"Frequency Sweep"

$$[m]\ddot{x} + [c]\dot{x} + [k]\ddot{x} = \vec{F}(+)$$

Support of all proportional damping

Steady-State Vibration Particular Soln

\$\times(t) = \times \text{exp}(jevt) \times real part

tompux

compux

amplitude

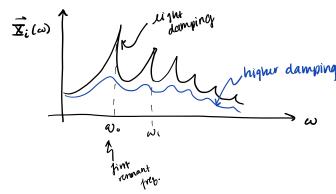
$$\vec{X} = \vec{X}_r + i \vec{X}_i$$

$$\vec{X}(t) = \Re \left\{ (\vec{X}, + j \vec{X}_i) (\cos \omega t + j - \sin \omega t) \right\}$$

$$= \vec{X}_i \cos \omega t - \vec{X}_i - \sin \omega t$$

• frequency truep:
given Fo t a ≤ ∞ ≤ b
[m], [c], [k]

find 豆(w)



* substitute time dependencies
$$((j\omega)^*[M] + (j\omega)[c] + [k]) \overrightarrow{X} = \overrightarrow{F}$$

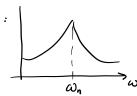
[D(w)]
$$\vec{X} = \vec{F}$$
.

The call his the synamic stiffness

$$\vec{X}(\omega) = [D(\omega)]^{-1} \vec{F}_{\delta}$$

· Why peaks in FRF = frequency remonse function?

in One DoF:



· associated eigenvalue problem

$$([k]-\omega_{n,s}[w]) \underline{\varphi}^{u} = \underline{0}$$

$$\vec{\mathbf{X}} = \sum_{n=1}^{\infty} C_n \vec{\phi}_n - \left[\vec{\Phi} \right] \{ c \}$$

$$\begin{bmatrix} \vec{\phi}_1 & \vec{\phi}_2 & \dots & \vec{\phi}_n \end{bmatrix} \dots$$

[4] ([K] - w2[m])[4] = [4] F

$$\begin{bmatrix} \Phi \end{bmatrix}^T \begin{bmatrix} k \end{bmatrix} \begin{bmatrix} \Phi \end{bmatrix} = diag(\omega_n^2)$$

 $\begin{bmatrix} \Phi \end{bmatrix}^T \begin{bmatrix} m \end{bmatrix} \begin{bmatrix} \Phi \end{bmatrix} = \begin{bmatrix} I \end{bmatrix} N \times N$

$$C_n = \frac{\left(\underline{\Gamma} \Phi \right)^T \overline{F}_0 \Big)_n}{\omega_n^2 - \omega^2}$$

putting it all together into one final anower:

$$\vec{X}(\omega) = \sum_{n=1}^{N} \frac{\vec{\varphi}_{n} \vec{F}_{o}}{\omega_{n^{2}} - \omega^{2}} \vec{\overline{\Psi}}_{n}$$

Leigenvector

scalar #,

call this the

MODAL AMPLITUDE