

Dimensional Analysis

[L] length
 [M] mass
 [T] time

[J] luminosity (candela)
 [θ] temperature
 [I] current

[N] mole

we'll mostly deal w/ these

Height of a projectile - example

$$x_m = \text{maximum ht projectile goes in air}$$

$$x_m = f(g, m, v_0)$$

our goal is to develop a testable hypothesis

$$x_m = f(g, m, v_0) \rightarrow [x_m] = [m^a v_0^b g^c]$$

$$\underline{T^0} \underline{M^0 L} = m^a \left(\frac{L}{T}\right)^b \left(\frac{L}{T^2}\right)^c = m^a L^{b+c} T^{-b-2c}$$

$$\begin{array}{l} L: b+c=1 \\ T: -b-2c=0 \\ M: a=0 \end{array} \quad \left. \begin{array}{l} c=-1 \\ b=2 \\ a=0 \end{array} \right\} \rightarrow x_m \sim \frac{v_0^2}{g}$$

single tilde means we're leaving some constant intentionally out

we came up with a prediction
 w/out using calculus, etc.
 ... now can find unknown constant

$$x_m \sim \frac{v_0^2}{g} \rightarrow x_m = \alpha \frac{v_0^2}{g}$$

$$\ddot{x}(t) = -\frac{g R^2}{(R+x)^2}$$

$x(0) = 0 \quad \dot{x}(0) = v_0$
 initial conditions

R = radius of Earth

this is the annoying term ...

$R+x \approx R$ (assuming x is really small compared to R)

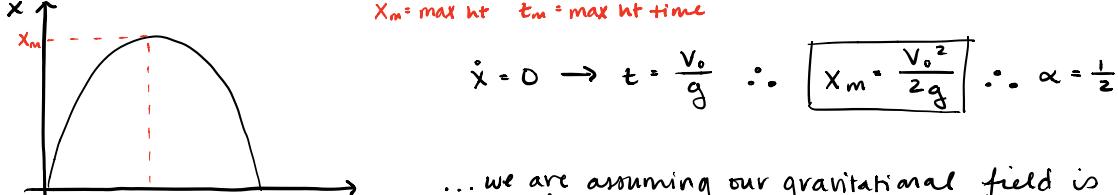
i.e. $\frac{x}{R} \ll 1$

$\ddot{x}(t) = -g$... then apply two initial conditions and integrate

$$\rightarrow x(t) = -\frac{1}{2} gt^2 + v_0 t$$

... now let's connect this with our dimensional analysis

$x_m = \text{max ht} \quad t_m = \text{max ht time}$



... we are assuming our gravitational field is constant for all x_i , which really isn't true

$$\dot{x} = 0 \rightarrow t = \frac{v_0}{g} \therefore \boxed{x_m = \frac{v_0^2}{2g}} \therefore \alpha = \frac{1}{2}$$

Drag on a sphere - example

... we usually want the drag to be as low as possible

Drag will depend on:

- the radius (R) - density (ρ)
- the velocity (V) - viscosity (μ)

$$D_f = f(R, V, \rho, \mu) \rightarrow [D_f] = [R^a V^b \rho^c \mu^d]$$

$$\begin{aligned} MLT^{-2} &= L^a \left(\frac{L}{T}\right)^b \left(\frac{M}{L^3}\right)^c \left(\frac{M}{LT}\right)^d \\ M LT^{-2} &= L^{a+b-3c-d} T^{-b-d} M^{c+d} \end{aligned}$$

$$\left. \begin{array}{l} L: a+b-3c-d=1 \\ T: -b-d=-2 \\ M: c+d=1 \end{array} \right\} \begin{array}{l} \text{take } d \text{ to be} \\ \text{unknown ...} \end{array} \quad \begin{array}{l} b=2-d \\ c=1-d \\ a=2-d \end{array} \quad D_f \sim R^{2-d} V^{2-d} \rho^{1-d} \mu^d$$

$$D_f \sim R^{2-d} V^{2-d} \rho^{1-d} \mu^d \sim R^2 V^2 \rho \left(\frac{\mu}{RV\rho}\right)^d$$

π^d dimensionless product/group

reciprocal of Re # $Re = \frac{RV\rho}{\mu}$

$D_f = \alpha R^2 V^2 \rho \pi^d$ ← these are both dimensionless

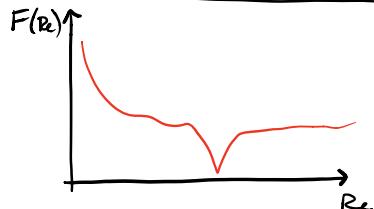
$$D_f = \alpha_1 R^2 V^2 \rho \pi^{d_1} + \alpha_2 R^2 V^2 \rho \pi^{d_2} \dots \text{this is just as valid as above}$$

$$D_f = \rho R^2 V^2 (\underbrace{\alpha_1 \pi^{d_1} + \alpha_2 \pi^{d_2} + \dots}_{F(\pi)})$$

$F(\pi)$ ← we measure this experimentally

... more complete version

$$D_f = \rho R^2 V^2 F(\pi)$$



We can use this approach to develop scale models

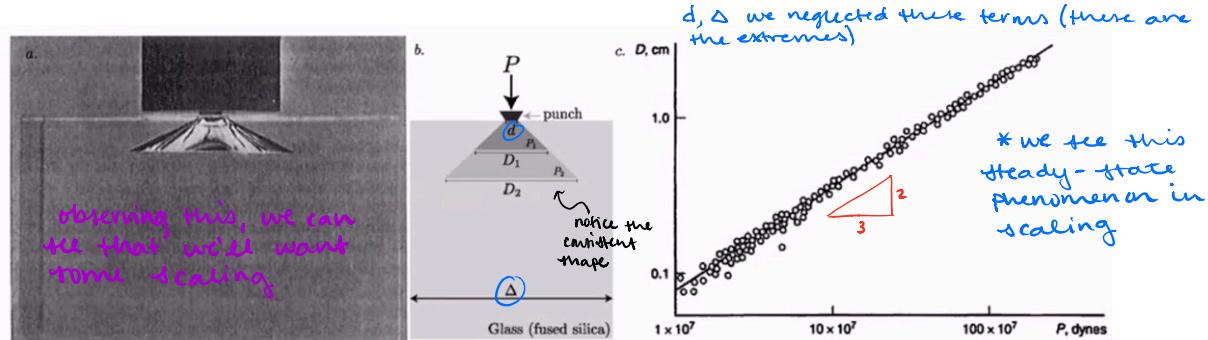
- we can run an experiment at a small scale to tell us how it will be in a large scale

model:

as long as keep dimensionless part the same, can vary other items

$$\frac{M_m}{R_m V_m \rho_m} = \frac{\mu}{R V \rho} \rightarrow V_m = \frac{\mu_m R_e}{\mu R_m \rho_m} V \quad \dots \text{this is implying } \underline{\text{physical similarity}}$$

example problem in brittle fracture



→ brittle fracture falls under elasticity theory

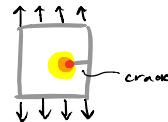
- something that breaks that can be put back together (so no plasticity)
- problem in fracture problems is that there's more boundaries than we were thinking about

→ strain Energy Release Rate

↳ which is related to the "stress intensity factor" (K)

$$\text{stress intensity factor} : K \sim \sigma \sqrt{s}$$

↑
ave. stress ↗ distance from crack



how does this crack grow as increase stress?

$$D = f(P, K, \nu)$$

↑ true ↑ poisson's ratio (dimensionless)

$$[P] = F = MLT^{-2}$$

$$[K] = \frac{F}{A\sqrt{L}} = MLT^{-2}L^{-1/2}L^{1/2} = \frac{MLT^{-2}}{L^{1/2}}$$

$$D \sim \left(\frac{P}{K}\right)^{2/3} \phi(\nu)$$

↳ unknown function of poisson's ratio

↑ this length sets the limit of when something too small, too large

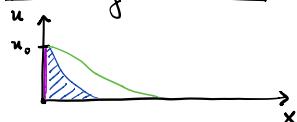
... scaling only valid in this intermediate s-s regime
"intermediate asymptotics"

example of boundary layer in mechanics:

cut tennis ball in 1/2, flip dome inside-out, boundary deviates from dome at the brim

... vs in fluid mechanics where boundary layer is typically at surface from some flow

Similarity Variables



u = concentration

$t = 0$

$t = t_1$

$t = t_2$

$$\text{Diffusion Equation: } D \frac{\partial^2 u}{\partial x^2} - \frac{\partial u}{\partial t}$$

$$u|_{x=0} = u_0$$

$$u|_{x=\infty} = 0$$

boundary conditions (b.c.)

$$u|_{t=0} = 0$$

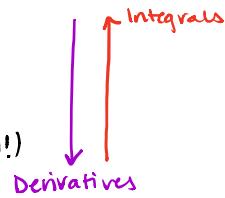
initial condition (i.c.)

Dimensional Analysis: Derivatives / Integrals

area function of x : $A(x) = x^2 \rightarrow [A] = L^2$

$$\frac{dA}{dx} = 2x \rightarrow \left[\frac{dA}{dx} \right] = \frac{1}{L} [A] = L$$

$$\frac{d^2A}{dx^2} = 2 \rightarrow \left[\frac{d^2A}{dx^2} \right] = \frac{1}{L^2} [A] = 1 \quad (\text{dimensionless!})$$



... back to diffusion equation example

$$D \frac{\partial^2 u}{\partial x^2} = \frac{\partial u}{\partial t} \quad \underbrace{u|_{x=0} = u_0}_{B.C.} \quad \underbrace{u|_{x=\infty} = 0}_{I.C.}$$

$$[Du_{xx}] = [u_t]$$

$$[u] = ML^{-3} \therefore [D] = L^2 T^{-1}$$

chemical concentration has dimensions of mass per volume

two independent variables, $x \neq t$

D is diffusion parameter

we want to find $u = f(x, t, D, u_0)$

$$\begin{aligned} [u] &= [x^a t^b D^c u_0^d] \rightarrow ML^{-3} = L^a T^b (L^2 T^{-1})^c (ML^{-3})^d \\ M L^{-3} &= L^{a+2c-3d} T^{b-c} M^d \end{aligned} \quad \left. \begin{array}{l} L: a+2c-3d=-3 \\ T: b-c=0 \\ M: d=1 \end{array} \right\} \begin{array}{l} \therefore \frac{d=1}{b=c=-\frac{a}{2}} \\ \therefore \frac{d=1}{b=c=-\frac{a}{2}} \end{array}$$

now collect all of these terms:

$$u \sim u_0 \left(\frac{x}{\sqrt{Dt}} \right)^a$$

$\eta = \frac{x}{\sqrt{Dt}}$ similarity ... this occur when have dimensionless group that includes variables the independent variables
... important to check that spatial parameter is in numerator

physically, what does this mean?

- we're going to have self-similar behavior (on curve)
- allows us to write in terms of η (t^n), reducing from PDE to ODE
- we've significantly reduced the complexity of our problem

$$u \sim u_0 F(\eta) \quad [u] = ML^{-3} \therefore D = L^2 T^{-1}$$

chain Rule:

$$\frac{\partial}{\partial t} [F(\eta)] = \frac{\partial F(\eta)}{\partial \eta} \frac{\partial \eta}{\partial t} \Rightarrow D \frac{\partial^2 u}{\partial x^2} = \frac{\partial u}{\partial t}$$

*point of this: reduce complicated PDE to simple ODE using a similarity transform

$$\begin{aligned} \frac{\partial}{\partial t} [u_0 F(\eta)] &= -u_0 F'(\eta) \frac{\eta}{2t} \quad \left. \begin{array}{l} \rightarrow u_0 F'(\eta) \frac{\partial \eta}{\partial t} \\ \rightarrow \frac{\partial \eta}{\partial t} = \frac{-x}{2D^{1/2} t^{3/2}} \end{array} \right\} \\ \frac{\partial^2 u}{\partial x^2} &= u_0 F''(\eta) \frac{1}{\partial t} \end{aligned}$$

... now stitch this all out together...

$$D \left[u_0 F''(\eta) \frac{1}{\partial t} \right] = -u_0 F'(\eta) \frac{\eta}{2t} \rightarrow \boxed{F''(\eta) = -\frac{1}{2} \eta F'(\eta)}$$

$$\boxed{F(0) = 1 \quad F(\infty) = 0}$$

the way to solve this problem is by making a variable substitution: let $G = F'$ $\therefore G' = -\frac{1}{2} \eta G$

$$\rightarrow G = \alpha \exp \left[-\frac{\eta^2}{4} \right]$$

$$\therefore F(\eta) = \beta + \alpha \int_0^\eta \exp \left[-\frac{u^2}{4} \right] du \rightarrow F(0) = 1 \therefore \beta = 1, F(\infty) = 0 \therefore 1 + \alpha \int_0^\infty \exp \left[-\frac{u^2}{4} \right] du = 0$$

↑ normalizing our concentration by the initial conc., why $\alpha = 1$

$$F(\gamma) = 1 - \underbrace{\frac{1}{\sqrt{\pi}} \int_0^{\gamma} \exp\left[-s^2/4\right] ds}_{\text{error function: } \operatorname{erf}(\gamma)}$$

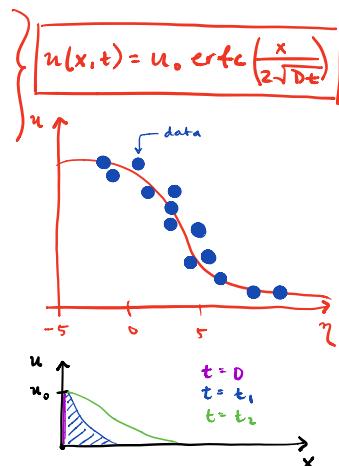
$$1 - \operatorname{erf}(\gamma) = \operatorname{erfc}(\gamma) \dots \text{complementary error function}$$

When might we expect to see a similarity variable?

-when the problem we're solving lacks a characteristic space or time variable

ex. hanging sheet of paper off of a table

(... more hangs off, starts to bend while it's hanging off only a little then can see finite length)



Buckingham π - Theorem

$$a = f(a_1, \dots, a_k, b_1, \dots, b_m)$$

↑
 dimensional parameter we're interested in parameters of independent dimensions parameters that can be expressed as products of powers of a_1, \dots, a_k
 i.e. $b_i = a_1^{r_1} \cdots a_k^{r_k}$

for any given problem, sometimes $m=0$

is meaning that all the governing parameters have independent dimensions sometimes k can be 0 as well

meaning that all quantities/governing parameters are dimensionless
... in general, neither of these are true and $K > 0 \neq m > 0$

construct dimensionless parameters:

$$\Pi = \frac{a}{a_1 \cdots a_k} \quad \Pi_1 = \frac{b_1}{a_1^{r_1} \cdots a_k^{r_1}} \quad \Pi_2 = \frac{b_2}{a_1^{r_2} \cdots a_k^{r_2}} \quad \Pi_m = \frac{b_m}{a_1^{r_m} \cdots a_k^{r_m}}$$

For instance,

Recall : Drag on a Sphere

$$D_f = \rho R^2 V^2 F\left(\frac{u}{\rho R V}\right)$$

↑ ↑ ↑ ↑ ↑ ↑
 a a_1 a_2 a_3 a'_1 a'_2 a'_3
 ↓ ↓ ↓ ↓ ↓ ↓
 a a_1 a_2 a_3 a'_1 a'_2 a'_3
 (meaning a_3 to
the power of 1)

$$\frac{D_f}{\pi R^2 V^2} = F \left(\frac{\mu}{\rho RV} \right)$$

in general, we
should be able to construct ...

Buckingham II-Theorem: The physical relationship between a dimensional quantity and several dimensional parameters can be rewritten as a relationship between a dimensionless parameter and several dimensionless products of the governing parameters. The number of dimensionless products is equal to the number of governing parameters minus the number of independent dimensions.

When are dimensionless products essential?

→ not too small, and not too large

Essential Dimensionless Products

$$\text{e.g. } \frac{1}{10} < \underline{\underline{\pi_m}} < 10$$

essential

... might get parameter or one over parameter

→ so in general, if dimensionless parameter π_m is small or large, can assume it to be neglected

e.g. brittle fracture problem

$$D = f(P, K, V, d, \Delta)$$

↓ If we put these in, would have gotten slightly different answer

$$D \sim \left(\frac{P}{K}\right)^{1/3} \phi(V, \frac{d}{(P/K)^{1/3}}, \frac{\Delta}{(P/K)^{1/3}})$$

length \uparrow \uparrow \uparrow \uparrow

we made an assumption:

$\pi_2 \ll 1$ and $\pi_3 \gg 1$

(very small) (very large)

$$D \sim \left(\frac{P}{K}\right)^{1/3} \phi(V, \frac{d}{(P/K)^{1/3}}, \frac{\Delta}{(P/K)^{1/3}})$$

length \uparrow \uparrow \uparrow \uparrow

we therefore decided to neglect these

more formally:

π_m that is small or large can be neglected
if $\phi(\dots)$ has a finite, non-zero limit as
 $\pi_m \rightarrow 0$ or $\pi_m \rightarrow \infty$

Why would we want to neglect things?
→ need to do an order of magnitude more of experiments which could be costly, time-killing

this is known as "complete similarity" - ability to throw out parameters that were safe to neglect ... also written as "similarity of the first kind"

Incomplete Similarity - or - Similarity of the Second kind

- if $\pi_m \rightarrow 0$ or $\pi_m \rightarrow \infty$ the function $\phi(\dots)$ does not have a finite and non-zero limit
- b_m can remain essential no matter how small or large its corresponding dimensionless parameter becomes
- if $\phi(\dots)$ has a power-like asymptotic representation then you can rewrite it as

$$\phi = \pi_m^\alpha \phi_i(\pi_1, \dots, \pi_{m-1}) + O(\pi_m^\alpha)$$

capital 'o' running higher order?

small compared with first term

allows us to write:

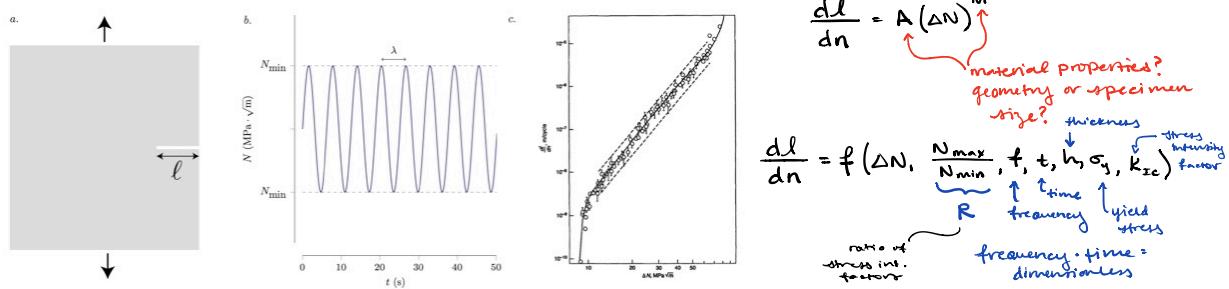
$$\pi^* = \phi_i(\pi_1, \dots, \pi_{m-1})$$

$$\frac{\pi}{\pi^*} = \frac{a}{a_1^{r-a_m} \dots a_k^{r-a_m} b_m}$$

this quantity that wants to neglect still appears

may depend on the dimensionless products in the problem
} α and π^* cannot be determined by dimensional analysis alone

Fatigue: the gradual failure of structures from cyclical loading
 - an example of Incomplete Similarity



$$\frac{dl}{dn} = A(\Delta N)^m$$

material properties?
 geometry or specimen size?
 thickness
 stress intensity factor

$$\frac{dl}{dn} = f(\Delta N, \frac{N_{\max}}{N_{\min}}, f, t, h, \sigma_y, k_{Ic})$$

R time frequency yield stress
 ratio of stress int. factors
 frequency · time = dimensionless

fatigue like w/o propagation of a crack

dimensional analysis: $\frac{dl}{dn} = \left(\frac{\Delta N}{\sigma_y}\right)^2 \phi\left(\frac{\Delta N}{K_{Ic}}, R, \frac{\sigma_y \sqrt{a}}{K_{Ic}}, f, t\right)$

\uparrow quantity is usually small $\uparrow z$ \uparrow ratio of ductile to brittle fracture
 neglect the $\sigma_y \sqrt{a}$ term

... assume complete similarity

$$\frac{dl}{dn} = \left(\frac{\Delta N}{\sigma_y}\right)^2 \phi(R, z) \quad \dots \text{realign to make consistent with empirical formula}$$

$$= \frac{\phi_i(R, z)}{\sigma_y^2} (\Delta N)^2 \cancel{A(\Delta N)^m}$$

\uparrow but then from experiments, find that $m \neq 2$ after comparing with our data

... we now need to assume incomplete similarity

$$\phi = \left(\frac{\Delta N}{K_{Ic}}\right)^\alpha \phi_i(R, z) \rightarrow \frac{dl}{dn} = \frac{(\Delta N)^{2+\alpha}}{\sigma_y^2 K_{Ic}^\alpha} \phi_i(R, z)$$

$$\frac{dl}{dn} = \boxed{\frac{\phi_i(R, z)}{\sigma_y^2 K_{Ic}^\alpha}} (\Delta N)^{2+\alpha}$$

α is a number but we won't know what it is, alpha could be a function of R and z , $\alpha(R, z)$