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Comparative Analysis of Circular and Rectangular Reinforced Concrete Tanks Based on Economical Design Perspective

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Abstract: The need for a water tank is as old as civilization, to provide storage of water for use in many applications. Design and cost estimation of water tanks is a time consuming task, which requires a great deal of expertise. All tanks are designed as crack free structure to eliminate any leakage. This project therefore studies the efficiency of rectangular or circular tanks, 40,000 liters capacities were used in order to draw reasonable inferences on tanks shape design effectiveness, relative cost implications of tank types and structural capacities. The basic tanks construction materials include steel reinforcement, concrete and formwork obtained from the prepared structural drawings. Result of the materials take-off revealed that circular tank consumed lesser individual materials as compared to rectangular one. This will give circular shaped tanks more favored selection over the rectangular shaped tank, although some other factors must still be assessed.

Keywords: Reinforced Concrete, Steel Reinforcement, Water Tank, Formwork

1. Introduction

Water is considered as the source living for every creation as it is a crucial element for healthy living. Safe drinking water is one of the basic elements for human to sustain a healthy life. High demand for safe and clean water is rising day by day as one cannot live without water. Thus, it becomes necessary to store water, water is stored generally in concrete water tanks and later on it is pumped to different areas to serve community.

An extensive literature review reveals that a minimum amount of research works had been done on this topic, especially in Nigeria. [1] Rationalized the design procedure for reinforced and pre-stressed concrete tanks so that an applicable Canadian design standard could be developed. The study investigates the concept of partial pre-stressing in liquid containing structures. The paper also includes experimental and analytical phases of total of eight full scale specimens, representing segments from typical tank walls, subjected to load and leakage tests. In analytical study a

computer model that can predict the response of tank wall segments is described and calibrated against the test results. The proposed design procedure addresses the leakage limit state directly. It is applicable for fully pre-stressed, fully reinforced and partially pre-stressed concrete water tanks. The conclusions that are drawn are as follows:

- i. A design method based on limiting the steel stress, does not produce consistent crack or compression zone depths under the application of pre-stressing nor under a combination of axial load and moment.
- ii. A design method based on providing a residual compressive stress in concrete does not utilize non-pre-stressed reinforcement effectively.
- iii. Relaxing the residual compressive stress requirement permits a more efficient design. The stresses in non-pre-stressed steel are higher, but remain below yield under service load. Therefore, less reinforcement is required.

- iv. Load eccentricity significantly affects the behavior of the pre-stressed concrete sections. The behavior with a small load eccentricity, less than about half the thickness, the section may be treated as a flexure member.
- v. The ratio of non pre-stressed steel to pre-stressed steel in partially pre-stressed concrete section has a significant effect on the member serviceability and strength. Choosing the ratio such that both non- pre-stressed and pre-stressed steel reach their strength simultaneously utilizes both types of steel at the ultimate limit state effectively.
- vi. Increasing the wall thickness is very effective in increasing the capacity of the section and improving its serviceability by increasing the compression zone depth and reducing the deformations.

Another Study was done on cost optimization of reinforced concrete circular grain silos based on the BS Code (2002) [2]. He proved that the minimum cost of the silo increases with increasing angle of internal friction between stored materials and concrete, the coefficient of friction between stored materials and concrete, and the number of columns supporting hopper. While [14] studied the economical design of concrete water Tanks by optimization method. He applied the optimization technique to the structural design of concrete rectangular and circular water tanks, [20] have brought out the revised version of BS 3370 (part 1 and 2) after a long time from its 1965 version in year 2009. This revised code is mainly drafted for the liquid storage tank.

1.1. Need for Storage Tank

Reservoir is a common term applied to liquid storage structure and it can be below or above the ground level. Reservoirs below the ground level are normally built to store large quantities of water whereas those of overhead type are built for direct distribution by gravity flow and are usually of smaller capacity.

Storage reservoirs and water tanks are used to store water, liquid petroleum, petroleum products and similar liquids. The force analysis of the reservoirs or tanks is about the same irrespective of the chemical nature of the product. All tanks are designed as crack free structures to eliminate any leakage. Water or raw petroleum retaining slab and walls can be of reinforced concrete with adequate cover to the reinforcement. Water and petroleum react with concrete and, therefore, no special treatment to the surface is required. Industrial wastes can also be collected and processed in concrete tanks with few exceptions.

The need for a water tank is as old as civilization, to provide storage of water for use in many applications. Water tanks can be classified as circular, rectangular, conical, depending on their location. The tanks can be made of steel or concrete. Tanks resting on ground are normally circular or rectangular in shape and are used where large quantities of water need to stored. Water tank parameters include the general design of the tank, and choice of construction materials and linings. Reinforced Concrete Water tank design

depends based on the location of tanks. The tanks can be made of RCC or even of cylinder for corrosion protection and to form an interstitial space.

1.2. Statement of Problem

Reinforced concrete water tanks are used to store and supply safe drinking water. With the rapid speed of urbanization, demand for drinking water has increased by many folds. Also, as demand for water tanks will continue to increase in coming years, quick cost prediction of circular rectangular tanks before its design will be helpful in selection of tanks for real design. Quick cost prediction of tanks of different geometry and capacity is a difficult job and a time consuming task especially for less experienced design engineers [18], [17]. Many times it is required to know the cost of a tank of known capacity and geometry before its detailed design [24]. Many researchers such as [16], [14], [11], [9] and [18] have studied the stability and the economic aspects of water tank design.

1.3. Significance of the Study

This research is concern with the comparison between circular and rectangular reinforce concrete tanks. It attempted to achieve some measure of the best practical solutions, that is, the optimum design of reinforced concrete water tanks for a specified performance.

1.4. Aim

The major aim is to reveal the degree of effectiveness of the geometric shapes for the functional requirement, with the view to achieving adequate strength and economy.

1.5. The Specific Objectives

The specific objectives of the study are:

- i. To make the analysis and design of water tank in accordance with BS8007code
- ii. To compare the economical design of circular and rectangular reinforce concrete tank.
- iii. To estimate the cost of construction of both circular and rectangular tanks and hence to access the possible cost implications of each choice.

2. Methodology

The design tool for circular and rectangular reinforced concrete water tanks was prompted by the rigorous and lengthy manual design of reinforced concrete water tank, fully dimensioned and listed in a schedule of the reinforcement which is used on site for the bending and fixing of the bars. Standard bar shapes and a method of scheduling were used as specified in BS8666, The British code of practice BS8007, which is a modification to BS8110, was also adopted as well. The principal features include:

- i. The use of a factor of safety $U_f=1.4$ for liquid loads.
- ii. The use of concrete grade C30 (with a maximum water/cement ratio of 0.55 and a minimum cement

content of 325kg/m³ that is, durability performance comparable to grade C40).

- iii. The use of a minimum cover of 25mm owing to assumed severe exposure condition on internal and at least one of both faces.
- iv. Maximum crack width limited to 0.3mm unless the aesthetic appearance is critical, when 0.1mm is used to avoid staining of the concrete.
- v. Maximum bar spacing of 300mm.
- vi. For a wall thickness is exceeding 200mm and floor thickness exceeding 300mm.
- vii. Anchorage bond stress for straight horizontal bars in sections subjected to direct tension must be reduced to 70 per cent of the usual values.
- viii. At least 75mm blinding concrete is required below ground slabs.

2.1. Design of Circular Reinforced Concrete Water Tank

Step 1: Given data

Capacity of the tank = 40,000L

Depth of water (h) = 5.9 – 0.2 = 5.7m

Overall depth (H) = 5.9m

Volume of water (V) = 40,000/1000 = 40 m³

Concrete cover = 0.25m

Free board = 0.2m

Concrete grade = Reinforcement Fe415

Step 2: Determination of tank diameter

$$A = \frac{40}{5.7} = 7.0175 \approx 7.018 \text{ m}^2$$

$$D = \sqrt{\frac{4A}{\pi}} = \sqrt{\frac{4 \times 7.018}{3.143}} = 3 \approx 3 \text{ m}$$

Step 3: Analysis of hoop tension and bending moment

One meter width of the wall is considered as the thickness of the wall is estimated as:

$$t = 30H + 50 = 30 \times 5.7 + 50 = 221 \text{ mm}$$

The thickness of the wall is assumed as 230mm

$$\therefore \text{Maximum hoop tension } T_{Max} = 0.575 \times \frac{wHD}{2} = 0.575 \times \frac{10 \times 5.7 \times 3}{2} = 49 \text{ kN}$$

$$\text{Maximum bending moment } M_{Max} = 0.0146 \times wH^3 = 0.0146 \times 10 \times 5.7^3 = 27 \text{ kNm}$$

Step 3: Design of section

Permissible compressive stress in concrete $\sigma_{cbc} = 7 \text{ N/mm}^2$

Permissible compressive stress in steel $\sigma_{st} = 150 \text{ mpa}$

Modular ratio = M = 13.33

Design constants are:

$$K = \frac{M \times \sigma_{cbc}}{M \times \sigma_{cbc} + \sigma_{st}} = \frac{13.33 \times 7}{13.33 \times 7 + 150} = 0.39$$

$$J = 1 - \left(\frac{K}{3} \right) = 1 - \left(\frac{0.39}{3} \right) = 0.87$$

$$Q = \frac{1}{2} \sigma_{cbc} JK = \frac{1}{2} \times 7 \times 0.87 \times 0.39 = 1.19$$

$$\text{Effective depth} = d = \sqrt{\frac{M_{Max}}{Qb}} = \sqrt{\frac{27.038 \times 10^6}{1.19 \times 1000}} = 150.73 \approx 151 \text{ mm}$$

Let the overall thickness be 230mm with effective cover of

25mm

$$\therefore d_{provided} = 230 - 25 = 205 \text{ mm}$$

$$A_{st} = \frac{M_{Max}}{\sigma_{st} J d} = \frac{27.038 \times 10^6}{150 \times 0.87 \times 205} = 1010.52 \text{ mm}^2$$

Spacing of 16mm diameter bar = $\frac{201 \times 1000}{1010.52} = 198.907 \approx 200 \text{ mm/c}$

Provided #16mm@200mm/c as vertical reinforcement on water face

$$\text{Hoop steel} = A_{st1} = \frac{T_{Max}}{\sigma_{st}} = \frac{147.488 \times 10^3}{150} = 983.25 \text{ mm}^2$$

Spacing of 12mm diameter bar = $\frac{113 \times 1000}{983.25} = 114.92 \approx 110 \text{ mm/c}$

Provided #12mm@110mm/c as hoop reinforcement on water face

$$\text{Actual area of steel provided} = A_{st} = \frac{113 \times 1000}{110} = 1027.3 \text{ mm}^2$$

Step 4: Check for tensile stress

$$\sigma_c = \frac{T_{Max}}{1000t + (m-1)A_{st}} = \frac{147.488 \times 10^3}{1000 \times 230 + (13.33-1) \times 1027.3} = 0.61 \text{ N/mm}^2$$

Permissible stress = 1.2N/mm² > 0.61N/mm² safe

Step 5: Top slab

The thickness of top slab shall be 150 since there is no load or stresses on it, minimum area of steel is 0.24% of concrete area should be provided

$$\therefore A_{st} = \frac{0.24}{100} \times b \times t = \frac{0.24}{100} \times 1000 \times 150 = 360 \text{ mm}^2$$

Reinforcement for each face = 180mm²

$$\text{Spacing of 8mm diameter bar} = \frac{50.24 \times 1000}{180} = 279 \text{ mm/c}$$

Provide #8mm @250mm/c as vertical and horizontal distribution steel

Step 6: Base slab

The thickness of base shall be 150mm the base rests on firm ground; hence only minimum reinforcement is provided

$$\therefore A_{st} = \frac{0.24}{100} \times b \times t = \frac{0.24}{100} \times 1000 \times 150 = 360 \text{ mm}^2$$

Reinforcement for each face = 180mm²

$$\text{Spacing of 8mm diameter bar} = \frac{50.24 \times 1000}{180} = 279 \text{ mm/c}$$

Provide #8mm @250mm/c as vertical and horizontal distribution on the outer face

2.2. Design of Rectangular Reinforced Concrete Water Tank

Step 1: Given data

Capacity = 40,000L = 40m³

Depth = 2.0m

Size = 4m × 5m

Free bore = 0.2m

Concrete = M₂₀

Reinforcement = Fe415

Step 2: Permissible stresses

$$\sigma_{cb} = 7 \text{ N/mm}^2$$

$\sigma_{st} = 100\text{N/mm}^2$ (on faces near water face)
 $\sigma_{st} = 125\text{N/mm}^2$ (on faces away from water)
 $M = 13$, $Q = 1.41$, $J = 0.84$

Step 3: Dimension of the tank

Length = $L = 5\text{m}$

Width = $B = 4\text{m}$

Ratio = $\frac{L}{B} = \frac{5}{4} = 1.25$

Step 4: designs of long walls and short walls

Long walls are designed as vertical cantilevers and short walls are spanning horizontally between long walls

Maximum bending moment at base of long wall

$$M_L = \frac{wH^3}{6} = \frac{10 \times 2.2^3}{6} = 17.75\text{KNm}$$

$$\text{Effective depth} = d = \sqrt{\frac{M_L}{Qb}} = \sqrt{\frac{17.75 \times 10^6}{1.41 \times 1000}} = 112.2 \approx 120\text{mm}$$

Using 16mm diameter bars and 25mm clear concrete cover

Effective depth = 120mm

Overall depth = 160mm

$$A_{st} = \frac{M_L}{Bjd} = \frac{17.75 \times 10^6}{1000 \times 0.84 \times 120} = 186.99 \approx 176\text{mm}^2$$

Spacing of 16mm diameter bar = $\frac{100 \times 201}{176} = 114.2 \approx 120\text{mm c/c}$

Provide #16mm @120mm c/c toward the top

Intensity pressure 1m above the top = $P = w(H - h) = 10(2.2 - 1) = 12\text{KN/m}^2$

Direct tension in long walls = $T_L = \left(\frac{12 \times 2}{2}\right) = 12\text{KN}$

$$A_{st1} = \frac{12 \times 10^3}{100} = 120\text{mm}^2$$

But minimum area = $0.3\% = \left(\frac{0.3}{100} \times 160 \times 1000\right) = 420\text{mm}^2$

Spacing of 10mm diameter bar = $\frac{1000 \times 79}{420} = 188\text{mm}$

Provided #10mm @200mm c/c on both faces

Design for short walls:

Intensity pressure 1m above the top = $P = w(H - h) = 10(2.2 - 1) = 12\text{KN/m}^2$

Effective span of horizontally spanning slab = $(4 + 0.16) = 4.16\text{m}$

Bending moment (corner section) = $M_S = \left(\frac{PL^2}{12}\right) = \left(\frac{12 \times 4.16^2}{12}\right) = 17.31\text{KNm}$

Tension transferred per meter height of short wall = $T_S = (12 \times 1) = 12\text{KN}$

$$\therefore A_{st} = \frac{M_S - T_S}{\sigma_{st} \times J \times d} + \frac{T_S}{\sigma_{st}} = \frac{17.31 \times 10^6 - 12 \times 10^3(113 - 100)}{100 \times 0.84 \times 113} + \frac{12 \times 10^3}{100} = 1927.21 \approx 1928\text{mm}^2$$

Spacing of 10mm diameter bar = $\frac{1000 \times 79}{1928} = 40.98\text{mm}$

Provide #16mm bars at 40mm c/c at mid-span section the bending moment is $PL^2/24$ and hence #10mm diameter bars at 80mm c/c away from water face.

Step 5: Design of cantilevering effect of short walls

Maximum bending moment = $B.M = \frac{1}{2} \times \frac{1}{3} wH = \frac{1}{2} \times \frac{1}{3} \times 10 \times 2.0 = 3.333\text{KNm}$

Effective depth using 10mm diameter = $d = (160 - 25 - 10 - 5) = 120\text{mm}$

$$\therefore A_{st} = \frac{3.333 \times 10^6}{100 \times 0.84 \times 120} = 396.785 \approx 397\text{mm}^2$$

But 0.3% of gross area = $\left(\frac{0.3}{100} \times 160 \times 1000\right) = 480\text{mm}^2$

Spacing of 10mm diameter bar = $\frac{1000 \times 79}{480} = 164.58\text{mm}$

Provide #10mm @200mm c/c both faces in the vertical direction

Step 6: Base slab

The thickness of base slab shall be 150mm the base rests on firm ground; hence only minimum reinforcement is provided

$$\therefore A_{st} = \left(\frac{0.24}{100} \times 150 \times 1000\right) = 360\text{mm}^2$$

Reinforcement for each face = 180mm^2

Spacing of 10mm diameter bar = $\frac{1000 \times 79}{180} = 438\text{mm}$

Provide #10mm @400mm c/c as vertical and horizontal distribution on the outer face.

3. Result Presentation

The summary for both circular and rectangular reinforced concrete tanks reinforcement is given in Table 1 and Table 2 respectively.

Table 1. Bar schedules for reinforced rectangular concrete tank.

Bar reference	Bar shape	Diameter (mm)	Length (mm)	Total number of bar
#16mm	Straight	16	2716	198
#16mm - A	Straight	10	2560	89
#16mm - B	Straight	10	5210	48
#16mm - C	U-shaped	10	660	54
#16mm - D	Straight	10	4210	108
#16mm - E	Straight	10	2410	12
#16mm - F	Straight	10	4210	25
#16mm - I	Straight	10	5210	20

Table 2. Bar schedules for reinforced concrete circular tank.

Reference	Bar-shape	Diameter (mm)	Number of bar	Length (mm)
#	Circular/Hoop	12	55	27930
#	Straight	16	298	5590
# - A	U-shape	8	37	9050
# - B	U-shape	8	39	9350

The taking - off, abstract, bill of quantity and detailed calculations are shown in the appendices while the summary is shown in Table 3.

Table 3. Bill of Quantities Summary.

Items	Circular tank		Rectangular tank	
General clearance of top soil	0.0144ha	₦7200.00k	0.003ha	₦150.00k
Excavation for foundation	21.60m ³	₦172800.00k	5.698m ³	₦45584.00k
Provision of concrete	58.99m ³	₦782240.00k	12.141m ³	₦161211.00k
Placing of concrete	58.99m ³	₦294950.00k	12.141m ³	₦60705.00k
Form work	126.95m ²	₦334960.00k	163.2m ²	₦42615.00k
Reinforcement	0.32204t	₦111137.00k	0.1277t	₦90299.00k
Total		₦1703287.00k		₦400564.00k

4. Discussion

Table 2 indicates that the quantities of materials need for the circular water tank were constantly more than those needed for the rectangular water tank at each varied capacity.

Assessing the relative reduction in the amounts of materials for the rectangular tanks, it was seen that the formwork would be significantly more challenged in the construction of the circular tanks, their presumed material quantity advantage could be given up for a selection of circular tank (through with potential increase in material requirement). This could be considered if the said reduction in materials is relatively small or variable. But, the final choice would depend on the client's desire and the advice of the professional taking off the job.

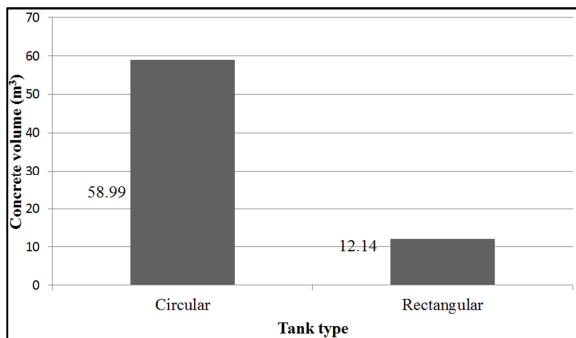


Figure 1. Concrete volume distribution chart.

From the Figure 1, although, both circular and rectangular water tanks have the same capacities but from the result, the amount of concrete in circular tank is greater than that of rectangular tank. Therefore it is advisable to use the rectangular tank in terms of cost but in case of resistance to all pressure exerted in the tank circular is better.

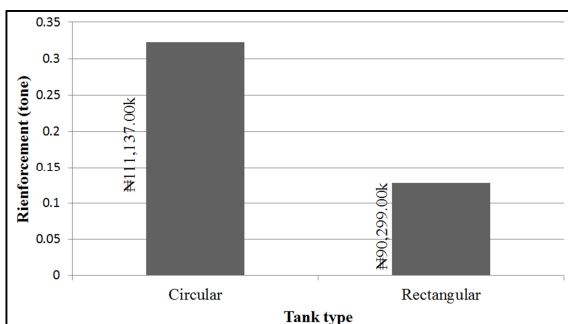


Figure 2. Reinforcement distribution chart.

Based on Figure 2, a circular tank is greater than rectangular tank with respect to their quantities of reinforcement. Both circular and rectangular water tanks have the same capacities but from the result design, the amount of reinforcement tonnage in circular tanks is greater than that of rectangular tank.

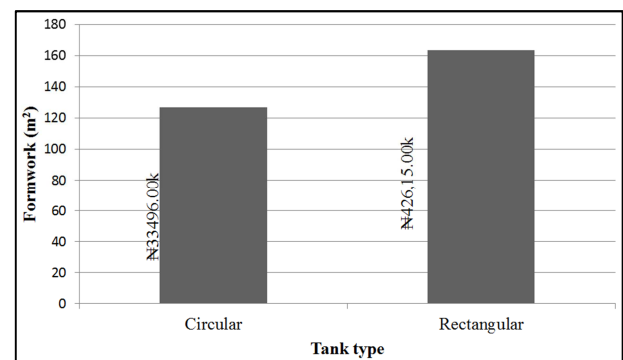


Figure 3. Formwork distribution chart.

According to Figure 3, both circular and rectangular water tanks have the same capacities however from the design output, the amount of formwork in meter square in rectangular tanks is greater than that of circular tank. In conclusion, circular tank has the higher quantities and amount in terms of concrete and reinforcement than that of rectangular tank. But rectangular tank is greater than circular tank in term of formwork. Moreover from the overall cost, the circular tank is greater than rectangular tank.

4.1. Conclusion

Generally, the construction material outputs for all water tanks shape would be based on the choice of the design considerations, with the size of their structural elements. Hence, there exists the possibility of having an equal capacity and similar geometrically shaped water tank but with some measurable difference in material requirement, for instance, a tank wall designed as a cantilever would come up with a relatively difference material quantity when compared with its material requirements. If designed as a two-way spanning wall (as for rectangular tank) or ring (or hoop) wall, (as for circular tank).

It can be clearly seen that materials needed for the construction of rectangular water tank is comparatively more than those required for circular one but ease of construction, is more difficult in circular water tank as compared to that of rectangular water tank. Hence it could be deduced that the

outcome of tank design and the possible cost implication of its material requirements coupled with the relative ease of construction would be considered for the proposed water tank of any capacity although some other factors must still be assessed.

4.2. Recommendation

The research studies the comparison between circular and rectangular reinforced concrete tanks based economical design point of view. For future research, the following investigations are recommended:

- i. Examination the response of reinforced concrete tanks under the effect of Hydrodynamic pressure resulting from earthquake loading.
- ii. Failures of tanks should be investigated by using a computer program that considers cracking and nonlinearity.
- iii. Additional experimental study of wall specimens subjected to both axial tensions and combined axial compression is needed.

List of Symbols

H: Overall depth
 h: Depth of water
 V: Volume
 Fe: Reinforcement grade
 A: Area
 D: Diameter
 t: Wall thickness
 T_{Max} : Maximum hoop tension
 M_{Max} : Maximum bending moment
 w: Weight of water
 σ_{cbc} : Permissible compressive stress in concrete
 σ_{st} : Permissible compressive stress in steel
 M: Modular ratio
 K, J, Q: Design constants
 d: Effective depth
 A_{st} : Area of steel
 #: Steel type
 \approx : Approximation
 σ_c : Tensile stress
 b: width
 M_L : Bending moment for long walls
 T_L : Direct tension for long walls
 P: Intensity pressure
 M_s : Bending moment for short walls
 T_s : Tension transferred for short walls
 B. M: Maximum bending moment
 @: at
 c/c: Center to center

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