IMPERIAL

Ice growth in CPMOD

Luca Boscagli 23/05/2025

PAL configuration

Fagan, A. F., Guzman, F. J., Podboy, D. P., Rabinowitz, M. J., Brusk, K. D., Podboy, D. M., Caldwell, S. J. (2024). Contrails Measurement and Testing Capabilities in NASA's Particulate Aerosol Laboratory. In AIAA SCITECH 2024 Forum (p. 1242).

- > 6 fuels
 - Jet-A
 - n-heptane
 - Butanol
 - > 3 type of SAF
- > ICE characterization based on
 - \triangleright ICE no. density $[\#/m^3]$
 - ICE mean diameter [nm]
 - ICE mass density $[g/m^3]$
- Sensitivity studies
 - Soot number density and size
 - Fuel-to-air ratio ($\Phi = 0.24 0.36$)
 - Not investigated for SAF
 - Flight altitude

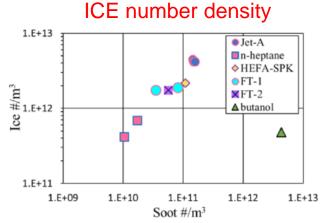


Fig. 16. Ice particle number density versus soot Fig. 17. Ice particle mean diameter versus soot particle number density for various fuels at 40,000 ft and -48°C ambient conditions and a nozzle temperature of 90°C.

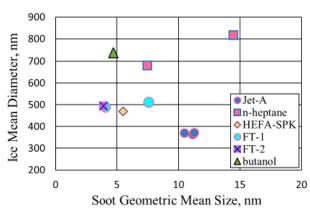
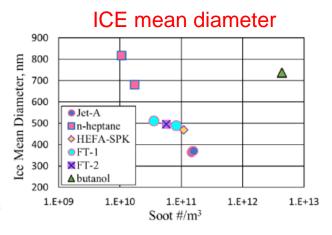


Fig. 18. Ice particle mean diameter versus geometric mean diameter of soot particles for various fuels at 40,000 ft and -48°C ambient conditions and a nozzle temperature of 90°C.



particle number density for various fuels at 40,000 ft and -48°C ambient conditions and a nozzle temperature of 90°C.

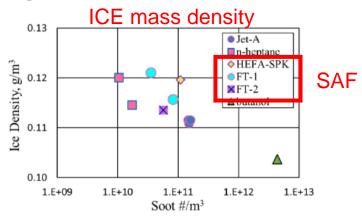


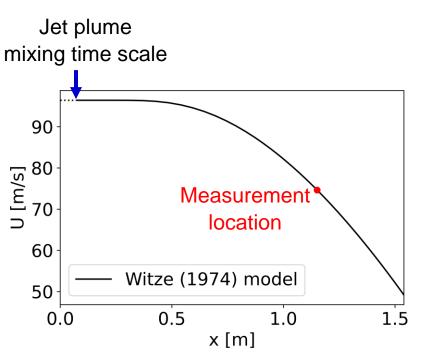
Fig. 19. Ice mass density versus soot particle number density for various fuels at 40,000 ft and -48°C ambient conditions and a nozzle temperature of 90°C.

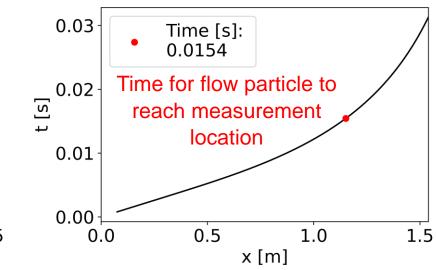
Jet centreline model

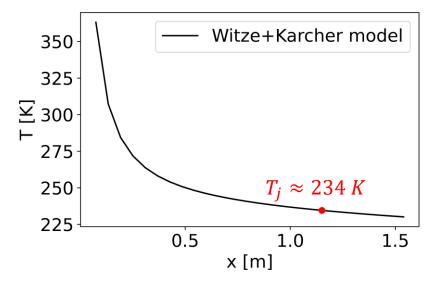
$$V_{j,0} = 96.4 \frac{m}{s}$$
 $T_{j,0} = 363.15 K$
 $T_a = 225.15 K$
 $p_a = p_j = 18753.93 Pa$

Convective time unit

$$t_c = \frac{L}{V_{j,0}} \approx 0.012s$$

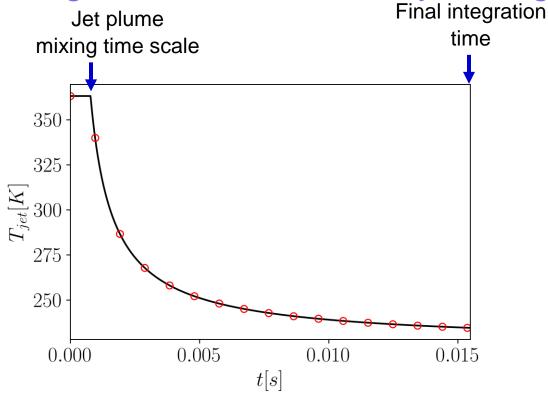




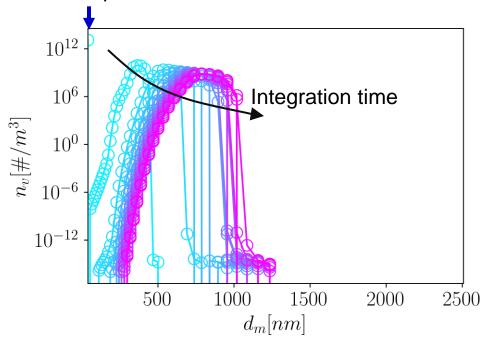


CPMOD studies

Ice growth in non-stationary homogeneous environment



t=0: monodispersive distribution



- Temperature follows jet cooling rate model
- Assumptions
 - ➤ Relative humidity, RH_{liq}=1.6 (constant no supersaturation consumption, nor dilution)
 - > Soot particle radius, $r_{p,0} = 20 nm$ (Lewellen, 2020)
 - > Soot particle (mass) density, $\rho_{p,0} = 1550 \frac{kg}{m^3}$ (Svenningsson et al, 2006, Petters & Kreidenweis, 2007)

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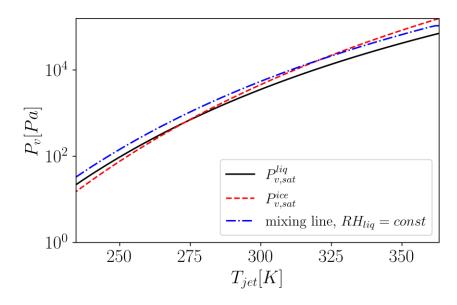
Ice depositional growth model

Saturation vapor pressures over ice and liquid

$$p_{\text{ice}} = \exp(9.550426 - 5723.265/T + 3.53068 \ln(T) - 0.00728332T); T > 110 \text{ K}.$$

$$\ln(p_{\text{liq}}) \approx 54.842763 - 6763.22/T - 4.210 \ln(T) + 0.000367T + \tanh\{0.0415(T - 218.8)\}(53.878 - 1331.22/T - 9.44523 \ln(T) + 0.014025T);$$
(10)

for 123 < T < 332 K.



Murphy, D. M., & Koop, T. (2005). Review of the vapour pressures of ice and supercooled water for atmospheric applications. Quarterly Journal of the Royal Meteorological Society: A journal of the atmospheric sciences, applied meteorology and physical oceanography, 131(608), 1539-1565.

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Ice depositional growth model

Linear growth rate – Karcher et al 1996

Where:

$$G(r_p) = \frac{1}{\left(\frac{1}{1+Kn} + \frac{4Kn}{3\alpha}\right)}$$
 - collision factor – accounts for transition from gas kinetic to continuum regime

$$Kn = \frac{\lambda_{water}}{r_p}$$
 - Knudsen number

 $\lambda_{water} = f(T, p)$ - water vapor mean free path

 $D_v = f(T, p)$ - diffusion coefficient of water vapor molecules in air

$$\rho_p = \frac{\rho_{p,0} r_{p,0}^3 + \rho_{ice} (r_p^3 - r_{p,0}^3)}{r_p^3}$$
 - with $\rho_{ice} = 917.0 \frac{kg}{m^3}$ (neglecting soot core, but can be refined based on Khou et al. 2015)

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Ice depositional growth model

Linear growth rate – Karcher et al 1996

In <u>BOFFIN+CPMOD</u>:

 $p_v = pX_{water}$ - with X_{water} : water mole fraction (field variable)

In CPMOD/PSR:

 $p_v = p_{v,sat}^{liq}RH$ – with RH: relative humidity (user input)

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