## DESCRIPTION OF THE MATHEMATICAL MODELS

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Wednesday 16<sup>th</sup> March, 2022

### 1. Introduction

This document describes the mathematical models in the simulation examples related to the article [1]. The simulation codes can be downloaded using the link below. The considered models are particular cases of the boundary controlled heat equations on one and two-dimensional spatial domains considered in [1, Sec. 5]. The simulation codes utilise the free **RORPack** MATLAB library (link below) for controller construction and simulation of the controlled system. In addition, the one-dimensional example uses the free **Chebfun** MATLAB library (link below) for solving the boundary value problems in construction of the controller parameters.

# Download links:

github.com/lassipau/CDC22-Matlab-simulations/ (Simulation codes)
github.com/lassipau/rorpack-matlab/ (RORPack library)
www.chebfun.org (Chebfun library)

### 2. The Heat Equation on a Rectangle

We consider a heat equation on a square  $\Omega = [0, 1] \times [0, 1]$  defined by

$$x_{t}(\xi,t) = \Delta x(\xi,t), \quad x(\xi,0) = x_{0}(\xi)$$

$$\frac{\partial x}{\partial n}(\xi,t) = u(t), \qquad \xi \in \Gamma_{1}$$

$$\frac{\partial x}{\partial n}(\xi,t) = w_{dist}(t), \qquad \xi \in \Gamma_{2}$$

$$\frac{\partial x}{\partial n}(\xi,t) = 0, \qquad \xi \in \Gamma_{0}$$

$$y(t) = \int_{\Gamma_{0}} x(\xi,t)d\xi.$$

Here  $\frac{\partial x}{\partial n}$  denotes the outward normal derivative and  $\Gamma_0$ ,  $\Gamma_1$ ,  $\Gamma_2$ , and  $\Gamma_3$  are parts of the boundary  $\partial\Omega$  of the rectangle defined by (see Figure 1)

$$\Gamma_{1} = \{ (\xi_{1}, \xi_{2}) \in \mathbb{R}^{2} \mid 0 < \xi_{1} < 1/2, \ \xi_{2} = 0 \}$$

$$\Gamma_{2} = \{ (\xi_{1}, \xi_{2}) \in \mathbb{R}^{2} \mid \xi_{1} = 0, \ 0 < \xi_{2} < 1 \}$$

$$\Gamma_{0} = \partial \Omega \setminus (\Gamma_{1} \cup \Gamma_{2})$$

$$\Gamma_{1} = \{ (\xi_{1}, \xi_{2}) \in \mathbb{R}^{2} \mid 0 < \xi_{1} < 1, \ \xi_{2} = 1 \}.$$

The system fits in the setting of the example in [1, Sec. 5] with suitable choices of  $b, c \in L^2(\partial\Omega; \mathbb{R})$  and  $B^1_d(\cdot) \in L^2(\partial\Omega; \mathbb{R}^{1 \times n_{d1}})$ 

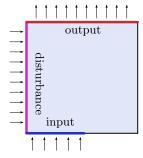


FIGURE 1. Input-output configuration for the 2D heat equation.

In the simulation, the state feedback and output injection operators are use chosen based on LQR/LQG design. Then  $K_0x = \int_{\Omega} x(\xi)k_0(\xi)d\xi$  for some  $k_0 \in L^2(\Omega)$  and the results in [1, Sec. 4] show that for  $\omega = \pm \omega_k \in \mathbb{R}$  the values  $P_K(i\omega)$  and  $P_{KI}(i\omega)$  required in the controller construction could be computed by solving the boundary value problem

$$i\omega x_0(\xi) = \Delta x_0(\xi) + \psi_n(\xi),$$

$$\frac{\partial x_0}{\partial n}(\xi) = u_0 + \int_{\Omega} x_0(\zeta) k_0(\zeta) d\zeta, \qquad \xi \in \Gamma_1$$

$$\frac{\partial x_0}{\partial n}(\xi) = 0, \qquad \qquad \xi \in \Gamma_2 \cup \Gamma_0$$

$$y_0 = \int_{\Gamma_3} x_0(\xi) d\xi.$$

With the choices  $u_0 = 1 \in \mathbb{C}$  and  $\psi_n = 0 \in L^2(0,1)$  we then have  $y_0 = P_K(i\omega)$ , and for  $u_0 = 0$  and  $\psi_n \in L^2(0,1)$  we get  $y_0 = P_{KI}(i\omega)\psi_n$ . However, based on the results in [1, Sec. 4], the parameter  $H_K$  can alternatively be computed as the (approximate) solution of the Sylvester equation

$$G_1H_K = H_K(A + BK_0) + G_2(C_{\Lambda} + DK_0)$$
 on  $D(A + BK_0)$ ,

and the simulation code takes advantage of this possibility. In the code  $H_K$  is computed using another Finite Difference approximation of the original PDE system. Subsequently, the parameter  $B_1$  can be correspondingly approximated by  $B_1 = H_K B + G_2 D$  (where D = 0 for our system).

Figure 2 shows an example output of the simulation.

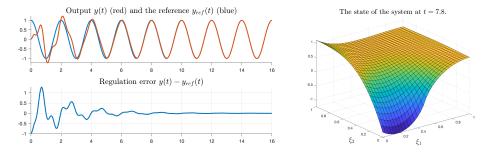


FIGURE 2. Simulation of the 2D heat equation. Output y(t) and tracking error (left) and the temperature profile at t = 7.8s (right).

# 3. The One-Dimensional Heat Equation

Consider a one-dimensional heat equation on  $\Omega = [0, 1]$  with non-collocated boundary inputs and outputs,

$$x_t(\xi, t) = (a(\xi)x_{\xi})_{\xi}(\xi, t) + b_d(\xi)w_d^0(t)$$
  
-x\_\xi(0, t) = u(t) + w\_d^1(t), x\_\xi(1, t) = w\_d^2(t)  
y(t) = x(1, t), x(\xi, 0) = x\_0(\xi),

where the spatially varying heat conductivity satisfies  $a(\cdot) \in C([0,1])$ ,  $a(\xi) > 0$  for all  $\xi \in [0,1]$ , and  $w_d^0(t)$ ,  $w_d^1(t)$ , and  $w_d^2(t)$  are external disturbance signals. It is well-known that this PDE defines a regular linear system on  $X = L^2(0,1)$ . The system is unstable due to the eigenvalue at  $0 \in \mathbb{C}$ .

For stabilizing the system (1) with state feedback and output injection we can choose, e.g.,  $K_0 = -\langle \cdot, \mathbf{1} \rangle_{L^2}$  and  $L = -\mathbf{1}(\cdot) \in L^2(0,1)$ , where  $\mathbf{1}(\xi) = 1$  for all  $\xi \in [0,1]$ . Since  $K_0 x = -\int_0^1 x(\xi) d\xi$ , the results in [1, Sec. 4] show that for  $\omega = \pm \omega_k \in \mathbb{R}$  the values  $P_K(i\omega)$  and  $P_{KI}(i\omega)$  required in the controller construction can be computed by solving the boundary value problem

(2a) 
$$i\omega x(\xi) = (a(\xi)x_{\xi})_{\xi}(\xi) + \psi_n(\xi)$$

(2b) 
$$-x_{\xi}(0) = u_0 - \int_0^1 x(\xi)d\xi, \quad x_{\xi}(1) = 0$$

(2c) 
$$y_0 = x(1)$$
.

With the choices  $u_0 = 1 \in \mathbb{C}$  and  $\psi_n = 0 \in L^2(0,1)$  we then have  $y_0 = P_K(i\omega)$ , and for  $u_0 = 0$  and  $\psi_n \in L^2(0,1)$  we get  $y_0 = P_{KI}(i\omega)\psi_n$ . Based on the results in [1, Sec. 4], the simulation code solves the the boundary value problem numerically using the **Chebfun** library and the solution is computed for a finite number of functions  $\psi_n$  taken from any orthonormal basis of  $L^2(0,1)$  (by default  $\{1\} \cup \{\sqrt{2}\cos(2\pi n \cdot)\}_{n=1}^{\infty} \cup \{\sqrt{2}\sin(2\pi n \cdot)\}_{n=1}^{\infty}$ ).

Figure 3 shows an example output of the simulation.

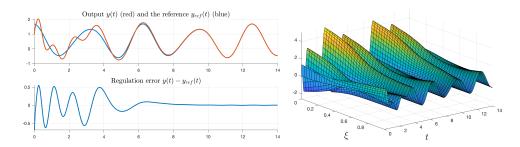


FIGURE 3. Simulation of the 1D heat equation. Output y(t) and tracking error (left) and the controlled temperature profile (right).

### References

[1] Lassi Paunonen and Jukka-Pekka Humaloja. On robust regulation of PDEs: from abstract methods to PDE controllers. In *Proceedings of the 61st IEEE Conference on Decision and Control*, Cancún, Mexico, December 6–9, 2022 (submitted). Preprint available at arxiv.org

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