ORF 522 Linear Optimization

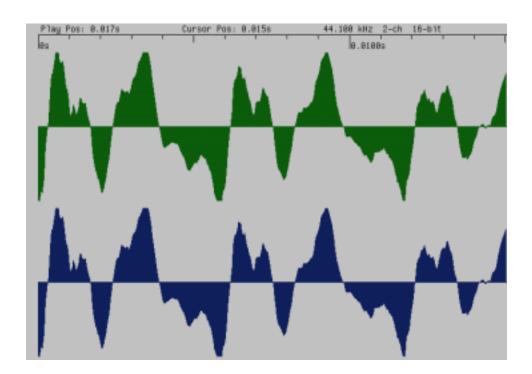
Lecture 19

Applications in Electrical Engineering

Digital Signal Processing¹

1

An Audio Signal



Digitization

44,100 samples/sec-channel

Each sample is a 2 byte (16 bit) integer (i.e., between -32768 and 32767).

Stereo needs 176 kBytes/sec = 634 MBytes/hour.

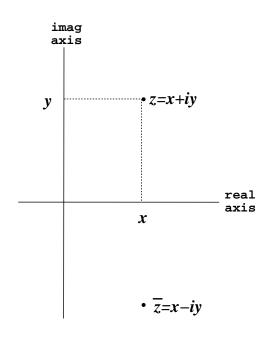
A Glimpse at the Data

0	-32768	20	23519	40	16975	60	12719
1	-32768	21	25247	41	16191	61	12223
2	-32768	22	27535	42	14799	62	11055
3	-30753	23	29471	43	12367	63	10479
4	-28865	24	31919	44	8607	64	10367
5	-29105	25	32767	45	5599	65	9951
6	-29201	26	32767	46	4927	66	10399
7	-26513	27	32767	47	5599	67	10255
8	-23681	28	32767	48	6799	68	8591
9	-18449	29	32031	49	9135	69	6671
10	-11025	30	29759	50	9839	70	5199
11	-6913	31	28399	51	8575	71	3823
12	-4337	32	28095	52	7615	72	2783
13	-1329	33	28399	53	5983	73	1567
14	1743	34	28751	54	5343	74	-785
15	6223	35	28751	55	6287	75	-4433
16	12111	36	26911	56	7183	76	-8737
17	17311	37	24063	57	8687	77	-12001
18	21311	38	21247	58	10927	78	-14369
19	23055	39	18415	59	12479	79	-16305

Complex Variables—A Brief Tutorial

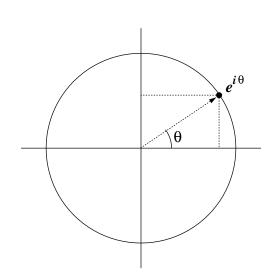
Complex Number: z = x + iy, where $i = \sqrt{-1}$

Complex Conjugate: $\bar{z} = x - iy$



Magnitude: $|z|^2 = z\overline{z} = x^2 + y^2$

The Unit Circle: $e^{i\theta} = \cos \theta + i \sin \theta$, $|e^{i\theta}|^2 = \cos^2 \theta + \sin^2 \theta = 1$



Input

Complex random sequence:

$$\dots, u_{-2}, u_{-1}, u_0, u_1, u_2, \dots$$

Assume:

$$\mathbf{E}u_k = 0$$

Autocorrelation:

$$s_k = \mathbf{E} u_j \bar{u}_{j+k}$$

Assumption: independent of j (random sequence is called stationarity).

Spectral Density = Fourier Transform:

$$S(\omega) = \int_{-\infty}^{\infty} s_t e^{i\omega t} dt$$
$$= \sum_{k} s_k e^{ik\omega}$$

Power:

$$\mathbf{E}|u_0|^2 = s_0 = \frac{1}{2\pi} \int_{-\pi}^{\pi} S(\omega) d\omega$$

Example

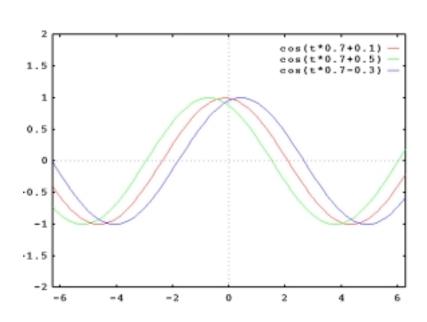
A sine/cosine wave with frequency ω_0 but undetermined phase:

$$u_k = e^{i(k\omega_0 + \theta)}$$

= $\cos(k\omega_0 + \theta) + i\sin(k\omega_0 + \theta)$

where

$$\theta = \text{Uniform}(-\pi, \pi)$$



$$\mathbf{E}u_k = \frac{1}{2\pi} \int_{-\pi}^{\pi} e^{i(k\omega_0 + \theta)} d\theta = \frac{1}{2\pi} e^{ik\omega_0} \int_{-\pi}^{\pi} e^{i\theta} d\theta = 0$$

$$s_k = \frac{1}{2\pi} \int_{-\pi}^{\pi} e^{i(j\omega_0 + \theta)} e^{-i((j+k)\omega_0 + \theta)} d\theta = e^{-ik\omega_0}$$

The spectral density is a delta function at ω_0 :

$$S(\omega) = \cdots = 2\pi \delta_{\omega_0}(\omega)$$

Power:

$$P = \frac{1}{2\pi} \int_{-\pi}^{\pi} S(\omega) d\omega = 1$$

Finite Impulse Response (FIR) Filter

Finite Impulse Response

$$h_{-n+1}, \ldots, h_{-1}, h_0, h_1, \ldots, h_{n-1}$$

Assumption: $h_{-k} = h_k$ (called linear phase filter)

Autocorrelation

$$g_k = \sum_j h_j h_{j+k}$$

Fourier Transform of $\{h_k\}$

$$H(\omega) = \sum_{k} h_k e^{ik\omega}$$
$$= h_0 + 2 \sum_{k=1}^{n-1} h_k \cos(k\omega)$$

Fourier Transform of $\{g_k\}$

$$G(\omega) = \sum_{k} g_{k} e^{ik\omega}$$

$$\vdots$$

$$= |H(\omega)|^{2}$$

Output

At time k, the output includes the input from time k-j multiplied by the impulse response h_j :

$$y_k = \sum_j h_j u_{k-j}.$$

The output is a convolution of the input and the filter.

Autocorrelation:

$$r_k = \mathbf{E} y_j \bar{y}_{j+k}$$

 \vdots
 $= \sum_j g_j s_{k-j}.$

Again, just a convolution.

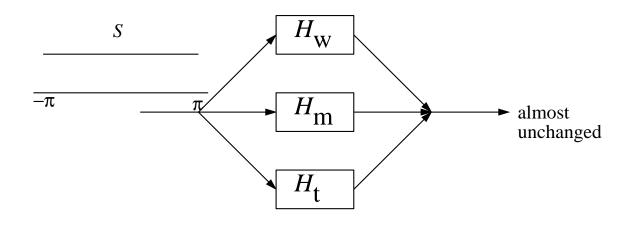
Spectral Density:

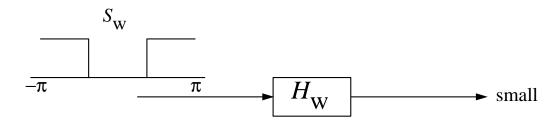
$$R(\omega) = \sum_{k} r_{k} e^{ik\omega}$$

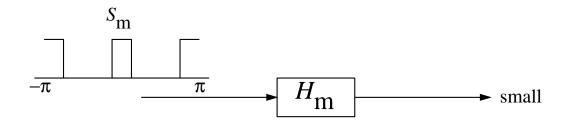
$$\vdots$$

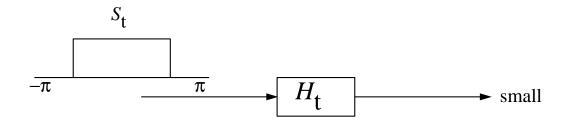
$$= G(\omega)S(\omega)$$

A Design Specification









A Convex Optimization Problem

minimize:

ρ

subject to:

$$\frac{1}{2\pi} \int_{-\pi}^{\pi} (H_{\mathbf{W}}(\omega) + H_{\mathbf{m}}(\omega) + H_{\mathbf{t}}(\omega) - 1)^{2} d\omega \leq \epsilon$$

$$\left(\frac{1}{2\pi} \int_{-\pi}^{\pi} H_{\mathbf{W}}^{2}(\omega) S_{\mathbf{W}}(\omega) d\omega\right)^{1/2} \leq \rho$$

$$\left(\frac{1}{2\pi} \int_{-\pi}^{\pi} H_{\mathbf{m}}^{2}(\omega) S_{\mathbf{m}}(\omega) d\omega\right)^{1/2} \leq \rho$$

$$\left(\frac{1}{2\pi} \int_{-\pi}^{\pi} H_{\mathbf{t}}^{2}(\omega) S_{\mathbf{t}}(\omega) d\omega\right)^{1/2} \leq \rho$$

where

$$H_{S}(\omega) = h_{0}^{S} + 2\sum_{k=1}^{n-1} h_{k}^{S} \cos(k\omega), \quad s = w, m, t$$

Note: The integrals can be approximated by sums. They can also be integrated explicitly.

The ampl Model

```
# length 27 (-13,...,13) linear phase FIR filter
param n := 14;
param N := 1000;
param pi := 4*atan(1);
param eps := 1.0e-4;
set OMEGA := setof {j in -N..N} pi*j/N;
param Sw {omega in OMEGA} := (if abs(omega) > 0.4*pi then 1 else 0)
param Sm {omega in OMEGA} := (if abs(omega) < 0.2*pi</pre>
      \parallel abs(omega) > 0.8*pi then 1 else 0);
param St {omega in OMEGA} := (if abs(omega) < 0.6*pi then 1 else 0)
var rho >= 0;
var hw \{0..n-1\};
var hm \{0..n-1\};
var ht \{0..n-1\};
var Hw {omega in OMEGA} =
    hw[0] + 2* sum {k in 1..n-1} (hw[k]*cos(k*omega));
var Hm {omega in OMEGA} =
    hm[0] + 2* sum {k in 1..n-1} (hm[k]*cos(k*omega));
var Ht {omega in OMEGA} =
    ht[0] + 2* sum {k in 1..n-1} (ht[k]*cos(k*omega));
minimize power_bnd: rho;
subject to passband:
    sqrt(sum {omega in OMEGA} (Hw[omega]+Hm[omega]+Ht[omega]-1)^2)
    <= sqrt(N)*sqrt(2*pi*eps);</pre>
subject to wooferband:
    sqrt(sum {omega in OMEGA} Hw[omega]^2 * Sw[omega])
    <= sqrt(N)*rho;
subject to midrangeband:
    sqrt(sum {omega in OMEGA} Hm[omega]^2 * Sm[omega])
```

```
<= sqrt(N)*rho;
subject to tweeterband:
    sqrt(sum {omega in OMEGA} Ht[omega]^2 * St[omega])
    <= sqrt(N)*rho;

let hw[0] := 2;
let hm[0] := 2;
let ht[0] := 2;
solve;

printf {omega in OMEGA}: "%7.4f %10.3e \n",
    omega, 20*log10(abs(Hw[omega])) > 3w.out;

printf {omega in OMEGA}: "%7.4f %10.3e \n",
    omega, 20*log10(abs(Hm[omega])) > 3m.out;

printf {omega in OMEGA}: "%7.4f %10.3e \n",
    omega, 20*log10(abs(Hm[omega])) > 3t.out;
```

The Iteration Log

OPTIMAL SOLUTION FOUND

LOQO 4.01: verbose=2 timing=1 variables: non-neg 1, free 42, bdd 0, total 43 constraints: eq ranged 0, ineq 4, Ο, total 4 87, 1764 nonzeros: Primal Dual Sig Iter | Obj Value Infeas Obj Value Fig Infeas Status 0.0000000e+00 5.47e + 00-4.5048766e+01 8.20e+01nonzeros: L 990, arith_ops 31041 2 8.1566802e-02 2.67e + 00-2.2246490e+01 3.11e+01 4.2789358e-02 9.91e-01 1.14e+01 -8.2537485e+001.3387496e-01 2.06e-01 -1.6740002e+00 2.32e+00 5 1.6865099e-02 1.16e-01 1.0434433e-01 1.86e-01 1 1.3181610e-03 1.40e-01 -8.0805850e-03 1.50e-02 2 3 7 7.5265116e-05 1.44e-01 4.5425492e-04 9.05e-04 5.9279466e-06 1.39e-01 -3.6288050e-05 6.97e-05 8 4 3.1343416e-06 7.84e-02 1.8886582e-05 3.31e-05 5 1 9 2.6317200e-07 6.24e-02 -1.6970215e-06 1.62e-0510 11 6.9794369e-08 6.42e-02 3.1953216e-07 5.72e-06 7 12 1.5662519e-08 1.32e+00 -4.2603108e-10 2.60e-06 8 3.9640273e-08 7.34e-07 13 1.0162506e-08 2.59e-01 DF 7.3901217e-09 2.07e-01 4.5719497e-08 4.30e-07 7 14 DF 6.8298003e-09 1.83e-01 8.6045607e-08 2.07e-07 15 7 DF 1.6399637e-03 4.01e-07 2.3814666e-07 1.78e-01 3 28 DF 29 9.4878775e-04 2.17e-01 3.3674241e-04 9.48e-03 3 3 30 1.4551883e-03 1.01e-01 9.6862590e-04 6.88e-03 31 1.7563445e-03 4.66e-02 1.3613840e-03 4.52e-03 3 1.25e-02 3 32 2.0179127e-03 1.6853065e-03 2.00e-03 4 33 2.1373955e-03 1.72e-03 1.9841897e-03 3.99e-04 34 2.1589812e-03 1.17e-04 2.1435636e-03 2.86e-05 5 35 2.1603608e-03 6.05e-06 2.1595563e-03 1.48e-06 6 2.1604314e-03 3.03e-07 2.1603910e-03 7.43e-08 36 PF DF 1.52e-08 2.1604329e-03 3.72e-09 37 2.1604349e-03 PF DF

The Output

