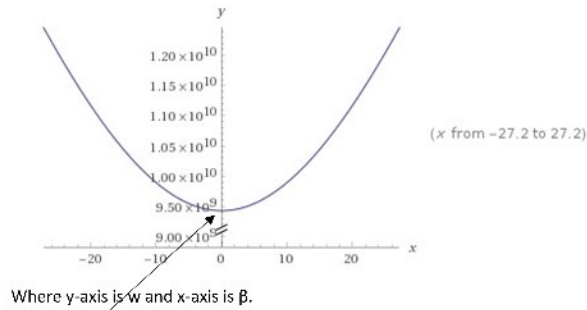


Part 1: Rectangular waveguide simulation

Analysis:

(a) Given the cross-section dimensions of the rectangular waveguide, plot its dispersion diagram (as in Fig. 2).



9.5 GHz=resonance frequency

(b) Mark the measured resonance frequencies on the theoretically computed dispersion diagram.

$$w_0 = \frac{\pi c}{a} = \pi * 3 * 10^8 * 100 * 10^{-3} = 9.42 \text{ GHz}$$

Which corresponds to the resonance frequency found from the above graph (approximately).
 $a=100\text{mm}$

(c) Given the cavity length L , verify that the resulted wavenumbers βn satisfy the resonance condition presented in Eq. (5) for $n = 1, 2, 3 \dots$

$$\omega_n = c \sqrt{\left(\frac{\pi}{a}\right)^2 + \left(\frac{n\pi}{L}\right)^2}$$

$L = 680 \text{ mm}$ $\beta = n\pi/L$ (Waveguide 1)

$N=1 \rightarrow w=9.53\text{e}9, \beta=4.61$

$N=2 \rightarrow w=9.82\text{e}9, \beta=9.24$

$N=3 \rightarrow 1.03\text{e}10, \beta=13.86$

We can observe that the numbers we get by calculus match our graph. The resonance condition is respected.

(d) Compare the S_{11} and S_{21} curves, and discuss their similarities and differences.

For $f \rightarrow \text{flow}$, we can observe that S_{21} is highly negative dB while S_{12} remains at 0dB.

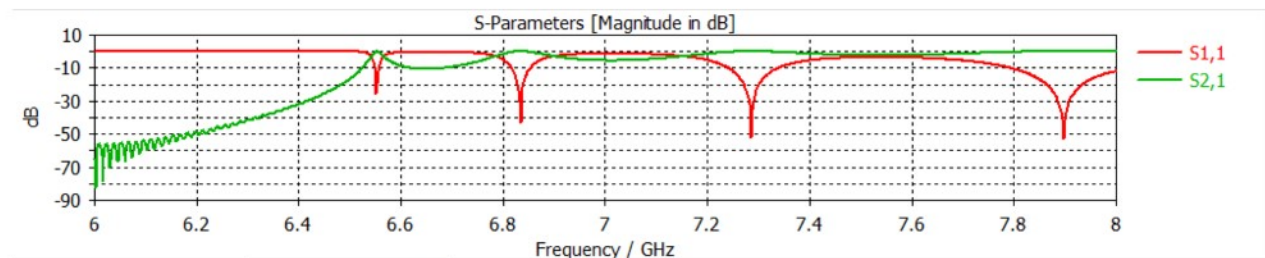
At some point, $f=6.55\text{GHz}$, S_{21} reaches 0db. This means that reflections are eliminated.

The S parameters are measured as the ratio between the incident wave to any port.

* S_{21} =TRANSMISSION coefficient

* S_{11} =REFLECTION coefficient

Looking at the curve, once we get some significant transmission, 0dB is 1 so full transmission (no reflection), However we can still observe some resonance frequencies where the reflection coefficient gets some negative value in dB, this means the reflection loss gets low at specific frequencies=resonance frequencies.



Hollow_rect.cst:

$$\text{If } \epsilon_{\text{psilon}} = 1, f_{c,mn} = \frac{1}{2\pi} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

-First mode: $m = 1, n = 0 \rightarrow f = 6.56\text{GHz}$

-Second mode: $m = 0, n = 1 \rightarrow f = 14.73\text{GHz}$

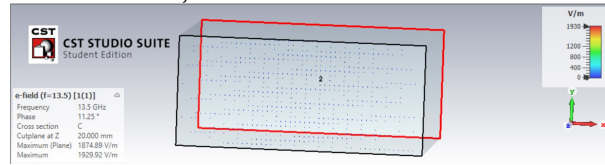
-Third mode: $m=n=1 \rightarrow f = 16.16\text{GHz}$



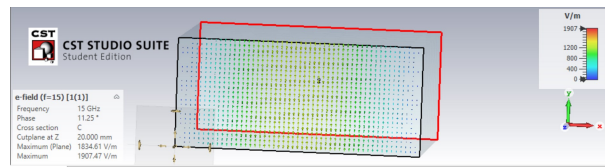
electric field cross section 2d wave

-second mode: $m=0, n=1 \rightarrow f = 14.750116$

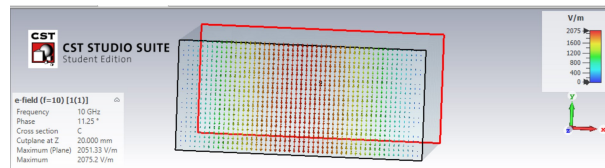
-Third mode: $m=n=1 \rightarrow f = 16.16\text{GHz}$



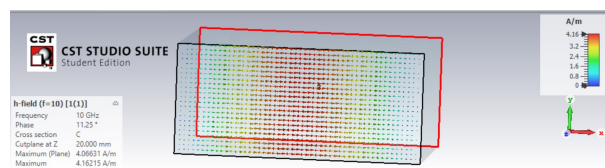
Electric field cross section 2nd mode
(vertical alignment for \vec{E})



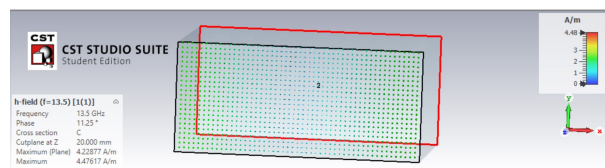
\vec{E} field cross section 3rd mode



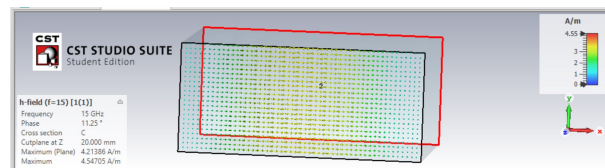
\vec{E} field cross section 1st mode



\vec{H} field cross section 1st mode
(horizontal alignment for \vec{H})



\vec{H} field cross section 2nd mode



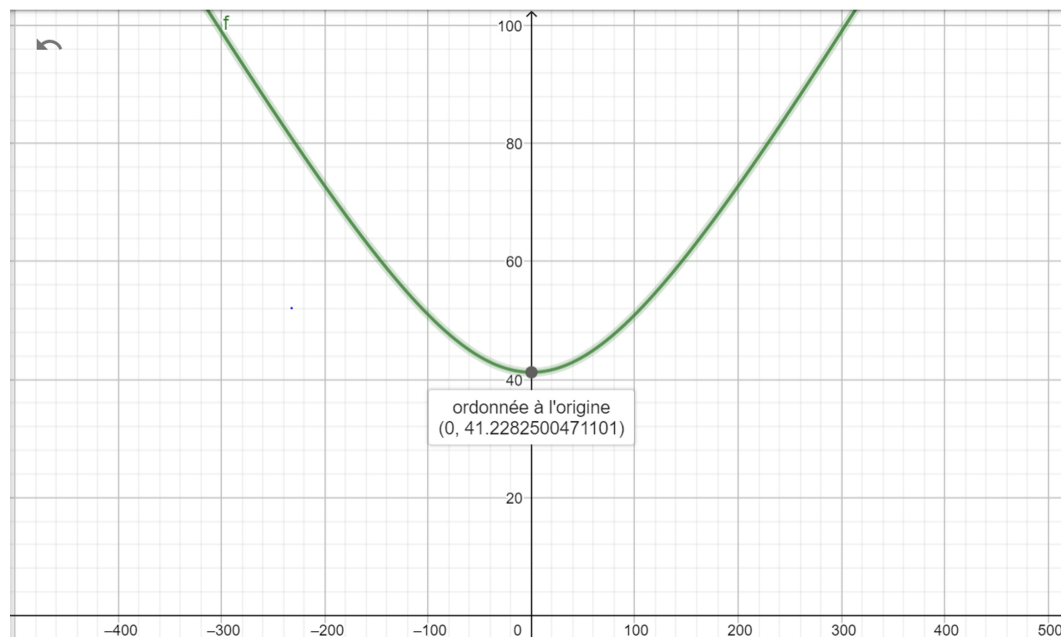
\vec{H} field cross section 3rd mode -
→ magnitude of the \vec{E}, \vec{H} fields increases for lowest frequencies and

Now we change the material to Teflon of dielectric constant 2.1

And we have: $w_{co} = \frac{\pi c}{a\sqrt{\epsilon}} = 2.85e10 \rightarrow f = 4.53\text{GHz}$

(a)

In the following graph, the x axis corresponds to beta while the y axis corresponds to $w \cdot 10^9$



From the graph we get 41.23GHz which is close to what we found in calculations.

(b) $a=22.86\text{mm}$

$$w_{co} = \frac{\pi c}{a\sqrt{\epsilon}} = 2.85e10 \rightarrow f = 4.53\text{GHz}$$

© $a=22.86\text{mm}$ $L=680\text{mm}$

$$\omega_n = c \sqrt{\left(\frac{\pi}{a}\right)^2 + \left(\frac{n\pi}{L}\right)^2}$$

$L = 680\text{ mm}$ $\text{Beta} = n \cdot \pi / L$ (Waveguide 1)

$N=1 \rightarrow w=4.13e10, \text{Beta}=4.61$

$N=2 \rightarrow w=4.13e10, \text{Beta}=9.24$

$N=25 \rightarrow 5.39e10, \text{Beta}=115.5$

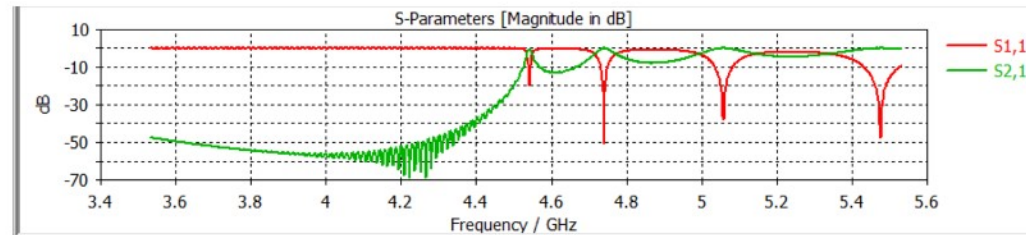
Again, we can see that the calculations match with the graph

(d)

Remind that:

* S_{21} =TRANSMISSION coefficient

* S_{11} =REFLECTION coefficient

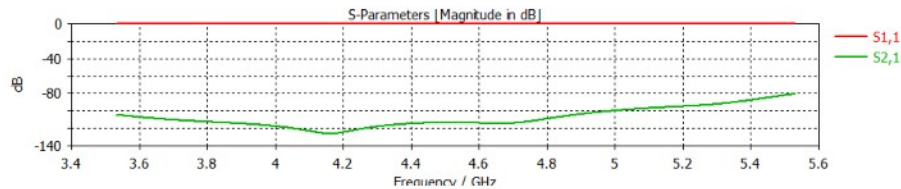


We observe the same general shape as when the rectangular was filled with vacuum but in the teflon case we can observe that as the dielectric constant affect directly w and f , the cutoff frequency changed to 4.5GHz, where the transmission coefficient gets to 1=0dB (reflection gets eliminated). And again, we have some resonance frequencies where S_{11} gets deeply negative dB values.

Now we change the stubs and probes to PEC and the rectangular waveguide interior is back to vacuum.

We can observe that now, as expected (from the fact that we are dealing with a transverse/perpendicular electric field) we'll get full reflection (constant 0dB=1) and no transmission (high negative dB).

Meaning, the input matches to the port while no radiation loss to the material (heating...).



Part 2: Home Experiment

The microwave is displaying $f=2.45\text{GHz}$

$$\lambda = \frac{c}{f_{co}} = 0.122$$

$$Vp = \frac{c}{\sqrt{\epsilon_r}}$$

I decided to put chocolate for the experiment.

The distance between the two adjacent melt spots is $d=6.15\text{cm}=0.0615\text{m}$

If we do $2 \cdot d \cdot f$ we should get c = speed of light

Let's check that:

$2 \cdot 0.0615 \cdot 2.45e9 = 3.0135e8$ which is pretty close to c !!

The small difference can be explained by experimental inaccuracies or by the fact that we might have let the chocolate melt for too long.

Why is that?

The microwave carries EM radiations (as wave) that proceed at the speed of the light. The only things that differ are the wavelength and frequency.

The distance between the two melted spots correspond to half a wavelength. This is because we prevent the plate from turning by turning it upside down. Otherwise, the melt points would distribute across the food and so the whole plate will warm up. But when not turning, the peaks are rather stable and the melt spots remain at the same place/static.

wave speed = frequency x wavelength $\rightarrow 2.45\text{G} \cdot 0.122 = c$

The effect of such melted spots on the food heating quality in microwave is that when the plate is not turning, the rest of the food will slowly heat up from the heat of these 2 melted spots only.

That is the reason why, in microwaves the food is placed on a rotating plate, so that the peaks of heat

are distributed over the plate, and the whole food heats up.