
 - ⇒ Roe flux reduces to central discretization

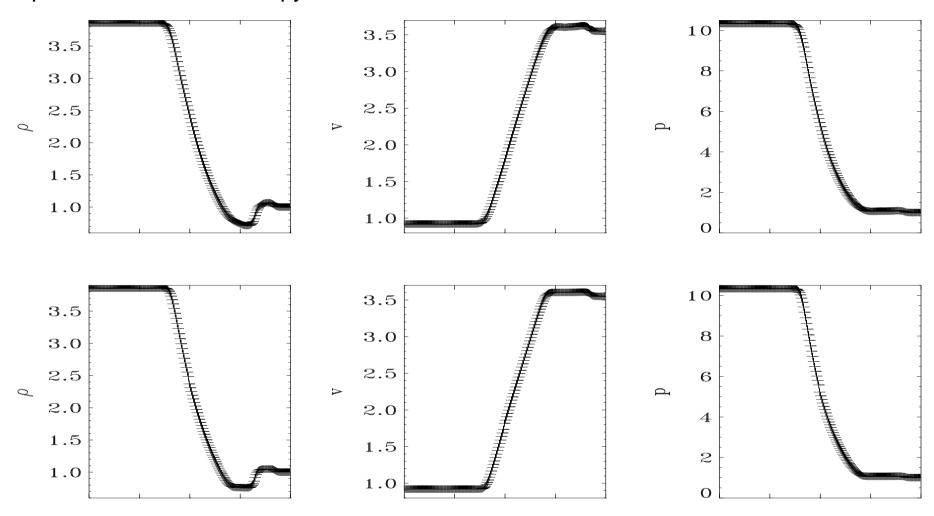
$$F_{i+1/2} = \frac{1}{2} \left(F(U_i) + F(U_{i+1}) \right)$$

- ⇒ discontinuities are insufficiently smeared out
- ⇒ entropy-violating solution may occur (must increase through shock)
- 'sonic entropy fix' for Roe scheme
 - \Rightarrow replace eigenvalues λ_1 and λ_3 in the vicinity of zero
 - \Rightarrow if $|\lambda_1| < \epsilon$ or $|\lambda_3| < \epsilon$

$$\lambda_p \to \frac{1}{2} \left(\frac{\lambda_p^2}{\epsilon} + \epsilon \right)$$

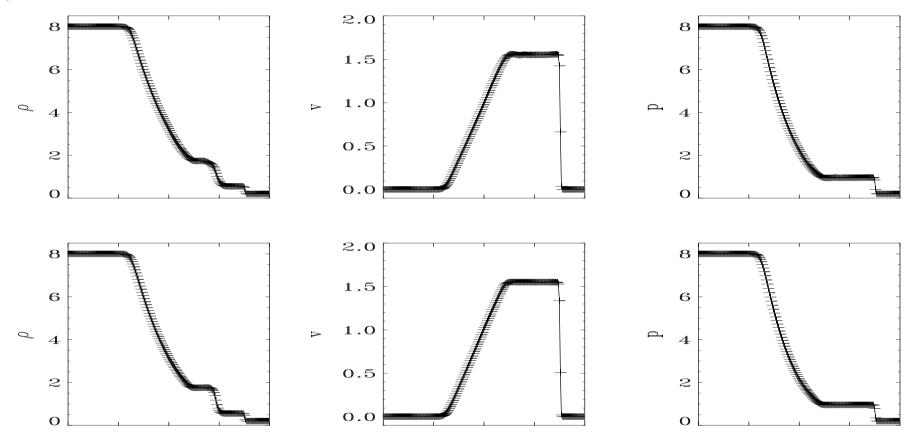
 \Rightarrow with ϵ a small value, at play where $\mid v \mid \simeq c$

Repeat Mach 3 with entropy fix:



 \Rightarrow **Roe**: (bottom) improvement over <u>TVDLF</u> (top)

• supersonic shock tube test:

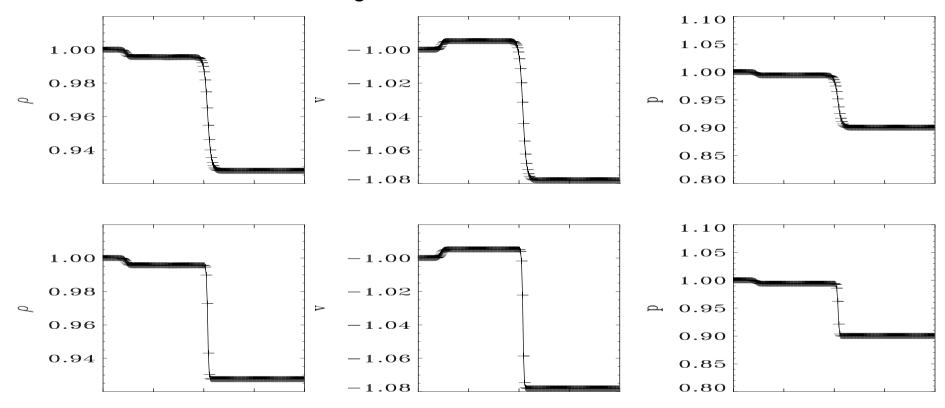


 \Rightarrow improvement over TVDLF, better at CD

• case of a slowly moving very weak shock, show t=0.175

$$\Rightarrow U_l = (\rho_l, v_l, p_l) = (1, -1, 1) \text{ and } U_r = (0.9275, -1.0781, 0.9)$$

⇒ leftward rarefaction and rightward shock

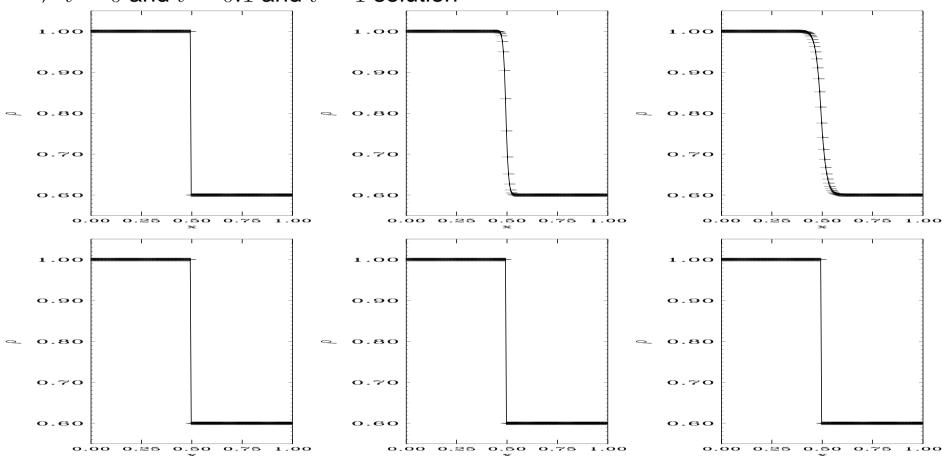


⇒ Roe (bottom) much better than TVDLF (top: many cells in shock)!

stationary contact discontinuity :

$$\Rightarrow U_l = (\rho_l, v_l, p_l) = (1, 0, 0.5) \text{ and } U_r = (0.6, 0, 0.5)$$

 $\Rightarrow t = 0$ and t = 0.1 and t = 1 solution



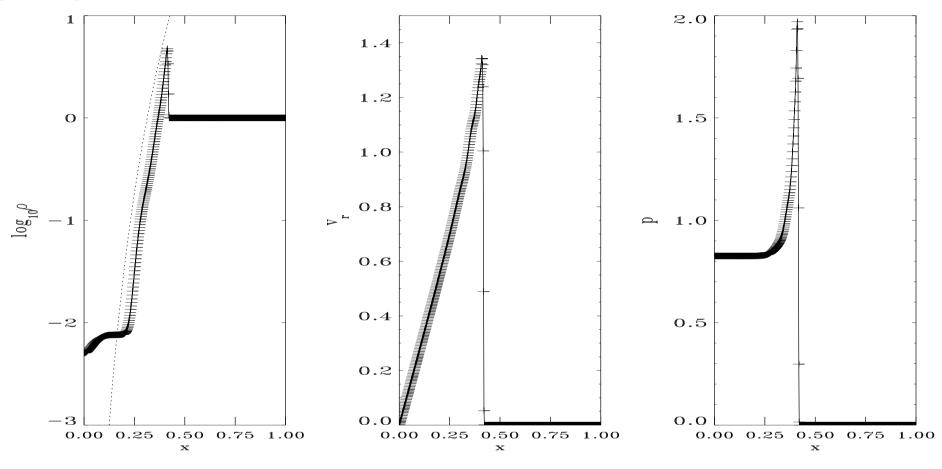
⇒ Roe (bottom): CD recognized as steady solution, no diffusion!!!

- summarizing
 - ⇒ non-trivial calculation of Roe flux (more involved than TVDLF)
 - ⇒ need for entropy fix for transonic expansion fans
 - ⇒ better representation of CD, especially stationary CD
 - ⇒ ok with slowly traveling weak shocks
- note: conclusions for 2nd order variants of TVDLF and Roe-based TVD
 - ⇒ both heavily used in multi-D HD simulations

Sedov blast wave

- astrophysical application: 'supernova' explosion or 'blast wave'
 - ⇒ modeled as 1D Euler Riemann Problem in spherical symmetry
- initial conditions $v_r = 0$, $\rho = 1$, and $\gamma = 1.4$
 - \Rightarrow extreme p jump $p_{exp}=763.944$ for $r\in[0,0.05]$ and $p_{ext}=10^{-5}$
 - \Rightarrow take 512 grid points on r=[0,1] run till time t=0.1 with TVD

good agreement with analytical result



- $\Rightarrow p$ goes to constant value at center
- $\Rightarrow v_r$ goes to linear profile in r/R(t) with R(t) shock position
- \Rightarrow density goes to profile $(r/R(t))^{3/(\gamma-1)}$ (overplotted)