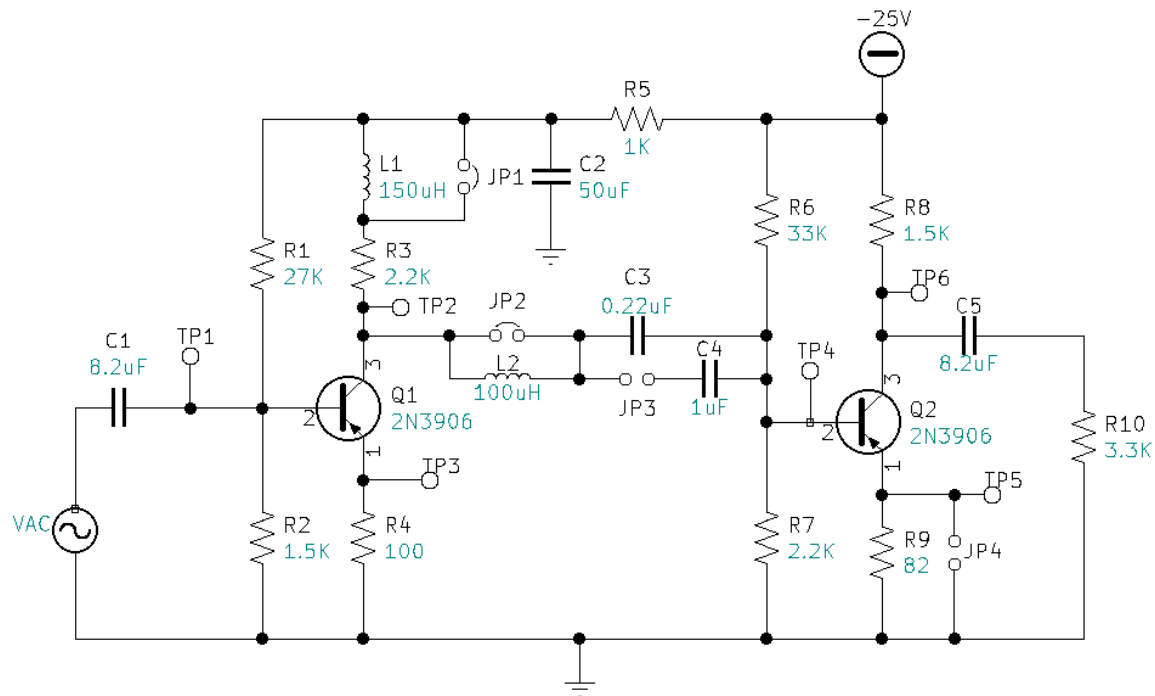
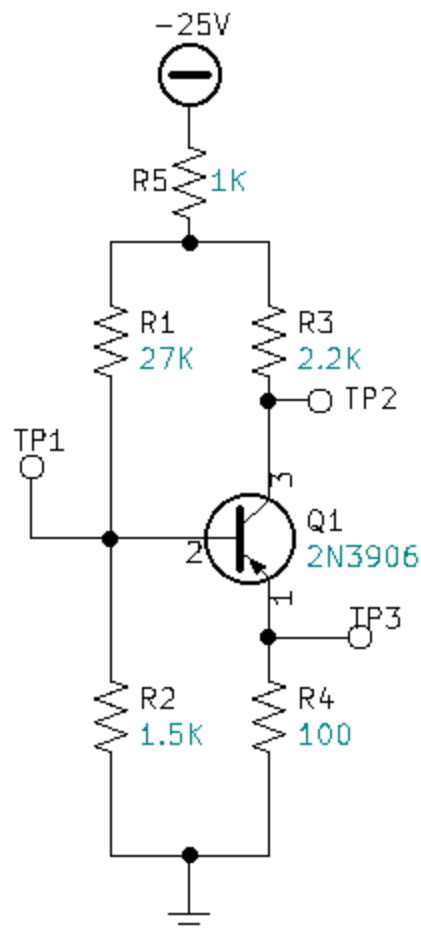


Consider the following circuit:



NOTE: On the 2-stage schematic, $V_{CC}=25V$. There is a jumper on JP1 and JP2. No Jumper on JP3 and JP4.

DC Redraw for Stage 1:



DC Calculations for Stage 1:

Kirchhoff Loop Equation 1:

- $V_{CC} - V_{R5} - V_{R1} - V_{BE} - V_{RE} = 0$
- $I_{R5}(1K) + I_{R1}(27K) + I_E(82) = 24.3V$

Kirchhoff Loop Equation 2:

- $V_{CC} - V_{R5} - V_{R1} - V_{R2} = 0$
- $I_{R5}(1K) + I_{R1}(27K) + I_{R2}(1.5K) = 25V$

Kirchhoff's Current Law:

- $I_{R5} = I_{R1} + I_{CQ1}$
- $I_{R2} = I_{R1} - I_{BQ1}$

Substitute Currents:

- $(I_{R1} + I_{CQ1})(1K) + I_{R1}(27K) + I_E(100) = 24.3V$
- $(I_{R1} + I_{CQ1})(1K) + I_{R1}(27K) + (I_{R1} - I_{BQ1})(1.5K) = 25V$

Manipulate into terms of I_{R1} and I_B :

- $(I_{R1} + (I_B \times B))(1K) + I_{R1}(27K) + (I_B \times (B + 1))(100) = 24.3V$
- $(I_{R1} + (I_B \times B))(1K) + I_{R1}(27K) + (I_{R1} - I_B)(1.5K) = 25V$

Beta = 100:

- $(I_{R1} + (I_B \times 100))(1K) + I_{R1}(27K) + (I_B \times (100 + 1))(100) = 24.3V$
- $(I_{R1} + (I_B \times 100))(1K) + I_{R1}(27K) + (I_{R1} - I_B)(1.5K) = 25V$

Simplify:

- $(1K I_{R1} + (100K I_B) + I_{R1}(27K) + (10.1K I_B) = 24.3V$
- $(1K I_{R1} + (100K I_B) + I_{R1}(27K) + (1.5K I_{R1} - 1.5K I_B) = 25V$

Simplify:

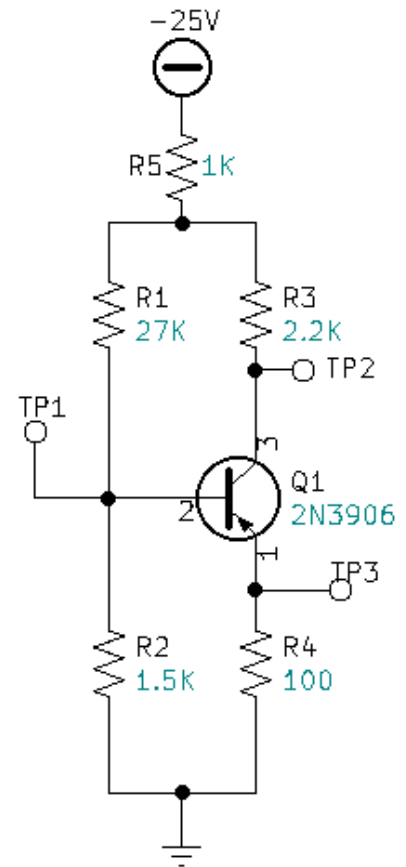
- $28KIR_1 + 110.1KIB = 24.3V$
- $29.5KIR_1 + 98.5KIB = 25V$

Simultaneous Equation Solution:

- $IR_1 = 732.626\mu A$
- $IB = 34.391\mu A$

DC/Bias Voltages:

- $VR_1 = IR_1 \times R_1$
 - $VR_1 = 732.626\mu A \times 27K$
 - $VR_1 = 19.78V$
- $VR_2 = IR_2 \times R_2$
 - $VR_2 = (IR_1 - IB) \times R_2$
 - $VR_2 = (732.626\mu A - 34.391\mu A) \times 1.5K$
 - $VR_2 = 1.047V$
- $VR_4 = (IBX(B + 1)) \times R_4$
 - $VR_4 = (34.391\mu A \times (101)) \times 100$
 - $VR_4 = 347.349mV$
- $VR_3 = (IBX(B)) \times R_3$
 - $VR_3 = (34.391\mu A \times (100)) \times 2.2K$
 - $VR_3 = 7.566V$
- $VR_5 = (IBX(B) + IR_1) \times R_5$
 - $VR_5 = (34.391\mu A \times (100) + 732.626\mu A) \times 1K$
 - $VR_5 = 4.172V$



Kirchhoff, check math:

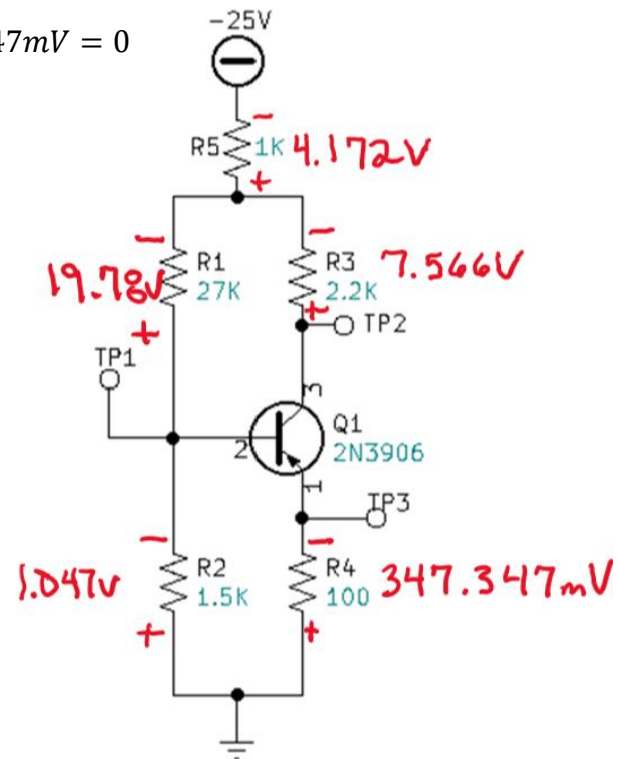
- $+25V - 4.172V - 19.78V - 1.047V = 0$
- $\boxed{0} = 0$

Find VCE:

- $+VCC - VR5 - VR3 - VCE - VR4 = 0$
- $+25V - 4.172V - 7.566 - VCE - 347.347mV = 0$
- $+13.142V - VCE = 0$
- $VCE = 13.142V$

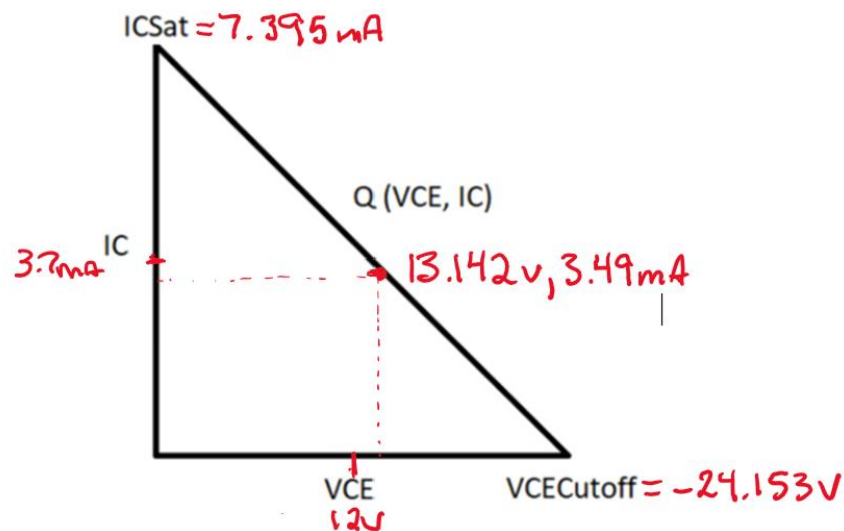
Test Point Voltages:

- $TP1 = VR2$
 - $TP1 = -1.047V$
- $TP2 = VCE + VR4$
 - $TP2 = -13.142V - 347.347mV$
 - $TP2 = -13.489V$
- $TP3 = VR4$
 - $TP3 = -347.347mV$

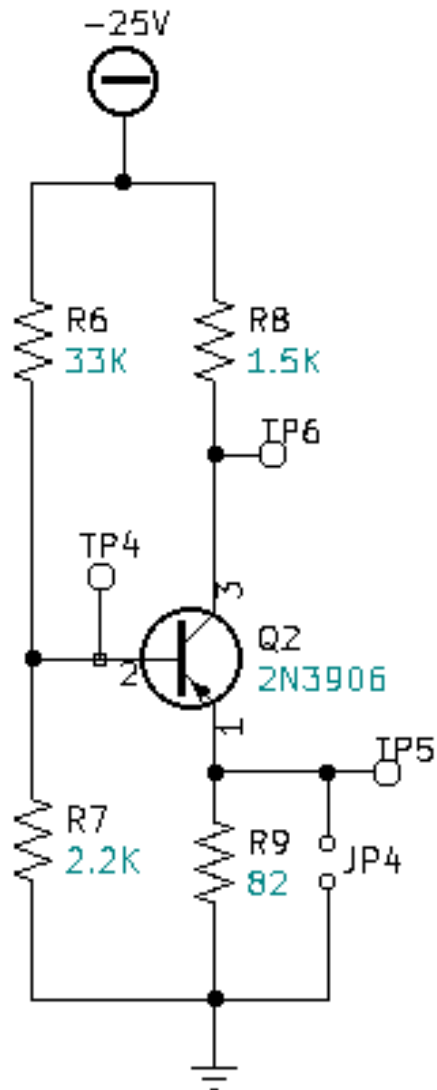


DC Load Line for Q1:

- $V_{CE_{Cutoff}} = \frac{V_{CC}}{R_5 + R_1 + R_2} (R_2 + R_3)$
 - $V_{CE_{Cutoff}} = \frac{25}{29.5K} (28.5K)$
 - $V_{CE_{Cutoff}} = 24.153V$
- $I_{C_{Saturation}} = \frac{V_{CC} - [\frac{V_{CC}}{R_5 + (R_C + R_E) // (R_1 + R_2)}] (R_5)}{R_C + R_E}$
 - $I_{C_{Saturation}} = \frac{25 - [\frac{25}{1K + (2.2K + 100) // (28.5K)}] (1K)}{2.2K + 100}$
 - $I_{C_{Saturation}} = \frac{25 - [\frac{25}{1K + (2.128K)}] (1K)}{2.3K}$
 - $I_{C_{Saturation}} = \frac{25 - [\frac{25}{(3.128K)}] (1K)}{2.3K}$
 - $I_{C_{Saturation}} = \frac{25 - 7.99233}{2.3K}$
 - $I_{C_{Saturation}} = 7.395mA$



DC Redraw for Stage 2:



DC Calculations for Stage 2:

Kirchhoff Loop Equation 1:

- $V_{CC} - V_{R6} - V_{R7} = 0$

Kirchhoff Loop Equation 2:

- $V_{CC} - V_{R6} - V_{BE} - V_{R9} = 0$

Substitute Currents & known values:

- $25V - 33K(IR_6) - 2.2K(IR_7) = 0$
- $25V - 33K(IR_6) - 0.7V - 82(IR_9) = 0$

Substitute Currents in terms of I_{R6} & I_B :

- $25V - 33K(IR_6) - 2.2K(IR_6 - I_B) = 0$
- $25V - 33K(IR_6) - 0.7V - 82(I_B(B + 1)) = 0$

Simplify:

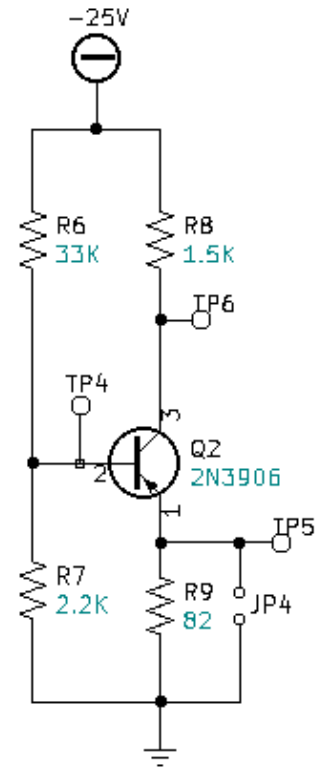
- $25V - 33K(IR_6) - 2.2KIR_6 + 2.2K(I_B) = 0$
- $25V - 33K(IR_6) - 0.7V - 82(I_B(101)) = 0$

Simplify:

- $35.2K(IR_6) - 2.2K(I_B) = 25V$
- $33K(IR_6) + 8.282K(I_B) = 24.3$

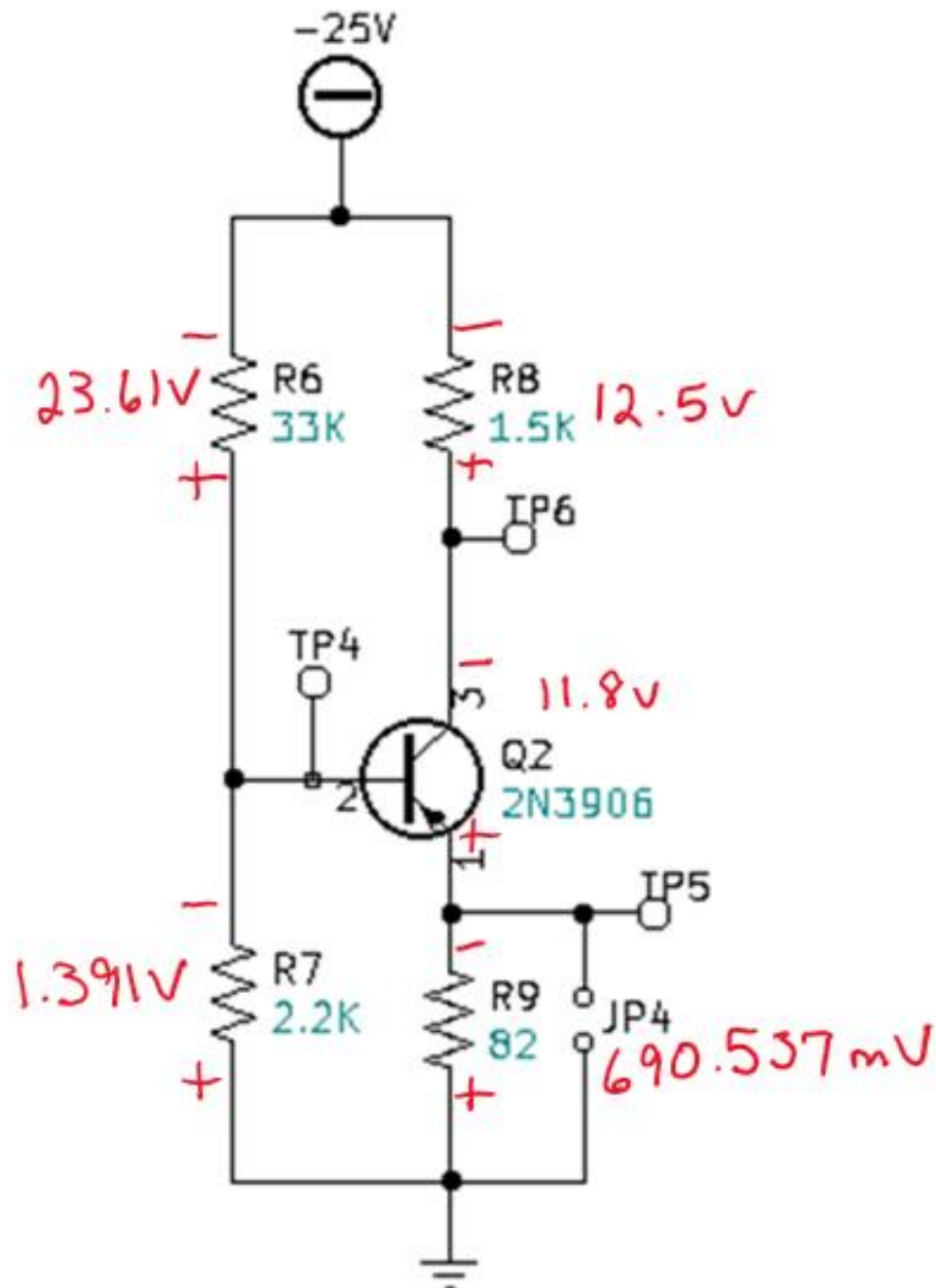
Simultaneous Equation Solution:

- $I_{R6} = 715.438\mu A$
- $I_B = 83.378\mu A$



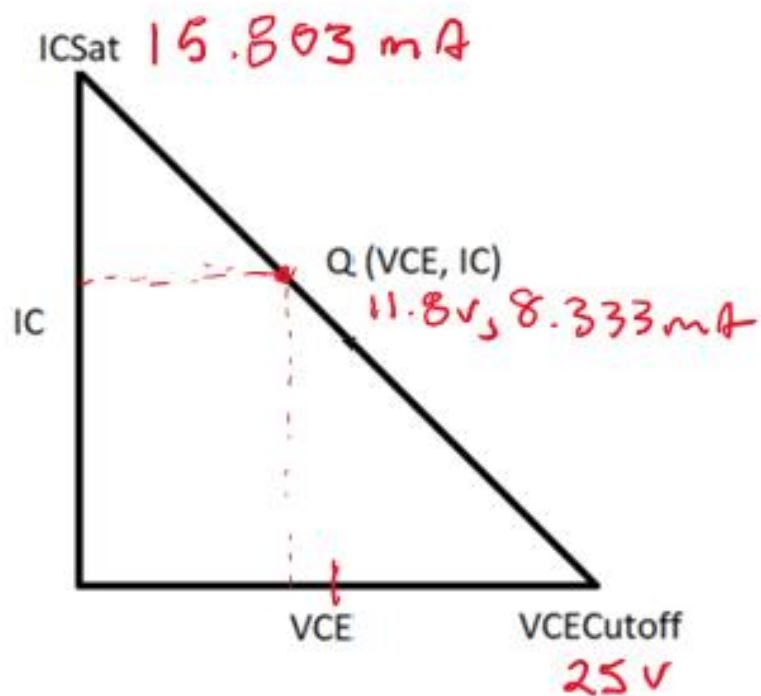
DC/Bias Voltages:

- $VR6 = IR6 \times R6$
 - $VR6 = 715.438 \times 33K$
 - $VR6 = 23.61V$
- $VR7 = IR7 \times R7$
 - $VR7 = (715.438 - 83.378\mu A) \times 2.2K$
 - $VR7 = 1.391V$
- $VR8 = IR8 \times R8$
 - $VR8 = IB(beta) \times 1.5K$
 - $VR8 = 83.378\mu A(100) \times 1.5K$
 - $VR8 = 12.51V$
- $VR9 = IR9 \times R9$
 - $VR9 = IB(beta + 1) \times 82$
 - $VR9 = 83.378\mu A(101) \times 82$
 - $VR9 = 690.537mV$
- $VCE = VCC - VR8 - VR9$
 - $VCE = 25 - 12.51 - 690.537mV$
 - $VCE = 11.8V$
- $TP4 = 1.391V$
- $TP5 = 690.537mV$
- $TP6 = 12.5V$



DC Load Line for Q2:

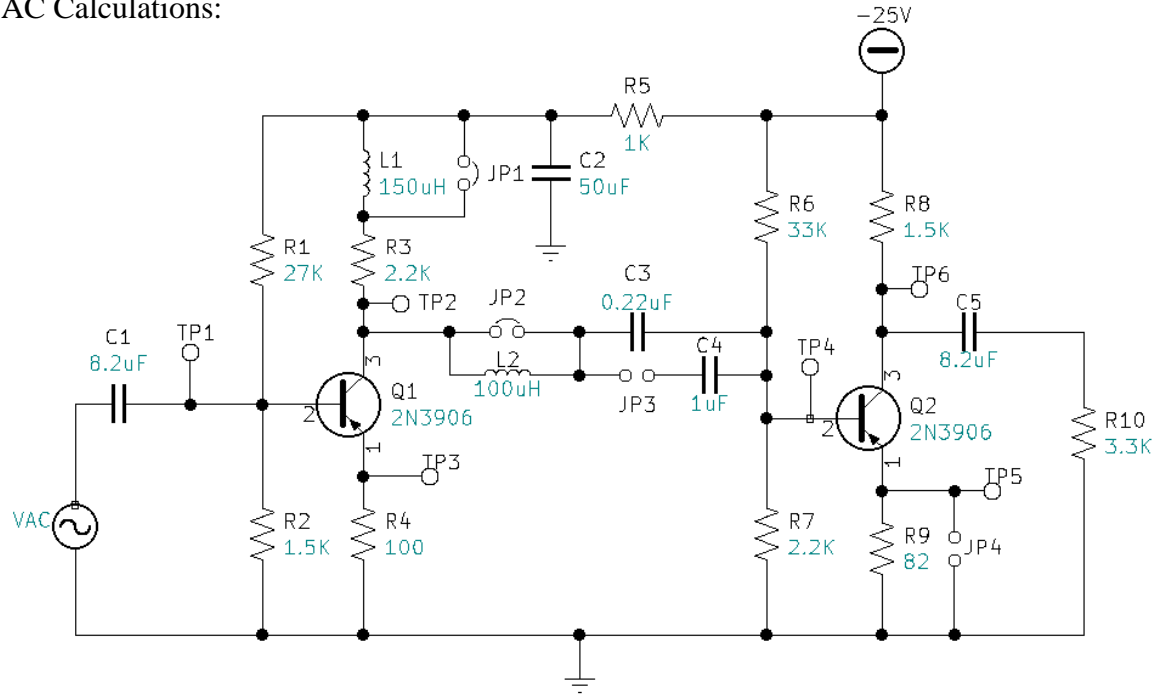
- $V_{CE_{cutoff}} = V_{CC}$
 - $V_{CE_{cutoff}} = 25V$
- $I_{C_{saturation}} = \frac{V_{CC}}{R_8 + R_9}$
 - $I_{C_{saturation}} = \frac{25}{1.5K + 82}$
 - $I_{C_{saturation}} = 15.803mA$



DC Calculations Tabulated:

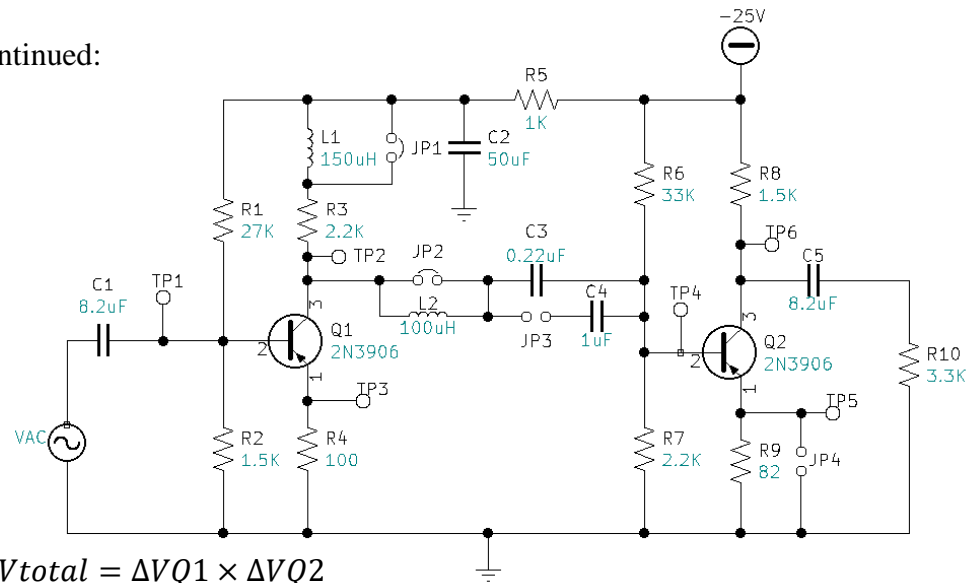
	A	B	C	
1	DC Values	Calculated	Measured	
2	VR1	19.78V		
3	VR2	1.047V		
4	VR3	7.566V		
5	VR4	347.347mV		
6	VR5	4.172V		
7	VR6	23.61V		
8	VR7	1.391V		
9	VR8	12.5V		
10	VR9	690.537mV		
11	VCEQ1	13.142V		
12	VCEQ2	11.8V		
13	TP1	-1.047V		
14	TP2	-13.489V		
15	TP3	-347.347mV		
16	TP4	-1.391V		
17	TP5	-690.537mV		
18	TP6	-12.5V		
19				

AC Calculations:



- $\Delta V_{Q2} = \frac{V_{out}}{V_{in}}$
 - $\Delta V_{Q2} = \frac{I_C(R8//R10)}{I_B(R9+r'e)(B+1)}$
 - $\Delta V_{Q2} = \text{Beta} \frac{(1.5K//3.3K)}{(82+3.087)(101)}$
 - $\Delta V_{Q2} = 100 \frac{(1.03125K)}{(8.594K)}$
 - $\Delta V_{Q2} = -12$
- $\Delta V_{Q1} = \frac{V_{out}}{V_{in}}$
 - $\Delta V_{Q1} = \frac{I_C((R3//R6//R7)/(R9+r'e)(B+1))}{I_B(R4+r'e)(B+1)}$
 - $\Delta V_{Q1} = \text{Beta} \frac{((2.2K//33K//2.2K)/(82+3.087)(101))}{(100+7.485)(101)}$
 - $\Delta V_{Q1} = 100 \frac{((2.2K//33K//2.2K)/(8.594K))}{(107.485)(101)}$
 - $\Delta V_{Q1} = 100 \frac{947.19}{10.856K}$
 - $\Delta V_{Q1} = -8.725$

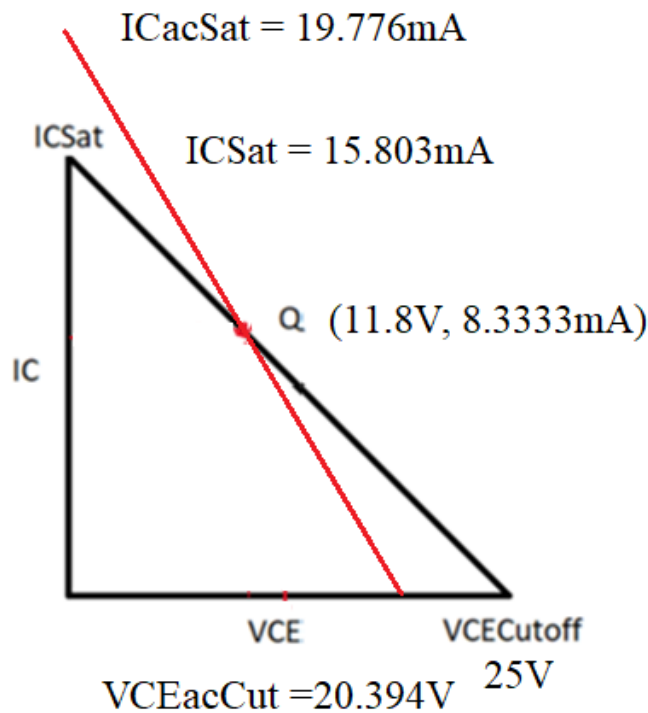
AC Calculations Continued:



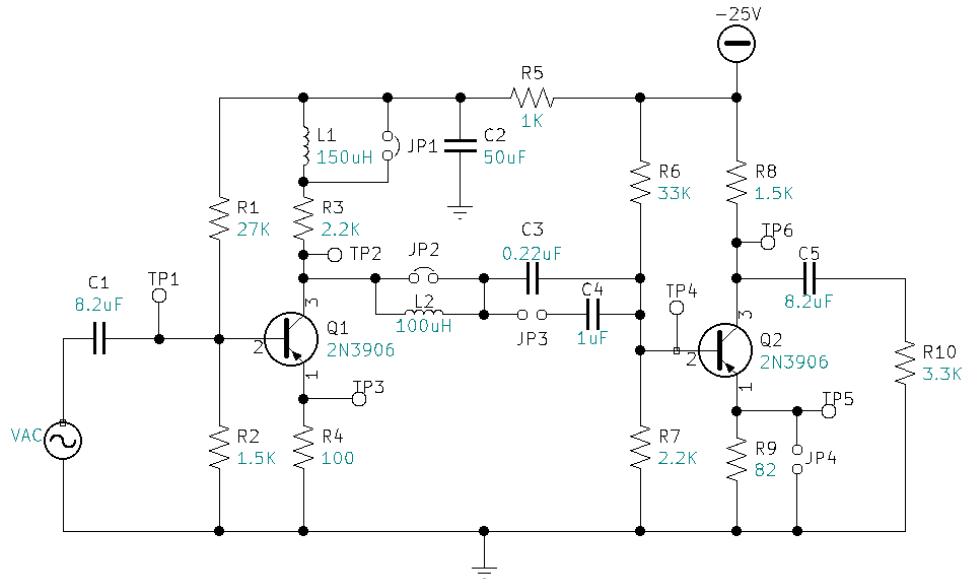
- $\Delta V_{total} = \Delta V_{Q1} \times \Delta V_{Q2}$
 - $\Delta V_{Total} = -8.725 \times -12$
 - $\Delta V_{Total} = 104.7$
- $Z_{out} = R_8$
 - $Z_{out} = 1.5K\Omega$
- $Z_{in} = (R_4 + r'_e)(B + 1) // R_1 // R_2$
 - $Z_{in} = (100 + 7.485)(101) // 27K // 1.5K$
 - $Z_{in} = (755.985) // 27K // 1.5K$
 - $Z_{in} = 493.466\Omega$
- $\Delta I_{total} = \frac{I_{out}}{I_{in}} = \frac{\frac{V_{out}}{R_L}}{\frac{V_{in}}{Z_{in}}} = \frac{V_{out}}{R_L} \times \frac{Z_{in}}{V_{in}} = \frac{V_{out}}{V_{in}} \times \frac{Z_{in}}{R_L}$
 - $\Delta I_{total} = \Delta V_{total} \times \frac{Z_{in}}{R_L}$
 - $\Delta I_{total} = 104.7 \times \frac{493.466}{3.3K}$
 - $\Delta I_{total} = 15.656$
- $\Delta P_{total} = \Delta V_{total} \times \Delta I_{total} = 104.7 \times 15.656$
 - $\Delta P_{total} = 1.639K$

- $V_{CEacCut} = V_{CE} + I_C(R_8 // R_{10})$
 - $V_{CEacCut} = 11.8 + 8.333mA(1.031K)$
 - $V_{CEacCut} = 11.8 + 8.333mA(1.031K)$
 - $V_{CEacCut} = 20.394V$

- $I_{CacSat} = I_C + \frac{V_{CE}}{R_8 // R_{10}}$
 - $I_{CacSat} = 8.333mA + \frac{11.8}{1.031K}$
 - $I_{CacSat} = 19.776mA$



- $V_{outMaxP} = V_{CEacCut} - V_{CE}$
 - $V_{outMaxP} = 20.394 - 11.8$
 - $V_{outMaxP} = 8.594vP$
- $V_{inMaxP} = \frac{V_{outMaxP}}{A_{VT}} = \frac{8.594}{104.7}$
 - $V_{inMaxP} = 82.082mVp$



Frequency Response Low:

Rules:

- Treat all caps like opens.
- Thevenize each and find F_c for each cap
- $F_{CL} = \sqrt{F_{C1}^2 + F_{C2}^2 + F_{C3}^2} \dots$

▪ $R_{thC1} = R2 // ((R4 + r'e1)(B + 1)) // (R1 + R5)$

- $R_{thC1} = 1.5K // ((100 + 7.485)(101)) // (27K + 1K)$
- $R_{thC1} = 1.258K$

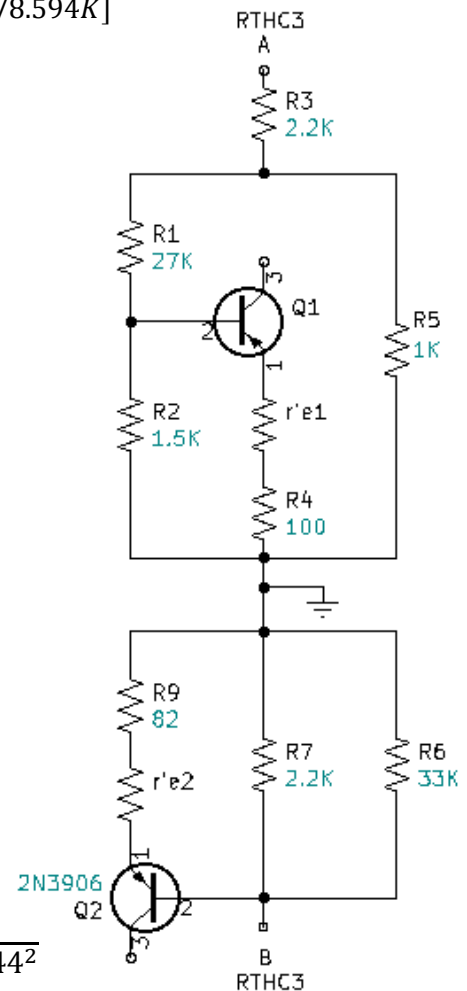
▪ $F_{cC1} = \frac{1}{2\pi R_{thC1} C1} = \frac{1}{2\pi \times 1.258K \times 8.2uF}$

- $F_{cC1} = 15.429Hz$

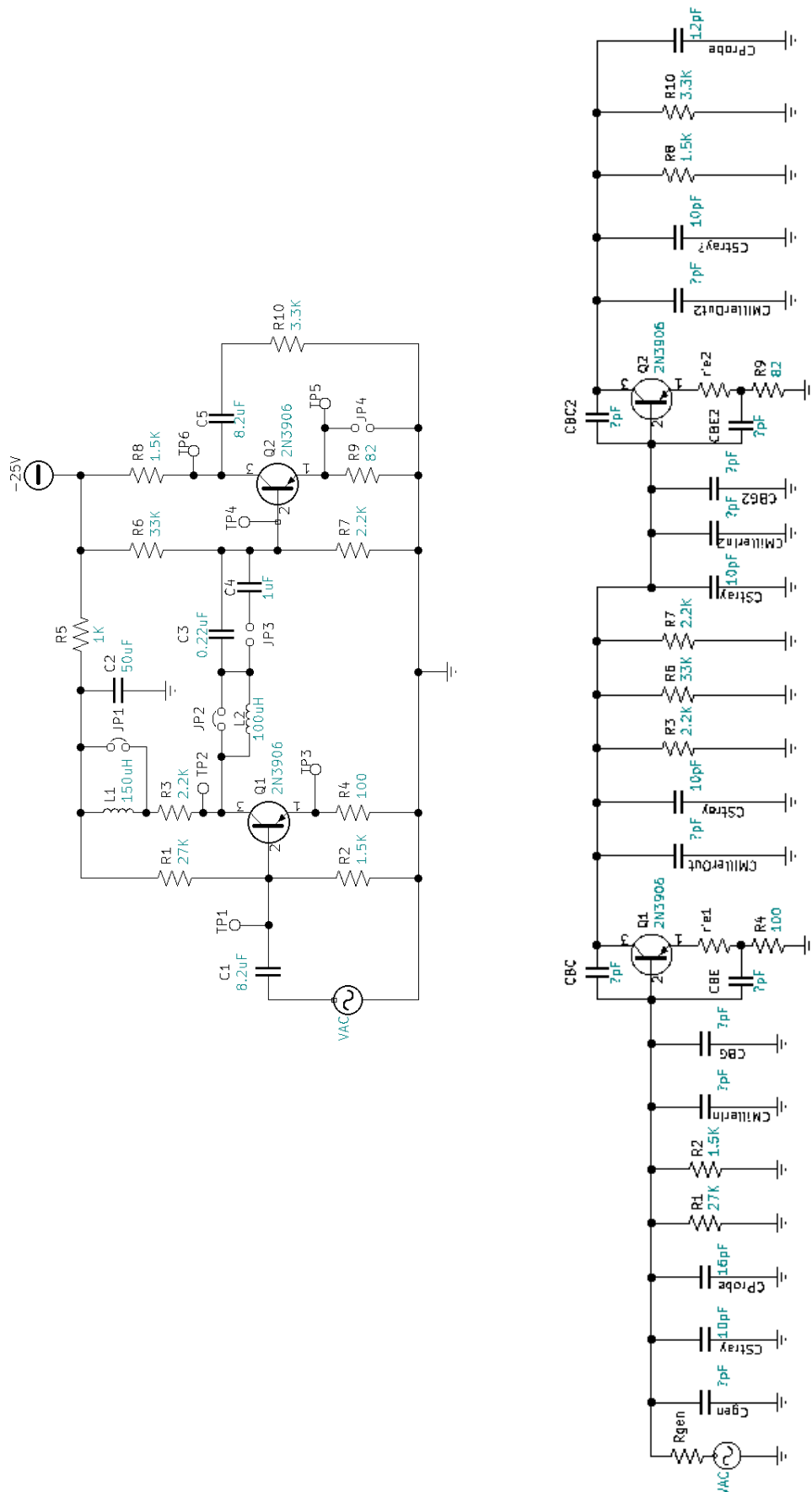
▪ $R_{thC2} = R5 // [(R1 + (R2 // ((r'e1 + R4)(B + 1)))]$

- $R_{thC2} = 1K // [(27K + (1.5K // ((7.485 + 100)(101)))]$
- $R_{thC2} = 1K // [(27K + (1.5K // (10.856K))]$
- $R_{thC2} = 1K // [(27K + 1.318K)]$
- $R_{thC2} = 1K // 28.318K$

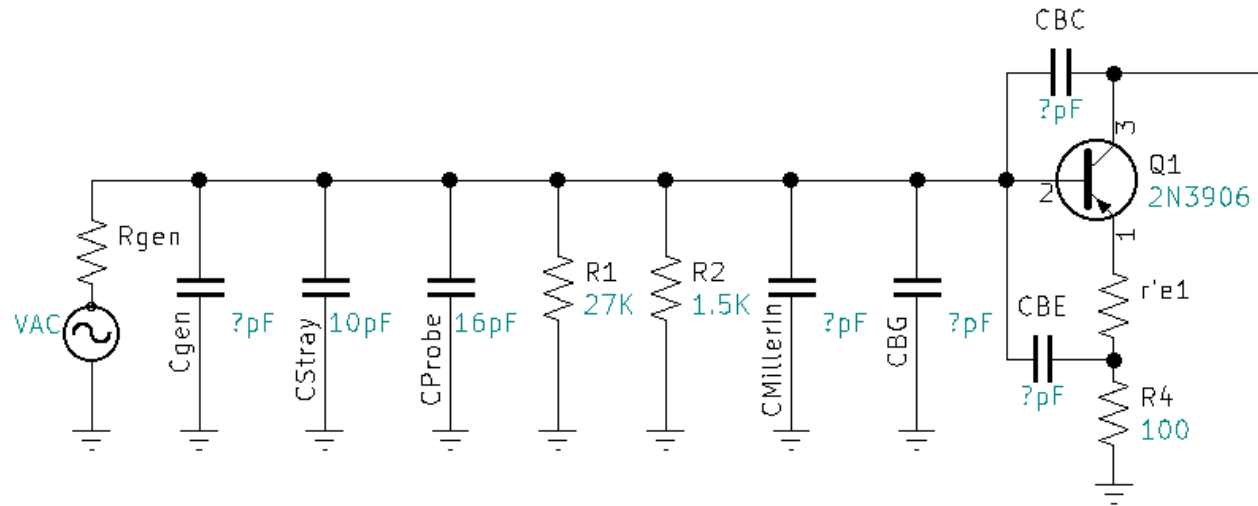
- $R_{thC2} = 965.891\Omega$
 - $F_{cC2} = \frac{1}{2\pi R_{thC2} C2} = \frac{1}{2\pi \times 965.892 \times 50\mu F}$
 - $F_{cC1} = 3.327\text{hz}$
 - $R_{thC3} = R3 + [R5 // (R1 + R2 // (R4 + r'e1)(B + 1))] + [R6 // R7 // (R9 + r'e2)(B + 1)]$
 - $R_{thC3} = 2.2K + [1K // (27K + 1.5K // (100 + 7.485)(101))] + [33K // 2.2K // (82 + 3.087)(101)]$
 - $R_{thC3} = 2.2K + [1K // (27K + 1.5K // 10.856K)] + [33K // 2.2K // 8.594K]$
 - $R_{thC3} = 2.2K + [1K // 28.318K] + [33K // 2.2K // 8.594K]$
 - $R_{thC3} = 2.2K + [965.891] + [1.663K]$
 - $R_{thC3} = 4.829K\Omega$
 - $F_{cC3} = \frac{1}{2\pi R_{thC3} C3} = \frac{1}{2\pi \times 4.829K \times 0.22\mu F}$
 - $F_{cC3} = 149.81\text{hz}$
 - $F_{cC3w/C4} = \frac{1}{2\pi R_{thC3} C3 + C4} = \frac{1}{2\pi \times 4.829K \times 1.22\mu F}$
 - $F_{cC3w/C4} = 27.015\text{hz}$
 - $R_{thC5} = R8 + R10 = 1.5K + 3.3K$
 - $R_{thC5} = 4.8K\Omega$
 - $F_{cC5} = \frac{1}{2\pi R_{thC5} C5} = \frac{1}{2\pi \times 4.8K \times 8.2\mu F}$
 - $F_{cC5} = 4.044\text{hz}$
- $$F_{CL} = \sqrt{F_{C1}^2 + F_{C2}^2 + F_{C3}^2 \dots}$$
- $F_{CL} = \sqrt{15.429^2 + 3.327^2 + F_{C(3/4)}^2 + 4.044^2}$
 - $F_{CL} = 150\text{hz} * w/C3 \text{ (open JP3)}$
 - $F_{CL} = 31.548\text{hz} * w/(Closed JP3, C3 + C4)$



Frequency Response High:



Frequency Response High (Front End):



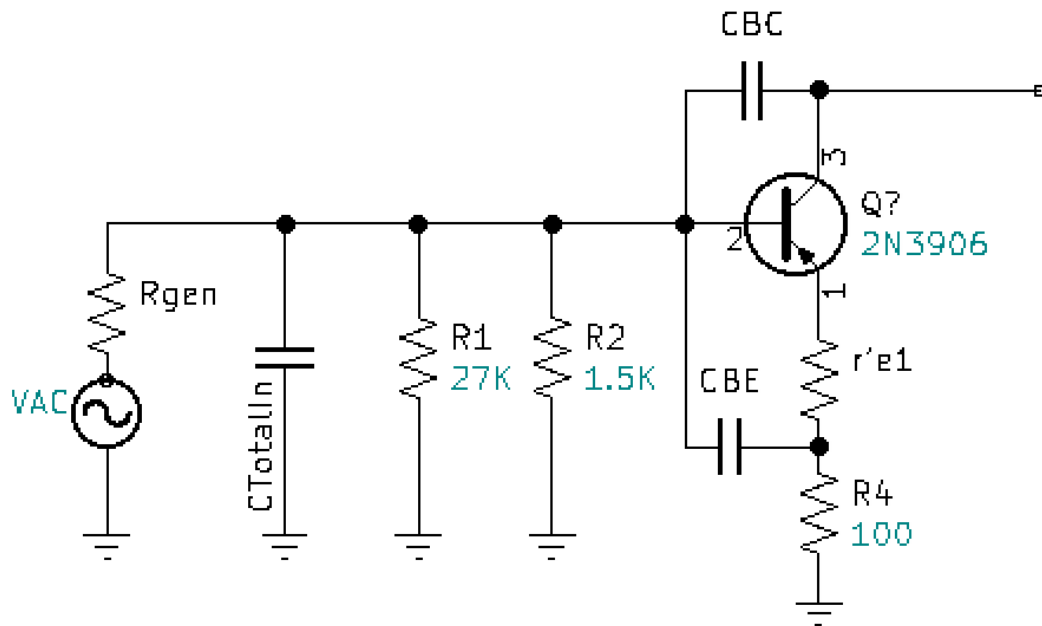
- $C_{totalIN} = C_{gen} + C_{stray} + C_{probe} + C_{millerIN} + CBG$
 - $C_{gen} \approx 40pF$ (User Manual)
 - $C_{stray} \approx 10pF$
 - $C_{probe} \approx 16pF$
 - $C_{millerIN} = CBC(1 + \Delta V_{CE})$
 - $CBC \approx 4pF \approx C_{ibo}$ (from the data sheet)
 - $C_{millerIN} = 4.5pF(1 + 8.725)$
 - $C_{millerIN} = 43.763pF$

SMALL-SIGNAL CHARACTERISTICS

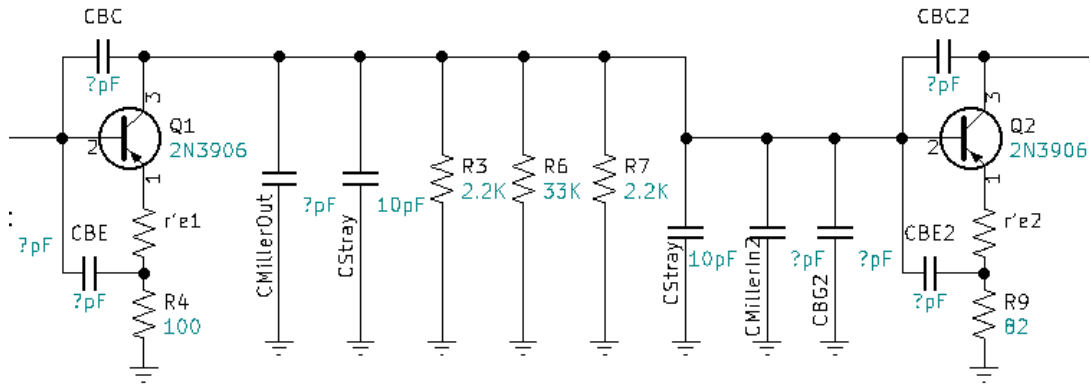
Current-Gain - Bandwidth Product	($I_C = 10 \text{ mA dc}$, $V_{CE} = 20 \text{ V dc}$, $f = 100 \text{ MHz}$)	f_T	250	-	MHz
Output Capacitance	($V_{CB} = 5.0 \text{ V dc}$, $I_E = 0$, $f = 1.0 \text{ MHz}$)	C_{obo}	-	4.5	pF
Input Capacitance	($V_{EB} = 0.5 \text{ V dc}$, $I_C = 0$, $f = 1.0 \text{ MHz}$)	C_{ibo}	-	10	pF

SMALL-SIGNAL CHARACTERISTICS

Current-Gain - Bandwidth Product	($I_C = 10 \text{ mA dc}$, $V_{CE} = 20 \text{ V dc}$, $f = 100 \text{ MHz}$)	f_T	250	-	MHz
Output Capacitance	($V_{CB} = 5.0 \text{ V dc}$, $I_E = 0$, $f = 1.0 \text{ MHz}$)	C_{obo}	-	4.5	pF
Input Capacitance	($V_{EB} = 0.5 \text{ V dc}$, $I_C = 0$, $f = 1.0 \text{ MHz}$)	C_{ibo}	-	10	pF



- $CBG = CBE(1 - \Delta V_{CC})$
 - $\Delta V_{CC} = \frac{IE(RE)}{IE(RE+r'e)} \text{ or } \frac{(RE)}{(RE+r'e)}$
 - $\Delta V_{CC} = \frac{(100)}{(100+7.485)} = 0.930$
 - $CBE = \frac{1}{(2\pi)(r'e)(f_T)} = \frac{1}{(2\pi)(7.485)(250M)} = 85.053pF$
 - $CBG = 85.053pF(1 - 0.93)$
 - $CBG = 5.954pF$
- $C_{totalIN} = C_{gen} + C_{stray} + C_{probe} + C_{millerIN} + CBG$
 - $C_{totalIN} = 40pF + 10pF + 16pF + 43.763pF + 5.954pF$
 - $C_{totalIN} = 115.717pF$



Frequency Response High (Middle):

- $C_{totalMid} = C_{MillerOut1} + C_{stray} + C_{stray} + C_{MillerIN2} + C_{BG2}$

- $C_{MillerOUT} = CBC \left(\frac{1 + \Delta V_{CE}}{\Delta V_{CE}} \right)$

- $CBC \approx 4pF \approx C_{ibo}$ (from the data sheet)

- $C_{MillerOUT1} = 4.5pF \left(\frac{1 + 8.725}{8.725} \right) = 5.016pF$

- $C_{MillerIN} = CBC(1 + \Delta V_{CE})$

- $C_{MillerIN2} = 4.5pF(1 + 12) = 58pF$

- $C_{BG} = CBE(1 - \Delta V_{CC})$

- $\Delta V_{CC} = \frac{IE(RE)}{IE(RE+r'e)} \text{ or } \frac{(RE)}{(RE+r'e)}$

- $\Delta V_{CC} = \frac{(82)}{(82+3.087)} = 0.964$

- $C_{BE2} = \frac{1}{(2\pi)(r'e)(f_T)} = \frac{1}{(2\pi)(3.087)(250M)} = 206.226pF$

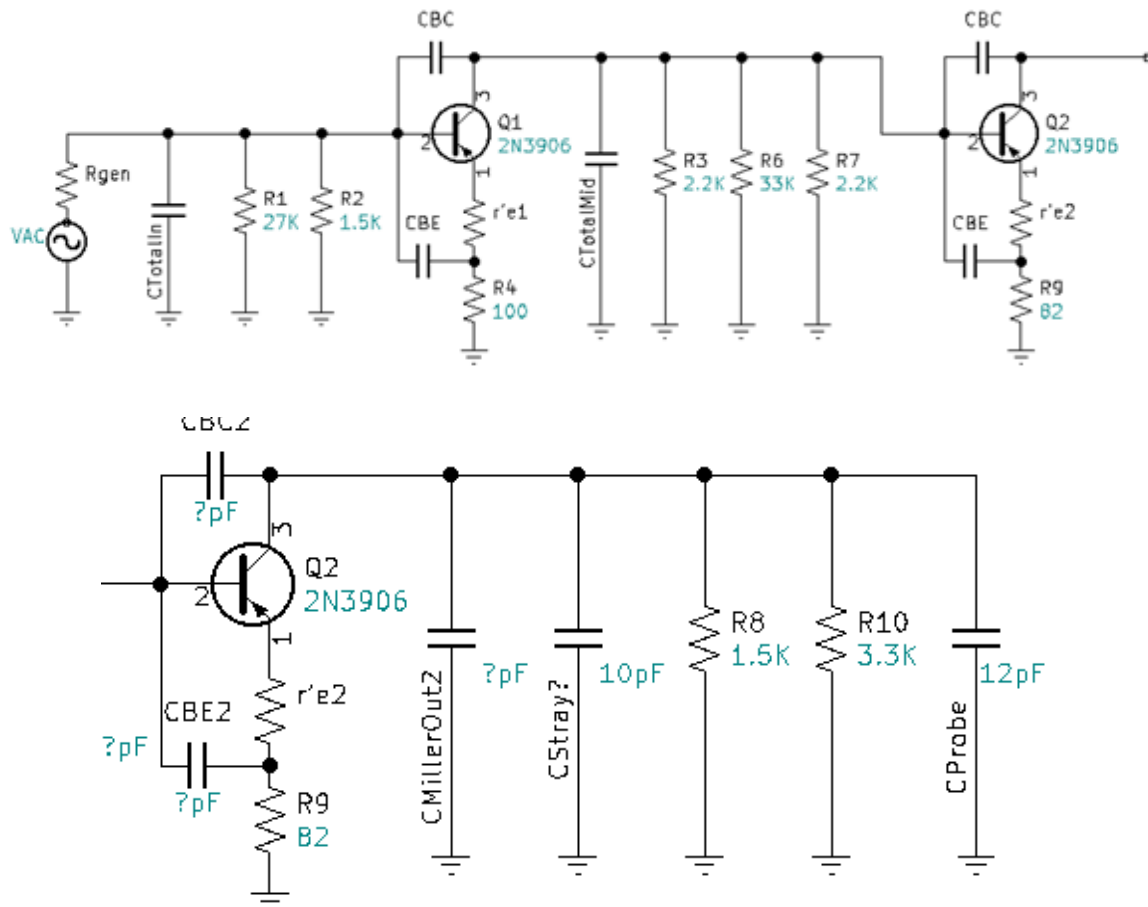
- $C_{BG2} = 206.226pF(1 - 0.964)$

- $C_{BG2} = 7.424pF$

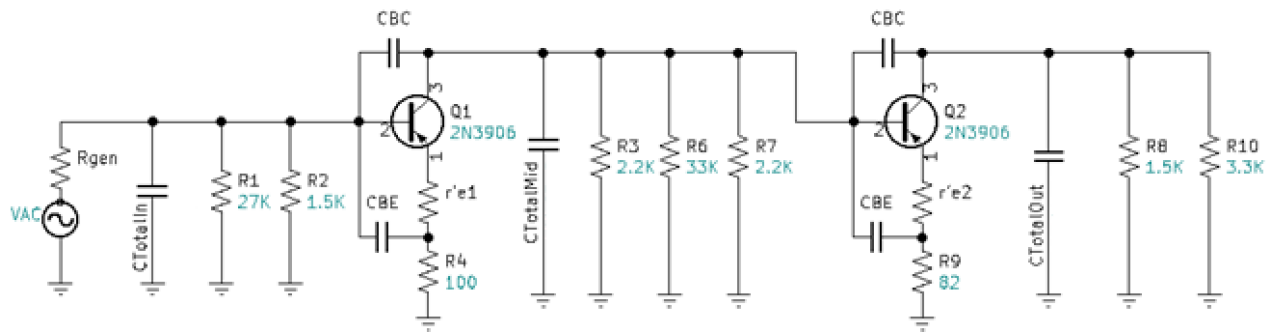
- $C_{totalMid} = 5.016pF + 10pF + 10pF + 58pF + 7.424pF$

- $C_{totalMid} = 90.44pF$

Frequency Response High (Back End):

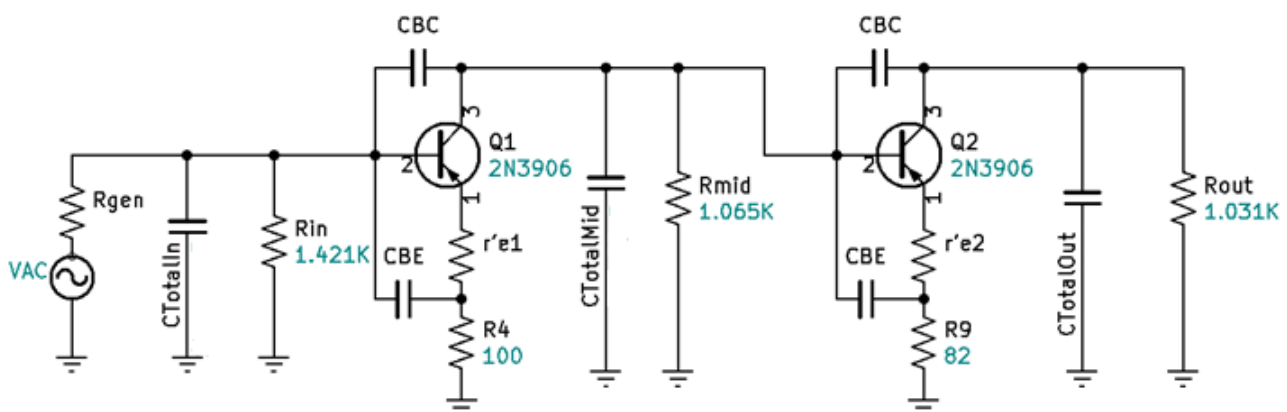


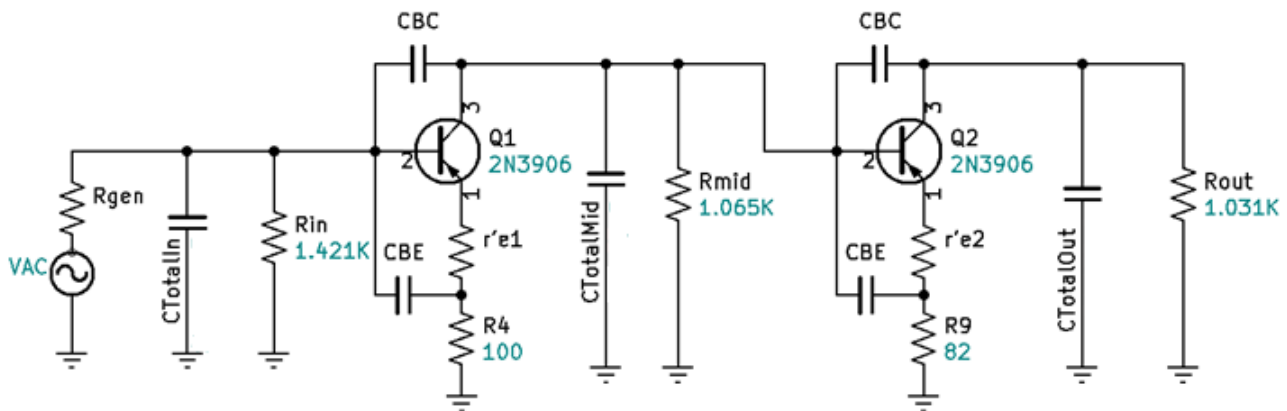
- $C_{totalOut} = C_{MillerOut2} + C_{stray} + C_{Probe}$
- $C_{MillerOUT} = CBC \left(\frac{1 + \Delta V_{CE}}{\Delta V_{CE}} \right)$
 - $CBC \approx 4pF \approx C_{obo}$ (from the data sheet)
 - $C_{MillerOut2} = 4.5pF \left(\frac{1+12}{12} \right)$
 - $C_{MillerOut2} = 4.767pF$
- $C_{totalOut} = 4.767pF + 10pF + 16pF$
- $C_{totalOut} = 30.767pf$



Simplify parallel resistances:

- $R_{in} = R1 // R2 = 27K // 1.5K$
- $R_{in} = 1.421K\Omega$
- $R_{mid} = R3 // R6 // R7 = 2.2K // 33K // 2.2K$
- $R_{mid} = 1.065K\Omega$
- $R_{out} = R8 // R10 = 1.5K // 3.3K$
- $R_{out} = 1.031K\Omega$





Thevenize for C_{Tin} , C_{Tmid} , & C_{Tout} :

- $R_{thCtin} = R_{gen} // R_{in} // [(r'e1 + R4)(B + 1)]$
 - $R_{thCtin} = 50 // 1.421K // [(7.485 + 100)(101)] = 48.0865\Omega$
- $R_{thCtmid} = R_{mid} // [(r'e2 + R9)(B + 1)]$
 - $R_{thCtmid} = 1.065K // [(3.087 + 82)(101)] = 947.571\Omega$
- $R_{thCtout} = R_{out} = 1.031K\Omega$

Find FCH for each stage:

- $FCH = \frac{1}{2\pi R_{Thev} CT}$
 - $FCH_{CTin} = \frac{1}{2\pi \times 48.0865 \times 115.717pF} = 28.6022Mhz$
 - $FCH_{CTmid} = \frac{1}{2\pi \times 947.571 \times 90.44pF} = 1.857Mhz$
 - $FCH_{Ctout} = \frac{1}{2\pi \times 1.031K \times 30.767pF} = 5.0174Mhz$

Find FCHtotal:

$$\begin{aligned}
 \bullet \quad FCH_{Total} &= \frac{.35}{\sqrt{\left(\frac{.35}{FCH_{IN}}\right)^2 + \left(\frac{.35}{FCH_{OUT}}\right)^2}} \\
 \bullet \quad FCH_{Total} &= \frac{.35}{\sqrt{\left(\frac{.35}{28.602Mhz}\right)^2 + \left(\frac{.35}{1.857Mhz}\right)^2 + \left(\frac{.35}{5.0174Mhz}\right)^2}} \\
 \bullet \quad FCH_{Total} &= 1.738Mhz
 \end{aligned}$$

	A	B	C	D	E	F
1	DC Values	Calculated	Measured	AC Values	Calculated	Measured
2	VR1	19.78V		r'e1	7.485Ω	
3	VR2	1.047V		r'e2	3.087Ω	
4	VR3	7.566V		Zin	493.466Ω	
5	VR4	347.347mV		Zout	1.5KΩ	
6	VR5	4.172V		AVQ1	-8.725	
7	VR6	23.61V		AVQ2	-12	
8	VR7	1.391V		AVT	104.7	
9	VR8	12.5V		AIT	15.656	
10	VR9	690.537mV		APT	1.639K	
11	VCEQ1	13.142V		VCEacCut	20.394V	
12	VCEQ2	11.8V		ICacSat	19.776mA	
13	TP1	-1.047V		VoutMaxP	8.594vp	
14	TP2	-13.489V		VinMaxP	82.082mVp	
15	TP3	-347.347mV		RthC1	1.258KΩ	
16	TP4	-1.391V		RthC2	965.891Ω	
17	TP5	-690.537mV		RthC3&C4	4.829KΩ	
18	TP6	-12.5V		RthC5	4.8KΩ	
19	ICSatQ1	7.395mA		FcC1	15.429hz	
20	VCECutQ1	-24.153V		FcC2	3.327hz	
21	Q1	13.142V, 3.49mA		FcC3	149.81hz	
22	ICSatQ2	15.803mA		FcC3&C4	27.015hz	
23	VCECutQ2	-25V		FcC5	4.044hz	
24	Q2	11.8V, 8.333mA		FCL	150hz (JP3 Open)	
25				FCL	31.548hz (JP3 jumped)	
26				FCH	1.738Mhz	