

Dipole Studies

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1 The Hamiltonian

Vector potential for quadruple is:

$$\mathbf{A} = \left(0, 0, -B_0x + \frac{B_0hx^2}{2(1+hx)} \right) \quad (1)$$

$$\mathbf{a} = \frac{q}{P_0} \mathbf{A} = \left(0, 0, -k_0x + \frac{k_0hx^2}{2(1+hx)} \right) \quad (2)$$

where q is the particle charge, P_0 is the reference momentum, and $k_0 = \frac{q}{P_0B_0}$ the normalised field strength.

The exact Hamiltonian for dipole in this case is:

$$\begin{aligned} H &= \frac{p_t}{\beta_0} - (1+hx) \sqrt{\left(p_t + \frac{1}{\beta_0}\right)^2 - p_x^2 - p_y^2 - \frac{1}{\beta_0^2 \gamma_0^2}} + (1+hx)k_0 \left(x - \frac{hx^2}{2(1+hx)}\right) \\ &= \frac{p_t}{\beta_0} - (1+hx) \sqrt{p_t^2 + 2\frac{p_t}{\beta_0} + 1 - p_x^2 - p_y^2} + (1+hx)k_0 \left(x - \frac{hx^2}{2(1+hx)}\right) \end{aligned}$$

The expanded to the second order in the transverse variables, while maintaining the exact dependence on p_t , Hamiltonian:

$$\tilde{H} = \frac{p_x^2}{2(1+\delta)} + \frac{p_y^2}{2(1+\delta)} + \frac{\mathbf{p}_t}{\beta_0} - (\mathbf{1} + \delta) - h(1+\delta)x + k_0x \left(1 + \frac{1}{2}hx\right) \quad (3)$$

where

$$(1+\delta) = \sqrt{p_t^2 + 2\frac{p_t}{\beta_0} + 1}, \quad (4)$$

and δ is the momentum deviation.

If we compare it to Ref[2], Eq.(4)

$$\tilde{H} = \frac{p_x^2}{2(1+\delta)} + \frac{p_y^2}{2(1+\delta)} + \frac{1-\beta_0^2}{2\beta_0^2}p_t^2 - h(1+\delta)x + k_0x \left(1 + \frac{1}{2}hx\right) \quad (5)$$

we can see that the term $\frac{1-\beta_0^2}{2\beta_0^2}p_t^2$ in (5) is nothing else but the expansion of the term $\frac{p_t}{\beta_0} - (1+\delta)$ in (3) to the second order.

2 The Equations of Motions

For both Hamiltonians, (3) and (5), the solutions of the equations of motions in the transverse plane are the same:

$$\begin{aligned} \frac{dx}{ds} &= \frac{\partial \tilde{H}}{\partial p_x} = \frac{p_x}{1+\delta} \\ \frac{dp_x}{ds} &= -\frac{\partial \tilde{H}}{\partial x} = -k_0(hx+1) + h(1+\delta) \\ \frac{dy}{ds} &= \frac{\partial \tilde{H}}{\partial p_y} = \frac{p_y}{1+\delta} \\ \frac{dp_y}{ds} &= 0 \end{aligned} \quad (6)$$

whereas the longitudinal ones for z are different due to second order expansion in p_t . For Hamiltonian (3) (the constant $\frac{1}{\beta_0}$ which has no significance for the dynamics was dropped) we have:

$$\begin{aligned}\frac{dz}{ds} &= \frac{\partial \tilde{H}}{\partial p_t} \\ &= -\frac{1}{(1+\delta)} \left(\mathbf{p}_t + \frac{1}{\beta_0} \right) - \frac{p_t + \frac{1}{\beta_0}}{1+\delta} hx - \frac{1}{2} \left(p_t + \frac{1}{\beta_0} \right) \frac{p_x^2 + p_y^2}{(1+\delta)^3} \\ &= -\frac{1}{(1+\delta)} \left(\mathbf{p}_t + \frac{1}{\beta_0} \right) - \frac{p_t + \frac{1}{\beta_0}}{1+\delta} \left(hx + \frac{1}{2} \frac{p_x^2 + p_y^2}{(1+\delta)^2} \right)\end{aligned}\quad (7)$$

while for Hamiltonian (5) we get:

$$\frac{dz}{ds} = \frac{\partial \tilde{H}}{\partial p_t} = \frac{1 - \beta_0^2}{\beta_0^2} \mathbf{p}_t - \frac{p_t + \frac{1}{\beta_0}}{1+\delta} \left(hx + \frac{1}{2} \frac{p_x^2 + p_y^2}{(1+\delta)^2} \right) \quad (8)$$

The equations of motion for p_t are obviously the same in both cases:

$$\frac{dp_t}{ds} = -\frac{\partial \tilde{H}}{\partial z} = 0 \quad (9)$$

3 The transfer map

The transfer map of the thick dipole is obtained by the integration of the equations of motion over the length L . We define

$$k = \sqrt{\frac{k_0}{1+\delta}} \quad (10)$$

$$C = \cos(\sqrt{hk}L),$$

$$S = \sin(\sqrt{hk}L);$$

The map for the transverse variable (in both cases) reads:

$$x(L) = C \cdot x_0 + \frac{S}{\sqrt{hk}(1+\delta)} \cdot p_{x_0} + \left(\frac{1}{k} - \frac{1}{h} \right) (1-C) \quad (11)$$

$$p_x(L) = -\sqrt{hk}(1+\delta) \cdot S \cdot x_0 + C \cdot p_{x_0} + (1+\delta) \cdot \left(\sqrt{\frac{h}{k}} - \sqrt{\frac{k}{h}} \right) \cdot S \quad (12)$$

$$y(L) = y_0 + \frac{p_{y_0}}{(1+\delta)} \cdot L \quad (13)$$

$$p_y(L) = p_{y_0} \quad (14)$$

For the longitudinal variables p_t stays the same in both cases, i.e.

$$p_t(L) = p_{t_0} \quad (15)$$

For z in case (7) the solution is:

$$\begin{aligned}
z(L) = & -\frac{1}{(1+\delta)} \left(\mathbf{p}_t + \frac{1}{\beta_0} \right) \cdot L - \\
& \frac{p_{t_0} + \frac{1}{\beta_0}}{1+\delta} \left(\frac{(h k x + k - h) \sqrt{h} \sqrt{k} S}{h k^2} - \frac{p_{x_0} (C - 1)}{(1+\delta) k} + \frac{(h - k) L}{k} \right) + \\
& -\frac{1}{2} \left(p_{t_0} + \frac{1}{\beta_0} \right) \frac{1}{(1+\delta)^3} \cdot \{ x_0^2 \cdot h \cdot k_0 \cdot (1+\delta) \cdot \left(\frac{L}{2} - \frac{1}{\sqrt{h} \sqrt{k}} \frac{C \cdot S}{2} \right) + \\
& p_{x_0}^2 \left(\frac{L}{2} + \frac{1}{\sqrt{h} \sqrt{k}} \frac{C \cdot S}{2} \right) + \\
& x_0 \cdot (1+\delta) \left(-(1+\delta) \sqrt{k} \frac{C \cdot S}{\sqrt{h}} + (1+\delta) \sqrt{h} \frac{C \cdot S}{\sqrt{k}} + (k_0 - (1+\delta) h) \cdot L \right) + \\
& p_{x_0} \cdot \left(-\frac{(1+\delta)}{k} \cdot C^2 + \frac{(1+\delta)}{h} \cdot C^2 + \frac{(1+\delta)}{k} - \frac{(1+\delta)}{h} \right) + \\
& x_0 \cdot p_{x_0} \cdot (1+\delta) (C^2 - 1) + p_{y_0}^2 L + \\
& -\sqrt[3]{\frac{1+\delta}{h}} \sqrt{k_0} \cdot \frac{C \cdot S}{2} + (1+\delta)^2 \frac{C \cdot S}{\sqrt{h} \sqrt{k}} - (1+\delta)^2 \frac{\sqrt{h} C \cdot S}{\sqrt[3]{k}} \frac{1}{2} + \\
& + (1+\delta)^2 \cdot \frac{k}{2h} L + (1+\delta)^2 \frac{h}{2k} L - (1+\delta)^2 L \Big\}. \tag{16}
\end{aligned}$$

and in case (8):

$$\begin{aligned}
z = & \frac{1 - \beta_0^2}{\beta_0^2} L \cdot \mathbf{p}_{t_0} - \frac{p_{t_0} + \frac{1}{\beta_0}}{1 + \delta} \left(\frac{(h k x + k - h) \sqrt{h} \sqrt{k} S}{h k^2} - \frac{p_{x_0} (C - 1)}{(1 + \delta) k} + \frac{(h - k) L}{k} \right) + \\
& - \frac{1}{2} \left(p_{t_0} + \frac{1}{\beta_0} \right) \frac{1}{(1 + \delta)^3} \cdot \{ x_0^2 \cdot h \cdot k_0 \cdot (1 + \delta) \cdot \left(\frac{L}{2} - \frac{1}{\sqrt{h} \sqrt{k}} \frac{C \cdot S}{2} \right) + \\
& p_{x_0}^2 \left(\frac{L}{2} + \frac{1}{\sqrt{h} \sqrt{k}} \frac{C \cdot S}{2} \right) + \\
& x_0 \cdot (1 + \delta) \left(- (1 + \delta) \sqrt{k} \frac{C \cdot S}{\sqrt{h}} + (1 + \delta) \sqrt{h} \frac{C \cdot S}{\sqrt{k}} + (k_0 - (1 + \delta) h) \cdot L \right) + \\
& p_{x_0} \cdot \left(- \frac{(1 + \delta)}{k} \cdot C^2 + \frac{(1 + \delta)}{h} \cdot C^2 + \frac{(1 + \delta)}{k} - \frac{(1 + \delta)}{h} \right) + \\
& x_0 \cdot p_{x_0} \cdot (1 + \delta) (C^2 - 1) + p_{y_0}^2 L + \\
& - \sqrt[3]{\frac{1 + \delta}{h}} \sqrt{k_0} \cdot \frac{C \cdot S}{2} + (1 + \delta)^2 \frac{C \cdot S}{\sqrt{h} \sqrt{k}} - (1 + \delta)^2 \frac{\sqrt{h} C \cdot S}{\sqrt[3]{k}} \frac{1}{2} + \\
& + (1 + \delta)^2 \cdot \frac{k}{2h} L + (1 + \delta)^2 \frac{h}{2k} L - (1 + \delta)^2 L \}. \tag{17}
\end{aligned}$$

As one can see, the difference is the coefficient in front of the linear term which is coming from the choice of the "quasi"-exact solutions for p_t or the second-order approximation. It makes sense to replace second-order expansion in p_t by the exact solution for the new MAD (?). In this particular case we can easily have the "exact" solution without adding any complication to the calculation.

Reference:

1. A.Wolski, *Beam Dynamics in HEP Accelerators*, chapter 3, p.101-105
2. A. Latina, *Implementation of a Thick Dipole in the MAD-X tracking module*