

# QUBIT 1 - PARAMETERS

Samuel Goldstein - July 2020

## Purpose

This write up covers the most important numbers for the design of Qubit 1, hopefully the first functional Xmon-fabrication. It also includes essential formulae for engineering of superconducting quantum circuits. The Xmon was originally suggested and implemented by [Barends](#), and has that name because of the shape of the qubit: A large X.

The numbers in our design differ from Barends' design (and that of the Martinis' group) for two reasons.

1. We expect **our decoherence to be faster** (first try, and it is on Si and not Sapphire), meaning that **our readout must be faster**. This in turn requires **a lower Q-factor** (allowing to scan less points), which then means that the **dispersion shift must be larger**. Now, this implies that the **resonator-qubit coupling is larger** (or that the detuning is smaller, but as  $\chi = g^2/\delta$ , so enlarging  $g$  is more effective. This means the horse-shoe capacitor is much larger, cancelling part of the Xmons' capacitance to ground, increasing its resonance by a few percent ( $\sim 2$  to  $300$  MHz).
2. With the oxidation parameters we tried (10 min @ 1 torr), we room temperature resistances up to  $10\text{ k}\Omega$ .

## The qubit

The idea here is that each "arm" of the qubit can be connected to one of the following:

- XY control - excitation of the qubit ( $|0\rangle \rightarrow |1\rangle$ )
- Z-control through the SQUID (tuning the qubit frequency)
- A readout resonator (dispersive readout)
- Possible coupling to other qubits or networks

The qubit frequency  $f_q$  is given by the charge energy and the Josephson energy (of the SQUID):  $E_c = e^2/2C$  and  $E_J$ . Note that  $I_c$  is the **SQUID's** critical current, i.e. half of that of each Junction (if

identical). The desired regime is that where the charge noise is low, i.e.  $E_J/E_C \gg 1$ .

The self-capacitance of the qubit,  $C$  is the capacitance to ground, given by coplanar geometry capacitance. Martinis wrote [this document](#) on how to calculate the capacitance, and Elisha prepared a Matlab m.file doing the math: If each finger in the **Xmon is 180  $\mu\text{m}$  long, the trace is 8  $\mu\text{m}$  and the gap to the surrounding grounds is 4  $\mu\text{m}$** , then  $C = 1.34\text{E-}13 \text{ fF}$ , giving  $E_c = 146\text{MHz} \times h$ .

[Chen](#) used SQUIDS with  $I_c \simeq 40 \text{ nA}$ , meaning junctions with  $I_c \simeq 20 \text{ nA}$  translating by Ambegaokar-Baratoff to around  $R_n \simeq 13 \text{ k}\Omega$ , which is a bit above what I can achieve according to the last experience... we could do another round of calibration with more intensive oxidation, or go for junctions with  $I_c \simeq 30 \text{ nA}$ , i.e. each of them with  $R_n \simeq 8.7 \text{ k}\Omega$ . We then have a combined critical current of  $60 \text{ nA}$ . We then get  $E_J = 5.75 \text{ GHz}$  and  $E_J/E_C > 200$ , which is sufficient.

The qubit frequency is:

$$f_q = \frac{1}{h} \left( \sqrt{8E_c E_J \left| \cos \left( \frac{\pi \Phi_{ext}}{\Phi_0} \right) \right|} - E_c \right)$$

Without flux,  $f_q = 5.92 \text{ GHz}$ .

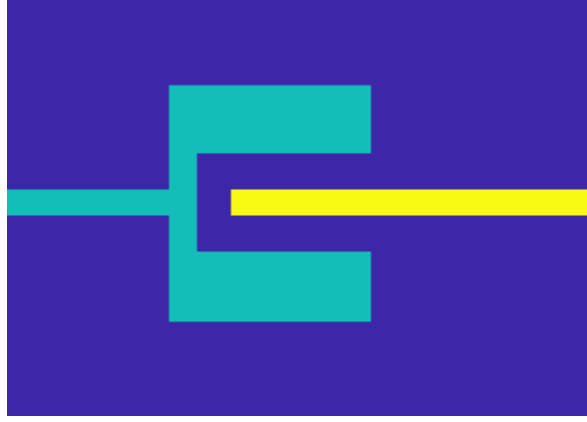
*This is the energy for excitation of the qubit. What happens, when  $\Phi_{ext} = \Phi_0$  and theoretically  $f_q < 0$ ?) Also, note that Chen includes the factor 8 before  $E_c E_J$  ... Elisha wrote a small write-up on that. The question seems to be weather you consider  $E_c$  for one side of one arm only...*

Quantity	Formulae	Chen's value	My suggestion
Qubit arm length	-	130 (Barends: up to 165)	180
SQUID critical current	$2I_c^{JJ}$	40 nA	60 nA
Josephson energy	$E_J = \frac{\Phi_0 I_c}{2\pi}$	19.8 GHz	29.8 GHz

## SQUID dimensions for appreciable flux

Given the  $1\text{k}\Omega$  resonators on most of the DC-lines our fridge, we want  $1\text{V}$  from the voltage generator to impose  $\Phi_0$ . If the height of the SQUID is  $H$ , its length  $L$ , and the distance of its upper edge from the center of the flux line is  $d$ , then the flux from  $1\text{mA}$  is:

$$\begin{aligned}\Phi_{ext} &= \int_d^{d+H} B dA = L \int_d^{d+H} B dh = LI_{flux} \mu_0 / 2\pi \times \int_d^{d+H} dh/h \\ &= \frac{LI_{flux} \mu_0}{2\pi} \ln\left(\frac{d+H}{d}\right)\end{aligned}$$



If  $H, L, d = 20, 30, 20 \mu m$ , we get  $\Phi_{ext} = 2\Phi_0$ , which is sufficient. Here we assumed  $\mu_r \simeq 1$  for aluminum. What about the screening parameter,  $\beta_L = 2LI_C/\Phi_0$ ? Note that  $L$  is the geometric inductance of the SQUID, typically in the nano-henry scale, making  $\beta_L < 0.01$ .

## Readout resonators

Each qubit is coupled capacitively to a resonator through a “horse shoe”, shown here to the right (yellow: resonator, green: Xmon). The given capacitance is found with the numerical script of capacitance between electrodes. The coupling frequency is

$$g_{ij} = \frac{C_c^{ij} \sqrt{f^i f^j}}{\sqrt{(C_s^i + C_c^{ij})(C_s^j + C_c^{ij})}}$$

where  $C_c^{ij}$  is the coupling capacitance between the two,  $C_s$  is the self capacitance (to ground of the electrode), and  $f$  the frequency. We get  $\sim 2.7$  fF for a distance of 5 micron, 45 micron coupling length and coupling width (“toes”) of 30 micron width.

With the parameters as shown on the image here to the right, we get a coupling capacitance of roughly 1 fF. What, then, is the coupling? This of course depends on the frequencies of the resonators. We

want to perform *dispersive* readout, where the coupling between the Xmon and the resonator induces a shift in the resonator frequency, when the Xmon is excited. This is actually the Stark shift:

$$H_{JC}^{disp} = \hbar \left( \frac{1}{2} \omega_q \sigma_z + \left( \omega_r + \frac{g^2}{\delta} \sigma_z \right) \left( a^\dagger a + \frac{1}{2} \right) \right)$$

This is the Jaynes-Cummings Hamiltonian, describing a two-level-system coupled to a resonator in the dispersive limit, where  $\delta = \omega_q - \omega_r \gg g$ . Here  $\omega_r \rightarrow \omega_r \pm g^2/\delta$  depending on the qubits state.

Choose horse shoe capacitor, width 55  $\mu\text{m}$ , length 70  $\mu\text{m}$ , gap to Xmon: 5  $\mu\text{m}$

Qubit name	Archimedes	Bohr	Casimir	Debye
$f_{RR}$ (readout res)	<b>6.75E+09</b>	<b>6.80E+09</b>	<b>6.85E+09</b>	<b>6.90E+09</b>
Required length	4.25276E-03	4.22171E-03	4.19112E-03	4.16097E-03
$\delta/g$	1.11E+02	1.15E+02	1.20E+02	1.25E+02
$g$	5.67E+07	5.71E+07	5.75E+07	5.79E+07
$\chi$	<b>5.11E+05</b>	<b>4.94E+05</b>	<b>4.79E+05</b>	<b>4.65E+05</b>

Couplings of readout resonators to readout line: 0.6 mm coupling length, ground between the two lines: 8  $\mu\text{m}$  (total distance of 18  $\mu\text{m}$  between edges of transmission line and resonator). This gives a coupling of 4.8 fF, and an external Q of 14000.

## Tunable resonators

XY control: Probe 20 micron wide, distance 13 micron, gives 0.11 fF coupling.

## Tunable resonators

The simplest **tunable** resonator is a  $\lambda/4$ -resonator, as we know it, where  $f = (LC)^{-1/2}$ , however instead of being closed (ground) in the end not coupled to the transmission line, it is connected to a SQUID, which is then grounded. Ida-Maria Svenson, from Delsing's group at Chalmers, does all the math in her thesis, but the bottom line is presented [here](#) (in a paper without her)

$$f = \frac{f_0}{1 + \frac{L_J}{L}}$$

Here  $L_J = \Phi_0 / (4\pi I_c |\cos(\pi\Phi_{ext}/\Phi_0)|)$  is the inductance of the SQUID (stemming only from the Junctions, as the geometric inductance is negligible in comparison), and  $L$  is the transmission line's

inductance to ground (typically  $\simeq 0.7 \text{ nH}$  for  $\lambda/4$  resonators around 6 GHz).

Note that this is true for “moderate” detunings. What happens, when  $\Phi_{ext} \rightarrow \frac{\Phi_0}{2} \Rightarrow L_J \rightarrow \infty$ ?

## Directly coupled resonators

These are qubits without XY control and without readout resonators. Instead, we simply couple the qubit to a feedline, which also serves as a readout line.

Design in four groups of 5 qubits: In each group we have the same junction size (expect the same critical current and thus  $E_J$  and we change the length of the junction arms (given a different  $E_C$ ).

With the parameters:

```
CouplingLength=[55]*1e-6;  
CouplingGap=[20]*1e-6;
```

... we get a coupling of  $\sim 0.4 \text{ fF}$