

AUTOMAATIOPÄIVÄT²⁴

13.-14.4.2021 | Virtual event

Rejection of Unknown Harmonic Disturbances in a Boundary Controlled Heat Equation

Lassi Paunonen, Tampere University

SPONSORS



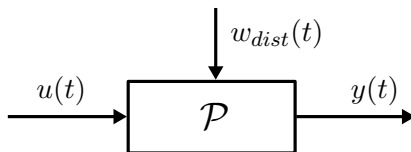
SUOMEN AUTOMAATIOSEURA RY
FINNISH SOCIETY OF AUTOMATION

In this presentation

- ➊ An overview of controlled Partial Differential Equations (“PDE Control”), and its applications.
- ➋ Disturbance rejection for a controlled heat equation model.

Part I: PDE Control and Applications – An Overview

Control of Partial Differential Equations



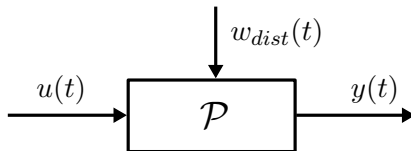
In most control problems (linear or nonlinear), the plant \mathcal{P} is an Ordinary Differential Equation with state $x(t)$ depending on time.

- RLC circuits, mechanical systems
- Different types of robotic models, etc

In **PDE Control**, \mathcal{P} is a **Partial Differential Equation**, whose state depends on several variables, typically,

$$x(t, z) \quad \text{where} \quad t = \text{time}, \quad z = \text{position}.$$

Control of Partial Differential Equations



In **PDE control**, \mathcal{P} is a **Partial Differential Equation**, whose state depends on several variables, typically,

$$x(t, z) \quad \text{where} \quad t = \text{time}, \quad z = \text{position}.$$

Such models describe the dynamics of, for example,

- temperature distributions (“**heat equation**”)
- flexible and vibrating structures (“**beam, plate, wave eqns**”)
- fluid flows (“**convection and transport equations**”)

Example: Robots with Flexible Components

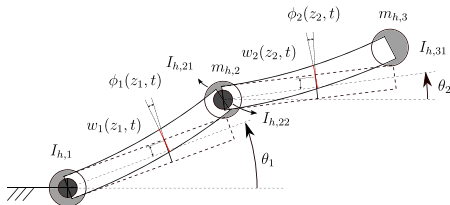


Fig. 2. Flexible two links manipulator.



Figure: Mattioni et. al. 2020 (left), www.nasa.gov (right).

Application: Control design for robotic arms with flexible links.

- The dynamics of flexible links modelled with **beam equations**
- Especially lightweight structures cause flexibility (space, nano)

Example: Control of Traffic Flows



Figure: Wikipedia.

- Dynamics of large configurations of vehicles can be modelled with **transport equations**
- Allows control design to reduce traffic jams
- Speed limits and lights can be used as control actuators
- PDE models can sometimes be used in control design even for small formations

Other Examples

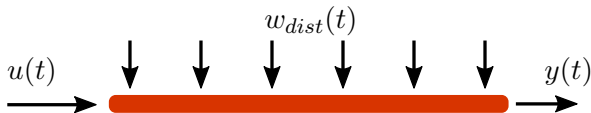
- Control of temperature profiles:
 - Control of room temperature models, heat exchange processes
 - Involves **convection-diffusion equations**
- Control of flows:
 - Mixing processes, pipe networks
 - Depending on the problem, may involve **convection** or **transport equations**
- Vibration control:
 - Vibrations in drilling equipment, large-scale buildings, wind turbine towers
 - Involves **wave, plate and beam equations**



Figure: Wikipedia.

Part II: Rejection of Harmonic Disturbances

Main Case: A Controlled Heat Equation



Consider the controlled PDE: for $x \in [0, 1]$

$$\begin{aligned}\frac{\partial v}{\partial t}(x, t) &= \frac{\partial}{\partial x} \left(c(x) \frac{\partial v}{\partial x}(x, t) \right) + B_d(x) w_{dist}(t) \\ \frac{\partial v}{\partial x}(0, t) &= u(t), \quad \frac{\partial v}{\partial x}(1, t) = 0, \\ y(t) &= v(1, t).\end{aligned}$$

$v(x, t)$ is the temperature of a metal bar of length $\ell = 1$, heat conductivity $c(x)$, heating control input at $x = 0$, isolated at $x = 1$. Temperature measurement at $x = 1$.

Problem (Output Tracking and Disturbance Rejection)

Choose a control law in such a way that

- The output $y(t)$ converges to a given reference level $y_{ref} \in \mathbb{R}$ asymptotically, i.e.

$$|y(t) - y_{ref}| \rightarrow 0 \quad \text{as } t \rightarrow \infty$$

despite the external disturbance $w_{dist}(t)$.

We assume the disturbance has the form

$$w_{dist}(t) = a_0 + \sum_{k=1}^q a_k \cos(\omega_k t + \varphi_k),$$

unknown frequencies $\{\omega_k\}_k$, amplitudes $\{a_k\}_k$ and phases $\{\varphi_k\}_k$.

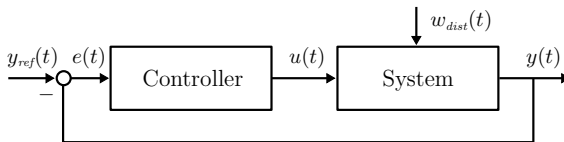
Problem (Output Tracking and Disturbance Rejection)

Choose a control law in such a way that

- The output $y(t)$ converges to a given reference level $y_{\text{ref}} \in \mathbb{R}$ asymptotically, i.e.

$$|y(t) - y_{\text{ref}}| \rightarrow 0 \quad \text{as } t \rightarrow \infty$$

despite the external disturbance $w_{\text{dist}}(t)$.



Solution

$$w_{dist}(t) = a_0 + \sum_{k=1}^q a_k \cos(\omega_k t + \varphi_k),$$

Background:

- If the frequencies $\{\omega_k\}_k$ were **known**, the problem could be solved using **internal model based control** (developed for PDEs by the TUT/TAU group and many others).

Solution:

- Combine a **frequency estimator** to approximate ω_k with $\hat{\omega}_k(t)$, and an **internal model based** controller.
- \leadsto Closed-loop system is a time-dependent PDE-ODE system, creates (interesting!) mathematical challenges, methods developed in [Afshar-Paunonen 2019, 2020].

Simulation Results

Parameters: $c(x) \equiv 1$, disturbance profile $B_d(x) = \sin(3.5x)$,

$$w_{dist}(t) = \cos(1.5t - 0.4) + 5 \cos(5t + 0.2) \quad (\omega_1 = 1.5, \omega_2 = 5)$$

$$y_{ref} = 56.$$

Choice of the frequency estimator:

- An adaptive estimator by Carnevale & Astolfi, [2008 ACC].
- Multi-frequency estimation
- Input-to-State Stable (required in control design)

Simulation Results

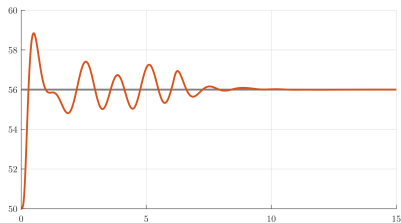


Figure: Controlled output.

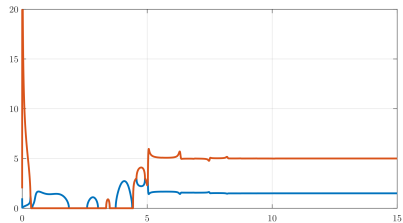


Figure: Frequency estimates.

Simulation Results

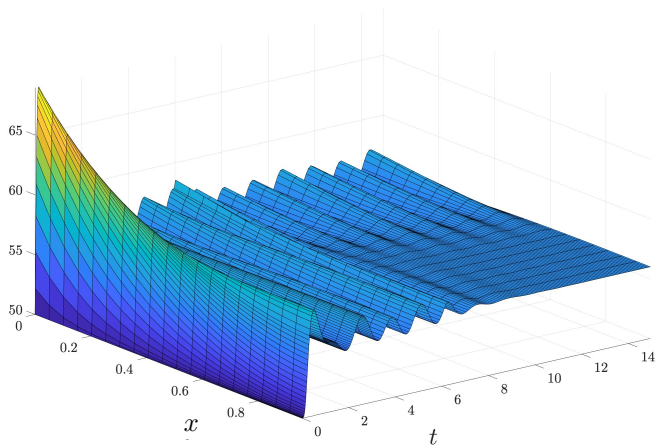


Figure: The controlled heat profile.

Robustness Analysis

Question

Can the control design handle uncertainty in the parameters of the heat equation?

	IM controller	Frequency estimator	Combination
Robustness:	OK	??	??

Robustness Analysis

Question

Can the control design handle uncertainty in the parameters of the heat equation?

	IM controller	Frequency estimator	Combination
Robustness:	OK	X	X

Short answer: **Very poorly.**

Simulation Results – Perturbed System

Perturbation: An unmodelled reaction term, magnitude $\approx 2 \cdot 10^{-5}$.

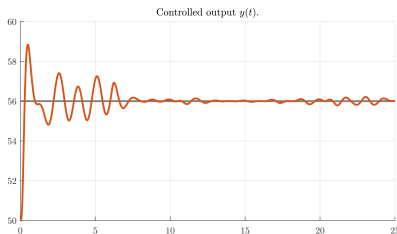


Figure: Controlled output.

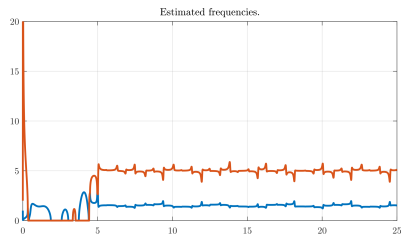


Figure: Frequency estimates.

Simulation Results – Perturbed System

Perturbation: An unmodelled reaction term, magnitude $\approx 10^{-3}$.

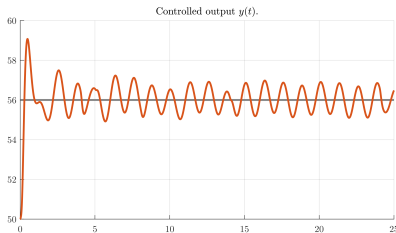


Figure: Controlled output.

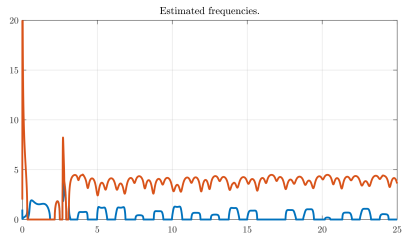


Figure: Frequency estimates.

Robustness Analysis

	IM controller	Frequency estimator	Combination
Robustness:	OK	X	X

Comments:

- The chosen frequency estimator is very sensitive to **persistent** noise.
- In this control design, perturbations cause noise due to “observer model mismatch”.
- Potential remedies: Better choices of frequency estimators, changes in the controller design structure, ...?

Summary

In this presentation:

- A brief overview of fundamentals of PDE Control and some of its applications.
- Control design for disturbance rejection in a controlled heat equation.
- Simulation results and analysis of robustness limitations.

Thank You!

<http://sysgrouptampere.wordpress.com>