

# HOFEM-AIRBUS 2D Emulation

**Group of Radiofrequency, Electromagnetism, Microwaves  
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<http://grema.webs.tsc.uc3m.es/>

**Departamento de Teoría de la Señal y Comunicaciones (TSC)**  
**Universidad Carlos III de Madrid, Spain**

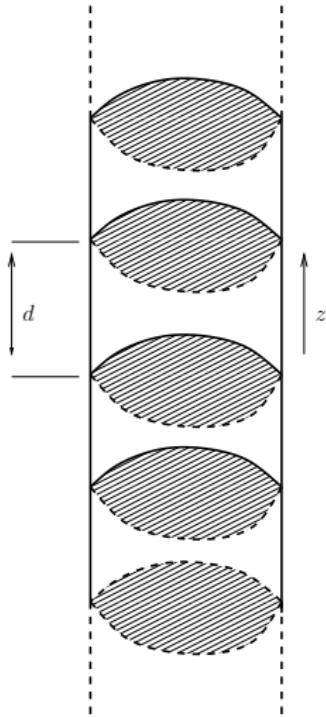


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We start considering the use of Green3D or Green2D the scattering of infinite cylinders using 3D simulator on a section (“slice”) of the cylinder

# HOFEM 2D Emulation



## 3D Green's Function

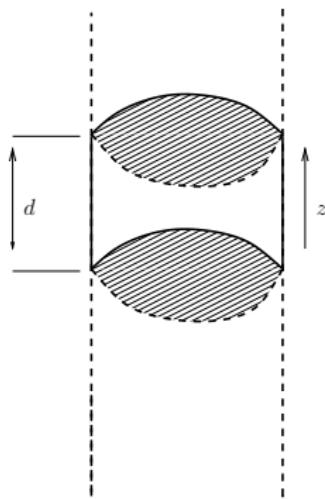
- Sum of infinite contributions (from each repeated cell)
- Ewald acceleration needed
  - ▶ It works great, though

$$\text{Green}(R) = \frac{1}{4\pi} \sum_{n=-\infty}^{\infty} \frac{e^{-jkR_n}}{R_n}$$

with

$$R_n = |\mathbf{r} - \mathbf{r}'_n|, \mathbf{r}'_n = \mathbf{r}'_0 + n\mathbf{d}$$

# HOFEM 2D Emulation (cont.)



## 2D Green's Function

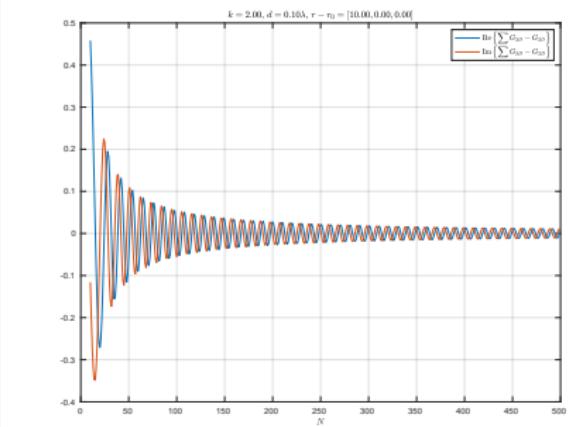
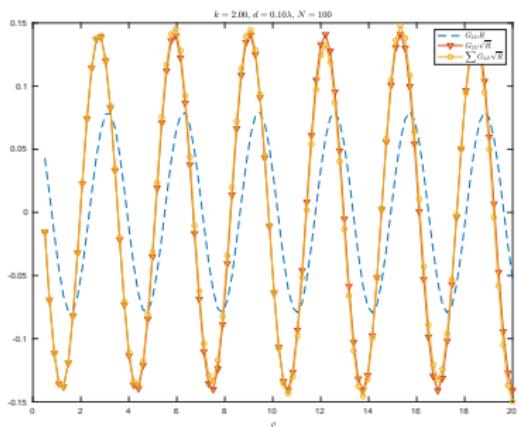
- No summation needed

$$\text{Green}(\rho) = \frac{1}{4j} H_0^{(2)}(k|\rho|)$$

# Near Field (FE-IIEE loop)

## Sanity Checks (MATLAB)

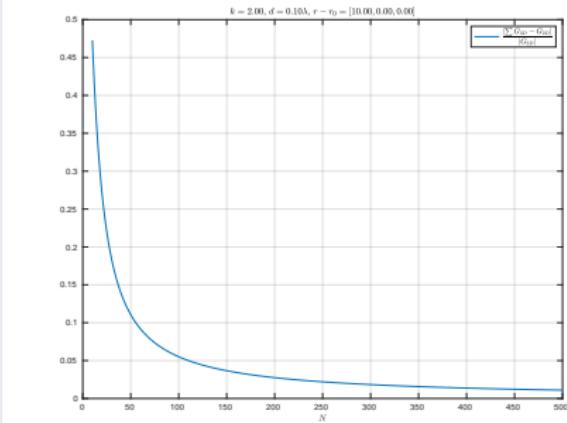
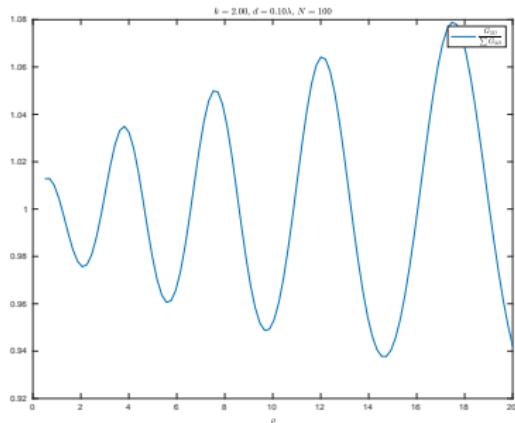
- Equivalence of infinite sum of 3D Green's function with 2D Green's function on the unit cell



# Near Field (FE-IIEE loop) (cont.)

## Sanity Checks (MATLAB)

Equivalence of infinite sum of 3D Green's function with 2D Green's function on the unit cell



# Near Field (FE-IIEE loop) (cont.)

## HOFEM Implementation

- Coded
- Tested

```
[#] EXECUTING IIEE TRUNCATION METHOD...
```

---

```
[#] CALCULATING SCATTERING FIELD...
```

```
[#] SCATTERING FIELD CALCULATED IN  
0.190 [sec]
```

---

```
[#] CALCULATING SCATTERING RHS...
```

```
[#] SCATTERING RHS CALCULATED IN  
0.014 [sec]
```

---

```
Iteration:  
1. (err 1.19E-02) 0.235 [sec]
```

---

```
[#] CALCULATING SCATTERING FIELD...
```

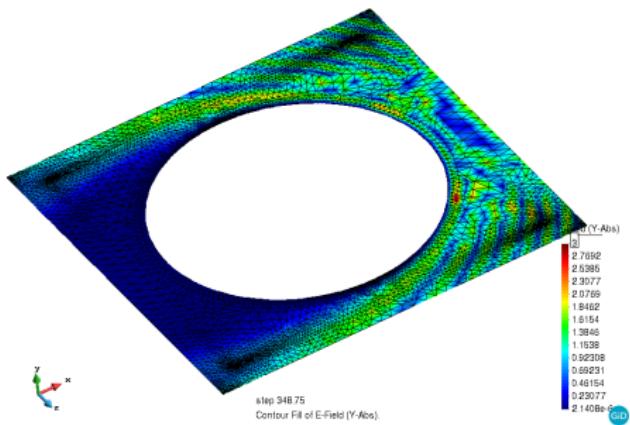
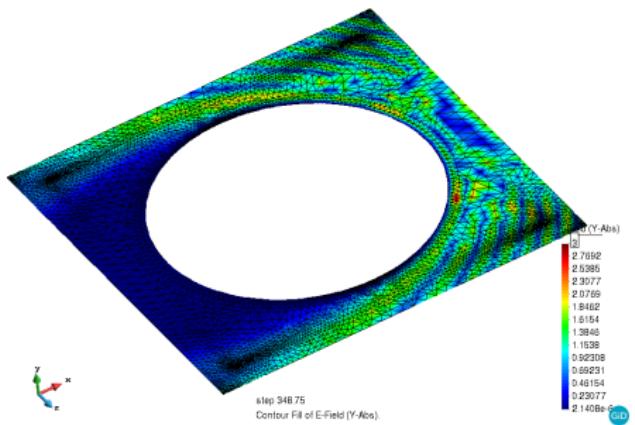
# Near Field (FE-IIEE loop) (cont.)

Code output (terminal):

```
Iteration : 1. (err 1.19E-02)
Iteration : 2. (err 8.31E-05)
Iteration : 3. (err 7.23E-07)
Iteration : 4. (err 6.10E-09)
```

```
Iteration : 1. (err 1.50E-02)
Iteration : 2. (err 1.02E-04)
Iteration : 3. (err 8.28E-07)
Iteration : 4. (err 7.00E-09)
```

# Near Field (FE-IIEE loop) (cont.)



# Far Field (postprocess)

## Equivalence of Green's Functions for Far Field

- Can we use an infinite sum of 3D Green's far-field functions to model the 2D Green's far-field?
  - ▶ NO
  - ▶ and it makes sense!

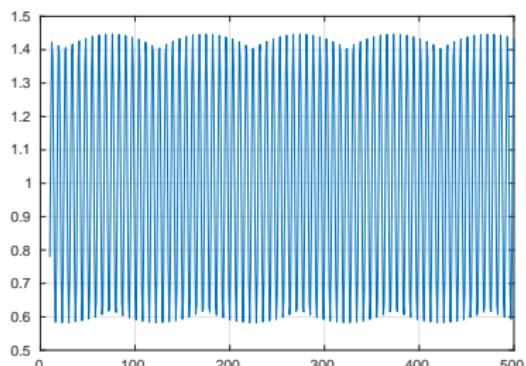
## Far Field as Fourier Transform

The Fourier Transform of a constant current contribution along  $z$  is a delta function in the spatial frequency domain, i.e., variable  $\theta$ :

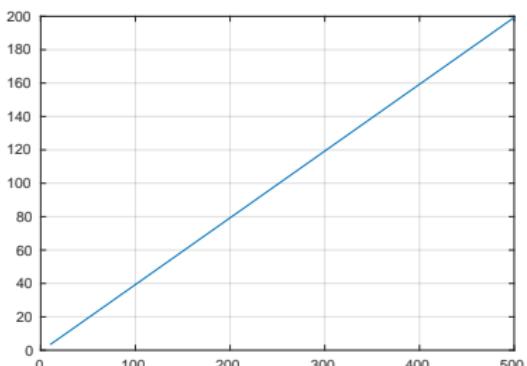
$$\text{Far Field}(\theta, \phi) = \delta(\theta - \pi/2) F(\phi) \quad (1)$$

# Far Field (postprocess) (cont.)

$\theta \neq 90^\circ$ : Oscillations



$\theta = 90^\circ$ : Divergence



# Far Field (postprocess) (cont.)

## HOFEM Implementation

- Coded (in progress)
- Tested (in progress)

## Rethinking . . .

AIRBUS: *hay un chico con nosotros que resuelve problemas de scattering de cilindros y no usa función de Hankel. Usa Green3D para calcular el campo (lejano) de scattering de una rodaja y le funciona.*

- Further study of differences between Green2D and Green3D
  - ▶ Obvious (after a maturation process) for far field
  - ▶ Not so obvious for near field (i.e., in its impact in FE-IIEE loop)

# Far Field (postprocess)

## Equivalence of Green's Functions for Far Field

- Can we use an infinite sum of 3D Green's far-field functions to model the 2D Green's far-field?
  - ▶ NO
  - ▶ and it makes sense!
  - ▶ No need of infinite sum (**far field Green3D/Green2D is enough**)
    - ★ Note that far field versions of Green3D (with  $r = \rho$ ) and Green2D are equal up to a constant

## Far Field as Fourier Transform

The Fourier Transform of a constant current contribution along  $z$  is a delta function in the spatial frequency domain, i.e., variable  $\theta$ :

$$\text{Far Field}(\theta, \phi) = \delta(\theta - \pi/2) F(\phi) \quad (2)$$

# Far Field (postprocess) (cont.)

## Green2D vs Green3D

$F(\phi)$  is the same (after normalization) considering asymptotic expressions of Green3D and Green3D

$$H_0^{(2)}(k\rho) \underset{\rho \rightarrow \infty}{\approx} \sqrt{\frac{2j}{\pi k\rho}} e^{-jk\rho} \quad \frac{e^{-jkR}}{4\pi R} \underset{r \rightarrow \infty}{\approx} \frac{e^{-jkr}}{4\pi r} e^{jkr' \cos \psi}$$

# Near Field (FE-IIEE loop)

Code output (terminal):

- From previous meeting

Green2D

```
Iteration : 1. (err 1.50E-02)
Iteration : 2. (err 1.02E-04)
Iteration : 3. (err 8.28E-07)
Iteration : 4. (err 7.00E-09)
```

Green3D

```
Iteration : 1. (err 1.19E-02)
Iteration : 2. (err 8.31E-05)
Iteration : 3. (err 7.23E-07)
Iteration : 4. (err 6.10E-09)
```

**How can it work?** Note we used Green3D itself (only one slide was considered)

# Near Field (FE-IIEE loop) (cont.)

Code output (terminal):

- Large  $S' - S$

Green2D

```
Iteration : 1. (err 1.50E-02)
Iteration : 2. (err 1.02E-04)
Iteration : 3. (err 8.28E-07)
Iteration : 4. (err 7.00E-09)
```

Green3D

```
Iteration : 1. (err 1.19E-02)
Iteration : 2. (err 8.31E-05)
Iteration : 3. (err 7.23E-07)
Iteration : 4. (err 6.10E-09)
```

- Small  $S' - S$

Green2D

```
Iteration : 1. (err 5.16E-01)
Iteration : 2. (err 1.22E-01)
Iteration : 3. (err 2.53E-02)
Iteration : 4. (err 4.34E-03)
Iteration : 5. (err 6.86E-04)
Iteration : 6. (err 1.21E-04)
Iteration : 7. (err 2.46E-05)
Iteration : 8. (err 5.06E-06)
```

Green3D

```
Iteration : 1. (err 7.65E-02)
Iteration : 2. (err 6.08E-03)
Iteration : 3. (err 5.46E-04)
Iteration : 4. (err 5.05E-05)
Iteration : 5. (err 4.59E-06)
Iteration : 6. (err 4.24E-07)
Iteration : 7. (err 4.14E-08)
Iteration : 8. (err 4.13E-09)
```

# Green2D vs Green3D

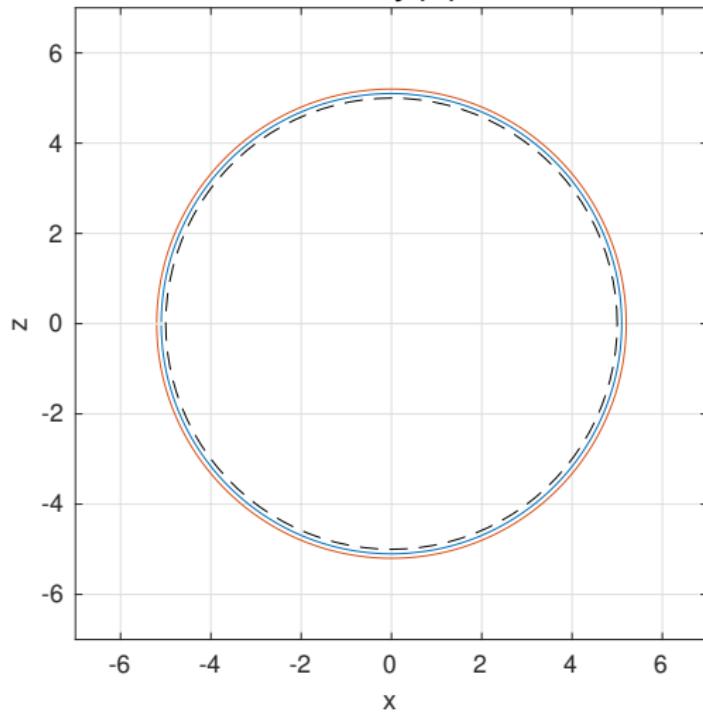
Comparison with analytical solution

- Most results displayed correspond to TM and E field
- H field (i.e., RotE) identical conclusions
- By duality (satisfied by HOFEM) TE results “should” be identical (tested).
- Most results shown here correspond to both  $S'$  and  $S$  conformal to the cylinder (circular boundary). Analogous results/conclusions are obtained with rectangular boundaries for  $S'$  and  $S$  (and combinations of them).

# Green2D vs Green3D (cont.)

Comparison with analytical solution

Geometry (m)



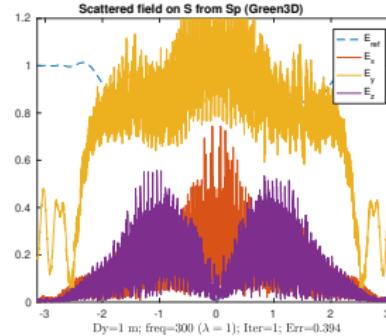
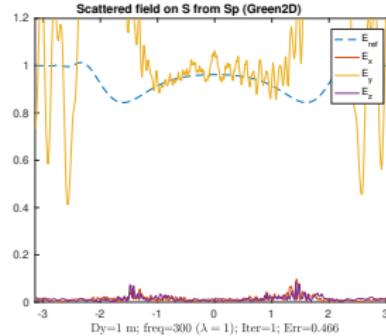
- 300 MHz
- Small  $S - S'$
- Thick slice

# Green2D vs Green3D (cont.)

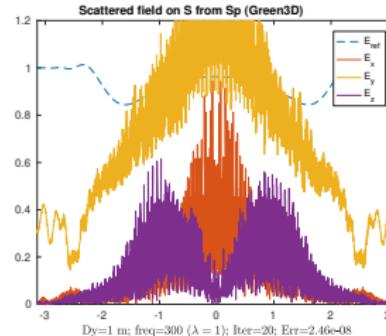
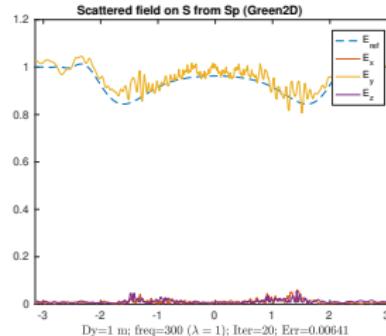
Comparison with analytical solution

Evolution scattered electric field ( $S'$  over  $S$ )

Iteration 1:



Iteration 20:

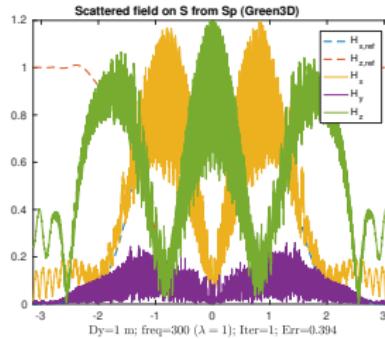
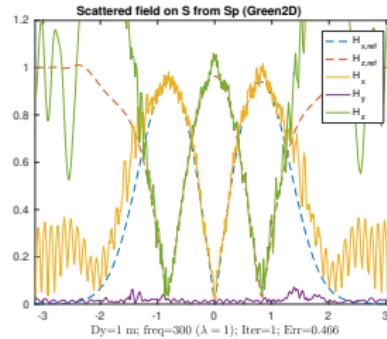


# Green2D vs Green3D (cont.)

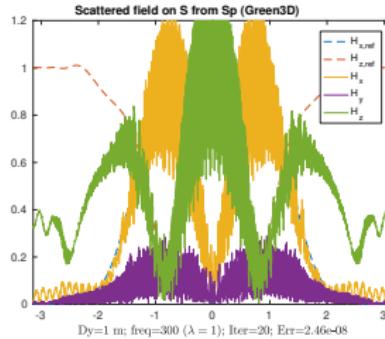
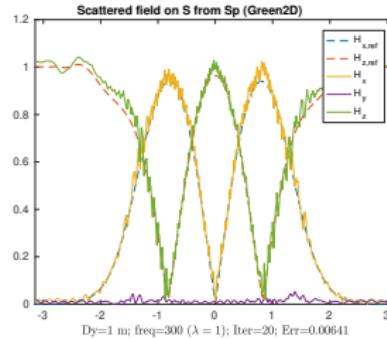
Comparison with analytical solution

Evolution scattered magnetic field ( $S'$  over  $S$ )

Iteration 1:



Iteration 20:

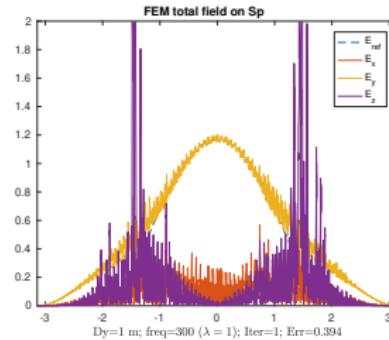
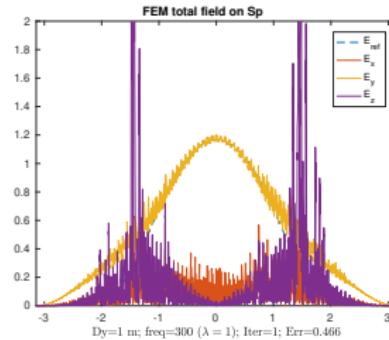


# Green2D vs Green3D (cont.)

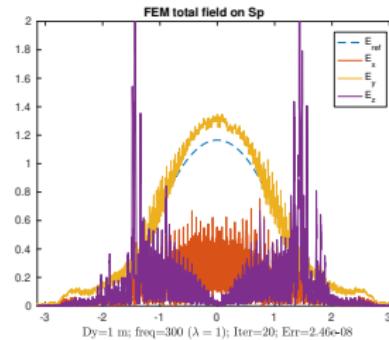
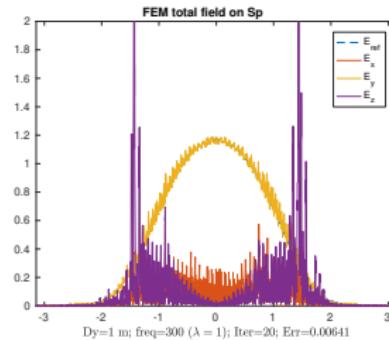
Comparison with analytical solution

Evolution electric field on  $S'$

Iteration 1:



Iteration 20:



# Green2D vs Green3D (cont.)

Comparison with analytical solution

- Higher error with Green3D
  - ▶ This is a case with small distance  $S - S'$  and large thickness
  - ▶ Nevertheless, the error is always significantly higher than Green2D
- Green3D does not converge to right solution
- Components  $E_x, E_z, H_y$  are not null
  - (issue of (\*) certainly added confusion on the debugging/verification of the code)
    - ▶ Much higher levels with Green3D
    - ▶ Green3D (the Green's function itself) generates non null  $E_x, E_z, H_y$  from  $E_z$  on  $S'$
    - ▶ Green2D (the Green's function itself) does not generate any  $E_x, E_z, H_y$ 
      - ★ Numerically, non-zero levels of  $E_x, E_z, H_y$  are generated because numerical FEM solution has non zero levels of  $E_x, E_z, H_y$  (tested!)
- Numerical noise always present due to discretization
  - ▶ Clearly visible in this case
  - ▶ Decreases with finer discretization —FEM mesh— (tested!)

(\*) Issue of GiD/HOFEM-GUI representation of fields on surface

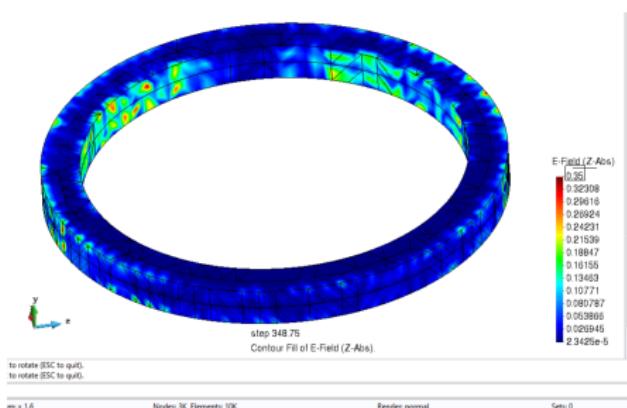
# Rethinking . . .

(\*) Issue of GiD/HOFEM-GUI representation of fields on surface

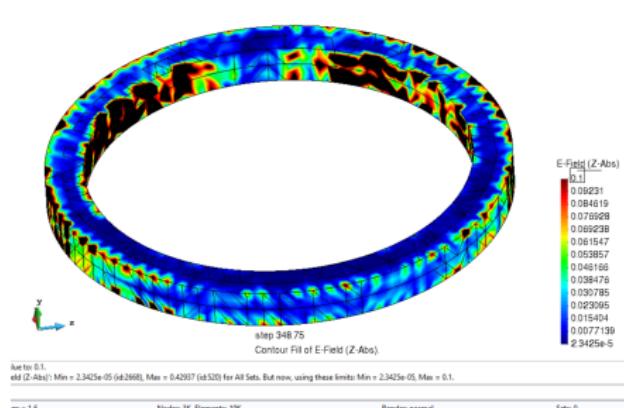
# GiD/HOFEM-GUI Field Representation on Surfaces

Examples with PEC surfaces

- $E_z$  should be null on the caps (top and bottom  $y = \text{cte}$ )



$|E_z|$  (default color scale)

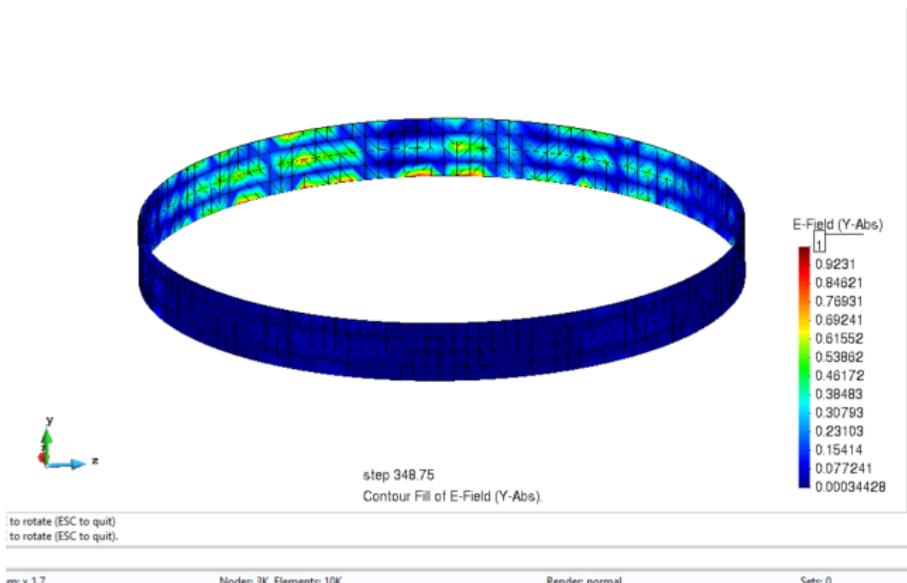


$|E_z|$  (saturated color scale)

# GiD/HOFEM-GUI Field Representation on Surfaces (cont.)

Examples with PEC surfaces

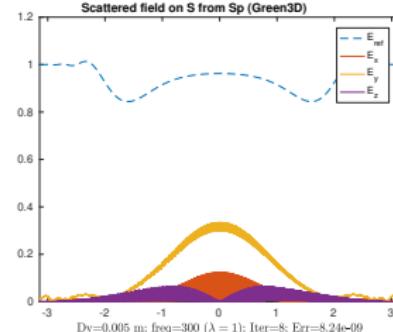
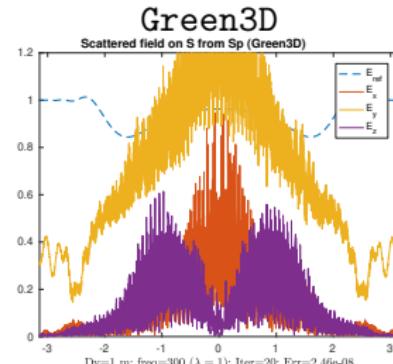
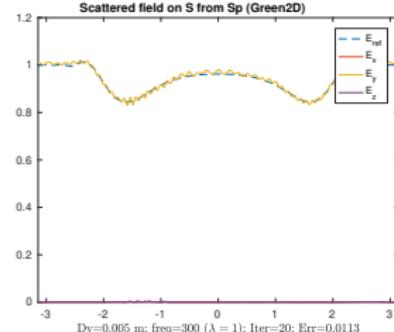
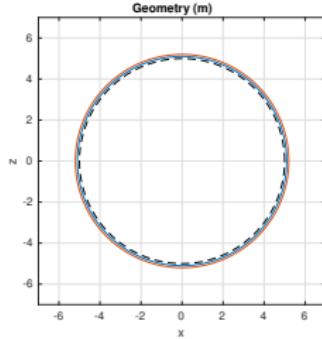
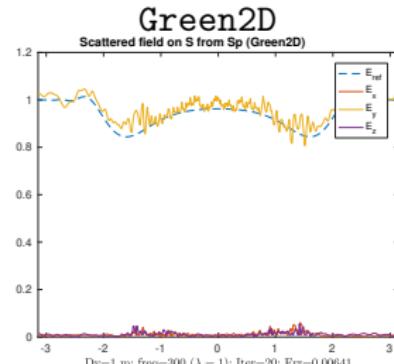
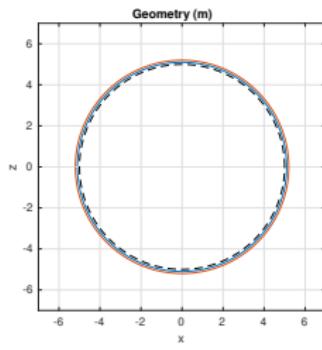
- $E_y$  should be null on the cylinder “sides” (i.e., on the PEC cylinder)



$|E_y|$  (only PEC cylinder surface shown)

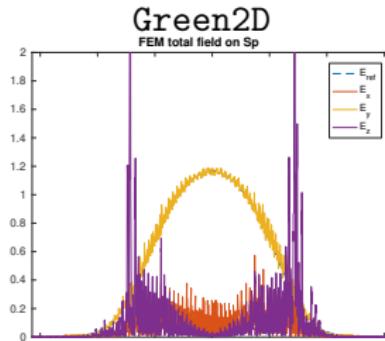
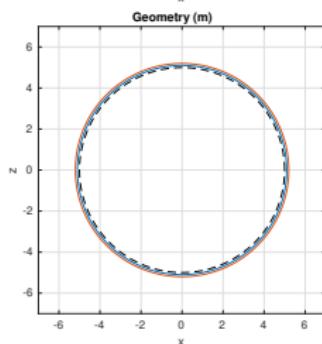
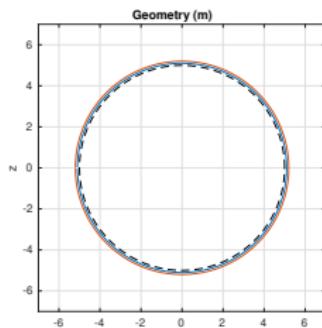
# Effect of “Thickness”

Scattered near field —Note error in figure captions: thickness is  $0.05 \lambda$  for the thin slice—

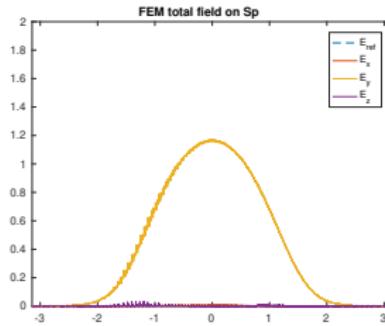


# Effect of “Thickness”

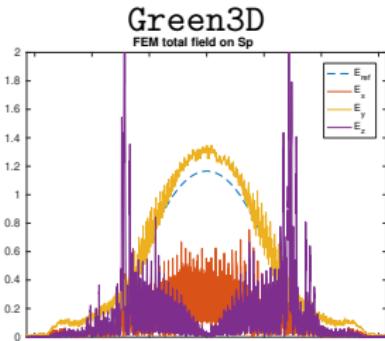
FEM solution —Note error in figure captions: thickness is  $0.05 \lambda$  for the thin slice—



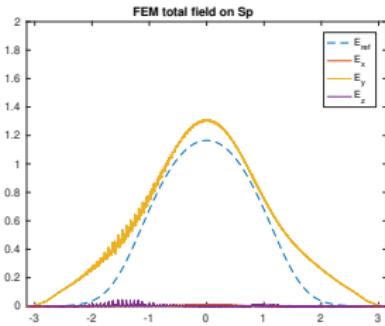
Dy=1 m; freq=300 ( $\lambda = 1$ ); Iter=20; Err=0.00641



Dy=0.005 m; freq=300 ( $\lambda = 1$ ); Iter=20; Err=0.0113



Dy=1 m; freq=300 ( $\lambda = 1$ ); Iter=20; Err=2.46e-08



Dy=0.005 m; freq=300 ( $\lambda = 1$ ); Iter=8; Err=8.24e-09

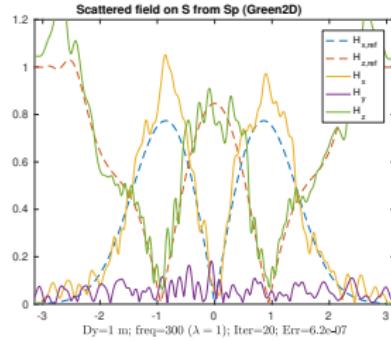
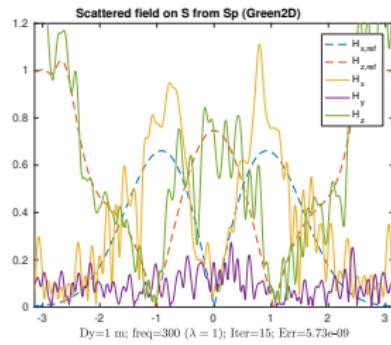
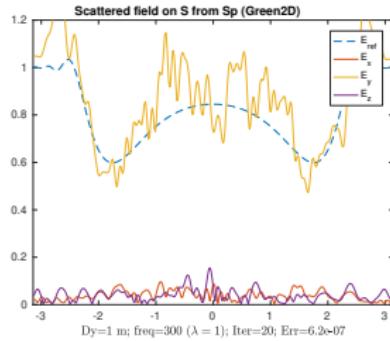
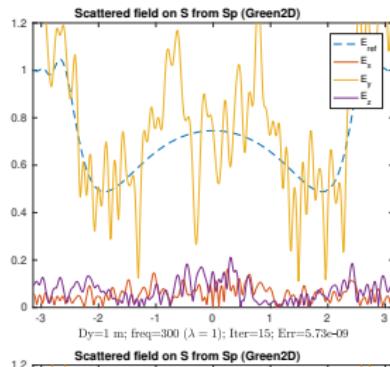
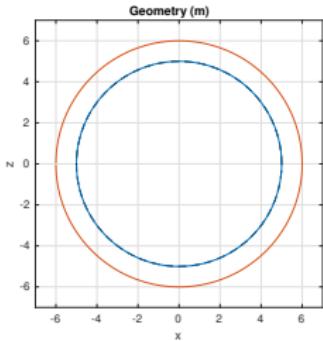
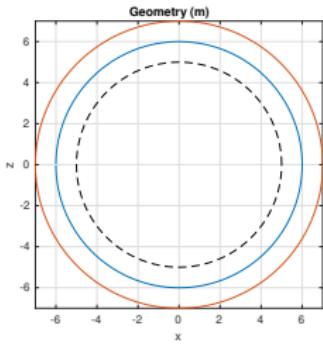
## Effect of “Thickness” (cont.)

FEM solution —Note error in figure captions: thickness is  $0.05 \lambda$  for the thin slice—

- The thickness is the main factor for error with Green3D
- Green2D behaves great!
- Always lower error with thin slices

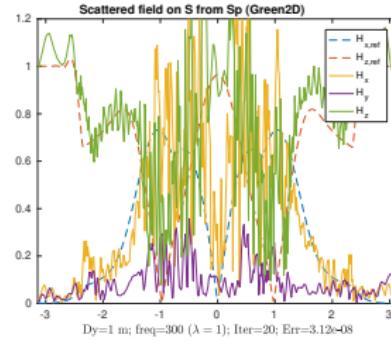
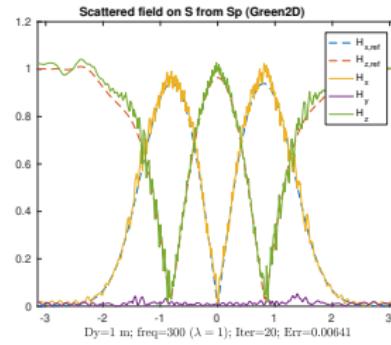
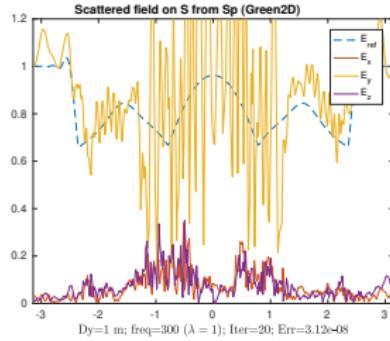
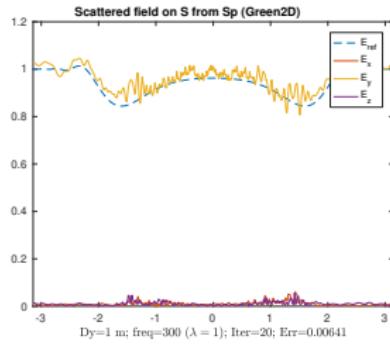
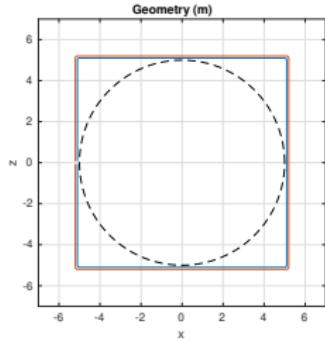
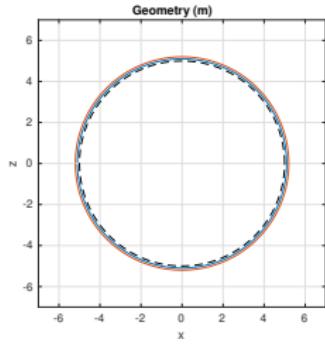
# Other Effects (paranoic mode)

Effect of  $S'$  on PEC cylinder



# Other Effects (paranoic mode)

Effect of  $S'$ , S Curved



# Green3D vs Green2D

## Conclusions

### Conclusions

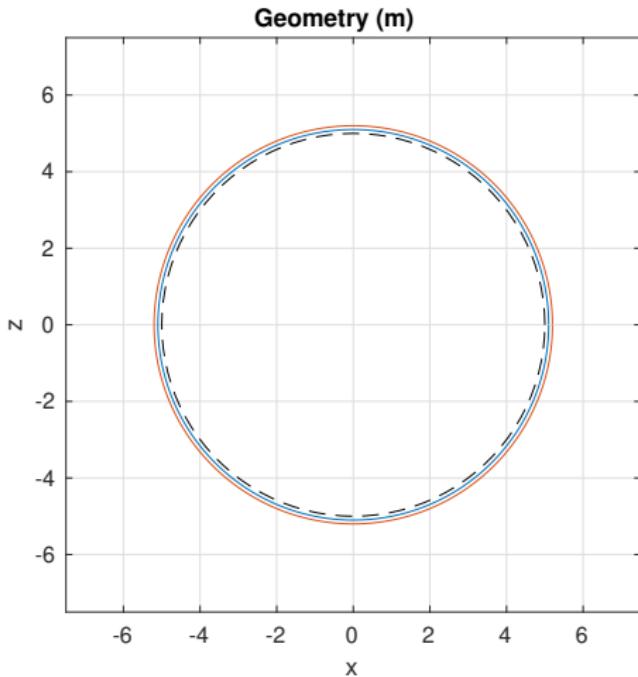
- Green3D itself not valid for 2D Emulation
  - ▶ FE-IIEE converges but
    - ★ Quality of solution far from great
    - ★ It may guide you to wrong solution
- Need to activate contributions of slice replicas along direction of cylinder (translation symmetry) **Green3D\_Ewald1D**

From now on we only use Green2D

- We check TE polarization for PEC cylinder
- We check for the dielectric coated cylinder

# Check TE polarization

Comparison with TM results

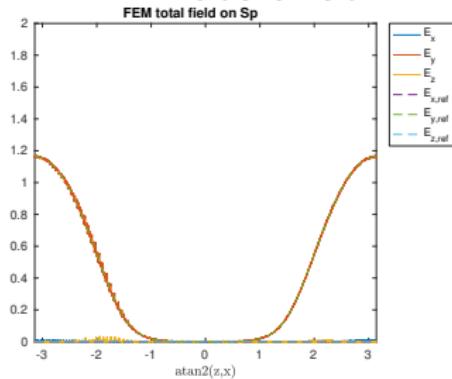


- Freq: 300 MHz. ( $\lambda = 1 \text{ m}$ )
- Thickness: 0.05 m

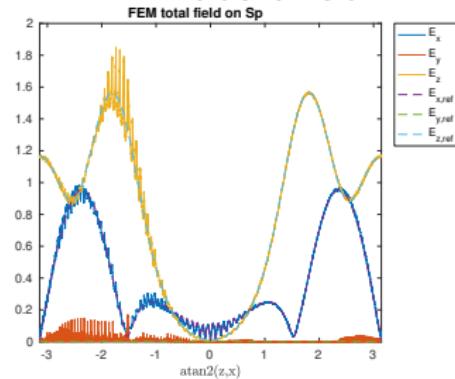
# Check TE polarization (cont.)

Comparison with TM results

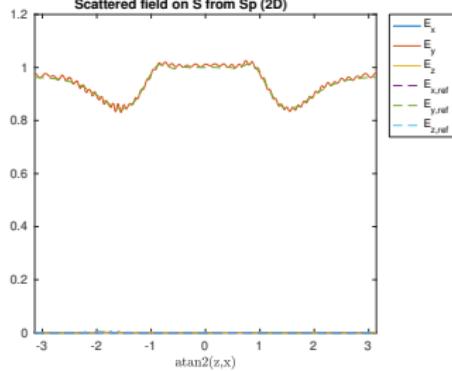
TM incident field



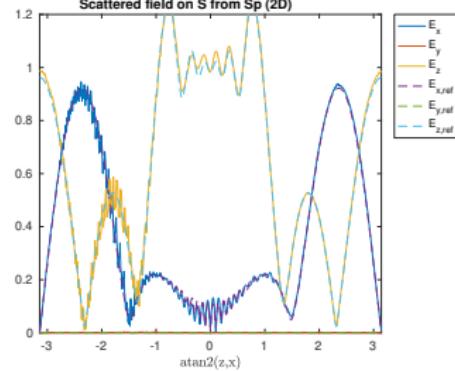
TE incident field



Scattered field on S from Sp (2D)



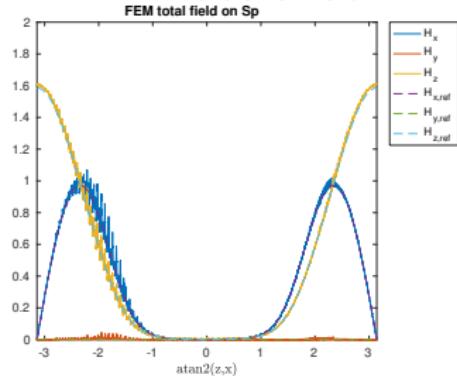
Scattered field on S from Sp (2D)



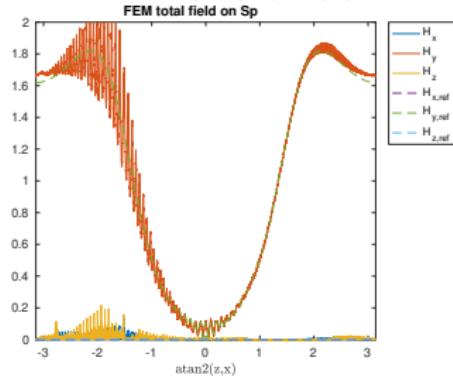
# Check TE polarization (cont.)

Comparison with TM results

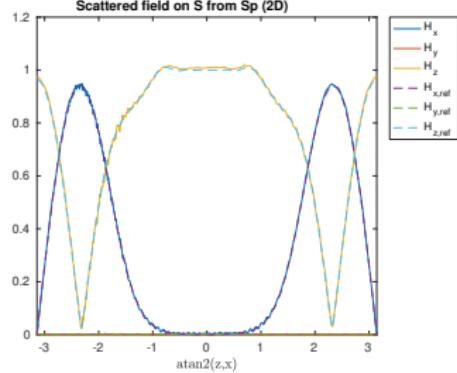
TM incident field



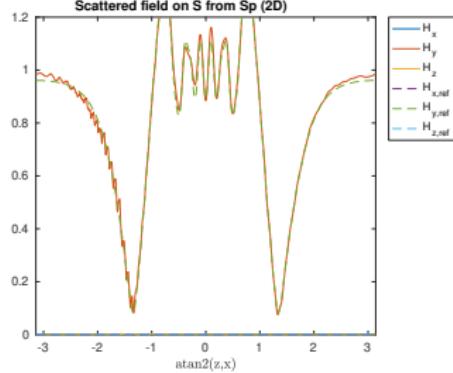
TE incident field



Scattered field on S from Sp (2D)

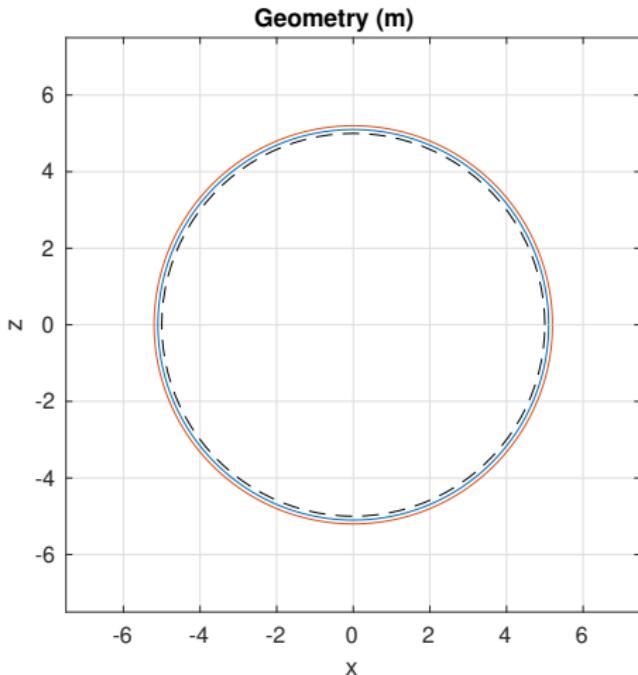


Scattered field on S from Sp (2D)



# Dielectric Coated Cylinders

Comparison with the analytical solution

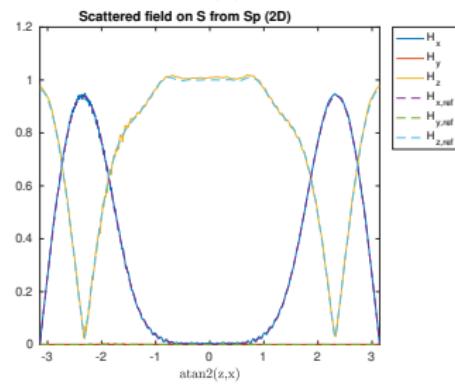
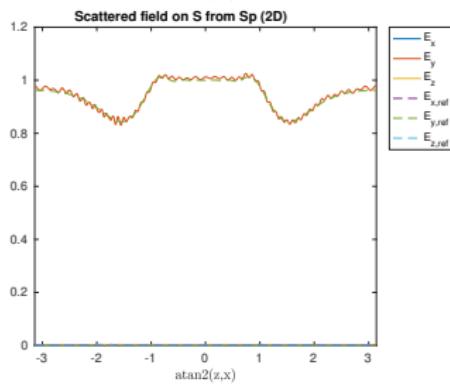
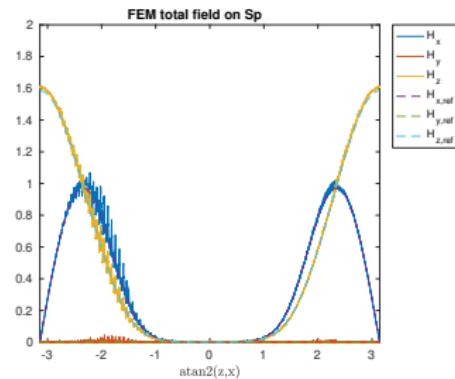
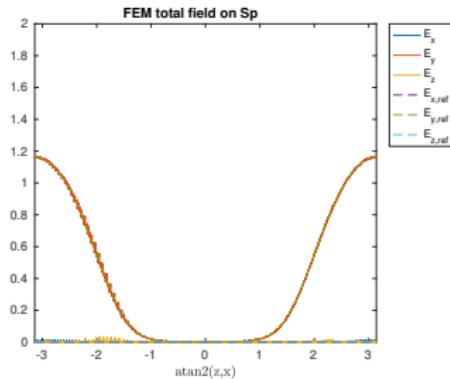


- Freq: 300 MHz. ( $\lambda = 1 \text{ m}$ )
- Thickness: 0.05 m
- Dielectric substrate between  $S$  and  $S'$  with relative permittivity  $\varepsilon_r$ .

# Dielectric Coated Cylinders (cont.)

Comparison with the analytical solution

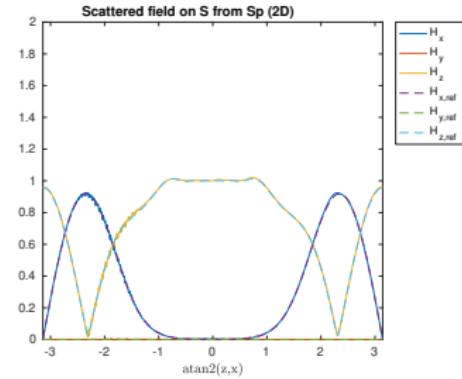
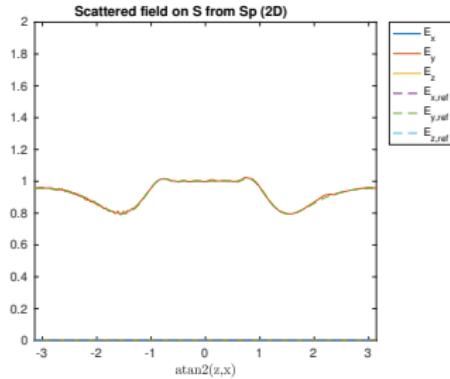
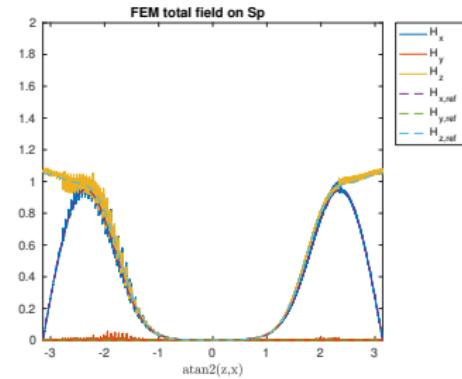
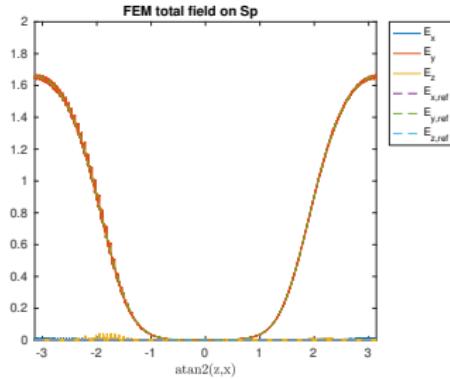
TM incident field  $\varepsilon_r = 1$



# Dielectric Coated Cylinders (cont.)

Comparison with the analytical solution

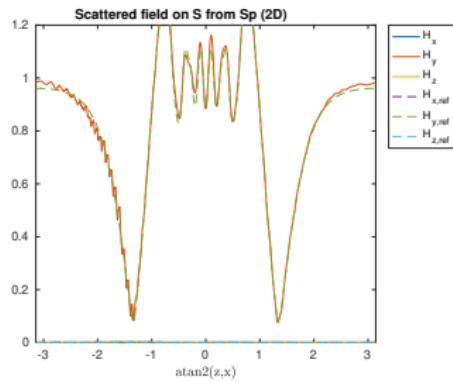
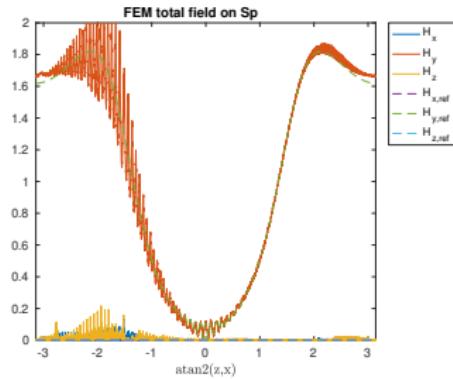
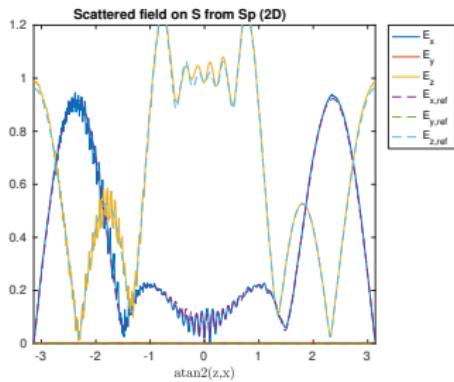
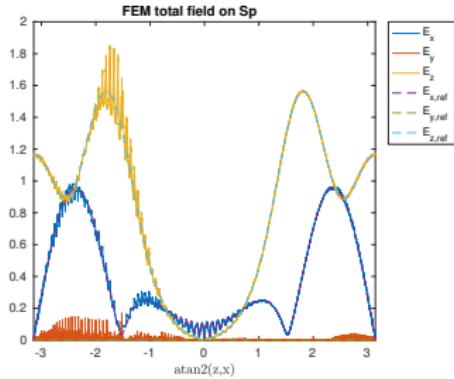
TM incident field  $\varepsilon_r = 4$



# Dielectric Coated Cylinders (cont.)

Comparison with the analytical solution

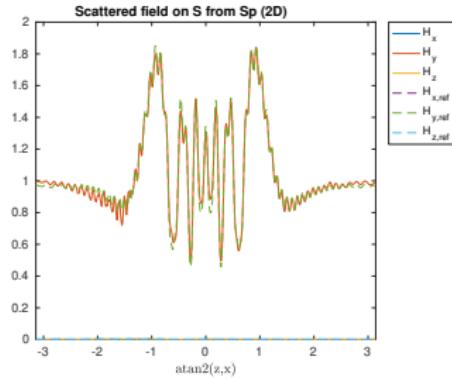
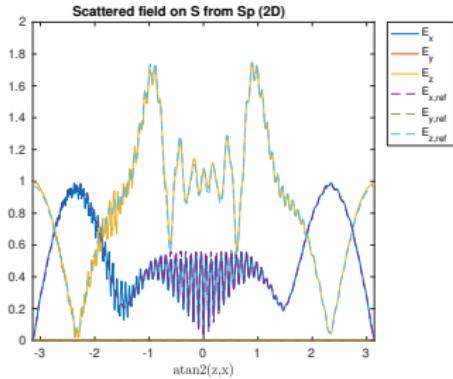
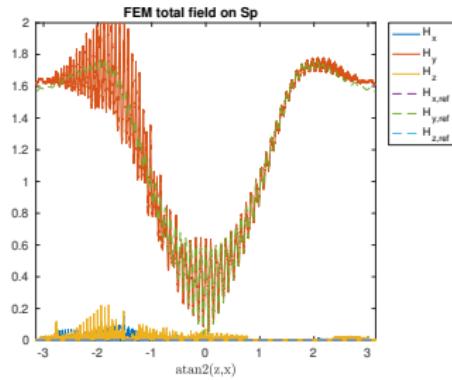
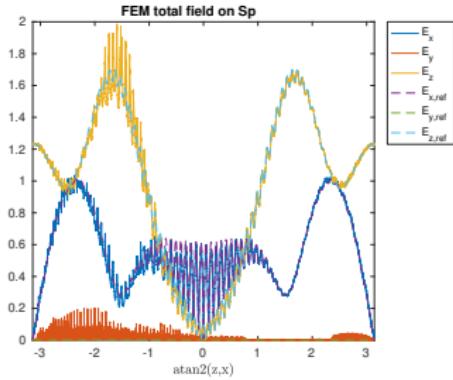
TE incident field  $\varepsilon_r = 1$



# Dielectric Coated Cylinders (cont.)

Comparison with the analytical solution

TE incident field  $\epsilon_r = 1.5$



# Green3D\_Ewald1D

## Ewald Method in HOFEM

where  $s$  is a complex variable. The periodic Green's function can be written in two parts by using the previous identity and splitting the path integration at the parameter  $\mathbf{E}$  as

$$G_p(\mathbf{r}, \mathbf{r}_s) = G_{p1}(\mathbf{r}, \mathbf{r}_s) + G_{p2}(\mathbf{r}, \mathbf{r}_s) \quad (5.41)$$

where  $G_{p1}(\mathbf{r}, \mathbf{r}_s)$  is given by

$$\begin{aligned} G_{p1}(\mathbf{r}, \mathbf{r}_s) &= \frac{1}{4\pi} \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{-j(k_x m D_x + k_y n D_y)} \\ &\quad \times \frac{2}{\sqrt{\pi}} \int_0^{\mathbf{E}} e^{\left(-R_{mn}^2 s^2 + \frac{k_z^2}{4s^2}\right)} ds \end{aligned} \quad (5.42)$$

and  $G_{p2}(\mathbf{r}, \mathbf{r}_s)$  is given by

$$\begin{aligned} G_{p2}(\mathbf{r}, \mathbf{r}_s) &= \frac{1}{4\pi} \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{-j(k_x m D_x + k_y n D_y)} \\ &\quad \times \frac{2}{\sqrt{\pi}} \int_{\mathbf{E}}^{\infty} e^{\left(-R_{mn}^2 s^2 + \frac{k_z^2}{4s^2}\right)} ds \end{aligned} \quad (5.43)$$

```
!Distancia de la celda unidad en X
Dx = & SQRT(DOT_PRODUCT(PBC_structure%offset_vector(1,1), PBC_structure%offset_vector(1,1)))
!Distancia de la celda unidad en Y
Dy = & SQRT(DOT_PRODUCT(PBC_structure%offset_vector(2,2), PBC_structure%offset_vector(2,2)))
E = SQRT(PI/Dx/Dy)

!Sum using Ewald transformation
DO m=-2,2
  DO n=-2,2
    alpha_mn = SQRT(CMPLX((PI*m/Dx)**2 + &
                           (PI*n/Dy)**2 + (PI*m/Dx)*Kx + &
                           (PI*n/Dy)*Ky + &
                           (1.0_DBLE/4.0_DBLE)*(Kx**2+Ky**2-K**2), 0.0_DBLE))
```

## Ewald 1D periodicity

- Naively we thought it was simply setting either  $m = 0$  or  $n = 0$
- **But it is NOT ... see next section on Ewald 1D**

Details on Ewald (1D periodicity)

# Ewald sum

- Technique for summing contribution from an infinite set of sources (in this case along  $z$  axis):

$$\sum_n G(R_n) = \frac{1}{4\pi} \sum_n e^{-j(k \cos \theta)nd} \frac{e^{-jkR_n}}{R_n}$$

where  $R_n = \sqrt{(x - x')^2 + (y - y')^2 + (z - z' + nd)^2}$ ,  $\theta$  is elevation angle.

- The Green function is decomposed in two terms:

$$\sum_n G(R_n) = \sum_n G_1(R_n) + \sum_n G_2(R_n)$$

- ▶ One of them decays quickly with  $R_n$ :  $|G_2(R_{n+1})| \ll |G_2(R_n)|$
- ▶ For the other one the Poisson summation formula is applied:

$$\sum_n G_1(R_n) = \sum_n \hat{G}_1(k_n)$$

where  $\hat{G}_1(k)$  is the Fourier transform of  $G_1(R)$ <sup>1</sup>.

---

<sup>1</sup>  $\hat{G}_1(k)$  is narrow in  $k$  because  $G_1(R)$  is wide in  $R$

# 1D from 2D periodicity Ewald sum

- No problem with *spatial* term:

$$\sum_m \sum_n G_2(R_{n,m}) \rightarrow \sum_n G_2(R_{n,0})$$

- But the *spectral* term...

$$\sum_m \sum_n \hat{G}_1(k_{n,m}) \rightarrow ??$$

The Fourier Transform of  $G_1(n, 0)$  must be computed from scratch:

$$\hat{G}_{1,n} = \frac{e^{j(z-z')(k_z - 2\pi \frac{n}{d})}}{2\pi d} g\left(\frac{\alpha_n^2}{4E^2}, \rho^2 E^2\right)$$

$$\rho^2 = (x - x')^2 + (y - y')^2 \quad \alpha_n^2 = \left(k \cos \theta + \frac{2\pi n}{d}\right)^2 - k^2$$

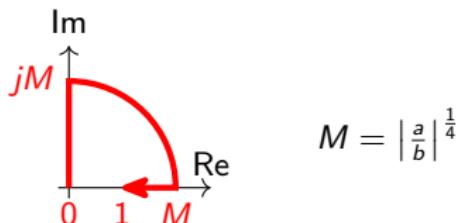
# 1D from 2D periodicity Ewald sum (cont.)

where we need the following numerical integration

$$g(a, b) = \int_0^1 \frac{e^{-\frac{a}{z^2} - bz^2}}{z} dz$$

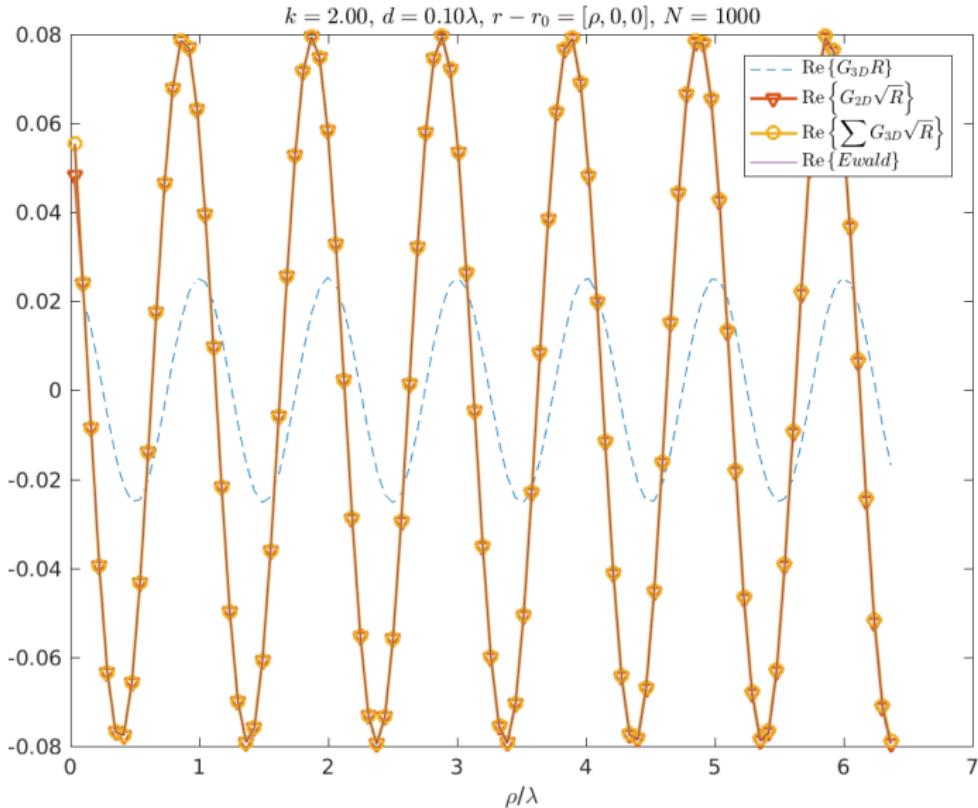
# Notes about $g(a,b)$

- It is a complex integral whose value (and convergence) depends on the chosen path.
- For calculating  $\hat{G}_{1,n}$ :
  - ▶  $a, b \in \mathbb{R}$
  - ▶  $b > 0$ ,
  - ▶ but  $a$  is negative for the first  $n$  values (At each  $n$  term in the sum  $a = \alpha_n^2/4E^2$ ).
- If  $a > 0$ , the integral can be done through real axis.
- If  $a < 0$ , the integral must be done through the following path:

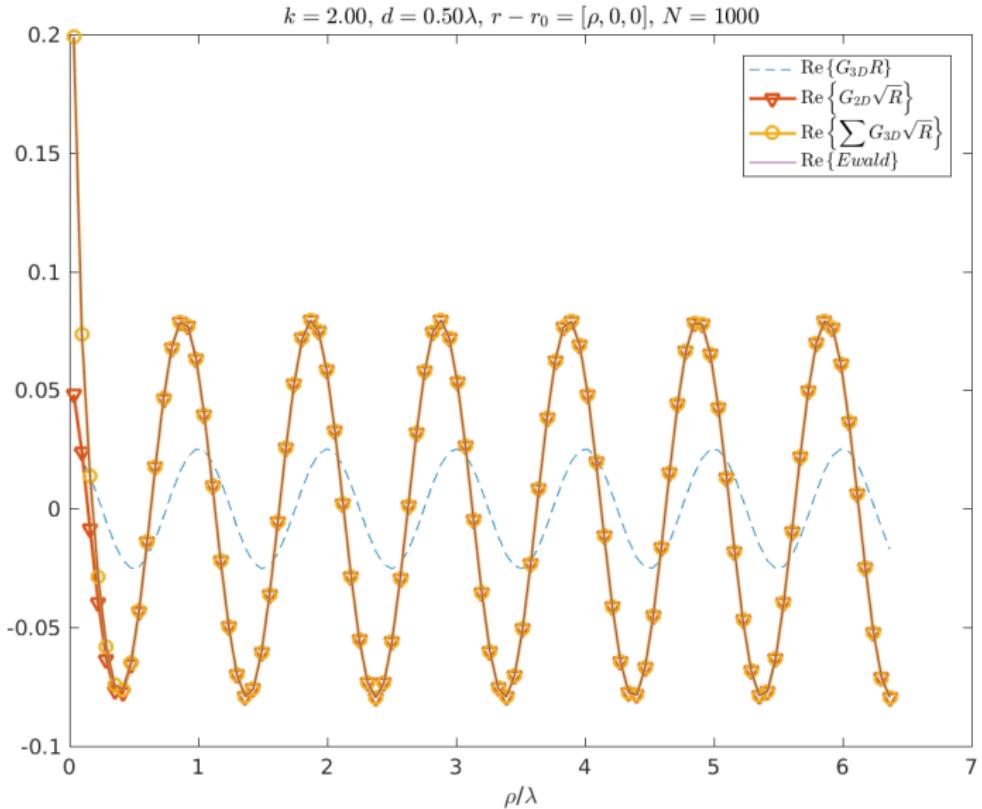


- If  $a = 0$ , integral does not converge. It happens for specific values of  $k$  and  $d$  (not a problem: Greens function is singular there).

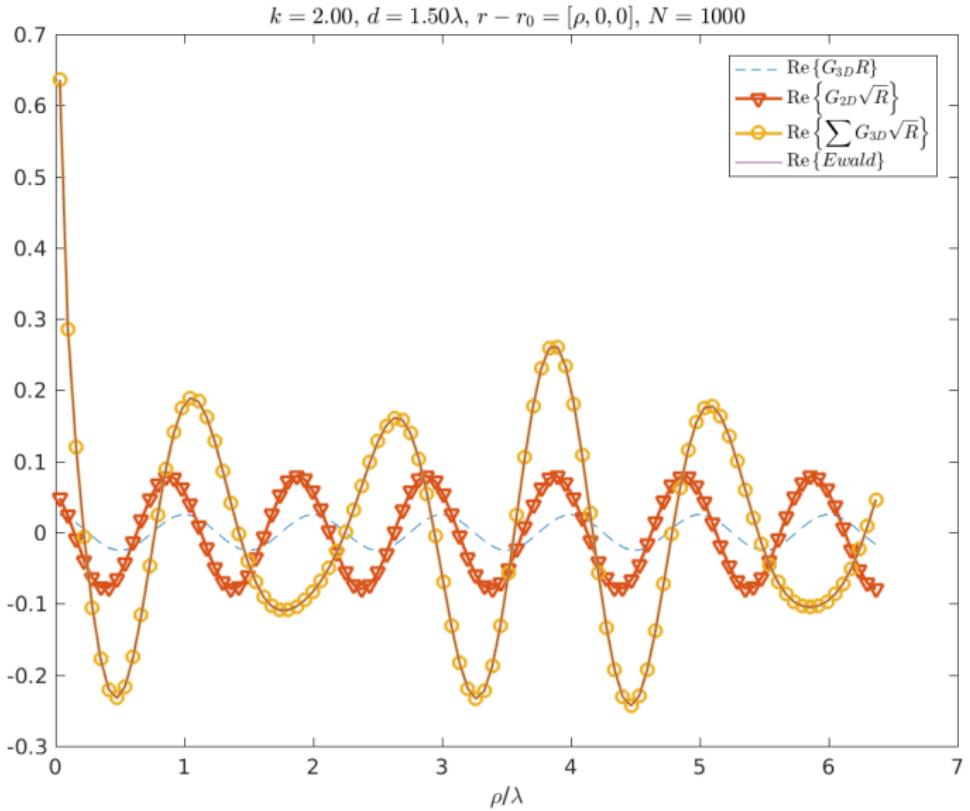
# Checking results (thin slice)



# Checking results (medium slice)

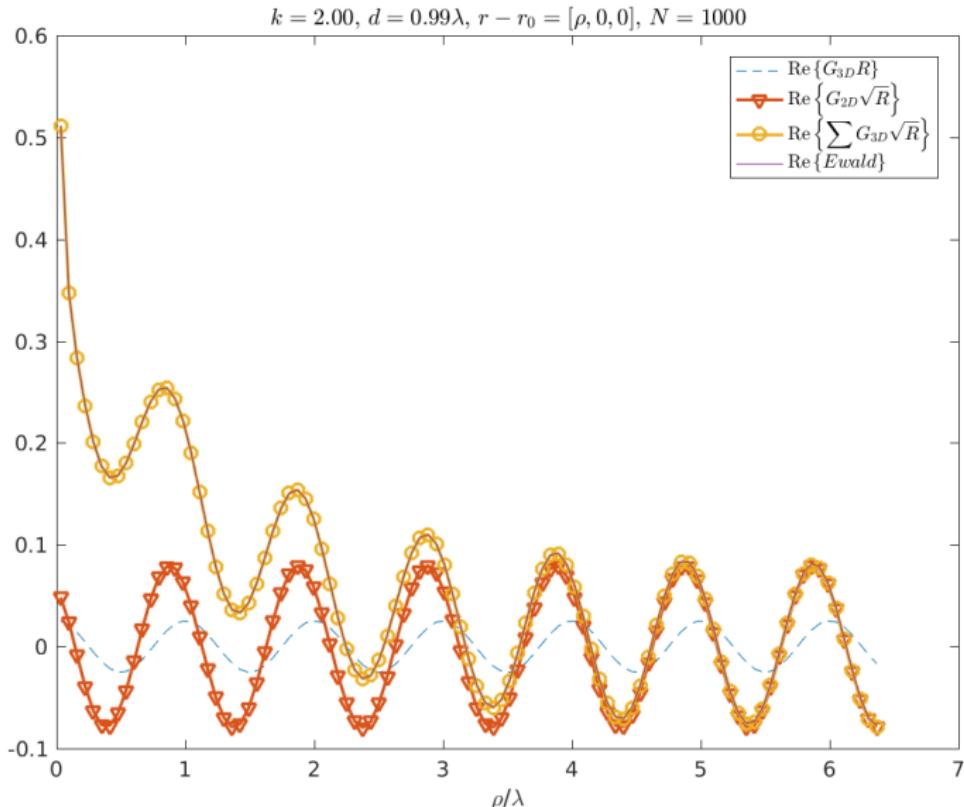


# Checking results (thick slice)



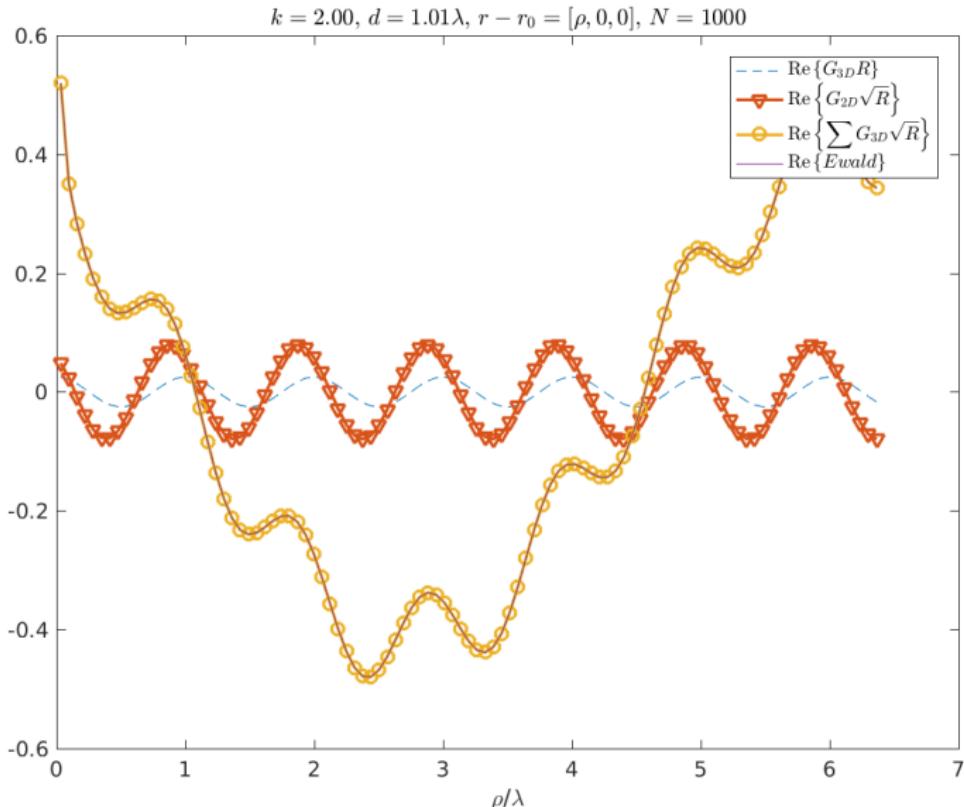
# Checking results (close to transverse Floquet resonance)

$$\alpha_0^2 \simeq 0$$

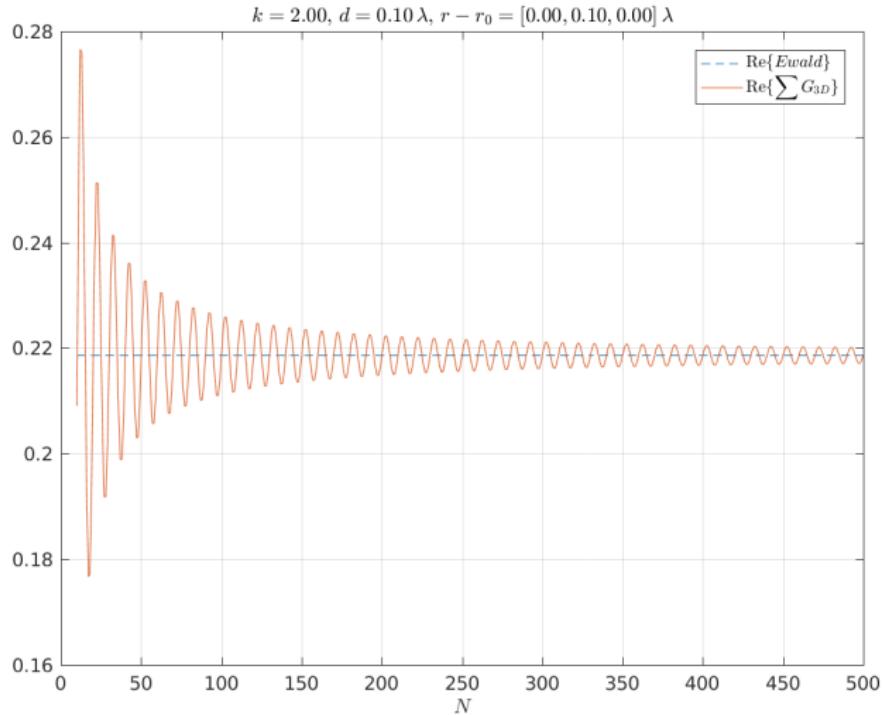


# Checking results (close to transverse Floquet resonance)

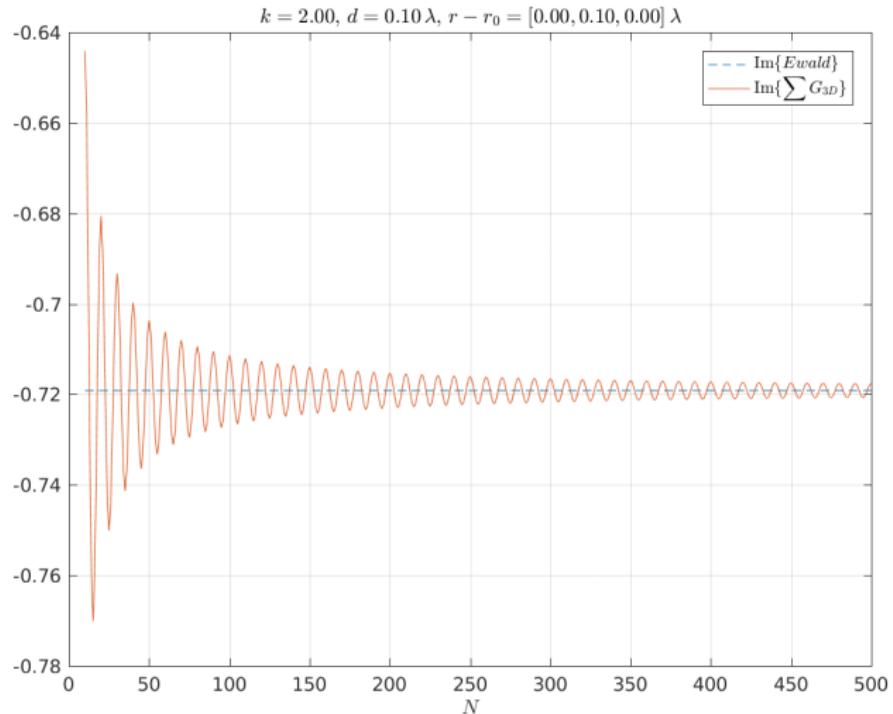
$$\alpha_0^2 \simeq 0$$



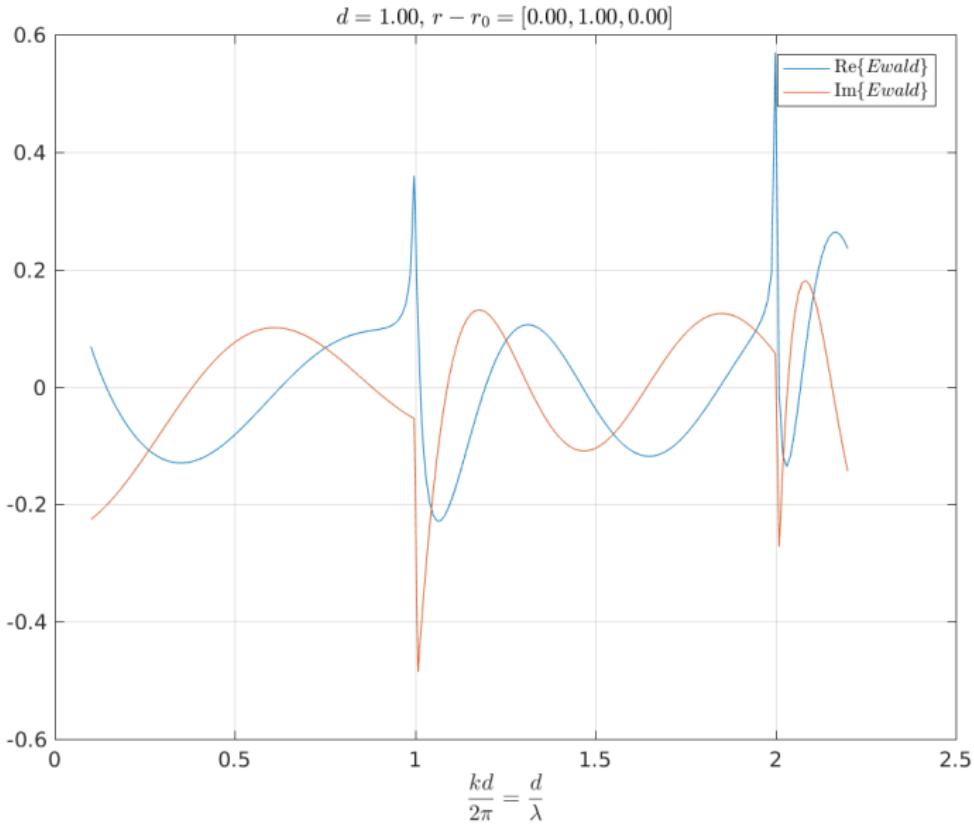
# Convergence of the direct sum



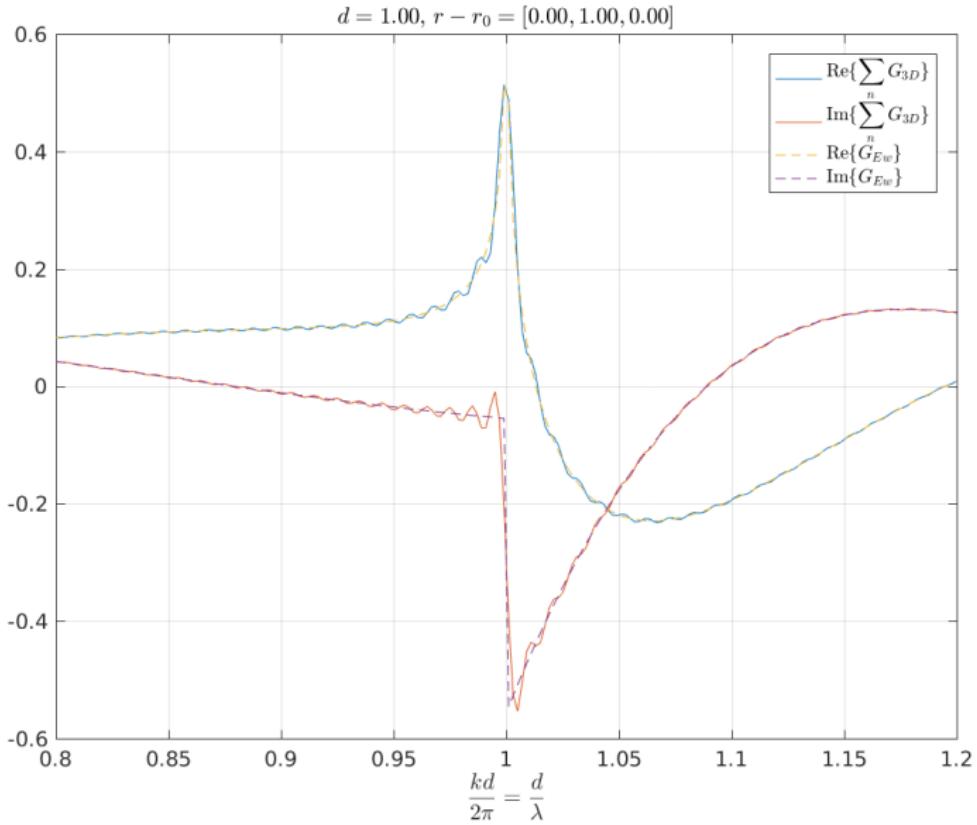
# Convergence of the direct sum (cont.)



# Dependence with frequency



# Singularities when $\alpha_n^2 \rightarrow 0$



## Additional notes

- CPU time cost similar to sum 100 terms of  $G_{3D}$ .
- Matlab prototype.
- Numerical integral may be improved using classic algorithms for calculate exponential integrals (see <sup>2</sup> and <sup>3</sup>) **Done!**: Calculation 10 times faster, but inestable for large values of  $\rho$  ( $\rho > d$ )
- Checked:

$$\int_{-\frac{d}{2}}^{\frac{d}{2}} G_{3D}(\rho, z) dz = G_{2D}(\rho)$$

where  $G_{3D}$  is numerically evaluated with Ewald, and  $G_{2D}$  is the Hankel function:  $\frac{1}{4j} H_0^{(2)}(k|\rho|)$ .

---

<sup>2</sup>F. Capolino *et al.*, "Efficient Computation of the 2-D Green's Function for 1-D Periodic Structures Using the Ewald Method", *IEEE-TAP*, 2005. Equation (23).

<sup>3</sup>F. Capolino *et al.*, "Efficient Computation of the 3D Green's Function with One Dimensional Periodicity Using the Ewald Method", *IEEE-APS*, 2006.

Fortran Module  
EMULATION\_2D\_scattering\_module.F90

# Fortran Module

EMULATION\_2D\_scattering\_module.F90

```
TYPE :: EMULATION_2D_scattering_type
PRIVATE
LOGICAL :: enabled_EMULATION_2D_scattering = &
    DEFAULT_ENABLED_EMULATION_2D_SCATTERING
CHARACTER(len=2) :: green_function_type = DEFAULT_GREEN_FUNCTION_TYPE
LOGICAL :: enabled_normal_incidence = DEFAULT_ENABLED_NORMAL_INCIDENCE
! Thickness (height) of 3D slice used to emulate 2D
REAL(KIND=DBL) :: slice_thickness = DEFAULT_SLICE_THICKNESS
END TYPE EMULATION_2D_scattering_type

PUBLIC :: &
    is_EMULATION_2D_scattering_enabled, &
    enable_EMULATION_2D_scattering, &
    disable_EMULATION_2D_scattering, &
    get_EMULATION_2D_scattering_green_function_type, &
    set_EMULATION_2D_scattering_green_function_type, &
    is_EMULATION_2D_scattering_normal_incidence, &
    enable_EMULATION_2D_scattering_normal_incidence, &
    disable_EMULATION_2D_scattering_normal_incidence, &
    get_EMULATION_2D_scattering_slice_thickness, &
    set_EMULATION_2D_scattering_slice_thickness, &
    EMULATION_2D_scattering_print, &
    EMULATION_2D_scattering_sanitycheck
```

# Fortran Module (cont.)

EMULATION\_2D\_scattering\_module.F90

## Input file .em

```
-----  
-- EMULATION 2D properties      --  
-----  
-- EMULATION 2D activation flag  
EMULATION_2D = true  
-- Set the type of green function used  
EMULATION_2D_green_function_type = "2D"  
-- Activation flag for normal incidence  
EMULATION_2D_normal_incidence = true  
-- Thickness of the slice used as pseudo2D problem  
EMULATION_2D_slice_thickness = 1.0
```

- The case of “normal incidence” is kept as a separate case
  - ▶ It does not require periodic meshes
- Value of “slice thickness” set up manually (desirable to be set automatically, e.g., GUI or HOFEM mesh preprocessing)

# Fortran Module

EMULATION\_2D\_scattering\_module.F90

## Input file .em

```
-----  
--      EMULATION 2D properties      --  
-----  
-- Orientation of the cylinder (axis unit vector)  
EMULATION_2D_cylinder_axis = {0.0,1.0,0.0}
```

- Cylinder axis in arbitrary direction
  - ▶ Cylinder axis is set up manually (desirable to be set automatically, e.g., GUI or HOFEM mesh preprocessing)

# Fortran Module (cont.)

EMULATION\_2D\_scattering\_module.F90

## Input file .em

```
-----  
--      EMULATION 2D properties      --  
-----  
-- Number of incidence angles to be analized  
EMULATION_2D_num_exterior_excitations = 1  
-- Type of plane wave ("Single", "Multiple")  
EMULATION_2D_exterior_type_1 = "Single"  
-- Angle of incidence (with respect to local spherical coordinate  
-- system with z axis along the cylinder axis)  
--   * First number is 'theta' (angle with respect to cylinder axis;  
--     90 corresponds to normal incidence)  
--   * Second number is 'phi' (angle of associated local cylindrical  
--     coordinate system)  
EMULATION_2D_exterior_angle_1 = {90,45}  
-- Polarization (TM or TE)  
EMULATION_2D_polarization_type_1 = "TM"
```

# Fortran Module (cont.)

EMULATION\_2D\_scattering\_module.F90

- Definition of angles for excitations with respect to local spherical coordinate system with z axis along the cylinder axis
  - ▶ Angles are transformed back and forth between local and global axis.
- Definition of polarization as either “TM” or “TE”
  - ▶ Vector components (polarization) are transformed back and forth between local and global axis.

# Fortran Module (cont.)

EMULATION\_2D\_scattering\_module.F90

## Input file farfield\_EMULATION\_2D.conf

```
!- Farfield mode (bistatic,monostatic)
Bistatic
!- Farfield component (|rE-longitudinal|, rE-longitudinal-real, rE-longitudinal-imag, rE-transverse-real, rE-transverse-imag, rE-transverse-imag, RCS-dB, RCS-longitudinal-dB, RCS-transverse-dB, Monostatic-RCS, RCS
!- Frequency index and number of rhs
1 1
!- Rhs index
1
!- Rhs phase
0
!- Rhs amplitude
1
```

# Fortran Module (cont.)

EMULATION\_2D\_scattering\_module.F90

## Input file farfield\_EMULATION\_2D.conf

```
!- Monitor number
1
!- Phi_cyl sampling points (num init stop)
37 0 360
!- RCS units
sigma-lambda
!- Array analysis (flag ,num_elem_u ,num_elem_v)
0 1 1
```

# Fortran Module (cont.)

EMULATION\_2D\_scattering\_module.F90

- Specialization to EMULATION 2D mode
  - ▶ Farfield-mode: only scattering
  - ▶ Farfield-component: “longitudinal” and “transverse” components with respect to cylinder
  - ▶ ...
- Only the angles “phi” need to be defined for the plot (plot associated to the transversal plane to the cylinder (perpendicular to its axis))
- Array analysis: we keep it as it might be of interest to consider finite 1D/2D periodic structures based on pseudo2D cylinders

# Fortran Module

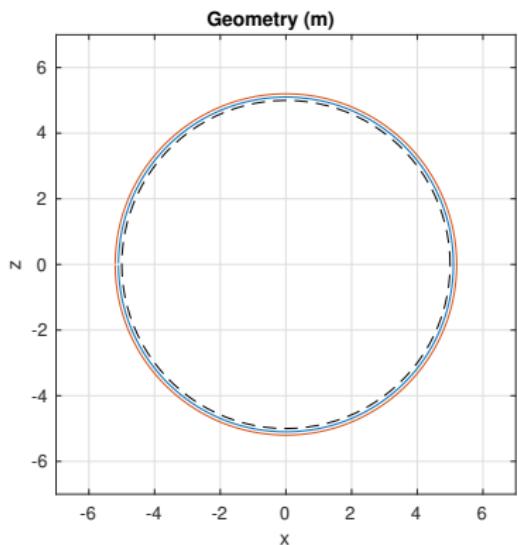
EMULATION\_2D\_scattering\_module.F90 —Update 8 Nov 2022—

- Near field: GreenD derivatives are rewritten in a compact way supporting computation of the scattering near field (within FE-IIEE loop) for arbitrarily oriented cylinders
- Far field: Perfect agreement between numerical and analytical solutions
  - ▶ Well... agreement up to a constant (not worried at all about it)

# Far-field Bistatic RCS calculation

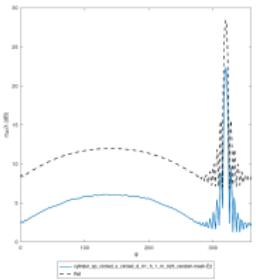
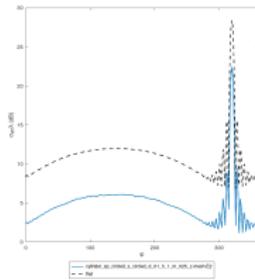
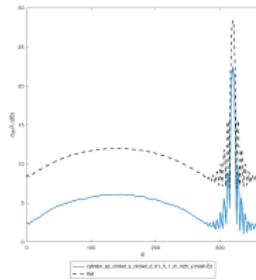
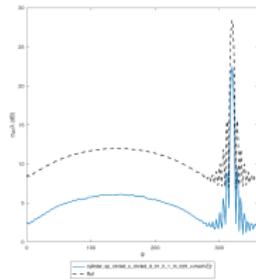
## Reference cases

The same geometry is analyzed with different orientations of the longitudinal axis:

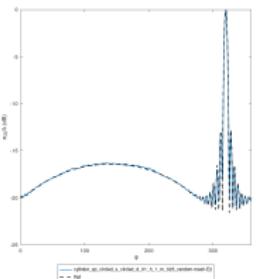
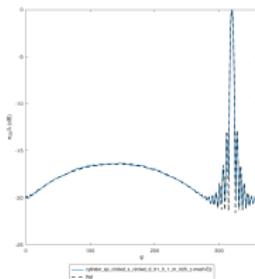
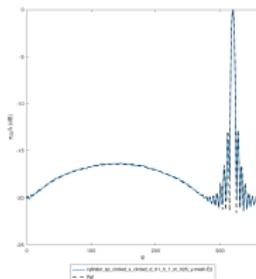
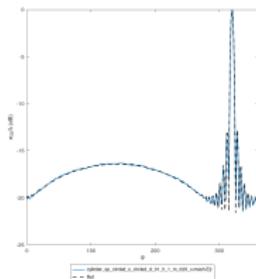


- Normal incidence
- Dashed black line:
- Blue line:  $S'$
- Red line:  $S$
- Different values of permittivity between PEC and  $S'$ :  $\epsilon_r$
- $f = 300 \text{ MHz}$  ( $\lambda = 1 \text{ m}$ , cylinder radius is  $5\lambda$ ).

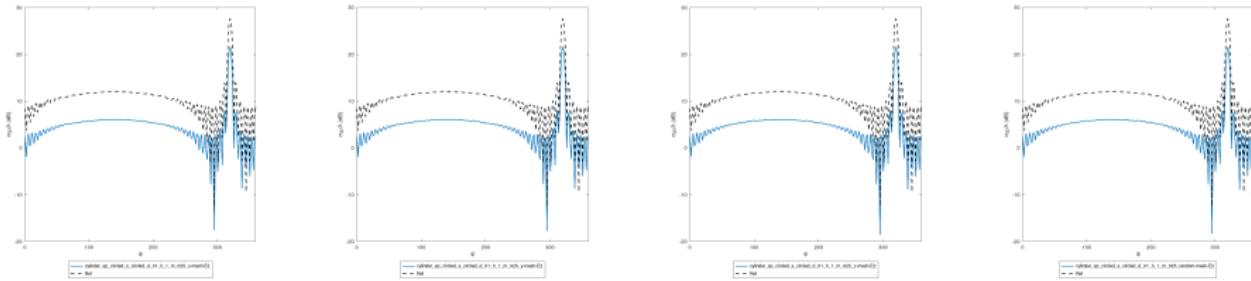
# TM polarization, $\varepsilon_r = 1$ (reference case)



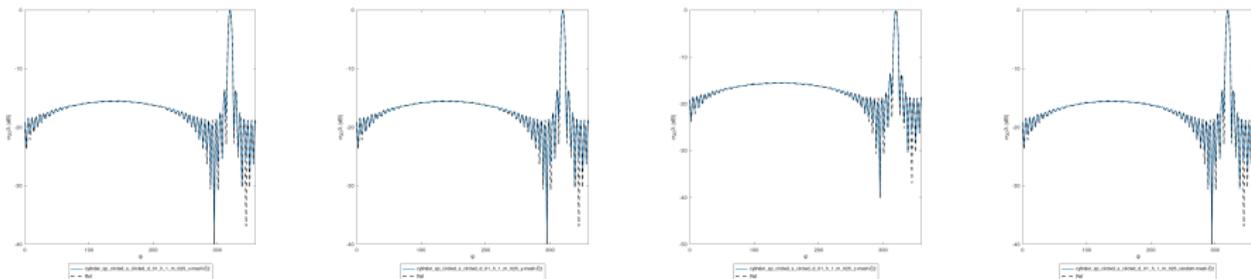
Analytical curves and FEM curves agree except for a constant factor.  
Normalized bistatic-RCS:



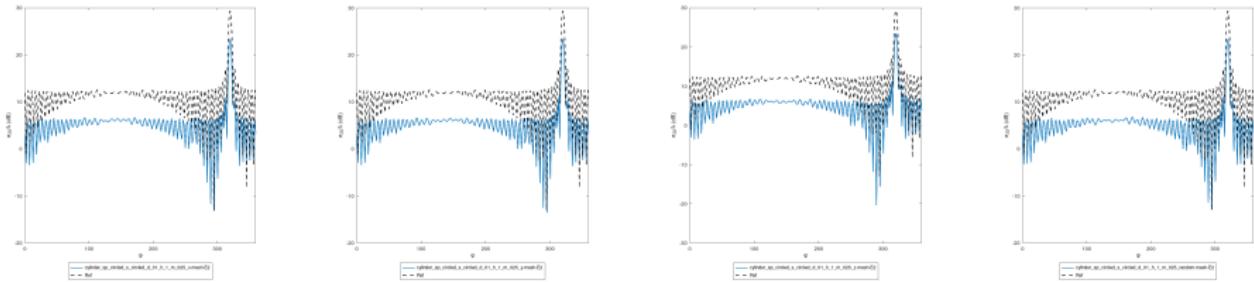
# TE polarization, $\varepsilon_r = 1$



Analytical curves and FEM curves agree except for a constant factor.  
Normalized bistatic-RCS:

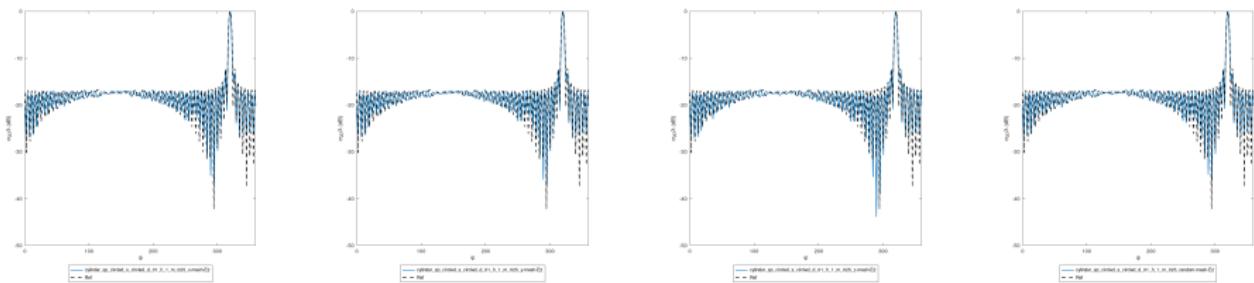


# TM polarization, $\varepsilon_r = 8$

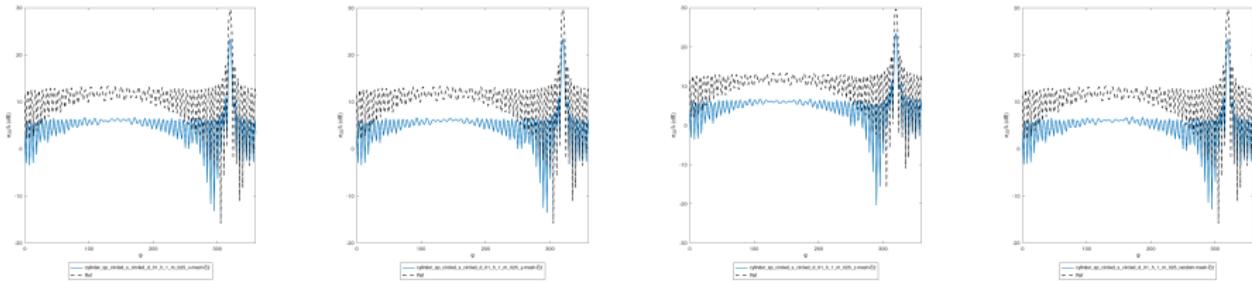


Analytical curves and FEM curves agree (minor discrepancies) except for a constant factor.

Normalized bistatic-RCS:

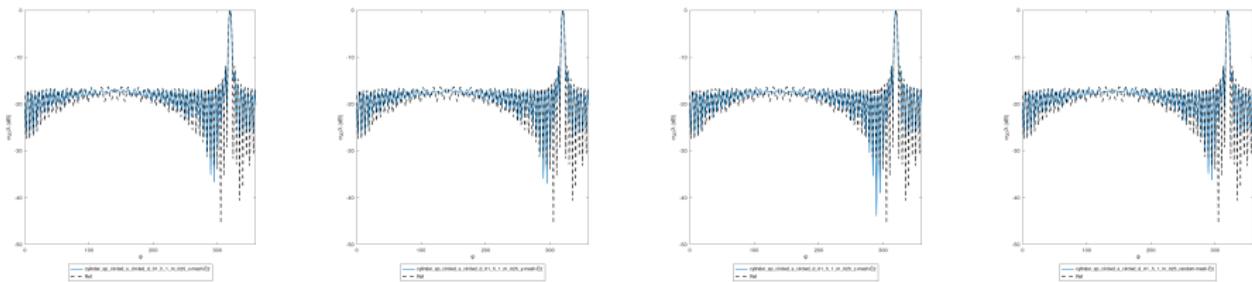


# TE polarization, $\varepsilon_r = 2$

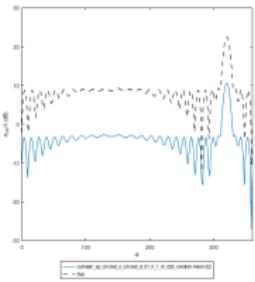
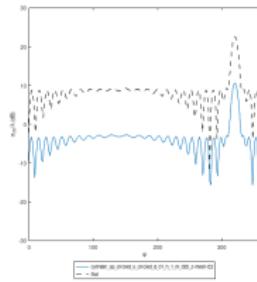
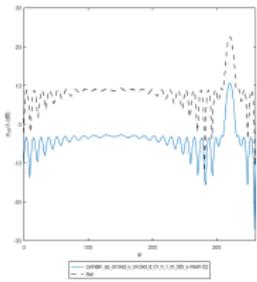
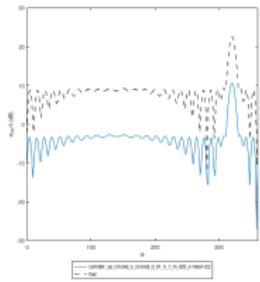


Analytical curves and FEM curves agree (some discrepancies) except for a constant factor.

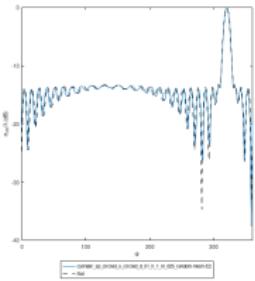
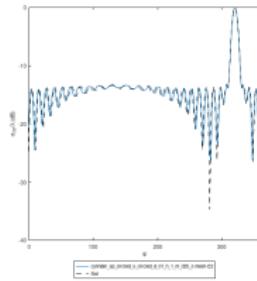
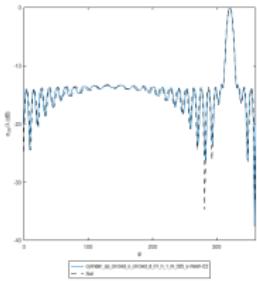
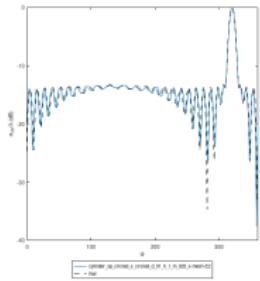
Normalized bistatic-RCS:



# TE polarization, $\epsilon_r = 2$ , $f = 150$ MHz



For a smaller problem (same mesh, double wavelength), almost full agree.  
Normalized bistatic-RCS:

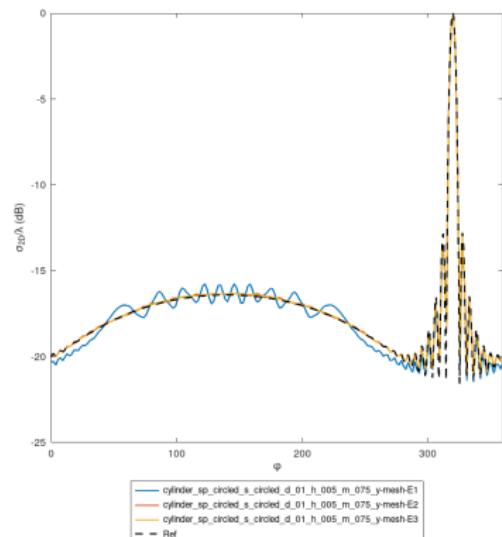
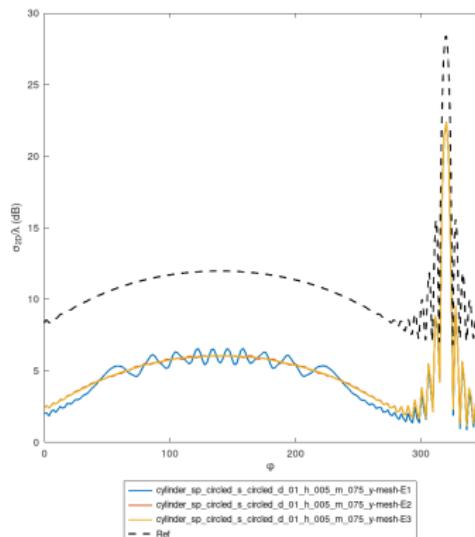


# Effect of IIEE iterative method in Far Field

TM polarization,  $\varepsilon_r = 1$ , (reference case)

Results for the following residual errors:

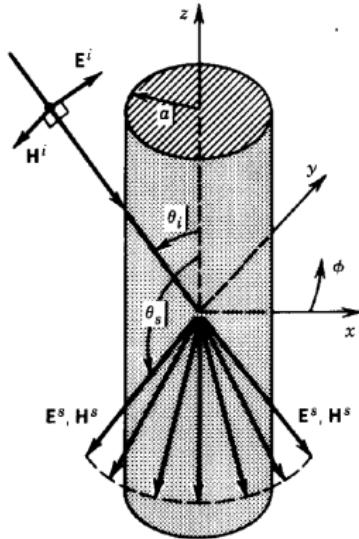
- M1:  $10^{-1}$  (blue)
- M2:  $10^{-2}$  (red)
- M3:  $10^{-3}$  (orange)



Note: Orange and red lines overlap.

Until now we were considering normal incidence to the cylinder  
Now we consider the extension to case of "Oblique Incidence"

# Oblique Incidence

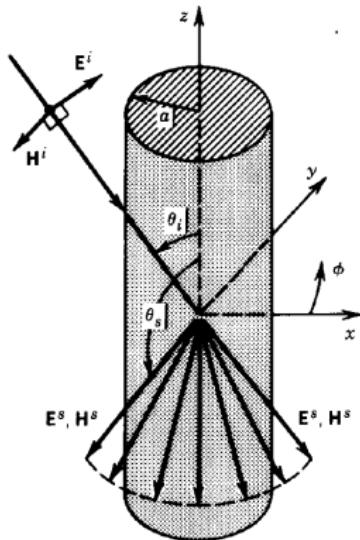


## Green Function

$$G = \int_{-\infty}^{\infty} \frac{e^{-jk\sqrt{\rho^2+z^2}}}{4\pi\sqrt{\rho^2+z^2}} e^{\pm j\beta_z z} dz$$
$$= \begin{cases} \frac{1}{4j} H_0^{(2)} \left( \rho \sqrt{k^2 - \beta_z^2} \right) & k^2 > \beta_z^2 \\ \frac{1}{2\pi} K_0^{(2)} \left( \rho \sqrt{k^2 - \beta_z^2} \right) & \beta_z^2 > k^2 \end{cases}$$

where  $\beta_z^2 = k^2 \cos^2 \theta_i < k^2$

# Oblique Incidence (cont.)



## Green Function

- For any  $\theta_i$  we have

$$G = \frac{1}{4j} H_0^{(2)} \left( \rho \sqrt{k^2 - \beta_z^2} \right) = \frac{1}{4j} H_0^{(2)} (k|\rho| \sin \theta_i)$$

where  $\beta_z^2 = k^2 \cos^2 \theta_i < k^2$

- The particularization to  $\theta_i = 90^\circ$  (normal incidence) yields to the well known result

$$G = \frac{1}{4j} H_0^{(2)} (k|\rho|)$$

# Oblique Incidence (cont.)

## FE-IIEE loop

- As in the case of normal incidence

- We use Green2D<sup>a</sup> on the whole 3D slice and we divide the scattered field at each target point by the “slice thickness”
- We work with  $\rho$  instead of  $r$ , i.e.,

$$|\rho - \rho'| = |(\mathbf{r} - \mathbf{r}') - ((\mathbf{r} - \mathbf{r}') \cdot \hat{\mathbf{z}})\hat{\mathbf{z}}|$$

where  $\hat{\mathbf{z}}$  stands for the direction along the cylinder axis<sup>b</sup>

- The  $z$ -dependence of the solution (including the scattering field) must be as

$$\mathbf{E}, \mathbf{H} \propto e^{jk \cos \theta_i z} = e^{-jk \cos \theta_s z}$$

Note that  $\beta_z = k \cos \theta_i = -k \cos \theta_s > 0$

<sup>a</sup>We may also use Green3D\_Ewald1D

<sup>b</sup>The code supports arbitrary orientations for the cylinder

# Oblique Incidence (cont.)

## FE-IIEE loop (cont.)

- Thus, for oblique incidence we need to take into account the relative “height” between  $\mathbf{r}$  and  $\mathbf{r}'$
- That is, we need to add a factor to the 2D Green function when summing up the contributions on given integration target points of “height”  $\mathbf{r} \cdot \hat{\mathbf{z}}$  from different integration point sources of “height”  $\mathbf{r}' \cdot \hat{\mathbf{z}}$ .

The factor is

$$e^{+jk \cos \theta_i (\mathbf{r} - \mathbf{r}') \cdot \hat{\mathbf{z}}} = e^{-jk \cos \theta_s (\mathbf{r} - \mathbf{r}') \cdot \hat{\mathbf{z}}}$$

or equivalently

$$e^{-jk \cos \theta_i (\mathbf{r}' - \mathbf{r}) \cdot \hat{\mathbf{z}}} = e^{+jk \cos \theta_s (\mathbf{r}' - \mathbf{r}) \cdot \hat{\mathbf{z}}}$$

# Oblique Incidence (cont.)

In other words,

$$G(|\mathbf{r} - \mathbf{r}'|) = \frac{1}{4j} H_0^{(2)}(k|\boldsymbol{\rho} - \boldsymbol{\rho}'| \sin \theta_i) e^{-jk \cos \theta_i |z - z'|}$$

Remarks:

- Symbol  $\hat{\mathbf{z}}$  stands for the direction along the cylinder axis
- The code supports arbitrary orientations for the cylinder
- Implementation status:
  - ▶ Coded
  - ▶ Not tested for oblique cylinder yet (requires PBCs)

# Oblique Incidence (cont.)

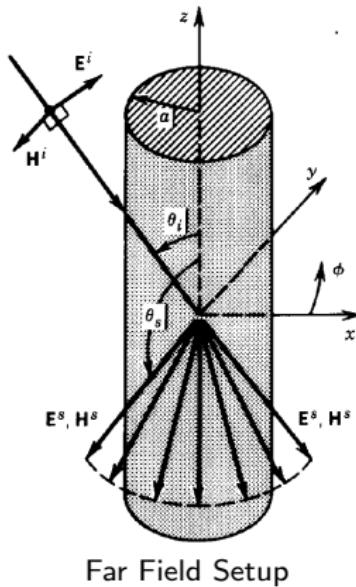
A remark on dielectric (and dielectric coated PEC) cylinders...

## Dielectric cylinders (also dielectric coated PEC)

- TM and TE are not longer solutions (**polarizations are coupled**) for oblique incidence
- In the limit, with angle tending to normal incidence, the polarizations are effectively decoupled
- Analogously, TM and TE coupling appears also when using IBC (even isotropic case) for oblique incidence

# Oblique Incidence

Far Field —Update 8 Nov 2022—



## Far Field

- Green's function

$$G_{\text{far}} \propto e^{+jk\rho \sin \theta_i} \underbrace{e^{-jk \cos \theta_i z}}_{F_{1z}(z)}$$

- Potential, fields

$$\text{Potentials, fields} \propto F_{2\phi}(k, \phi, \sin \theta_i) F_{2\theta}(\theta)$$

where

$$F_{2\theta}(\theta) = \int_{-\infty}^{\infty} F_{1z}(z) e^{+jk \cos \theta z} = \delta(\theta - (\pi - \theta_i))$$

Using far field version of Green2D on a 3D slice can be used to calculate  $F_{2\phi}$  (the variation with  $\phi$  of the scattering field: RCS, scattering width)

# Oblique Incidence (cont.)

Far Field —Update 8 Nov 2022—

More precisely...

- Green's Function

$$G_{\text{far}} = \frac{1}{4j} H_0^{(2)}(k\rho \sin \theta_i) \Big|_{k\rho \rightarrow \infty} \approx \sqrt{\frac{2j}{\pi \rho \sin \theta_i}} e^{-jk\rho \sin \theta_i}$$

# Oblique Incidence (cont.)

Far Field —Update 8 Nov 2022—

## Far Field Computation using 3D Slice

- We use Green2D on the whole 3D slice and we divide the scattered field at each target point by the “slice thickness”
- We need to take into account the  $z$ -dependence of the 3D (FEM) solution, i.e.,

$$\mathbf{E}, \mathbf{H} \propto e^{jk \cos \theta_i z}$$

# Oblique Incidence (cont.)

Far Field —Update 8 Nov 2022—

## Far Field Algorithm:

- ① We start from  $\mathbf{J}$ ,  $\mathbf{M}$  on  $S'$
- ② We “equalize”  $\mathbf{J}$ ,  $\mathbf{M}$  on  $z$ -dependence<sup>4</sup>

$$\mathbf{J} = \mathbf{J} e^{-jk \cos \theta_i z}$$

$$\mathbf{M} = \mathbf{M} e^{-jk \cos \theta_i z}$$

- ③ We transform  $\mathbf{J}$ ,  $\mathbf{M}$  to spherical coordinates on local coordinate system attached to the cylinder

$$\mathbf{J} \rightarrow (J_\theta, J_\phi)$$

$$\mathbf{M} \rightarrow (M_\theta, M_\phi)$$

- ▶ Note that for normal incidence the local  $\theta, \phi$  components are longitudinal  $J_z$ ,  $M_z$  and transverse  $J_\phi$ ,  $M_\phi$  components, respectively

# Oblique Incidence (cont.)

Far Field —Update 8 Nov 2022—

- ④ We compute vector potentials  $A_\theta, A_\phi, F_\theta, F_\phi$

$$\begin{array}{ll} J_\theta \rightarrow A_\theta & M_\theta \rightarrow F_\theta \\ J_\phi \rightarrow A_\phi & M_\phi \rightarrow F_\phi \end{array}$$

- ⑤ and from vector potentials we compute the far field components

$$(A_\theta, A_\phi, F_\theta, F_\phi) \rightarrow (E_\theta, E_\phi, H_\theta, H_\phi)$$

- ⑥ We do not forget to divide by “slice thickness”

$$(E_\theta, E_\phi, H_\theta, H_\phi) \rightarrow (E_\theta, E_\phi, H_\theta, H_\phi) / \text{“slice thickness”}$$

- ⑦ Due to decomposition of currents in **local**  $\theta$  and  $\phi$  components, we can naturally obtain the TM and TE components, i.e.,

$$\begin{array}{l} (E_\theta, H_\phi) \rightarrow \text{TM} \\ (E_\phi, H_\theta) \rightarrow \text{TE} \end{array}$$

# Oblique Incidence (cont.)

Far Field —Update 8 Nov 2022—

## Scattering Width $\sigma$

$$\boldsymbol{\sigma} = \begin{bmatrix} \sigma_{(TM,TM)} & \sigma_{(TM,TE)} \\ \sigma_{(TE,TM)} & \sigma_{(TE,TE)} \end{bmatrix}$$

- Note that for PEC cylinders we have  $\sigma_{(TM,TE)} = \sigma_{(TE,TM)} = 0$
- Implementation status:
  - ▶ Coded
  - ▶ Not tested for oblique cylinder yet (requires PBCs)

<sup>4</sup>The “equalization” can alternatively be applied on the Greens’s Function

# Integration EMULATION\_2D and PBCs

## Far Field

### Logic for Oblique Incidence —In progress (barely initiated)—

- cylinder\_axis and slice\_thickness obtained from PBC module
- Angle of incidence set up in file .em
  - ▶ Discard PBC info in file .em: periodic\_phi\_angle, periodic\_theta\_angle
  - ▶ PBC ← EMULATION\_2D info from file
    - ★ Example: EMULATION\_2D\_exterior\_angles\_1 = {45,140}
- Normal incidence can be run as a particular case
- If enabled\_normal\_incidence there is no PBC interaction (coded and working)
  - ▶ cylinder\_axis and slice\_thickness read from file .em<sup>5</sup>
  - ▶ Angle of incidence set up in file .em:
    - ★ Example: EMULATION\_2D\_exterior\_angles\_1 = {90,140}

<sup>5</sup>Nevertheless, that information could be obtained by preprocessing the mesh within HOFEM code (extra task, not considered at present)

Modifications relative to postprocessing (near field)

# Postprocessing changes

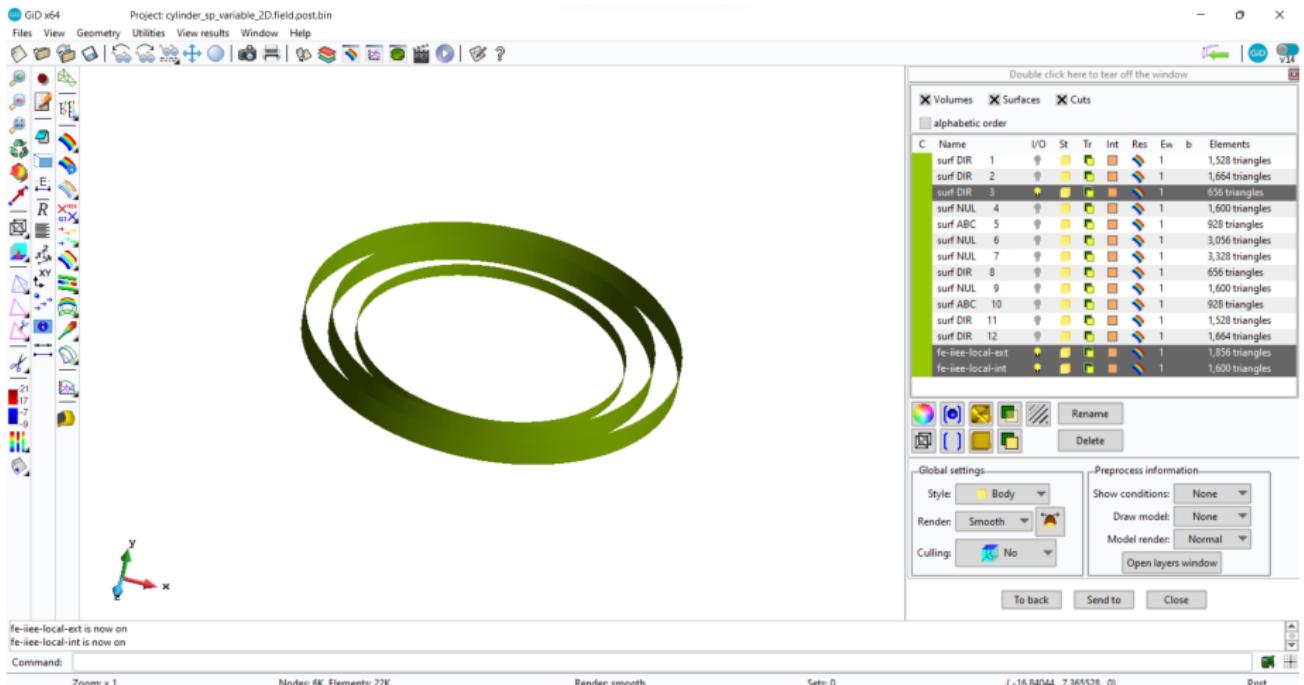
Extra information in nearfield

## Changes in nearfield postprocessing

- Added a 3-character string after `surf` to denote the kind of boundary condition that surface is (DIR, NEU, NUL, ABC, ...)
- Added to the surface set the surfaces involved in FE-IIEE method, denoted as `fe-iiee-local-ext`, and `fe-iiee-local-int`, corresponding to  $S$  and  $S'$  surfaces respectively.

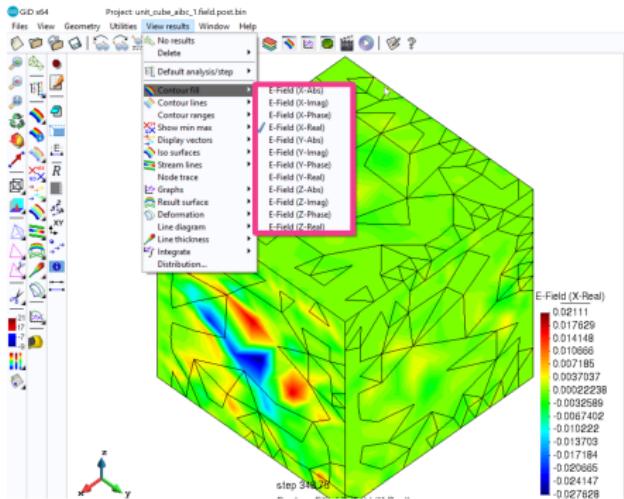
# Postprocessing changes (cont.)

Extra information in nearfield



# Postprocessing changes

Extra information in nearfield



- Included a new option to get all the available results for the near field.
- Implemented as a new option called **all-xyz**.

MPI related issues

# EMULATION\_2D MPI Broadcast

- From FREQ-SWEEP to POST-MODE we write and read from disk

## Write to Disk

```
SUBROUTINE write_EMULATION_2D_data_structure(filename)

CHARACTER(LEN=*) , INTENT(IN) :: filename
INTEGER:: ierror,fileunit

OPEN(NEWUNIT=fileunit , FILE=filename , STATUS="REPLACE" ,  &
      ACTION="WRITE" , FORM="UNFORMATTED" , IOSTAT=ierror)
IF (ierror /= 0) THEN
    CHKERRQ(ierror , 'write_EMULATION_2D_data_structure: &
                           Error opening file')
ENDIF
WRITE(fileunit , IOSTAT=ierror)   &
    EMULATION_2D_scattering_structure

CLOSE(fileunit)

END SUBROUTINE write_EMULATION_2D_data_structure
```

# EMULATION\_2D MPI Broadcast (cont.)

## Read from Disk

```
SUBROUTINE read_EMULATION_2D_data_structure(filename)

CHARACTER(LEN=*) , INTENT(IN) :: filename
INTEGER:: ierror,fileunit

OPEN(NEWUNIT=fileunit, FILE=filename, STATUS="OLD", &
      ACTION="READ", FORM="UNFORMATTED", IOSTAT=ierror)
IF (ierror /= 0) THEN
    CHKERRQ(ierror, 'read_EMULATION_2D_data_structure: Error &
                      opening file')
ENDIF
READ(fileunit, IOSTAT=ierror)   &
    EMULATION_2D_scattering_structure

CLOSE(fileunit)

END SUBROUTINE read_EMULATION_2D_data_structure
```

# EMULATION\_2D MPI Broadcast (cont.)

- MPI communication between processes within POST-MODE
  - ▶ At present it is simply by all MPI processes reading the EMULATION\_2D data structure from disk (and not only process 0)
  - ▶ **Use of custom MPI datatypes** (simple prototype under test at present)
    - ★ One MPI call: low latency, readability of the code
    - ★ Maintainability of the code: routines defined on each module to create MPI datatype associated to each derived datatype.

# EMULATION\_2D MPI Broadcast (cont.)

## Fortran Derived DataType

```
! Derived type to test MPI_Type_create_struct
TYPE :: my_derived_type_def
  LOGICAL :: mylogical = .TRUE.
  CHARACTER(len=4) :: mystring = 'hola'
  REAL(KIND=DBL) :: myreal = 1.0_DBL
END TYPE my_derived_type_def

TYPE(my_derived_type_def) :: my_derived_type
```

# EMULATION\_2D MPI Broadcast (cont.)

## MPI datatype creation (MPI\_Type\_create\_struct) (cont.)

```
!! Creamos el MPI Datatype que se use para pasar el tipo &
derivado
!! entre procesos MPI

CALL MPI_GET_ADDRESS(my_derived_type,address(1), ierror)
CALL MPI_GET_ADDRESS(my_derived_type%mylogical,address(2), &
ierror)
CALL MPI_GET_ADDRESS(my_derived_type%mystring,address(3), &
ierror)
CALL MPI_GET_ADDRESS(my_derived_type%myreal,address(4), ierror)

DO i=1,COUNT
    ! MPI-3.0 & former: disp = iaddr(i+1)-iaddr(i)
    displacements(i) = MPI_Aint_diff(address(i+1),address(i))
ENDDO

typelist(1) = MPI_LOGICAL
typelist(2) = MPI_CHARACTER
typelist(3) = MPI_DOUBLE_PRECISION
```

# EMULATION\_2D MPI Broadcast (cont.)

## MPI datatype creation (MPI\_Type\_create\_struct) (cont.)

```
block_lengths(1)=1
block_lengths(2)=4
block_lengths(3)=1

! build the derived data type
call MPI_Type_create_struct(COUNT,block_lengths,displacements,&
    typelist, my_mpi_derived_type_def,ierr)
if (ierr /= 0 ) then
    print *, 'got an error in type create:', ierr
    call MPI_Abort(MPI_COMM_WORLD, ierr, ierr)
endif
```

# EMULATION\_2D MPI Broadcast (cont.)

## Use of MPI datatype in MPI calls

```
! commit it to the system, so it knows we'll use it
! for communication
call MPI_TYPE_COMMIT(my_mpi_derived_type_def)
if (ierr /= 0) then
    print *, 'got an error in type commit:', ierr
    call MPI_Abort(MPI_COMM_WORLD, ierr, ierr)
endif

! use it
call &
MPI_BCAST(my_derived_type, 1, my_mpi_derived_type_def, 0, MPI_COMM_
```

## Free MPI datatype created

```
! We free the MPI Datatype created
call MPI_TYPE_FREE(my_mpi_derived_type_def, ierr)
```

# MPI Fortran interfaces

## USE mpi\_f08

```
USE mpi_f08
!! It requires compile-time argument checking with unique MPI
!! handle types and provides techniques to fully solve the
!! optimization problems with nonblocking calls. This is the &
!! only
!! Fortran support method that is consistent with the Fortran
!! standard (Fortran 2008 + TS 29113 and later). This method is
!! highly recommended for all MPI applications.
```

## USE mpi

```
USE mpi
!! It requires compile-time argument checking. Handles are &
!! defined
!! as INTEGER. This Fortran support method is inconsistent &
!! with the
!! Fortran standard, and its use is therefore not recommended.
```

# MPI Fortran interfaces (cont.)

## INCLUDE 'mpif.h'

```
INCLUDE 'mpif.h'  
!! The use of the include file mpif.h is strongly discouraged  
!! starting with MPI-3.0, because this method neither &  
guarantees  
!! compile-time argument checking nor provides sufficient  
!! techniques to solve the optimization problems with &  
nonblocking  
!! calls, and is therefore inconsistent with the Fortran &  
standard.
```