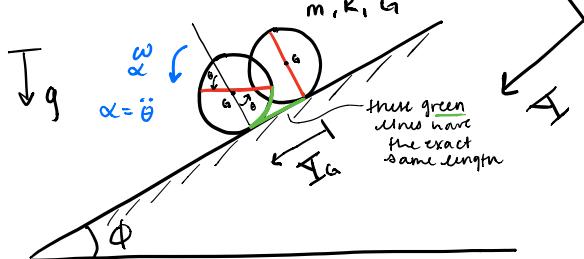


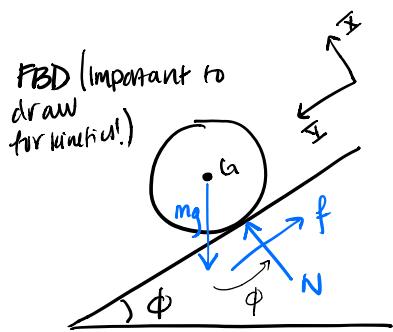
## Dynamics Lecture #16



{ Test #2: 4/1/2020 during class } → Ch. 14, 15, 16

Ex. Rolling wheel, no-slip

Calculate  $a_{G_I}$  and angular acceleration  $\alpha$  of wheel.



Rolling Constraint:  $T_G = R\theta$

$$\text{Take } \frac{d^2}{dt^2} : a_{G_I} = R\alpha \quad (4)$$

Two Momentum Principles:

I.  $\sum F = ma_{G_I}$  (linear momentum)

$$\begin{cases} N - mg\cos\phi = ma_{G_I} = 0 & \text{bc G can only move in I direction} \\ -f + mg\sin\phi = m a_{G_I} \neq 0 & \text{(2)} \end{cases}$$

don't need to write vectors since  
we choose cw or ccw  
→ choose  $M_G$  (⊕)  
bc consistent with the  $\alpha$

II.  $\sum M_G = I_G \alpha$  (angular momentum)  
- just the friction has a moment about point G

$$fR = I_G \alpha \quad (3)$$

(1), (2), (3), (4) : unknowns  $a_{G_I}$ ,  $\alpha$ ,  $f$ ,  $N$

From (2) and (4)  $f = mg\sin\phi - mR\alpha \quad (5)$

From (3),  $f = \frac{I_G}{R} \alpha \quad (6)$

use (5) + (6) to get  $\alpha$ :  $mg\sin\phi - mR\alpha = \frac{I_G}{R} \alpha$

$$\alpha \left( \frac{I_G}{R} + mR \right) = mg\sin\phi$$

$$\alpha = \frac{mg\sin\phi}{\frac{I_G}{R} + mR}$$

from (4)  $a_{G_I} = R\alpha$

$$a_{G_I} = \frac{mgR\sin\phi}{\frac{I_G}{R} + mR}$$

If the wheel is solid disc then  $I_G = \frac{1}{2}mR^2$  [moment of inertia of solid disc about its center]

$$\frac{I_a}{R} + MR = \frac{1}{2}MR + MR$$

$$= \frac{3}{2}MR$$

so if have solid wheel, then

$$\alpha = \frac{mg \sin \phi}{\frac{3}{2}MR} \Rightarrow \alpha = \frac{\frac{2}{3}}{R} \frac{g}{R} \sin \phi$$

$$a_{Gx} = R\alpha = \frac{\frac{2}{3}}{R} g \sin \phi$$

find  $f, N$ :

$$\text{from (1), } N = mg \cos \phi$$

$$\text{from (3), } f = \frac{I_a}{R}\alpha = \frac{I_a}{R} \frac{mg \sin \phi}{I_a/R + MR}$$

for a solid wheel:

$$f = \frac{1}{2}MR \frac{\frac{2}{3}}{R} g \sin \phi \rightarrow f = \frac{1}{3}mg \sin \phi$$

$\downarrow mg$  makes up the force!

no slip condition:  $f < \mu_s N$

for solid wheel, no slip if

$$\frac{1}{3}mg \sin \phi < \mu_s mg \cos \phi$$

or

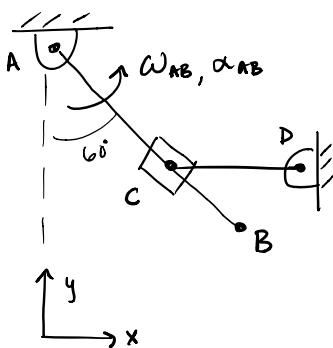
$$\mu_s > \frac{1}{3} \tan \phi \dots \text{this must be true if the wheel is not going to tip!}$$

$\sqrt{\mu_s = 0}$   
if there's no friction, the wheel will not roll, it will slide!

$\therefore$  Rolling without slip requires friction. [why tires made of sticky rubber]  
 [train wheels are steel, why rail vehicles  
cannot go uphill!]

## HW problem 1b-14D Review

\* STUDY THIS \*



$$\underline{\text{Link DC}} \quad \underline{\underline{v_c}} = \underline{\underline{v_D}} + \underline{\omega_{CD}} \times \underline{r_{DC}} \quad (1)$$

↑ unknown

Link AB

$$\underline{\underline{v_c}} = \underline{\underline{v_A}} + \underline{\omega_{AB}} \times \underline{r_{AC}} + (\underline{\underline{v_c}})_{rel} \quad (2)$$

From (1) and (2):

$$\begin{aligned} \underline{\omega_{CD}} \times \underline{r_{DC}} &= \underline{\omega_{AB}} \times \underline{r_{AC}} + (\underline{\underline{v_c}})_{rel} \quad (3) \\ \text{unknowns } \underline{\omega_{CD}}, (\underline{\underline{v_c}})_{rel} & \hookrightarrow \text{along AB direction} \end{aligned}$$

Link DC

$$\underline{\underline{a_c}} = \underline{\underline{a_D}} + \underline{\alpha_{CD}} \times \underline{r_{DC}} + \underline{\omega_{CD}} \times (\underline{\omega_{CD}} \times \underline{r_{DC}}) \quad (4)$$

↑ unknown

Link AB

$$\underline{\underline{a_c}} = \underline{\underline{a_A}} + \underline{\alpha_{AB}} \times \underline{r_{AC}} + \underline{\omega_{AB}} \times (\underline{\omega_{AB}} \times \underline{r_{AC}}) + 2\underline{\omega_{AB}} \times (\underline{\underline{v_c}})_{rel} + (\underline{\underline{a_c}})_{rel} \quad (5)$$

Equate (4), (5): unknowns  $\alpha_{CD}$ ,  $(\underline{\underline{a_c}})_{rel}$

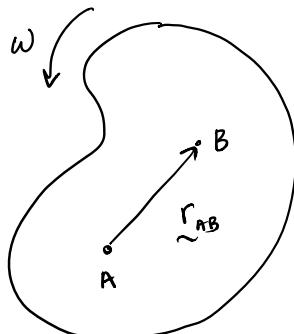
↪ along AB direction

$$(\underline{\underline{v_c}})_{rel} = (\underline{\underline{v_c}})_{rel} \underline{u}_{AB}$$

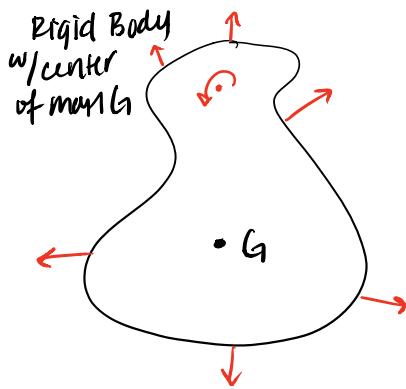
↑ magnitude of  $\underline{\underline{v_c}}$       ↑ unit vector along AB

$$(\underline{\underline{a_c}})_{rel} = (\underline{\underline{a_c}})_{rel} \underline{u}_{AB}$$

↑ unit vector in AB direction  
(direction of relative acceleration)

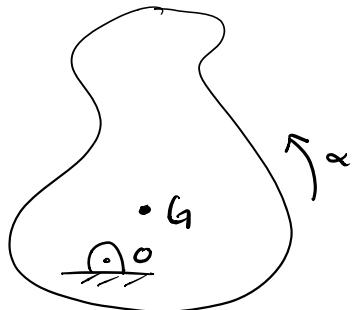


$$\underline{\underline{v_B}} = \underline{\underline{v_A}} + \omega \times$$



$$\left. \begin{array}{l} \text{I. } \sum \underline{\underline{F}} = m \underline{\underline{a}_G} \\ \text{II. } \sum M_G = I_G \alpha \end{array} \right\} \text{always valid equations}$$

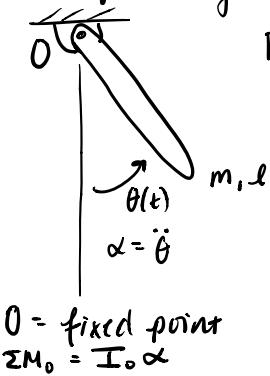
If the body has a fixed pt O,



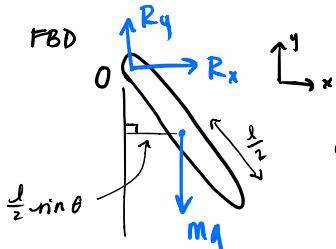
Can use  $\sum M_O = I_O \alpha$  instead of (II)  
but only if O = fixed point

IIa.  $\sum M_O = I_O \alpha \} \text{ valid only if } O \text{ is fixed pt.}$

### Ex. Rigid Body Pendulum



Derive the equation of motion for angle  $\theta(t)$ .



only moment about O is the gravity force

$$O = \text{fixed point}$$

$$\sum M_O = I_O \alpha$$

$$\Sigma M_O = I_O \alpha$$

$$-mg \frac{l}{2} \sin \theta = I_O \ddot{\theta}$$

or

$$I_O \ddot{\theta} + mg \frac{l}{2} \sin \theta = 0$$

differential equation  
for  $\theta$  over time

For a thin rod,  $I_O = \frac{1}{3}ml^2$

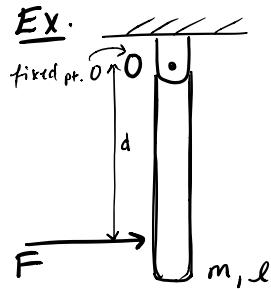
$$\text{so } \frac{1}{3}ml^2 \ddot{\theta} + mg \frac{l}{2} \sin \theta = 0$$

$$\text{or } \ddot{\theta} + \frac{3}{2} \frac{g}{l} \sin \theta = 0$$

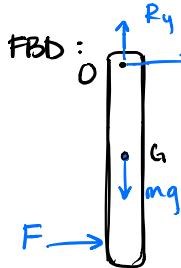
$$\text{or } \ddot{\theta} + \frac{g}{\frac{2}{3}l} \sin \theta = 0$$

*(3/2) bc  
its distributed  
mass is spread out  
over entire L/2  
length*

for pt. mass pendulum,  
 $\ddot{\theta} + \frac{g}{l} \sin \theta = 0$

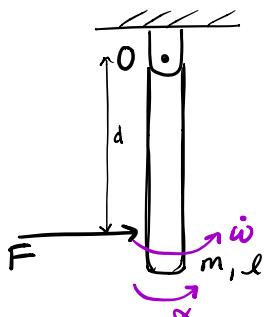


Pendulum initially at rest, then struck by force  $F$ .  
Find the initial reaction forces at pivot pt. O.



since need to find reaction forces, no help to find sum of moments about pt. O. So, we'll use:

$$\text{I. } \sum F_x = ma_x \\ \text{II. } \sum M_a = I_a \alpha$$



draw in angular acceleration

Initially,  
 $\omega = 0$  [no angular velocity at rest]  
 $\alpha \neq 0$  [moment strike bar, going to cause angular acceleration]

I. 
$$\begin{cases} \text{linear motion} \\ \text{angular motion} \end{cases} \left\{ \begin{array}{l} F + R_x = ma_{ax} = m \frac{l}{2} \ddot{\theta} = m \frac{l}{2} \alpha \stackrel{(1)}{=} \left[ \text{circular motion formula in tangential direction} \right] (\text{x direction acceleration}) \\ R_y - mg = ma_{ay} = m \frac{l}{2} \omega^2 = 0 \stackrel{(2)}{=} \left[ \text{centripetal acceleration, equal to } \phi \text{ since } \omega_i = 0 \right] \end{array} \right. \text{ know } \frac{v^2}{r} \text{ vs } \omega^2 \text{ side note} \right.$$

$$\text{II. } -R_x \frac{l}{2} + F(d - \frac{l}{2}) = I_a \alpha \stackrel{(3)}{=}$$

from (2)

$$R_y = mg$$

lots of algebra!!

to get  $R_x$ , use (1) and (3)

$$\frac{2}{m \cdot l} (F + R_x) = \frac{1}{I_a} (-R_x \frac{l}{2} + F(d - \frac{l}{2}))$$

$$F \left( \frac{2}{m \cdot l} - \frac{1}{I_a} \left( d - \frac{l}{2} \right) \right) = R_x \left( -\frac{l}{2} \frac{1}{I_a} - \frac{2}{m \cdot l} \right) \quad [\dots \text{ multiply by } \frac{m \cdot l}{2}]$$

$$R_x \left( -\frac{m \cdot l^2 / 4}{I_a} - 1 \right) = F \left( 1 - \frac{m \cdot l / 2}{I_a} \left( d - \frac{l}{2} \right) \right)$$

$$I_a \text{ for thin rod} = \underbrace{\frac{1}{12} m \cdot l^2}_{\text{center of percussion}}$$

$$R_x (-3 - 1) = F \left( 1 - \frac{6}{l} \left( d - \frac{l}{2} \right) \right)$$

$$R_x = \frac{1}{4} F \left( \frac{6d}{l} - 3 - 1 \right) \Rightarrow R_x = \frac{1}{4} F \left( \frac{6d}{l} - 4 \right)$$

\* Special case:  $R_x = 0$  when  $\frac{d}{l} = \frac{2}{3}$  \* applications in sporting equipment, if this bar is tennis racket and ball strikes in right place ... feel nothing!!! the sweet spot

center of percussion is place where strike bar and set no rxn force in x-direction!!

$\frac{d}{l} = \frac{2}{3}$  defines the center of percussion of the bar!!!