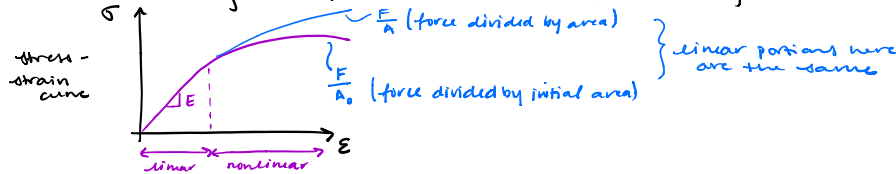


Nonlinear FEM/Nonlinear Continuum Mechanics

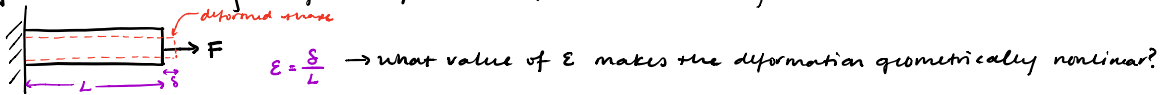
→ goal: ① understand when linear approximations breakdown
② see similarities to linear FEM

→ reasons to use nonlinear FEM vs. linear FEM

① material nonlinearity: ie beyond Hooke's Law, or for rubbery materials



② geometric nonlinearity: larger changes in shape (think stretching rubber band)



→ x ← single reference coordinate system

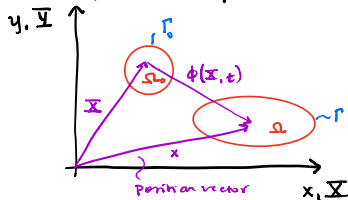
underlying assumption?

- ① geometry doesn't change much
- ② history of deformation doesn't matter

Define Motion & Kinematics

→ models of solids & fluids where properties can be characterized by smooth functions of spatial variables → means we ignore inhomogeneities like microstructure, grains, etc...

→ models of macroscopic behavior of matter



• volume ... Ω_0 = reference volume, Ω = current volume

• boundary ... Γ_0 = reference area, Γ = current area

$\phi(\mathbf{X}, t)$ = "motion"

\mathbf{X} = material, or Lagrangian coordinates = $\sum_{i=1}^{NSD} \mathbf{X}_i \mathbf{e}_i$ (NSD = # spatial dimensions, \mathbf{e}_i = unit vector)
 \mathbf{x} = Eulerian coordinates = $\sum_{i=1}^{NSD} x_i \mathbf{e}_i$
 or current configuration

Can describe deformation in 2 ways:

$(\mathbf{X}, t) \rightarrow$ material/Lagrangian $\rightarrow \mathbf{X}_i$ are fixed in time

$(\mathbf{x}, t) \rightarrow$ spatial/Eulerian $\rightarrow x_i$ coordinates do change with time

2 classes of problems:

→ solids: Lagrangian

- ① stresses generally depend on deformation history
- ② knowing reference/undeformed configuration is useful

→ fluids: Eulerian

- ① stresses are history independent (in general, for most fluids)
- ② coordinates can move/convert with fluid flow

Lagrangian & Eulerian FEM is equivalent (can convert between the two)

Motion: $x = \phi(\mathbf{X}, t)$

→ basically maps reference configuration to current configuration at time t
 $\mathbf{X} = \mathbf{x}(\mathbf{X}, 0) = \phi(\mathbf{X}, 0)$

→ using this motion, can measure displacement: difference between current and reference configurations

$$u(\mathbf{X}, t) = \phi(\mathbf{X}, t) - \phi(\mathbf{X}, 0) = \phi(\mathbf{X}, t) - \mathbf{X} \\ = \mathbf{x} - \mathbf{X}$$

$$u_i = x_i - X_i$$

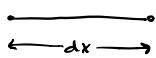
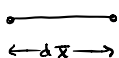
→ velocity will just be time derivative of displacement

$$\frac{\partial u(\mathbf{X}, t)}{\partial t} = \mathbf{v}$$

→ acceleration: $\frac{\partial^2 u(\mathbf{X}, t)}{\partial t^2} = \mathbf{a}$

Deformation Gradient (\mathbf{F}): use to characterize deformation and strain

initial configuration current configuration



$$\Rightarrow \boxed{\mathbf{F} = \frac{d\mathbf{x}}{d\mathbf{X}}} \quad \text{or: } d\mathbf{x} = \mathbf{F} d\mathbf{X}$$

→ does \mathbf{F} look like something we've used before? like Jacobian $J = \frac{dx}{d\xi}$

$$\hookrightarrow J = \det(\mathbf{F}) \leadsto \mathbf{F} \text{ in 2D: } \mathbf{F} = \begin{bmatrix} \frac{\partial x}{\partial X} & \frac{\partial x}{\partial Y} \\ \frac{\partial y}{\partial X} & \frac{\partial y}{\partial Y} \end{bmatrix}$$

- strain units: so why not use this deformation gradient \mathbf{F} as a strain measure?
- what would strain be if nothing changed shape?
 - strain should be zero if no deformation
 - if no deformation, $d\mathbf{X} = d\mathbf{x}$, then $\mathbf{F} = 1$ which is nonsensical for a strain, so need to define a different strain measure!