



ПОСЕБНИ ЗАХТЕВИ ПРОЈЕКТОВАЊА КОНСТРУКЦИЈА У РАЗЛИЧИТИМ КЛИМАТИМА (СРБИЈА, РУСИЈА, АЗИЈА И АФРИКА)

др Предраг Благојевић, дипл.инж.грађ.
Грађевинско-архитектонски факултет
Универзитета у Нишу





SADRŽAJ

- Temeljenje objekata
- Specifičnosti konstrukcijskih sistema
- Hidrotehničke konstrukcije
- Visoki stambeno-poslovni objekti
- Silosi
- Crkve
- Mostovi
- Tuđe greške u projektnom zadatku, projektovanju i izvođenju
- BIM tehnologija
- Reference za „veliku licencu“





Do sada projektovano i izvedeno objekata:

240+ stambenih i stambeno-poslovnih

60+ hidrotehničkih

20+ mostova

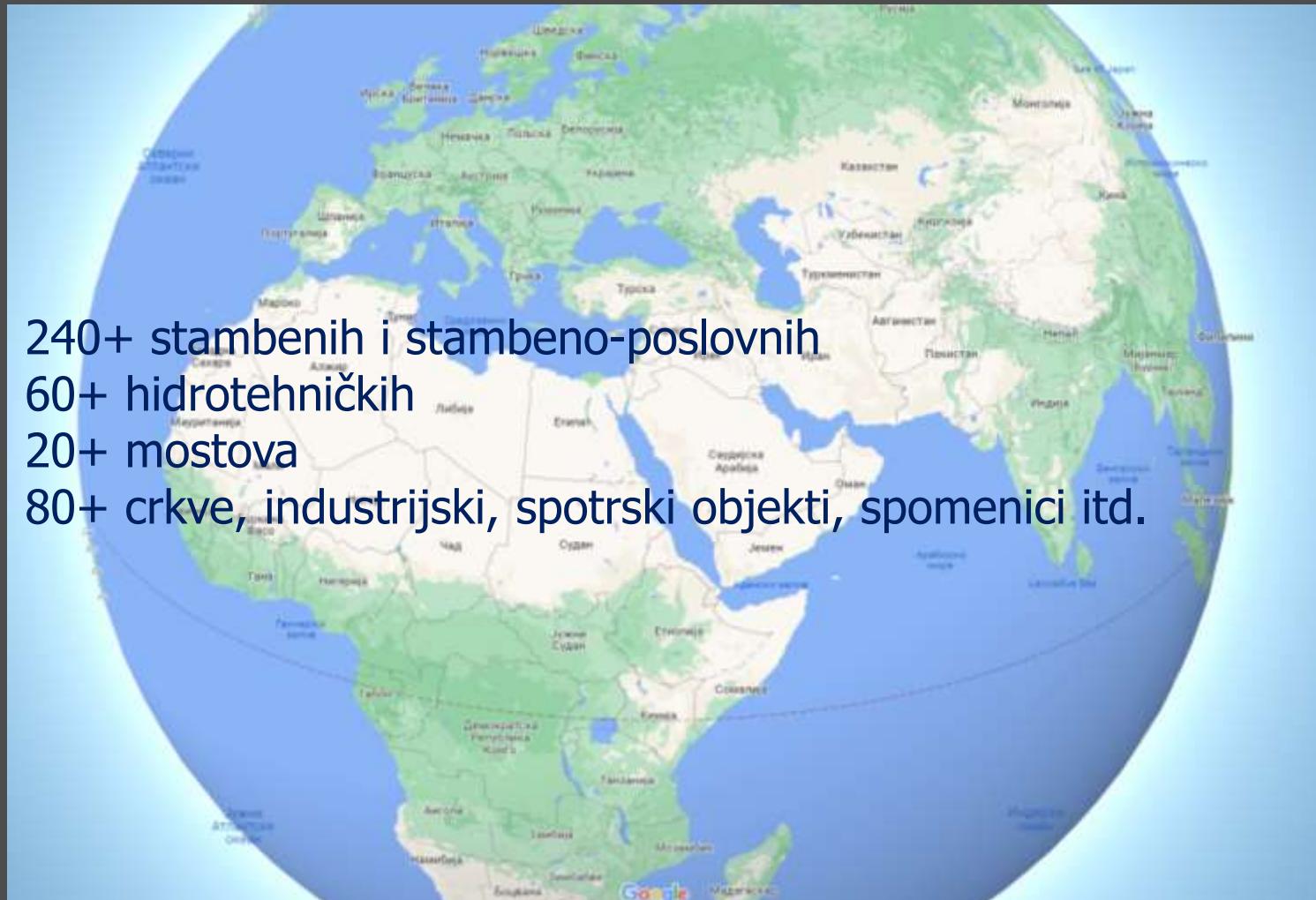
80+ crkve, industrijski, sportski objekti, spomenici itd.





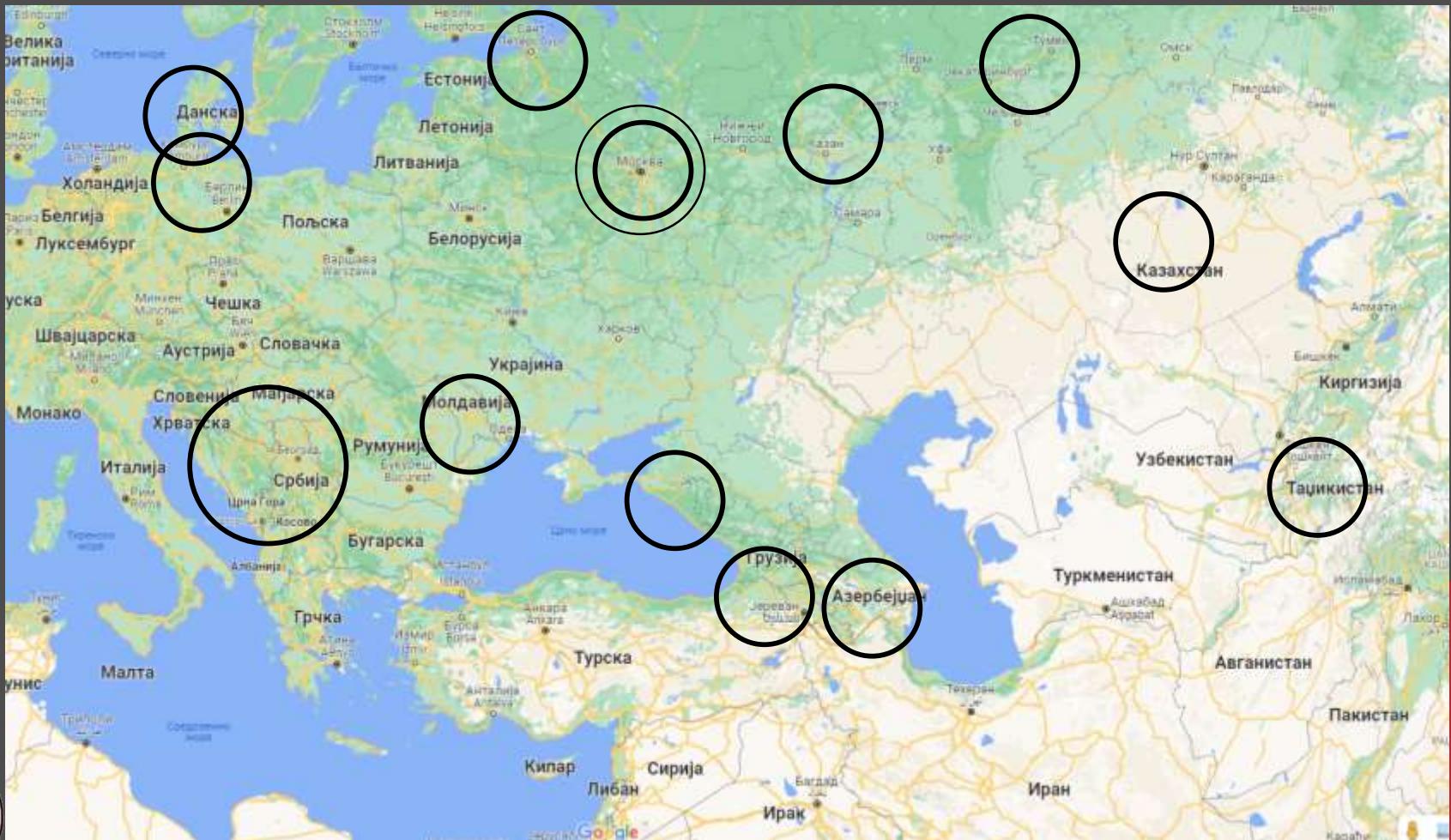
Do sada projektovano i izvedeno objekata:

240+ stambenih i stambeno-poslovnih
60+ hidrotehničkih
20+ mostova
80+ crkve, industrijski, sportski objekti, spomenici itd.





ЕВРОПА И ЦЕНТРАЛНА АЗИЈА





АФРИКА

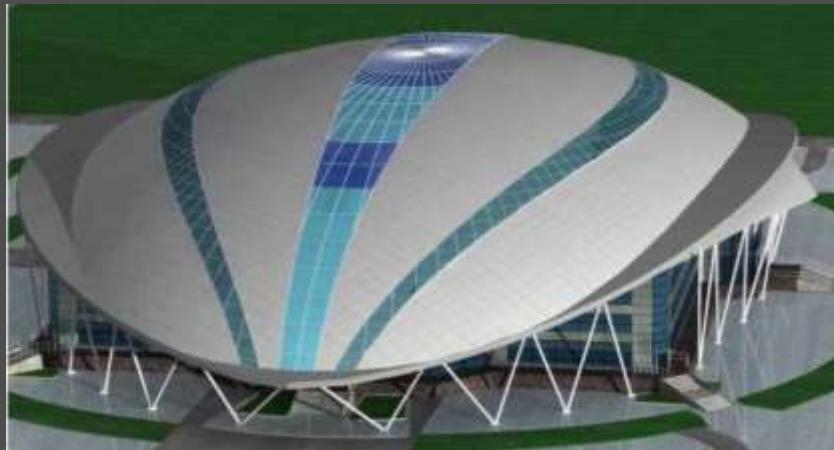




KAZAHSTAN

velodrom

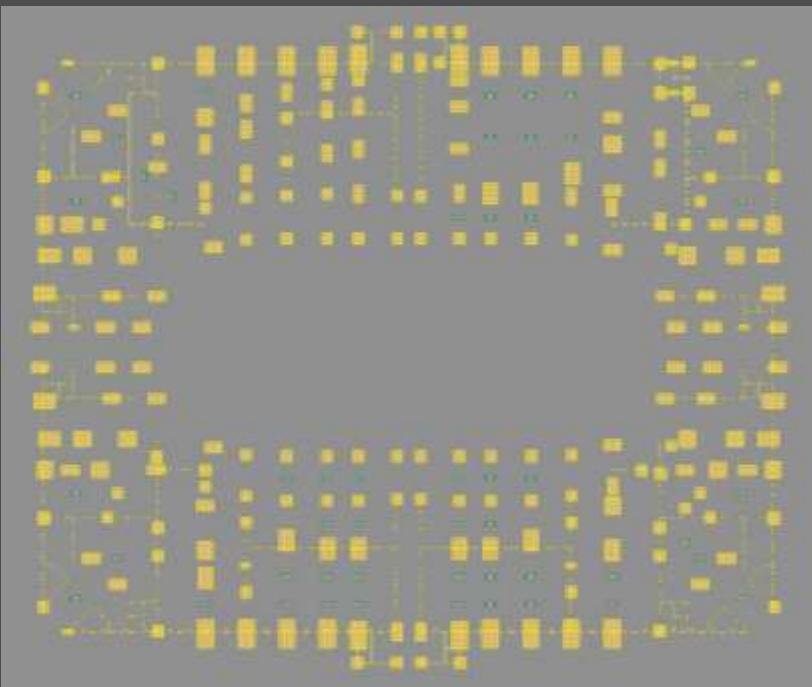
UŠTEDA
3.000.000 \$





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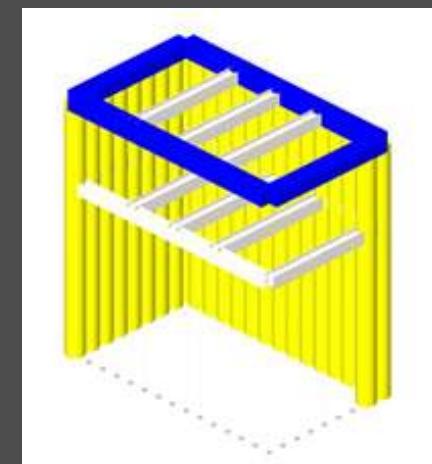
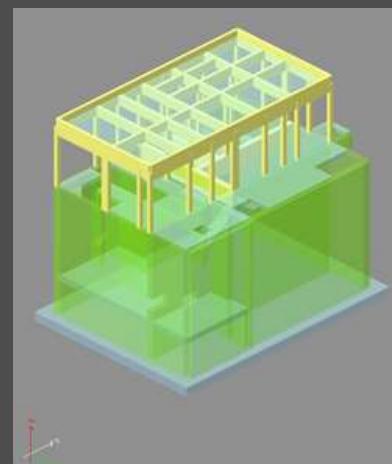
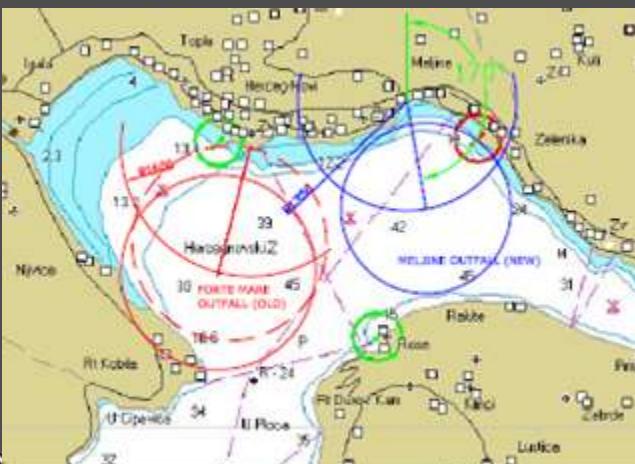
TEMELJNA KONSTRUKCIJA ZA VELODROM





CRNA GORA

POSTROJENJA ZA PREČIŠĆAVANJE OTPADNIH VODA OD IGALA DO BOKE KOTORSKE





CRNA GORA

POSTROJENJA ZA PREČIŠĆAVANJE OTPADNIH VODA OD IGALA DO BOKE KOTORSKE





CRNA GORA

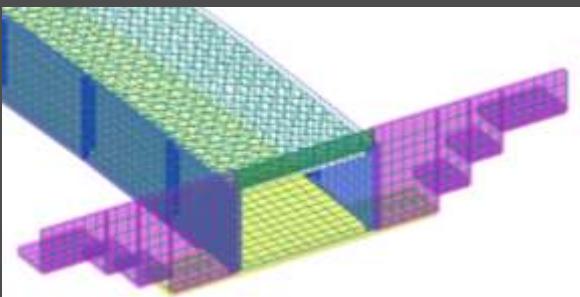
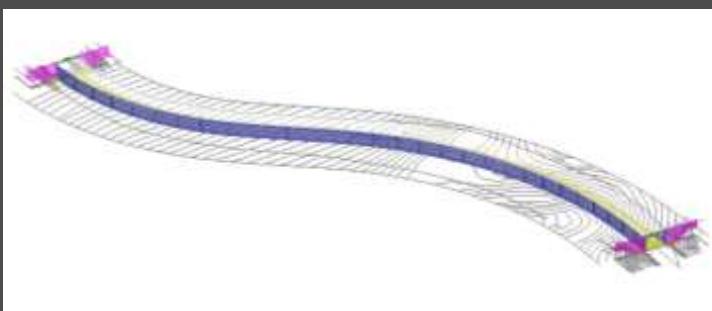
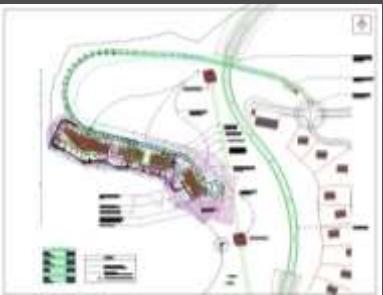
POSTROJENJA ZA PREČIŠĆAVANJE OTPADNIH VODA OD IGALA DO BOKE KOTORSKE





AZERBEJDŽAN

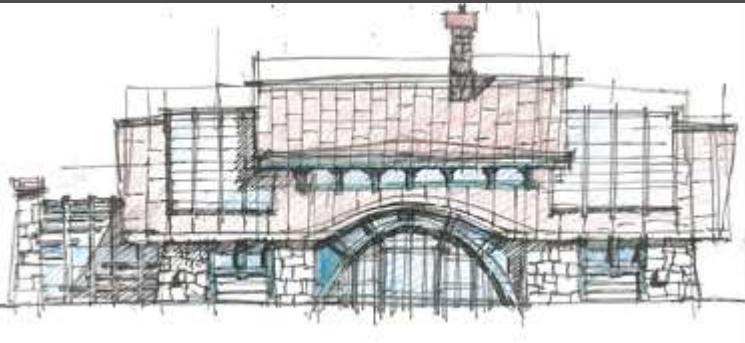
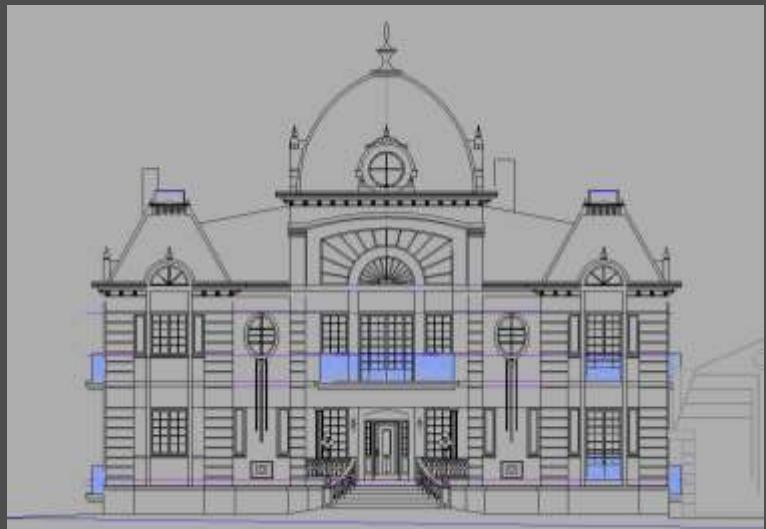
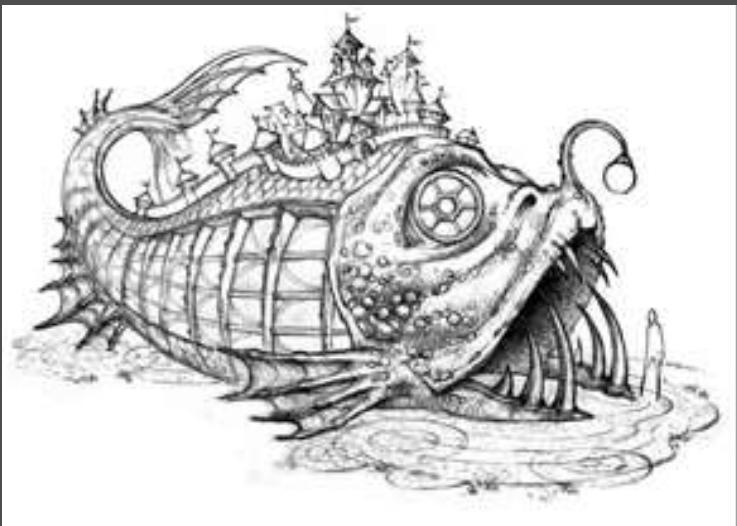
tunel





RUSIJA

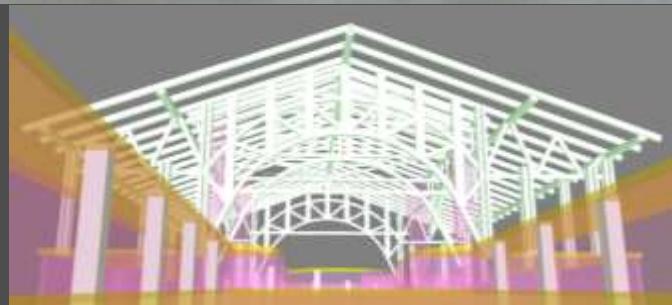
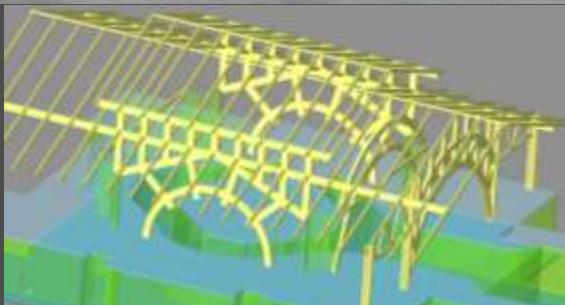
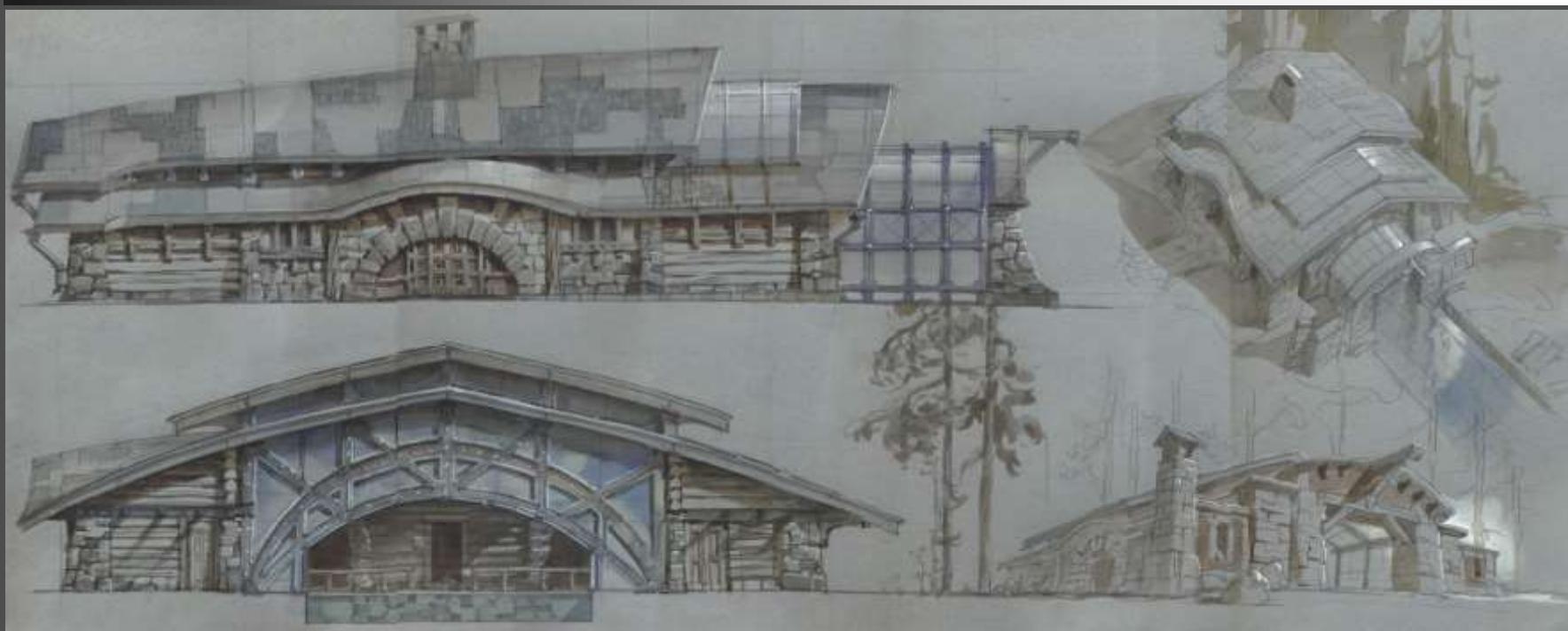
objekti iz bajki





RUSIJA

objekti iz bajki



pristupno predavanje





RUSIJA - MOSKVA

tržni centar za građevinski materijal



Opterećenje 10 kN/m^2
Ušteda u ceni konstrukcije – savremen proračun





RUSIJA - MOSKVA

fabrika obuće



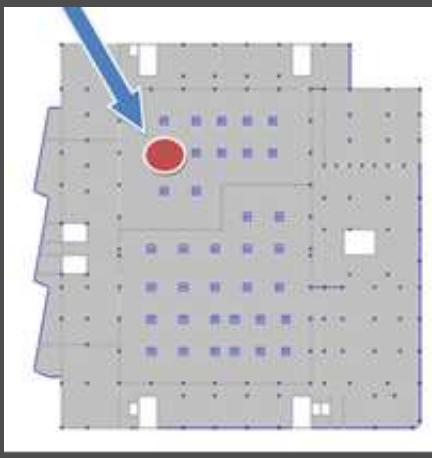
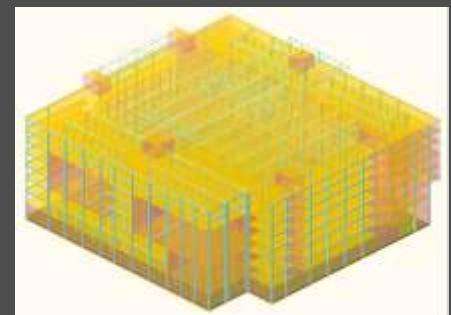
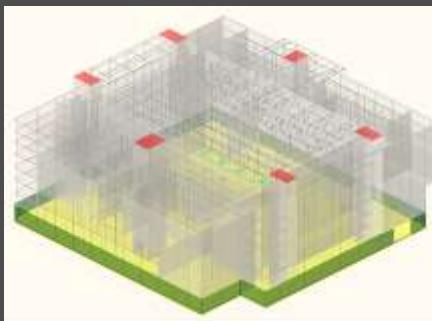
Ujednačavanje sleganja za objekte različite spratnosti





RUSIJA - MOSKVA

filmski i TV studio

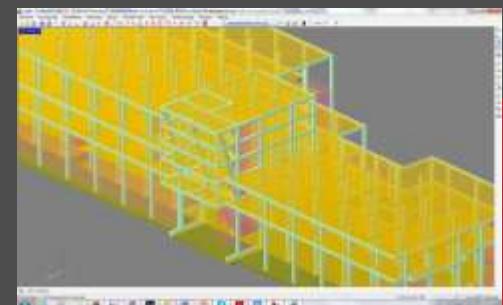
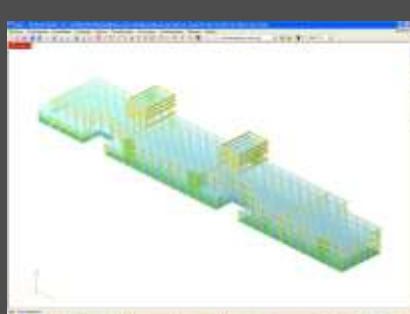
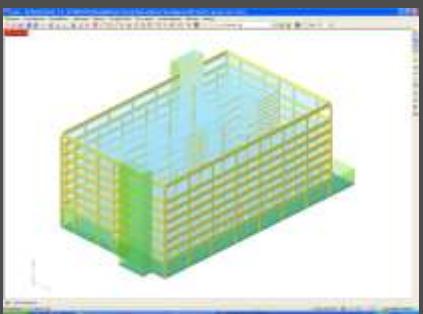


Upotreba VIRANDELOVIH nosača u organizaciji prostora



RUSIJA - RJAŽANJ

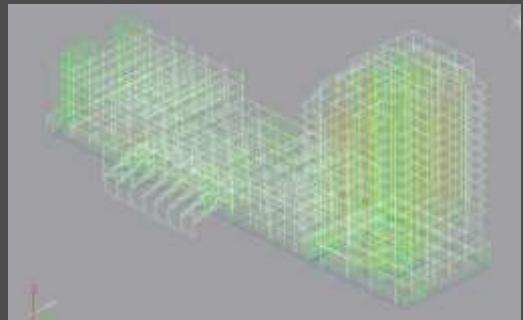
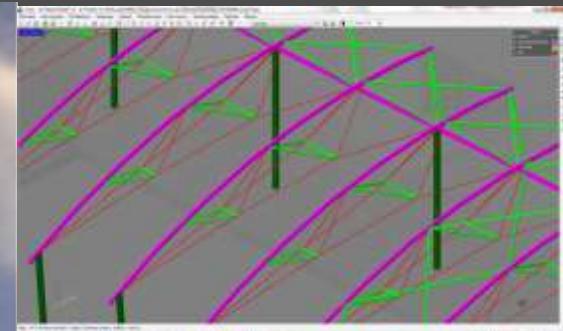
stambeno poslovni objekat (160 000 m²)





RUSIJA - MOSKVA

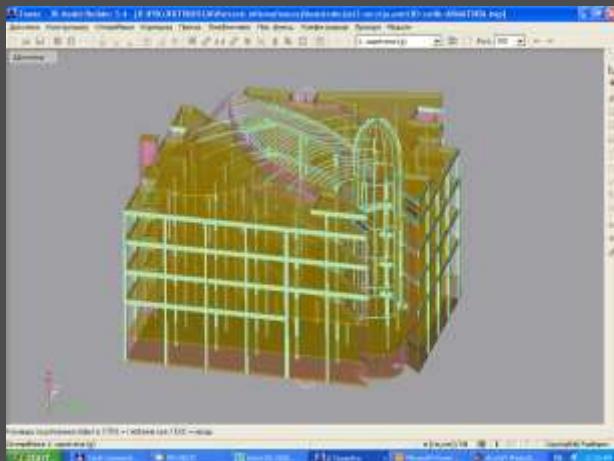
„AUDI“ poslovni objekat





RUSIJA - MOSKVA

muzej kosmonautike





RUSIJA - SOČI

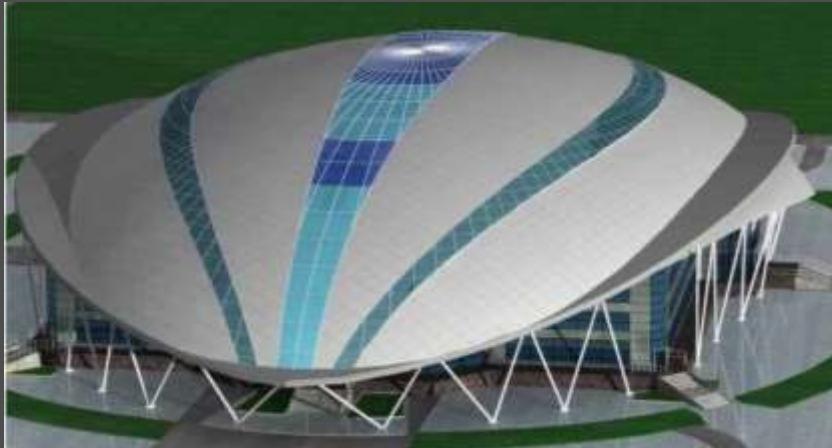
Hotel za zimske olimpijske igre





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velodrom



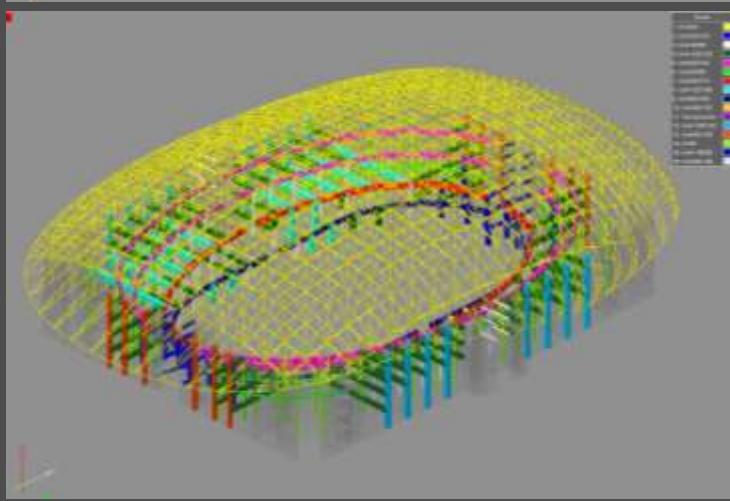
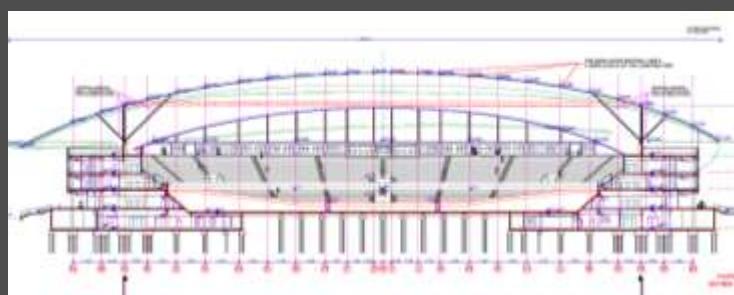
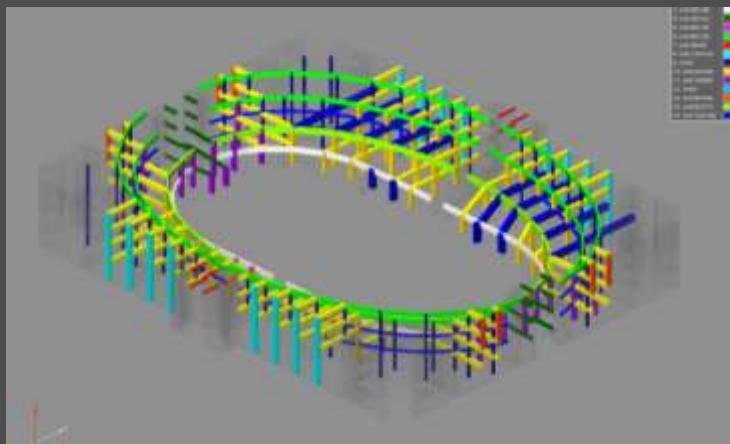
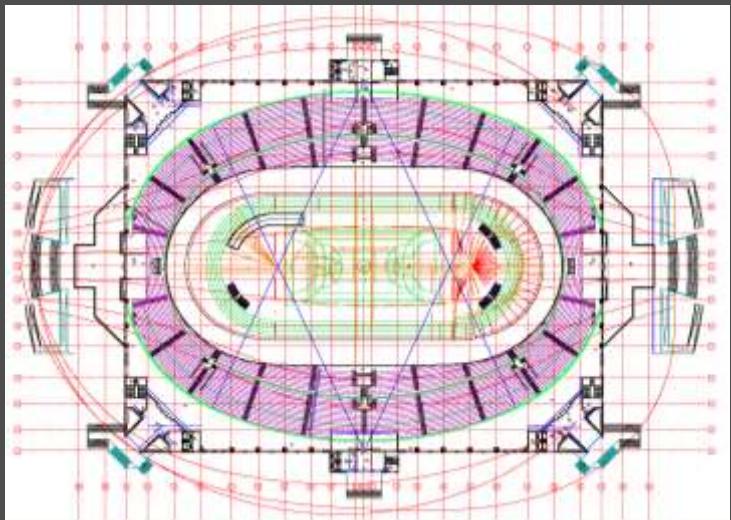
UŠTEDA
3.000.000 \$





KAZAHSTAN - ASTANA

velodrom





KAZAHSTAN

velodrom





KAZAHSTAN - ASTANA

velodrom





pristupno predavanje





ОСЛОНАЦ ЗА КРОВНУ РЕШЕТКУ





RUANDA – KIGALI

POSTROJENJE ZA PIJAĆU VODU





RUANDA – KIGALI

POSTROJENJE ZA PIJAĆU VODU





RUANDA – KIGALI

POSTROJENJE ZA PIJAĆU VODU





RUANDA – BURUNDI MOST



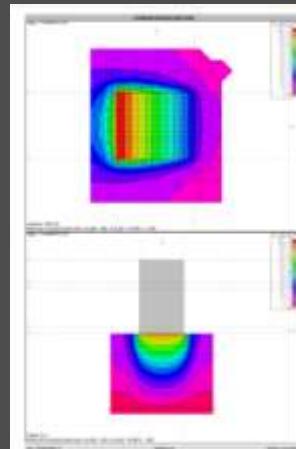


MOZAMBIK





TAĐŽIKISTAN





„POLJOPRIVREDNI KOMBINAT BEOGRAD“ SILOSI U PADINSKOJ SKELI





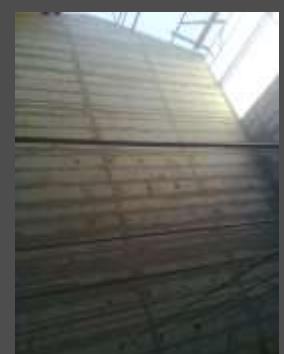
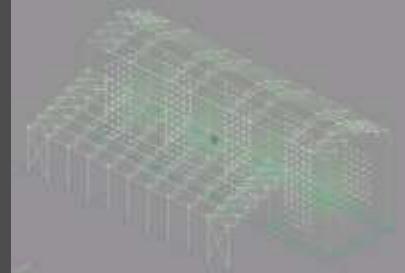
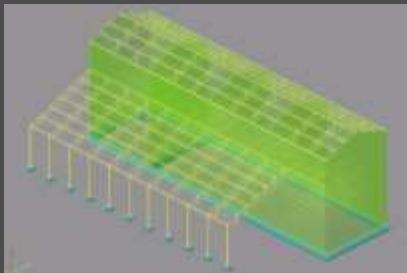
„POLJOPRIVREDNI KOMBINAT BEOGRAD“ FABRIKA STOČNE HRANE I SILOSI





Silosi za žitarice

(podno skladište za žitarice)





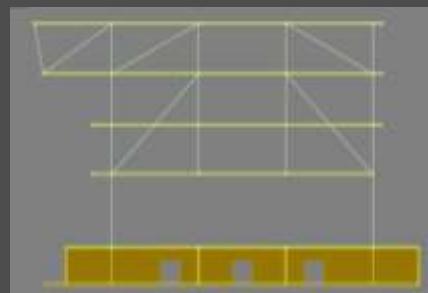
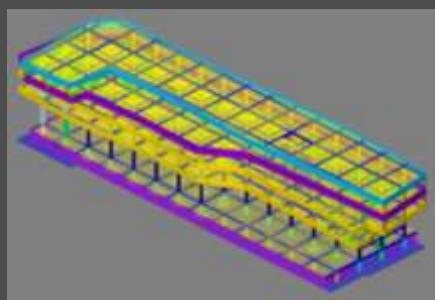
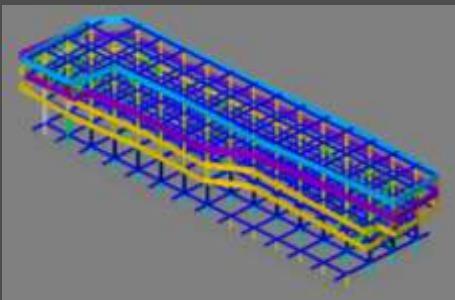
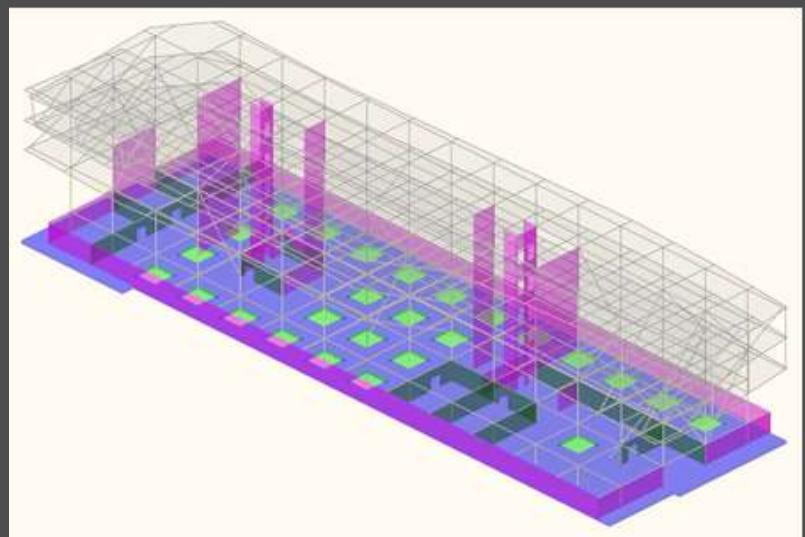
NIŠ

„PAKOM“ – POSLOVNI OBJEKAT





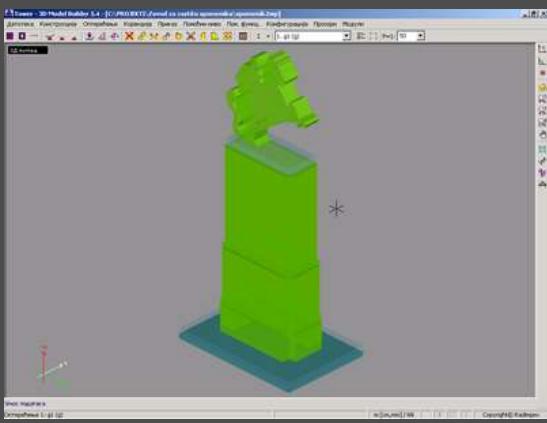
NIŠ NAUČNO TEHNOLOŠKI PARK





NIŠ

Споменик Краљу Александру





KRALJEVO SPORTSKA DVORANA



pristupno predavanje





JAGODINA

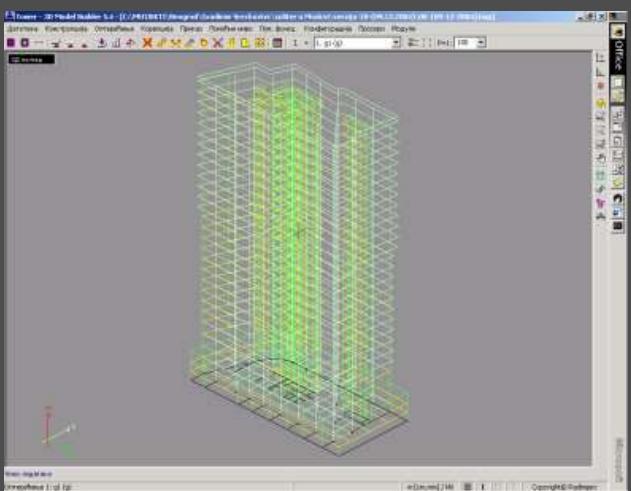
STAMBENO POSLOVNI OBJEKAT





RUSIJA - MOSKVA

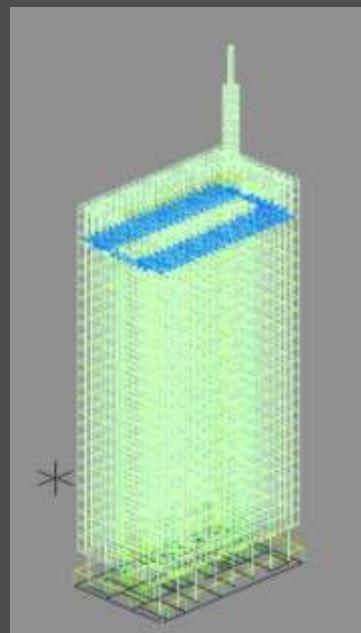
STAMBENO POSLOVNI OBJEKAT OD 33 SPRATA (40 000m²)





BEOGRAD

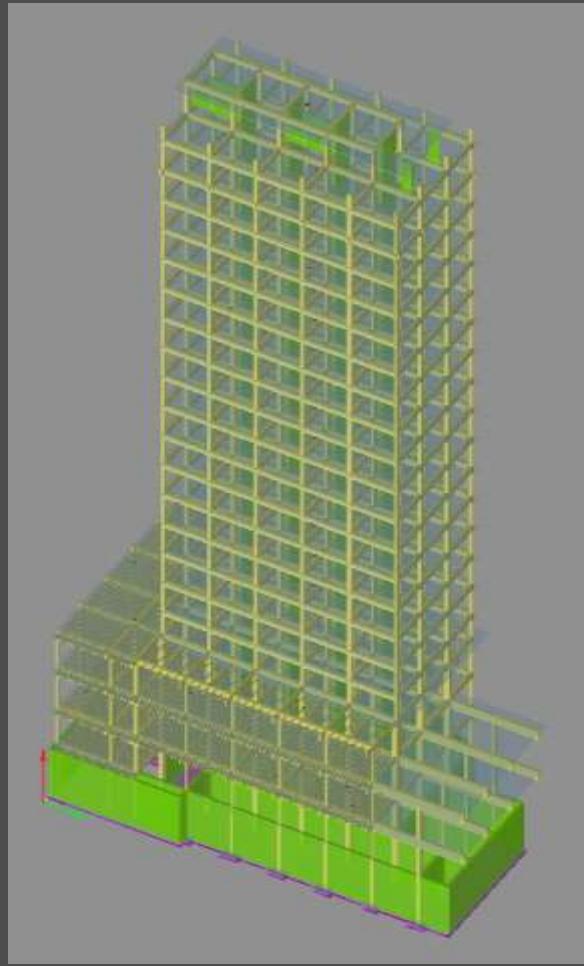
„UŠĆE“ - POSLOVNI OBJEKAT





BEOGRAD

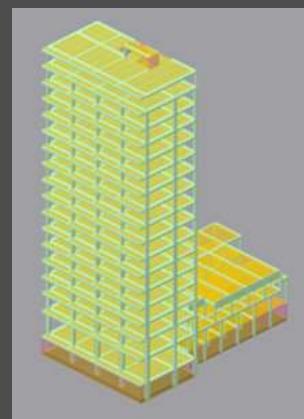
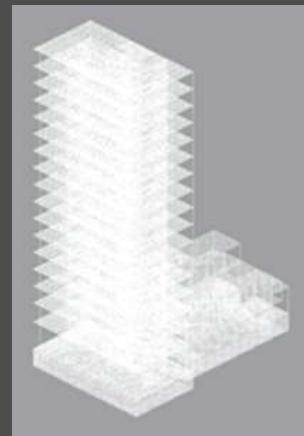
HOTEL „SLAVIJA“ – provera seizmičke otpotnosti





NIŠ

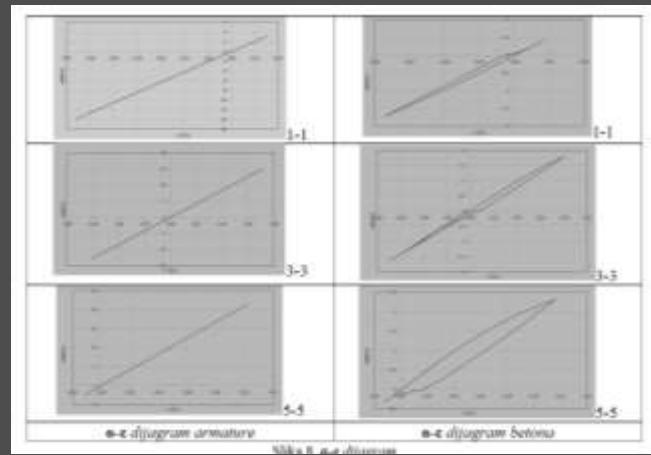
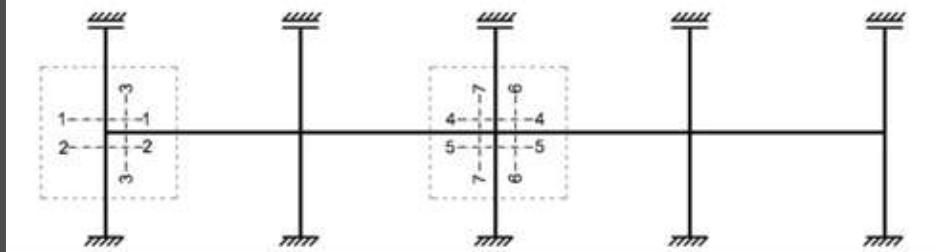
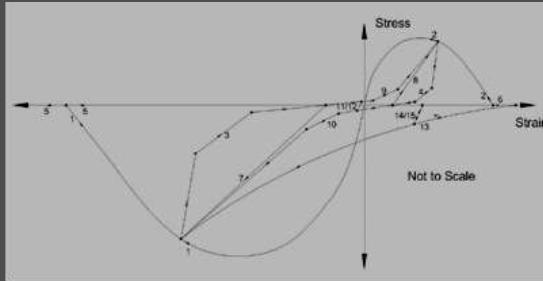
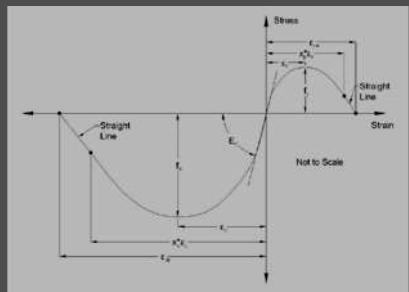
„AMBASADOR“ – HOTEL KONTROLNI PRORAČUN PRILIKOM REKONSTRUKCIJE





NIŠ

„AMBASADOR“ – HOTEL KONTROLNI PRORAČUN PRILIKOM REKONSTRUKCIJE





KAZAHSTAN

SKIJAŠKA SKAKAONICA – PROJEKAT NIJE REALIZOVAN





KAZAHSTAN

SKIJAŠKA SKAKAONICA – PROJEKAT NIJE REALIZOVAN





RUSIJA - MOSKVA

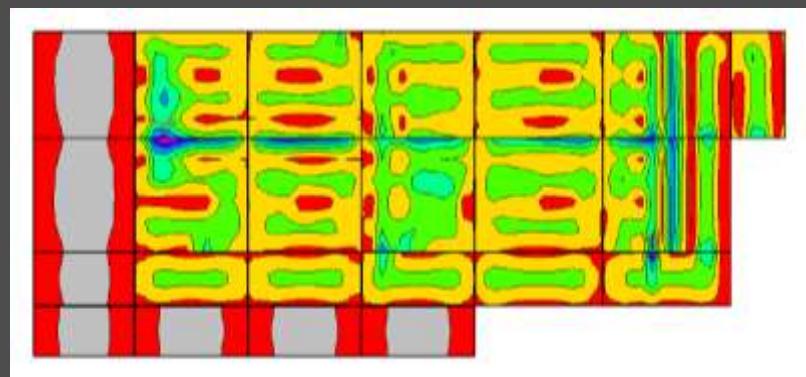
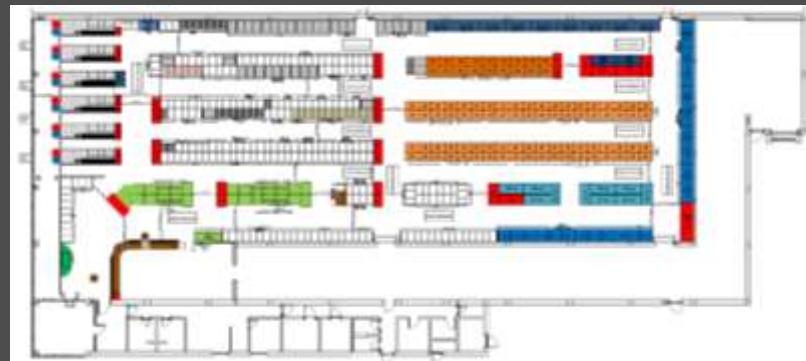
NOVO NASELJE – PROJEKAT NIJE REALIZOVAN





LIDL Valjevo

podna ploča od mikroarmiranog betona





LIDL Valjevo

Load Type	Safety Required			Value	Units
Infill-Bracing Section 12 (Chapter 9)	Single leg load			0.00	mm
	Back-to-back spacing	Agg. load	Brace load	0.00	mm
	Brace load	Agg. load	Brace load	0.00	mm
	Brace load	Brace load	Agg. load	0.00	mm
	Brace width			0.00	mm
	Brick height			0.00	mm
	Brick length			0.00	mm
	Minimum clear leg brace plate distance from post			0.00	mm
	Post width			0.00	mm
	agg. to back leg spacing (maximum 600 mm)			0.00	mm
Agg. Section 12 (Chapter 9)	agg. to back leg spacing (maximum 600 mm)			0.00	mm
	Maximum spacing between legs	Agg. load	Brace load	0.00	mm
	Minimum distance between legs	Agg. load	Brace load	0.00	mm
	Overall width width			0.00	mm
Appendix C	Brick width width			0.00	mm
	Brick height height			0.00	mm
	Height to head plate height			0.00	mm
UFGs Section 12 and 13	Post per square meter			0.00	kg/m ²
	Width width of the UFGs			0.00	mm
	Post width width of the UFGs			0.00	mm
Other Loads Section 12 and 13	Load per linear meter			0.00	N/mm
	Minimum leg load - ultimate condition			0.00	
	Spacing			0.00	mm
Massive (Chapter 9)	Minimum clear leg brace plate distance from post			0.00	mm
	Brace load			0.00	mm
	Other loads			0.00	mm
<p> ■ Agg. to back leg spacing ■ Back-to-back leg spacing ■ Agg. load ■ Brace load ■ Agg. to back leg spacing ■ Post per square meter ■ Width width of the UFGs ■ Height to head plate height ■ Maximum spacing between legs ■ Minimum distance between legs ■ Overall width width ■ Brick width width ■ Brick height height ■ Maximum clear leg brace plate distance from post ■ Brace load ■ Other loads </p>					

Ground-Supported Floor Slab - Design to TR834		SPANIC	
Project:	Supplementary (all)	Job Ref:	V1000
Consultant:		Date ref:	TR834-2023-001 Rev2
Customer:		Date:	21/03/2023
Design Data:			
f_{ck}	50 N/mm ²	characteristic cube compressive strength	
f_{ctk}	5 N/mm ²	characteristic cylinder compressive strength	
f_{tk}	15 N/mm ²	inner compressive strength ($f_{ck,0}$)	
$f_{tk,0}$	20 N/mm ²	inner axial tension strength ($f_{tk,0}^{(0)}$)	
$f_{ck,0}$	5.5 N/mm ²	characteristic axial tensile strength ($f_{ck,0}$)	
σ_{sc}	1.5 N/mm ²	second modulus of elasticity $215 GPa^{1/2}$	
E_{sc}	215 N/mm ²		
α_1	5	Poissos coefficient	
μ	0.5	coefficient of friction	
β_{sp}	0.0005 N/mm ²	influence of sulphate reaction	
T_0	-20 °C	temperature change (initial)	
h	150 mm	depth of slab on grade	
Area #	147.0 m ²	slab plate area (Area for length x width ratio 1.2 for panel)	
Dot Area #	20 m	Dummy area possible	
Ultimate Dead state safety factors:		γ_d	
Plain concrete and steel fibre reinforced concrete.		1.3	
Bar and fabric reinforcement		1.0	
Permanent (dead) actions including rock load		1.2	
Dynamic actions		1.3	
Variable actions		1.3	
Semi-elliptical limit state safety factors:			
All partial safety factors:		1.0	

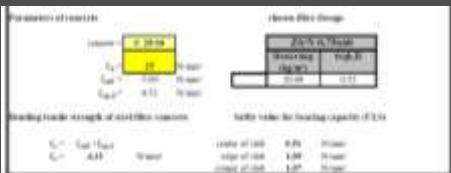
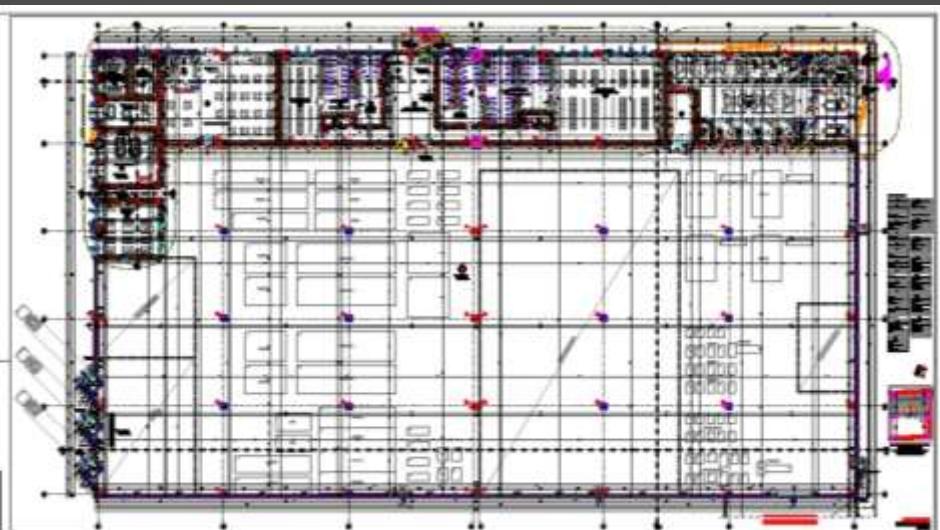
<p>Analysis:</p> <p>Concrete C20/28M</p> <table border="1" style="margin-left: auto; margin-right: auto;"> <tr> <th colspan="4">25% load increased max.</th> </tr> <tr> <th>Design Value</th> <th>f_{ck} N/mm²</th> <th>α_{sl} %</th> <th>AB</th> </tr> <tr> <td>28</td> <td>1.3</td> <td>40</td> <td>53.81</td> </tr> </table> <p>$f_{ck} = 1.3 \times 1.27 = 1.67 \text{ N/mm}^2$</p> <p>$f_{ck} = 1.3 \times (200)^{0.5} = 1.3 \times 1.27 = 1.67 \text{ N/mm}^2$</p> <p>$M_{u1} = 1.67 \times 1000 \times 100^2 / 8 = 2.08 \times 10^6 \text{ N-mm}$</p> <p>$M_{u2} = 1.67 \times 1000 \times 100^2 / 8 = 2.08 \times 10^6 \text{ N-mm}$</p> <table border="1" style="margin-left: auto; margin-right: auto;"> <tr> <th colspan="3">Safety factors</th> </tr> <tr> <th>No.</th> <th>f_s</th> <th>ϕ</th> </tr> <tr> <td>1</td> <td>0.85</td> <td>0.85</td> </tr> <tr> <td>2</td> <td>0.85</td> <td>0.85</td> </tr> </table> <p>Meyerhoff's Field Line Theory:</p> <p>$M_u = M_{u1} + M_{u2}$ radius of neutral surface</p> <p>$M_u = M_{u1} - M_{u2}$ negative lagging moment capacity</p> <p>$M_u = M_{u1} + M_{u2} / k_1 + k_2 / 2(1 + k_1/k_2)$ positive lagging moment capacity</p> <p>3. General Strength/Stresses from load:</p> <p>$M_u = 2.08 \times 10^6 \text{ N-mm}$ $\lambda_1 = 1.3$ factor accounted in calculation for AB</p> <p>$S = 0.536 \text{ N/mm}^2 = (1.3 \times 1.67) \times 10^6 / 100^2$</p> <p>$S = 23.0 \text{ N/mm}^2 = (1.3 \times 1.67) \times 10^6 / 100^2$ Hansen's equations</p> <p>Load arrangement for max lagging moment:</p> <p>Load arrangement for min lagging moment:</p>	25% load increased max.				Design Value	f_{ck} N/mm ²	α_{sl} %	AB	28	1.3	40	53.81	Safety factors			No.	f_s	ϕ	1	0.85	0.85	2	0.85	0.85	
25% load increased max.																									
Design Value	f_{ck} N/mm ²	α_{sl} %	AB																						
28	1.3	40	53.81																						
Safety factors																									
No.	f_s	ϕ																							
1	0.85	0.85																							
2	0.85	0.85																							





„JOHNSON ELECTRIC“ u Nišu

podna ploča od mikroarmiranog betona



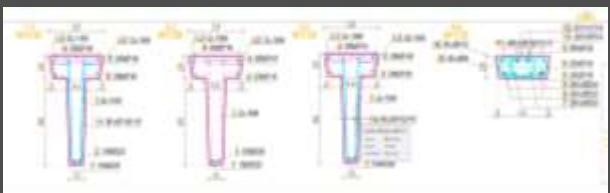
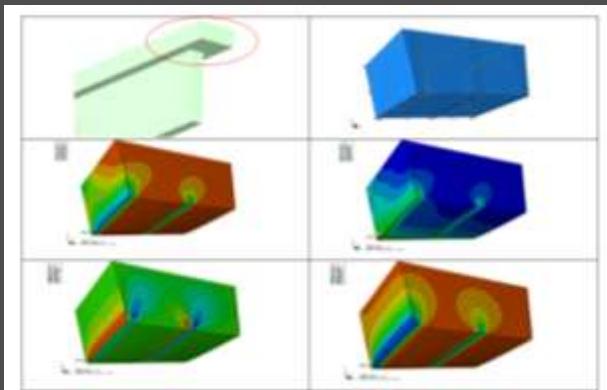
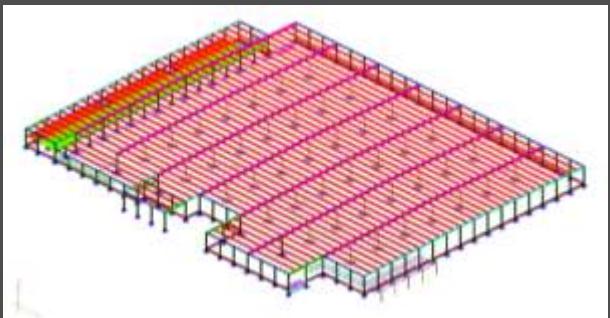
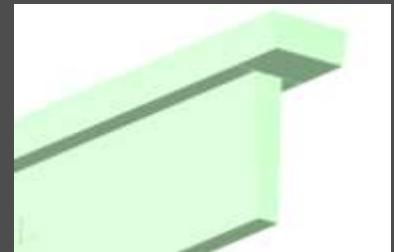
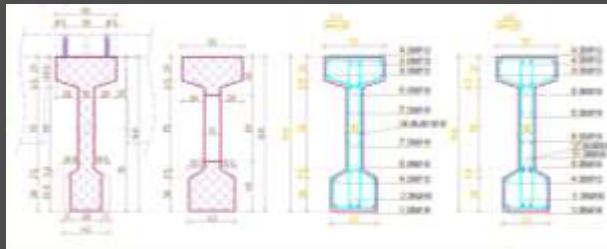
pristupno predavanje





Фабрика „АРТИВ“ у Лесковцу

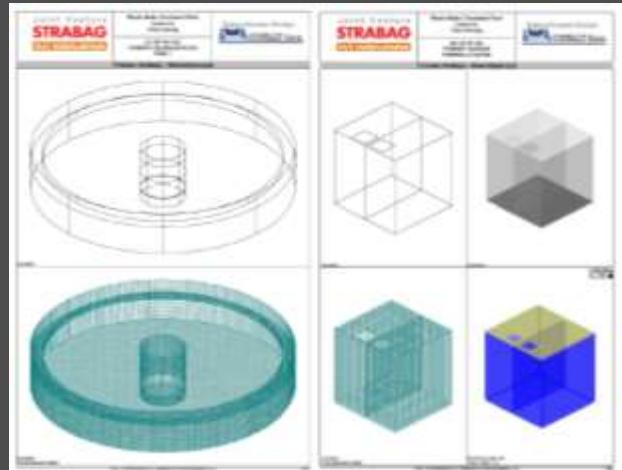
санација ослонаца кровних носача





LESKOVAC

POSTROJENJE ZA PREČIŠĆAVANJE VODE – KAPACITET 80000 EJ





pristupno predavanje





LESKOVAC

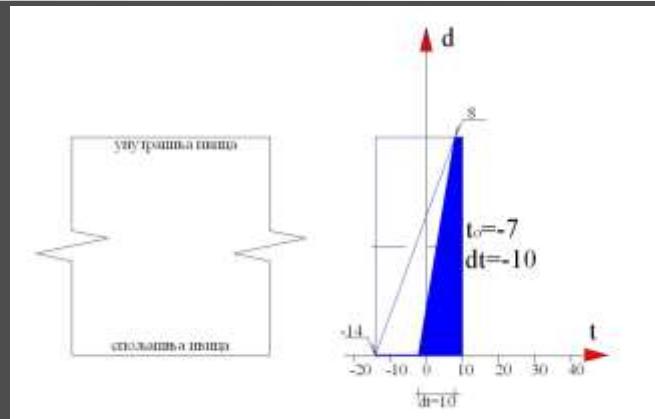
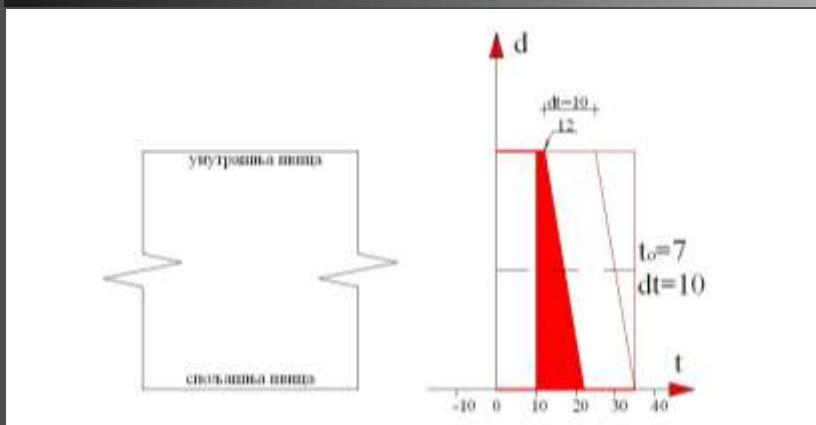
POSTROJENJE ZA PREČIŠĆAVANJE VODE – KAPACITET 80000 EJ





LESKOVAC

POSTROJENJE ZA PREČIŠĆAVANJE VODE – KAPACITET 80000 EJ



Температурни утицаји у плочи

$t_0 :$	7.00	°C
$dt :$	10.00	°C

A diagram of a rectangular plate showing a triangular temperature profile on its right side. The top vertex of the triangle is at t_0 and the bottom vertex is at $t_0 + dt$. The width of the base of the triangle is also dt .

Прихвати Одустани

Температурни утицаји у плочи

$t_0 :$	-7.00	°C
$dt :$	-10.00	°C

A diagram of a rectangular plate showing a triangular temperature profile on its right side. The top vertex of the triangle is at t_0 and the bottom vertex is at $t_0 + dt$. The width of the base of the triangle is also dt .

Прихвати Одустани



LESKOVAC

POSTROJENJE ZA PREČIŠĆAVANJE VODE – KAPACITET 80000 EJ

Tabela 5 - Računske granične temperature

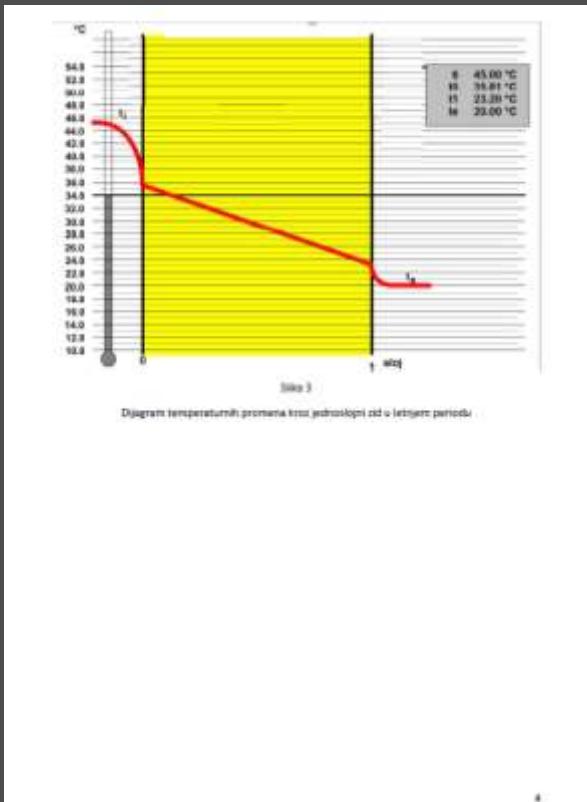
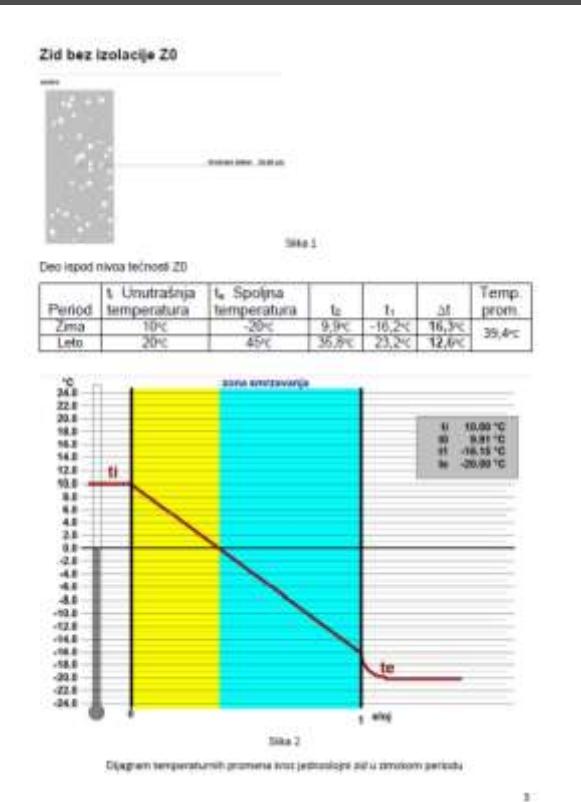
Osnovni materijal mosta	Najviša temperatura	Referentna temperatuta	Najniža temperatuta	Promena temperatuta
	°C			
Metali i spregnuti materijali	+ 45	+ 10	- 25	± 35
Beton (armirani i prednapregnuti)	+ 35	+ 10	- 15	± 25
Kamen	+ 30	+ 10	- 10	± 20





LESKOVAC

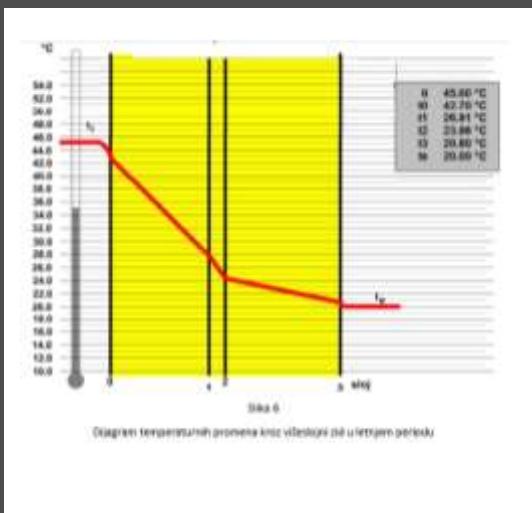
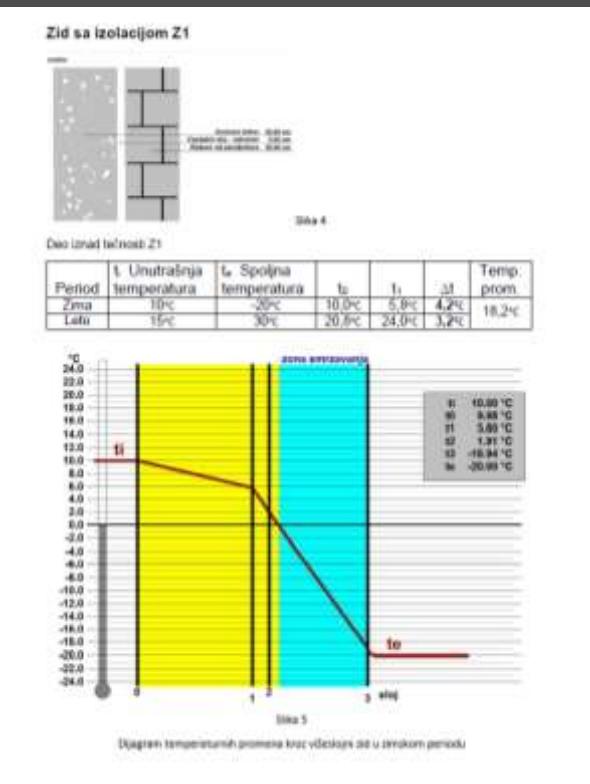
POSTROJENJE ZA PREČIŠĆAVANJE VODE – KAPACITET 80000 EJ





LESKOVAC

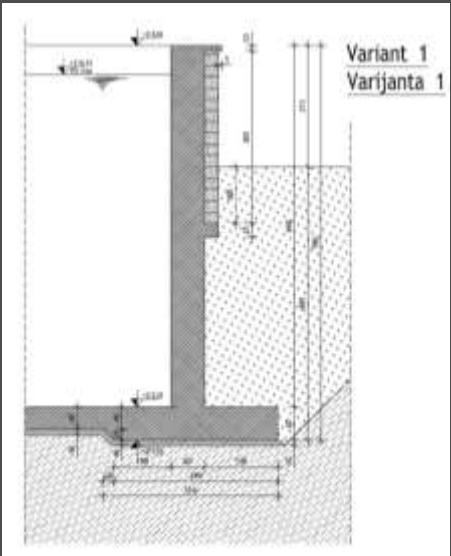
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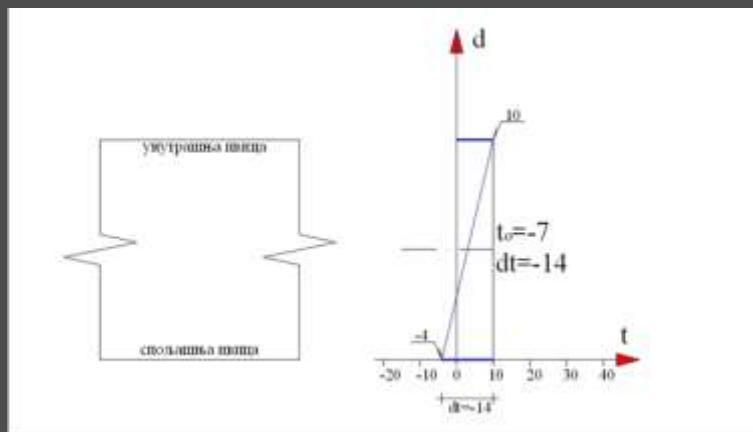
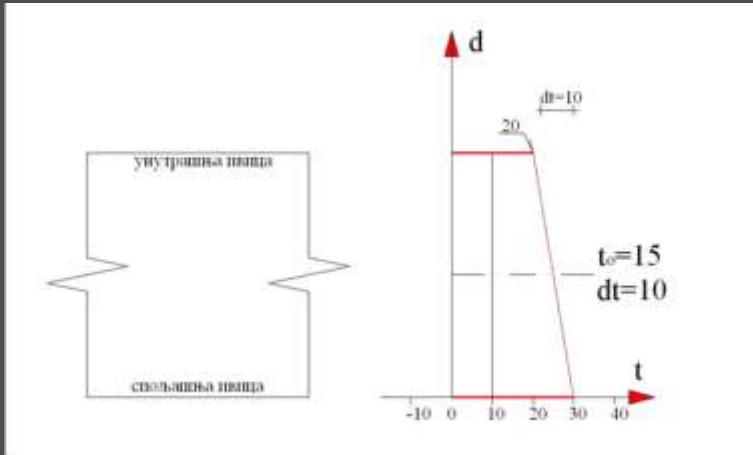


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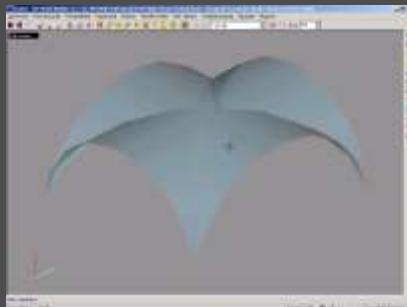
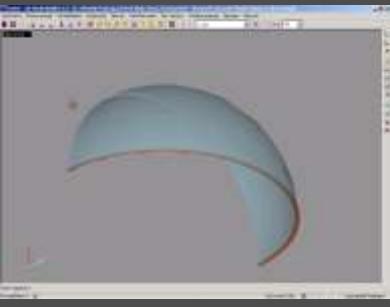
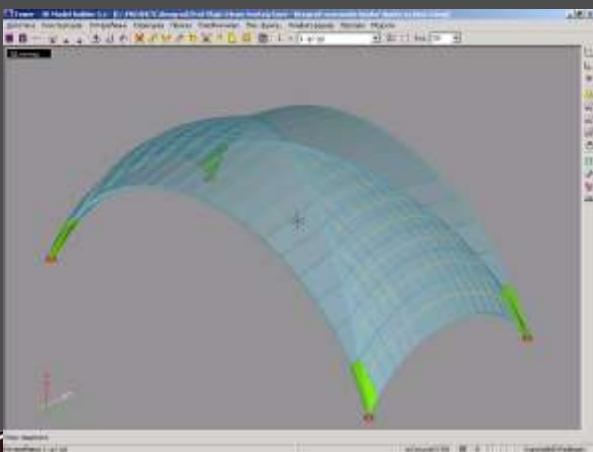
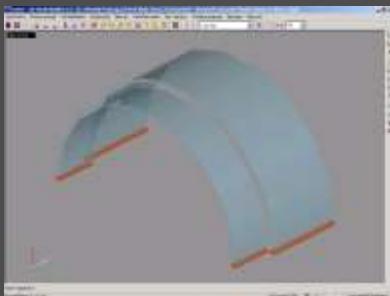
	јан	феб	мар	апр	мај	јун	јул	авг	септ	окт	нов	дек	јан
ТЕМПЕРАТУРА, °C													
Средња и максимална	4,4	7,1	15,7	28,3	33,2	26,9	29,3	29,4	24,0	18,0	11,2	5,6	17,6
Средња и минимална	-0,7	-2,7	3,1	5,2	13,0	34,7	13,9	10,3	7,9	1,2	-2,0	-9,5	-9,5
Нормална креација	8,1	11,1	19,1	31,0	34,4	19,7	21,4	27,2	16,3	11,2	4,8	1,1	1,1
Нормална креација	20,0	23,7	26,7	30,8	36,0	30,8	32,1	38,4	27,4	23,6	21,4	14,7	14,7
Изодијутични максимуми	-35,3	-25,9	-15,0	-6,3	0	2,7	8,4	4,6	0,5	-6,7	-16,6	-23,7	-30,0
Ср. бр. кратких дана	24	20	12	3	0	0	0	0	3	12	19	93	93
Ср. бр. трошака дана	0	0	0	0	2	7	13	15	0	0	0	42	42
РЕДАЦИЈЕ ВРЕЋА (%)													
Промене	82	77	70	68	69	68	67	66	73	77	81	83	75
СРЕДЊЕ И ЕКСТРЕМНЕ ВРЕДНОСТИ 1981-2010													
СРЕДЊЕ СЛJАДИ СРЧАЦ													
Промене	66,4	90,1	140,8	144,0	214,3	255,2	294,8	328,6	103,4	147,3	95,4	50,9	1026,1
Број кратких дана	4	9	5	5	7	12	14	10	6	5	3	3	79
Број обично дана	15	12	11	10	9	5	4	3	6	9	12	16	112
ЛАДАНИЈЕ (mm)													
Ср. највећи	42,2	49,7	48,9	40,5	55,0	94,1	84,2	47,2	51,4	51,1	61,9	55,2	475,4
Ср. донесена вода	28,5	32,5	32,0	30,9	40,8	93,7	89,1	47,9	39,7	32,7	55,9	40,3	441
Ср. бр. дана >= 0,5 год	13	13	12	13	15	8	7	9	10	12	14	137	137
Ср. бр. дана >= 10,0 год	1	1	1	1	2	3	1	2	2	3	2	19	19
ПОДАЦЕ (Број дана год...)													
погаји	9	8	5	1	0	0	0	0	0	0	0	35	35
окажани покриданци	15	12	12	10	12	2	2	0	2	2	4	49	49
изложени	4	3	2	0	2	2	0	0	2	2	1	39	39
изложен	0	0	0	0	0	0	0	0	0	0	0	0	0





BEOGRAD

HRAM SVETOG SAVE





NIŠ

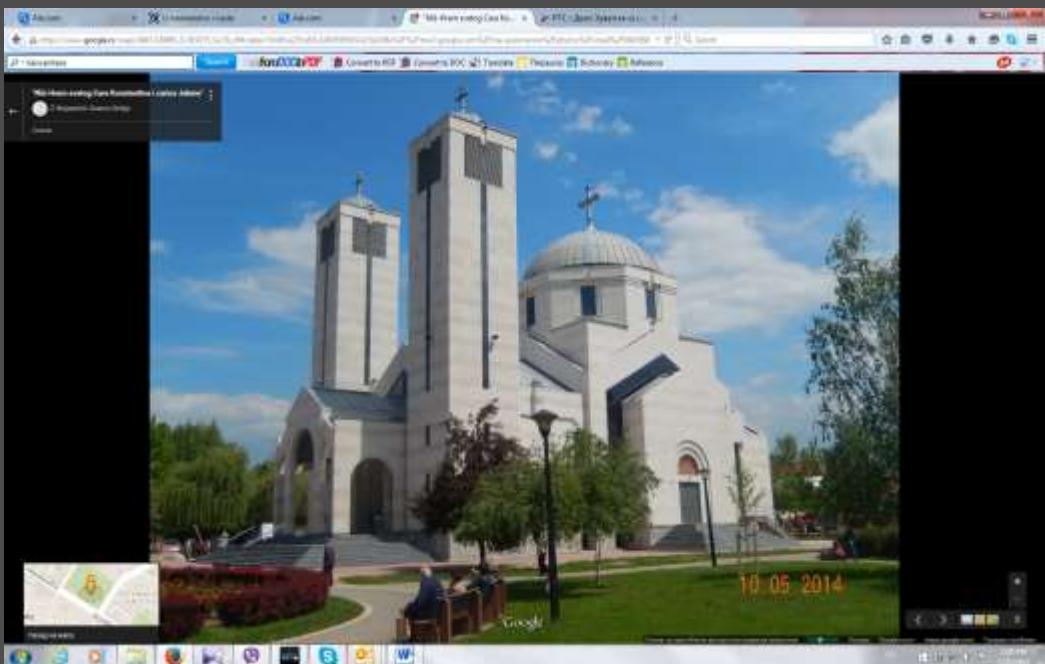
SABORNA CRKVA – REKONSTRUKCIJA POSLE POŽARA





NIŠ

HRAM SVETOG CARA KONSTANTINA I CARICE JELENE

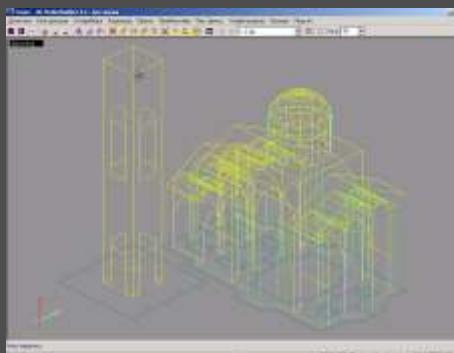
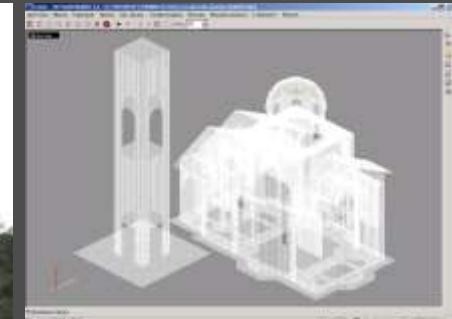


pristupno predavanje



LUKOVSKA BANJA

CRKVA SV. ĐORĐA





PROLOM BANJA

CRKVA PREOBRAŽENJA GOSPODNEG





ZVEČAN-SUNČANA DOLINA

CRKVA SVETOG KRALJA STEFANA DEČANSKOG





NIŠ

ZVONIK ISPRED HRAMA VASKRSEЊA





JOŠANJČKA BANJA

SPOMEN KOMPLEKS „MILUNKA SAVIĆ“





MOST PREKO REKE JUŽNE MORAVE





MOST U CENTRU NIŠA PREKO REKE NIŠANE OŠTEĆEN BOMBARDOVANJEM I REKONSTRUISAN



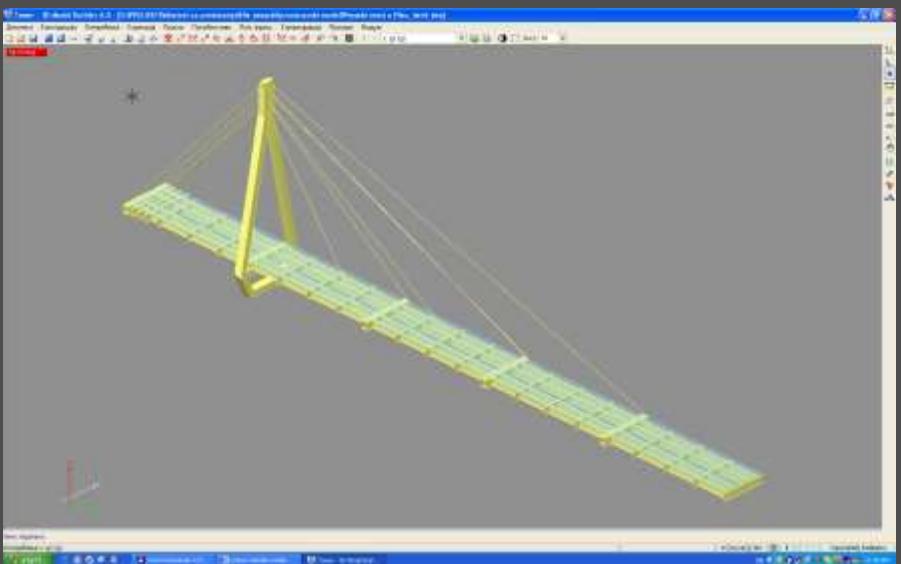


MOSTOVI PREKO REKE JABLJANICE OŠTEĆENI BOMBARDOVANJEM



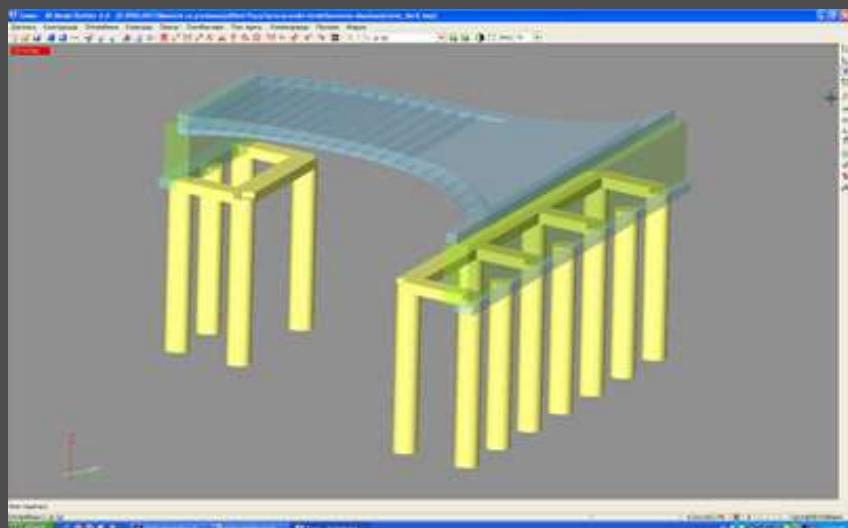


PEŠAČKI MOST U NIŠU





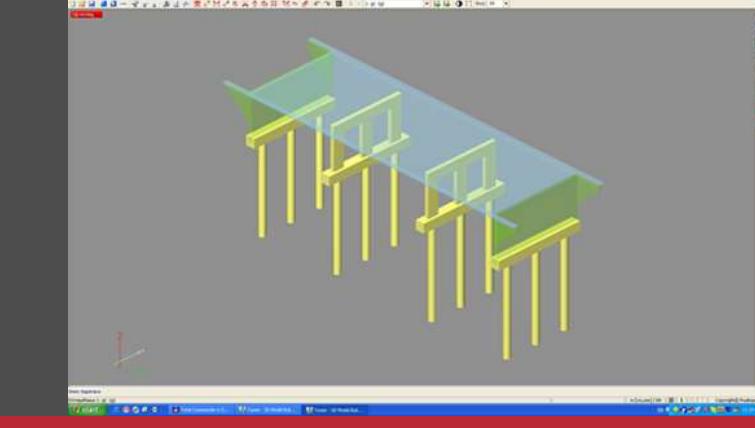
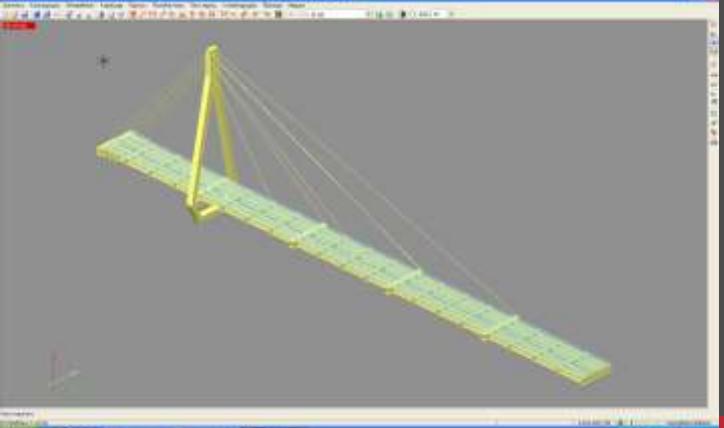
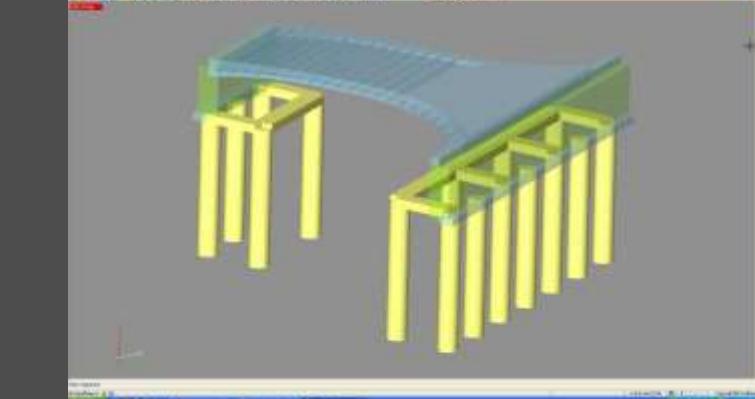
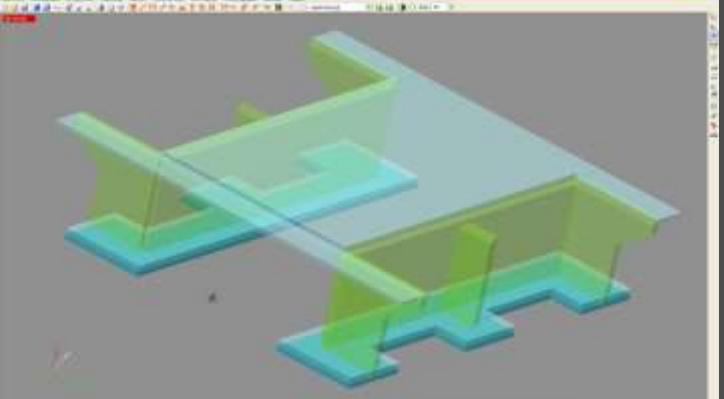
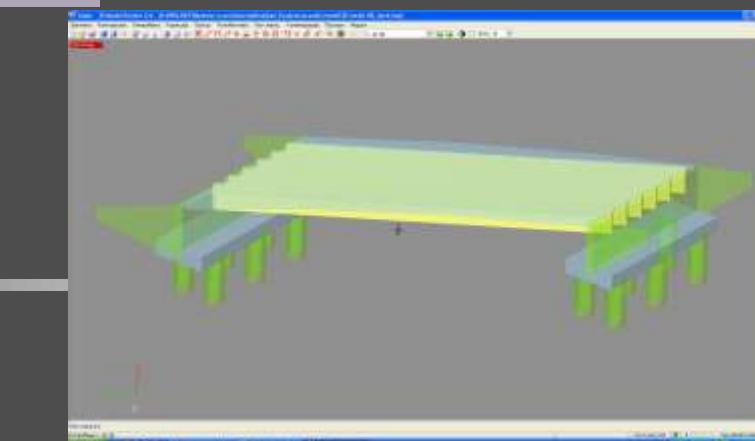
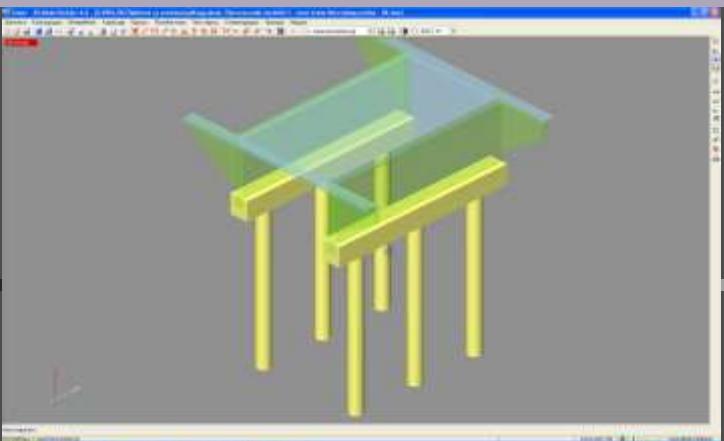
MOST U NOVOM PAZARU PREKO REKE RAŠKE

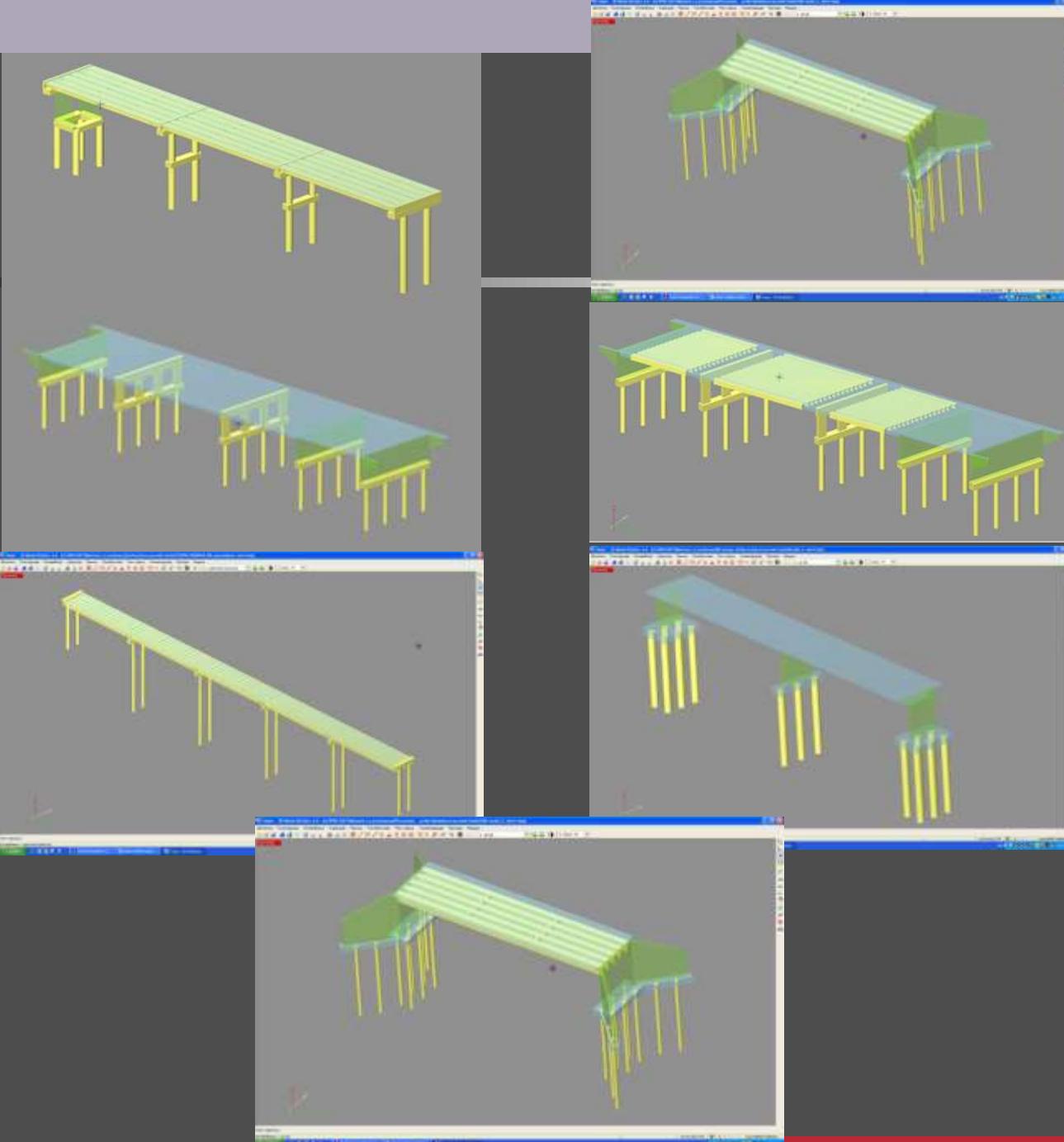




MOST U KRAGUJEVCU PREKO REKE LEPE NICE





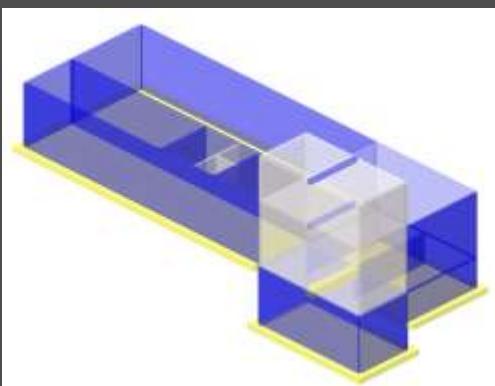




OTKLANJANJE (TUĐIH) GREŠKA U PROJEKTOVANJU

LESKOVAC

„JEANCI SERBIA“ – FABRIKA ZA PROIZVODNJU TEKSASA





OTKLANJANJE (TUĐIH) GREŠAKA U IZVOĐENJU

SVRLJIG MOST PREKO SVRLJIŠKOG TIMOKA



pristupno predavanje



OTKLANJANJE (TUĐIH)
GREŠAKA U
IZVOĐENJU

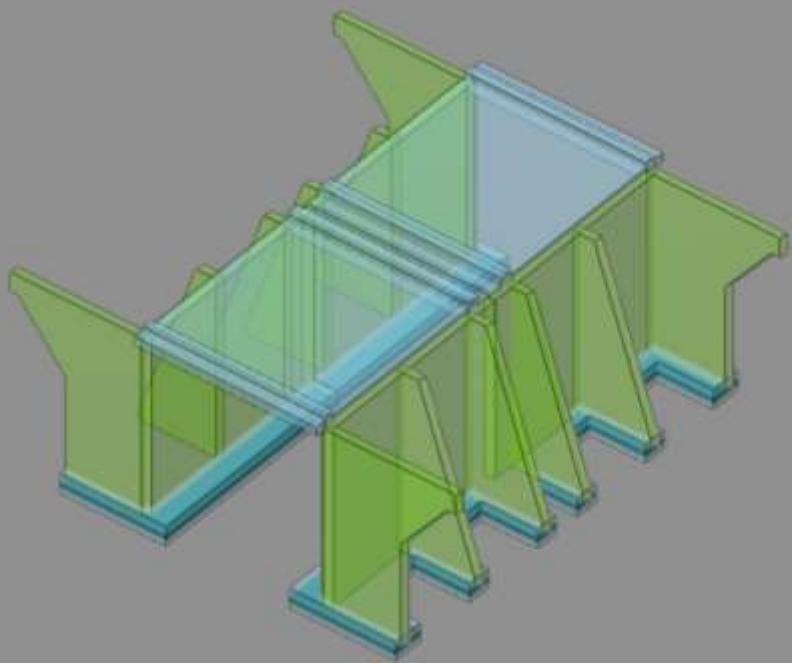
SVRLJIG

MOST PREKO SVRLJIŠKOG TIMOKA



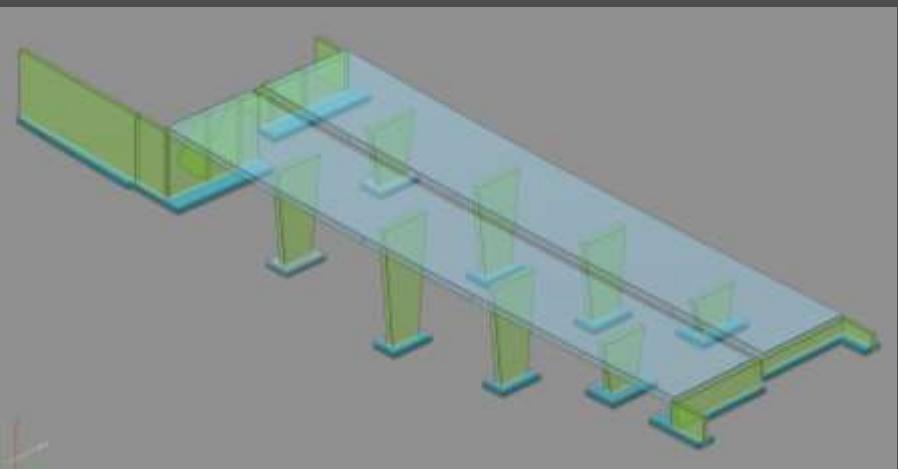


OTKLANJANJE (TUĐIH) GREŠAKA U PROJEKTNOM ZADATKU



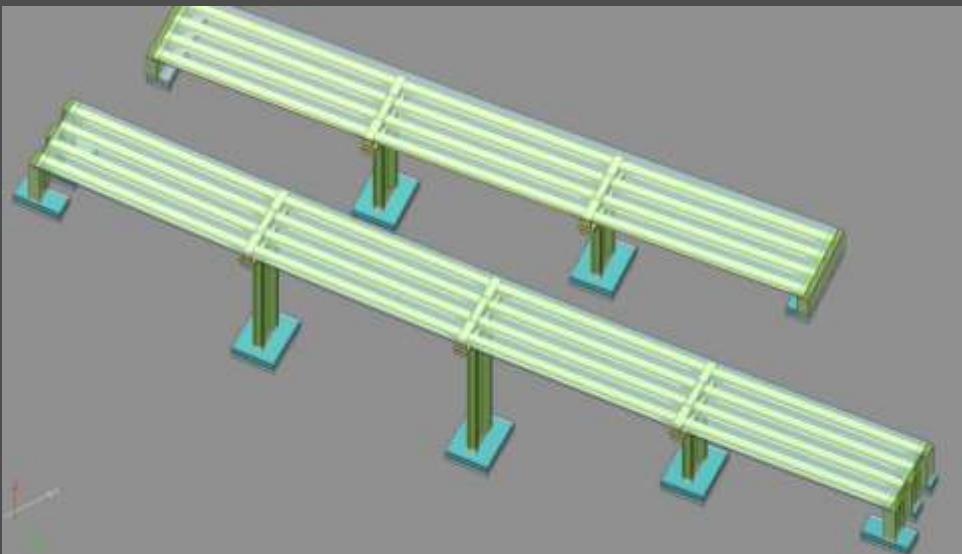


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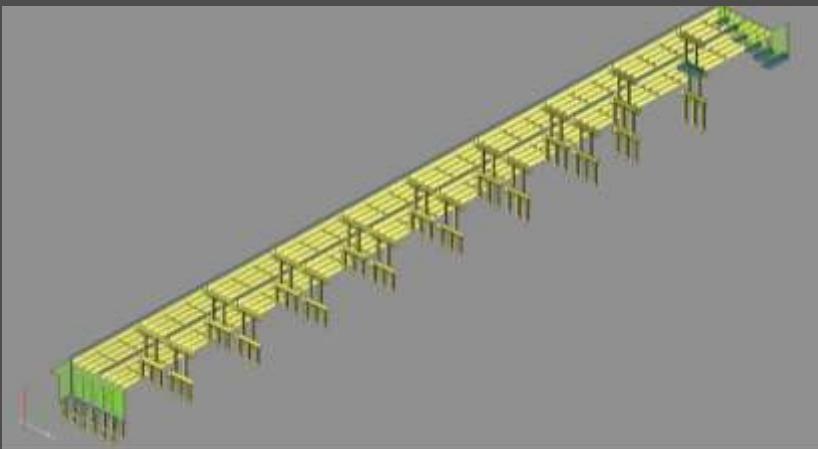
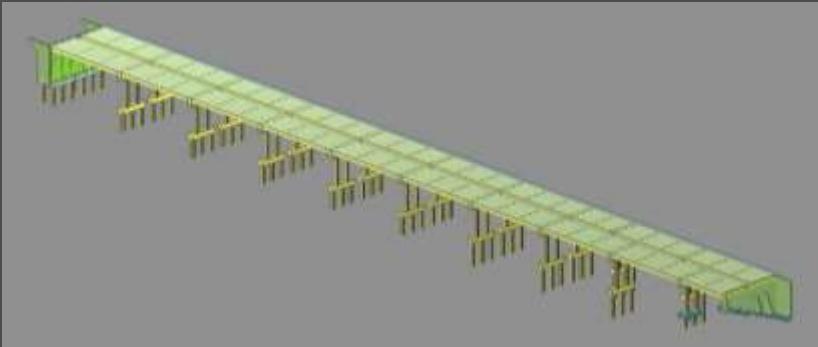


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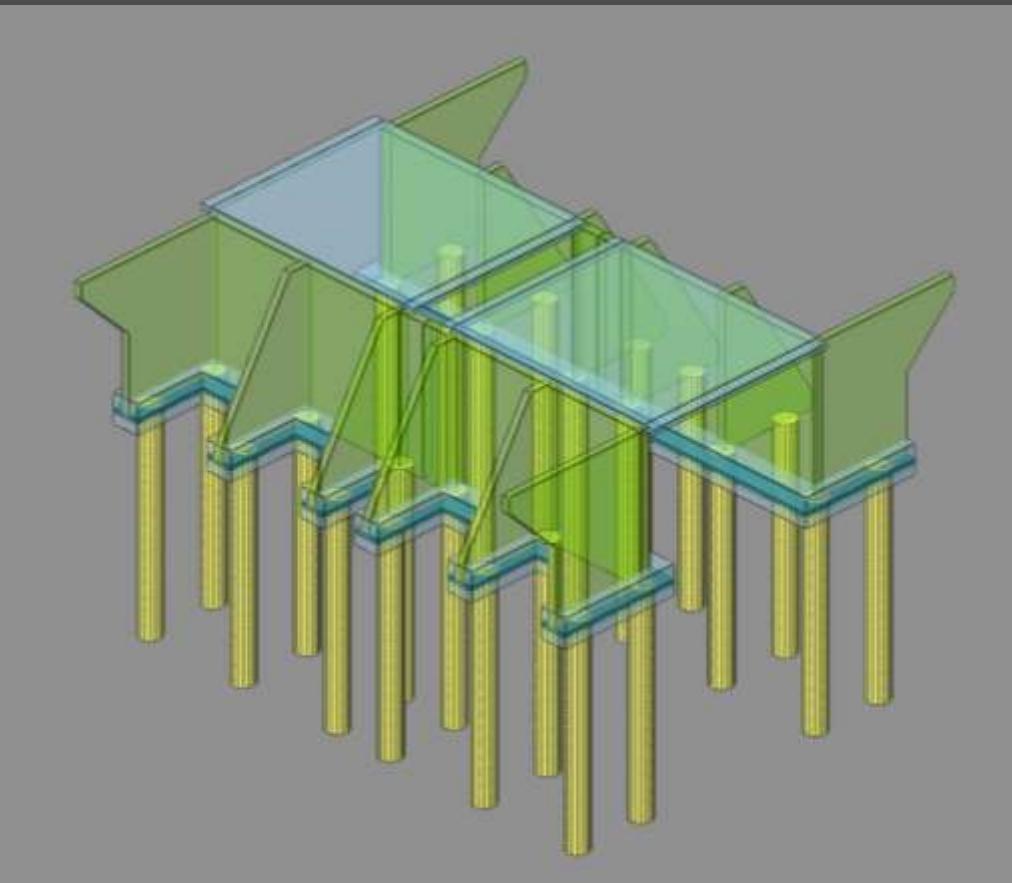


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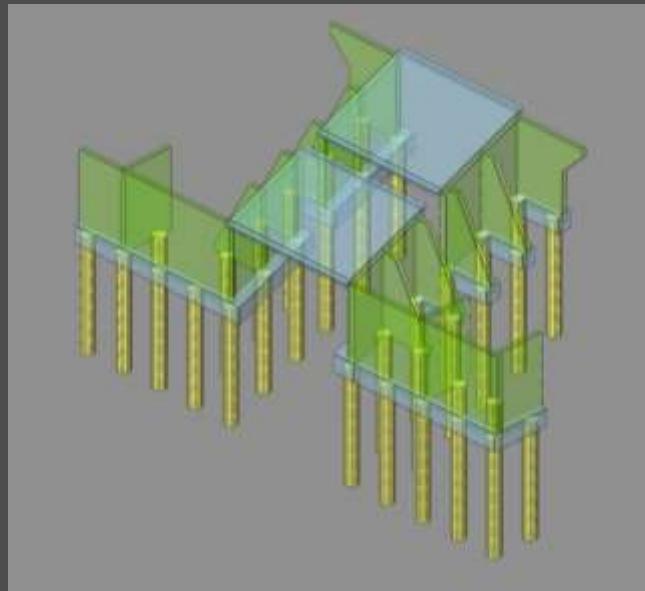


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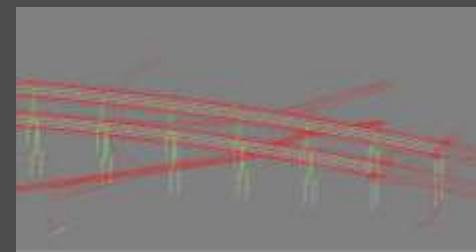
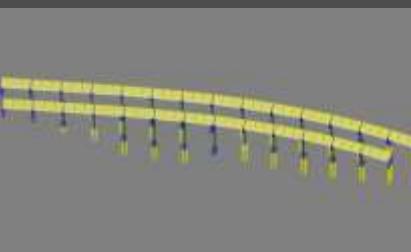
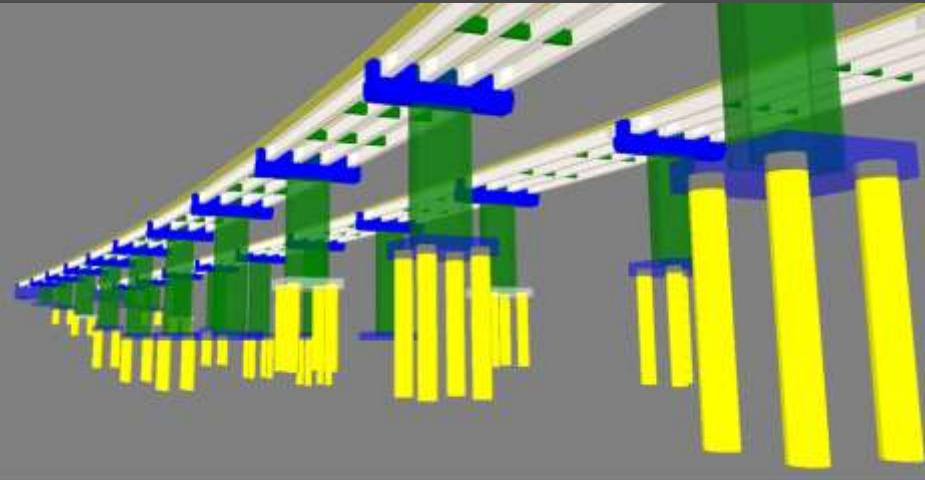


OTKLANJANJE (TUĐIH) GREŠAKA U PROJEKTNOM ZADATKU





OTKLANJANJE (TUĐIH) GREŠAKA U PROJEKTNOM ZADATKU





BIM



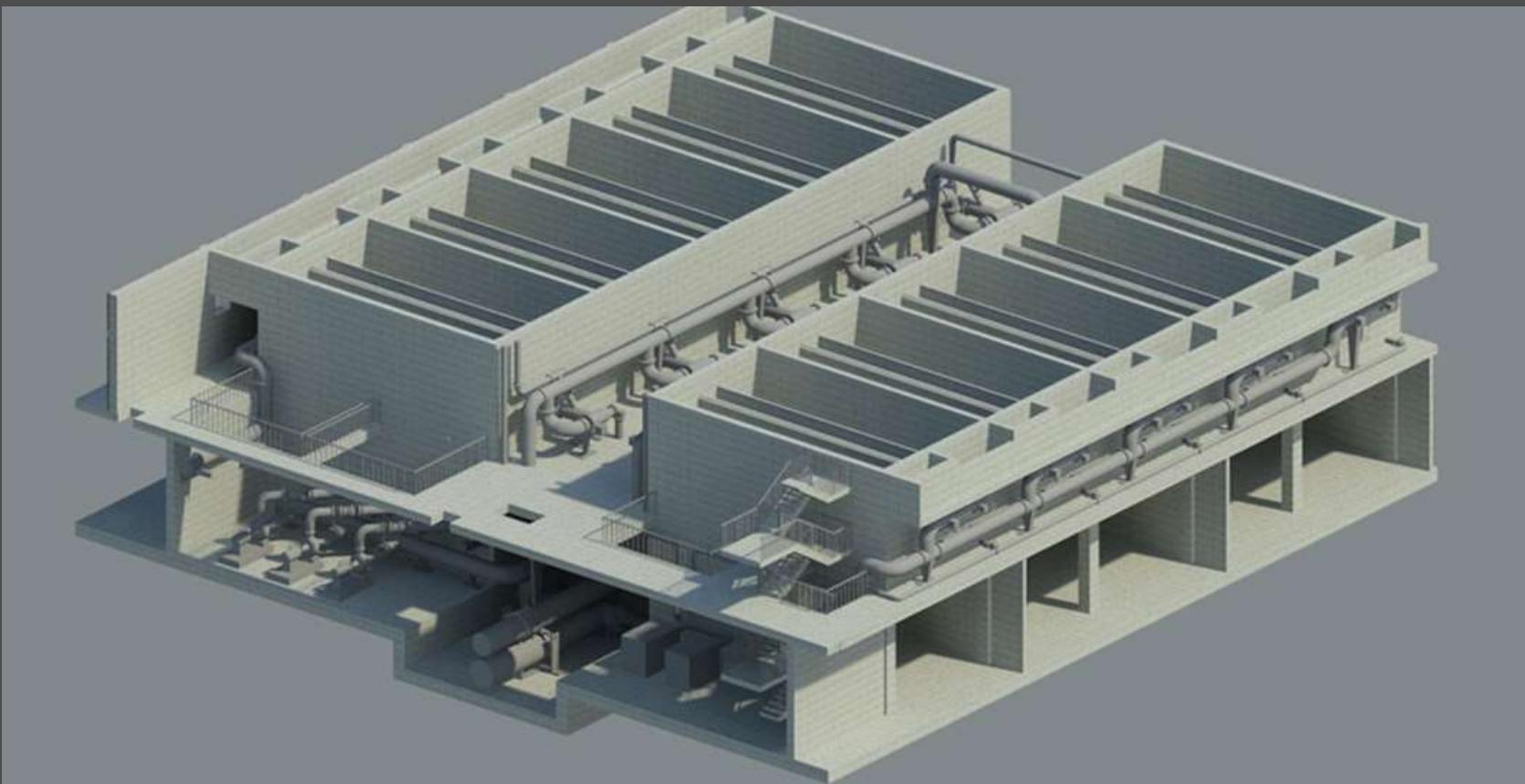
pristupno predavanje



BIM

NOVI SAD

POSTROJENJE ZA PIJAĆU VODU „ŠTRAND“

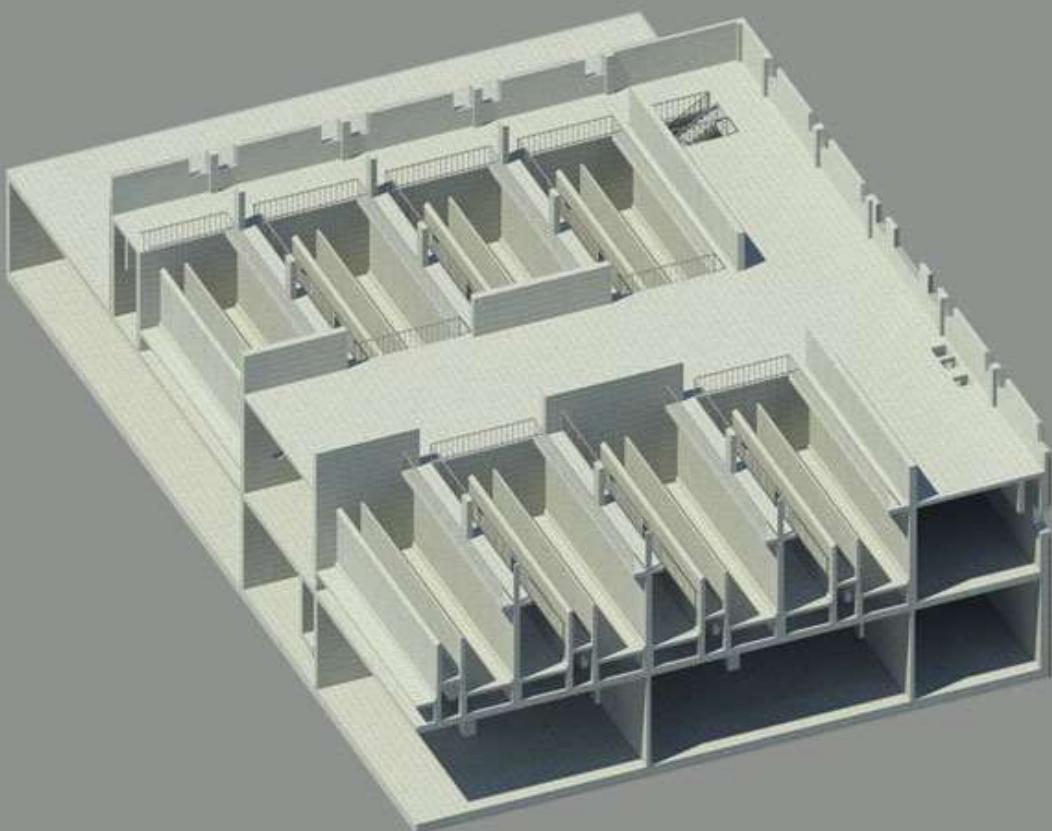




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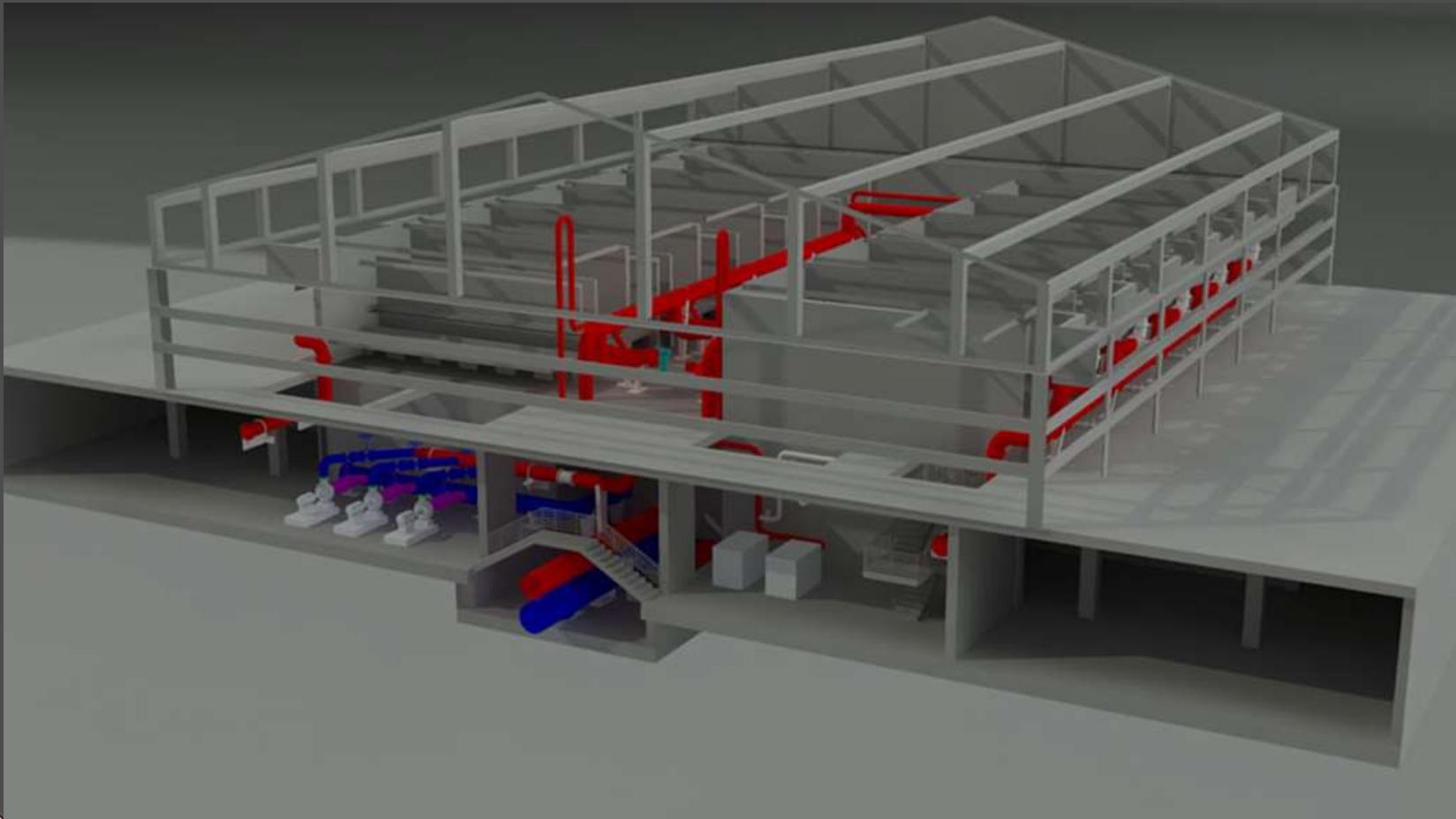




BIM

NOVI SAD

POSTROJENJE ZA PIJAĆU VODU „ŠTRAND“





BIM

NOVI SAD

POSTROJENJE ZA PIJAĆU VODU „ŠTRAND“





BIM

NOVI SAD

POSTROJENJE ZA PIJAĆU VODU „ŠTRAND“





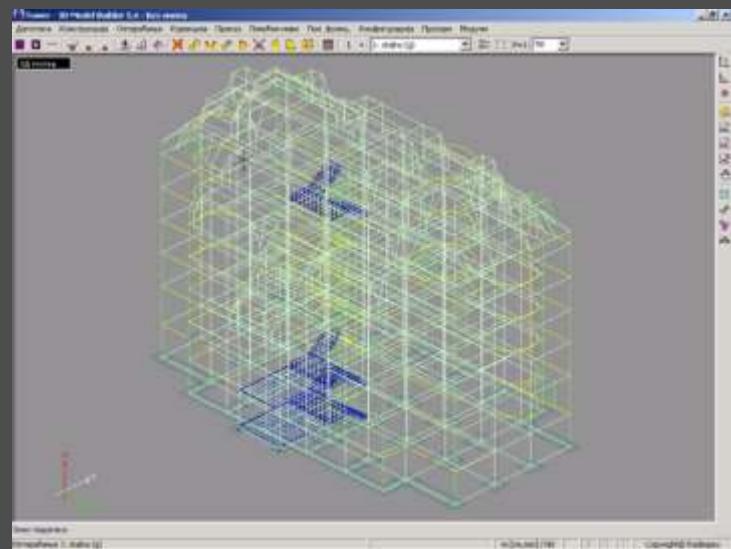
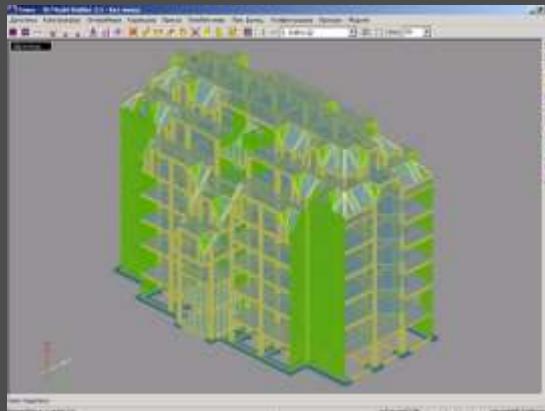
OBJEKTI KATEGORISANI KAO REFERENCA ZA „VELIKU LICENCU“





KOPAONIK - VILA „NIKOLA“

objekat u zaštićenoj zoni



pristupno predavanje



KOPAONIK - HOTEL APARTMANSKOG TIPOV objekat u zaštićenoj zoni





KOPAONIK

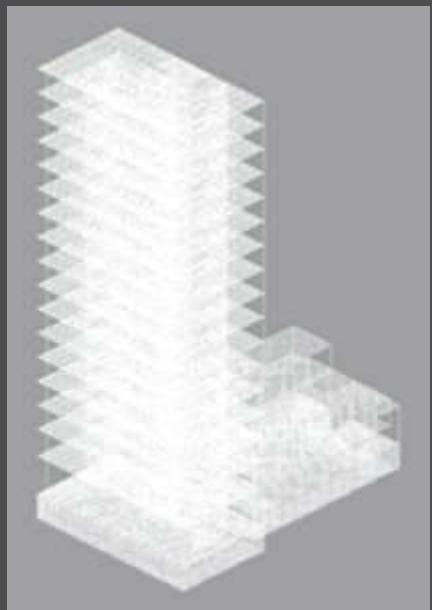
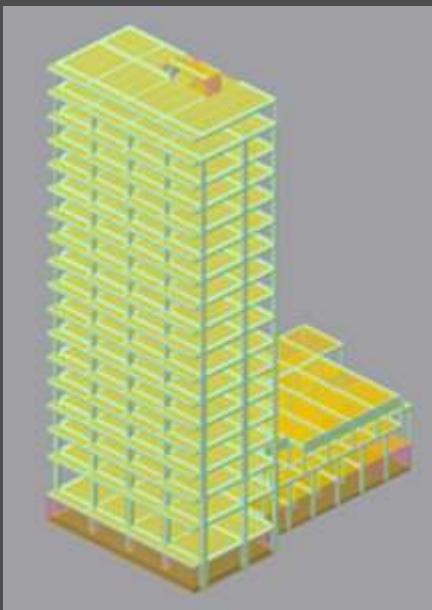
HOTEL „NEBESKE STOLICE“ DRUGA FAZA

objekat u zaštićenoj zoni



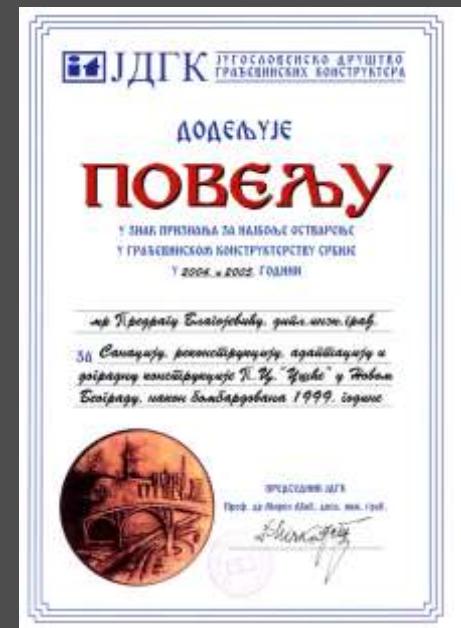
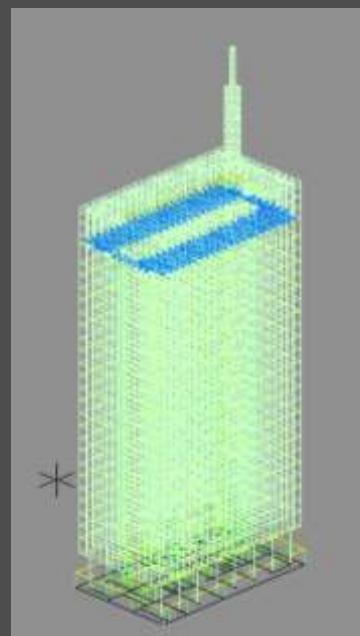


NIŠ - HOTEL „AMBASADOR“ objekat visine preko 50m



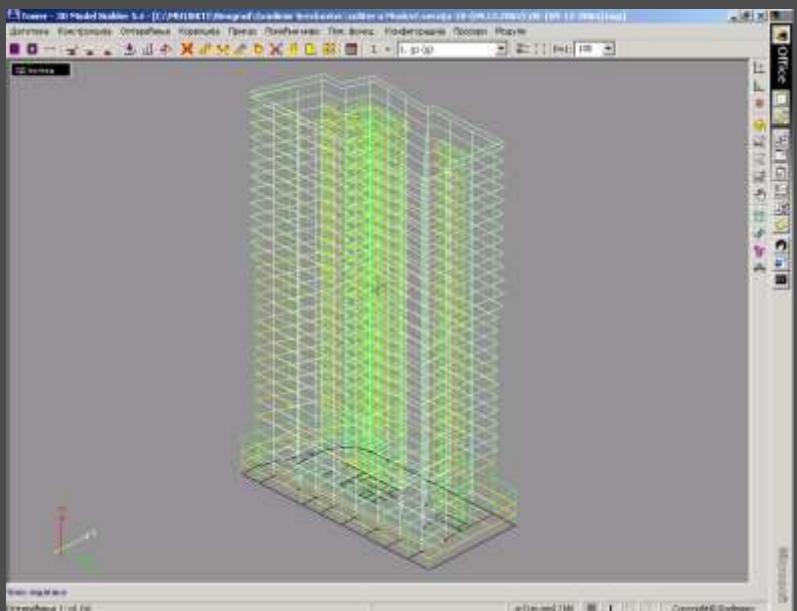
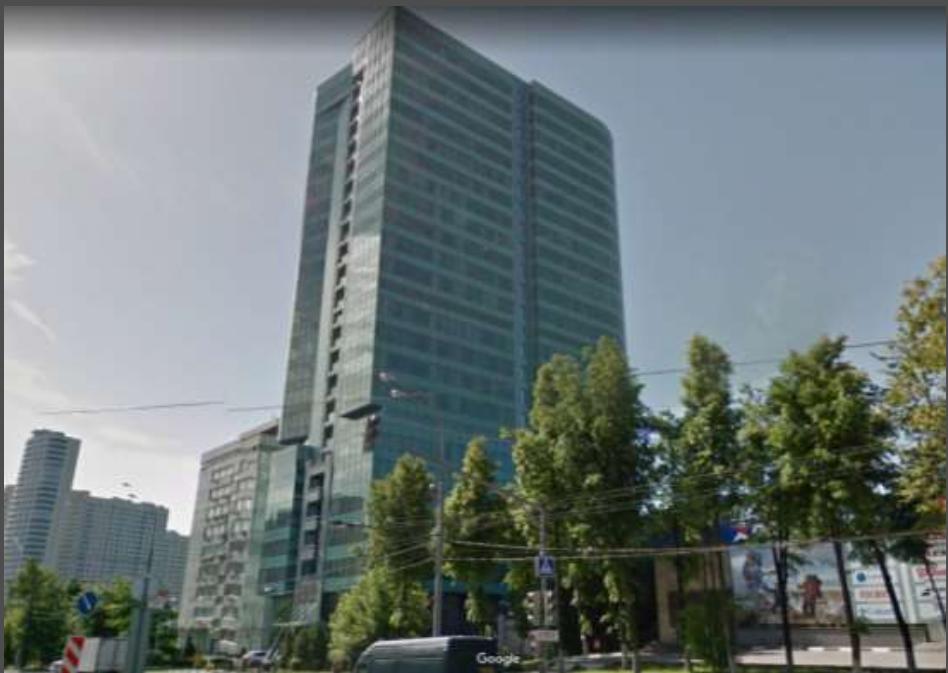


BEOGRAD - POSLOVNI CENTAR „UŠĆE“ objekat visine preko 50m





MOSKVA - STAMBENO POSLOVNI OBJEKAT objekat visine preko 50m

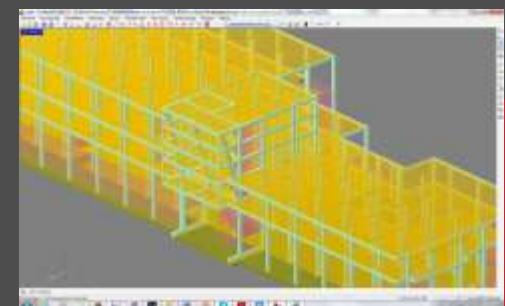
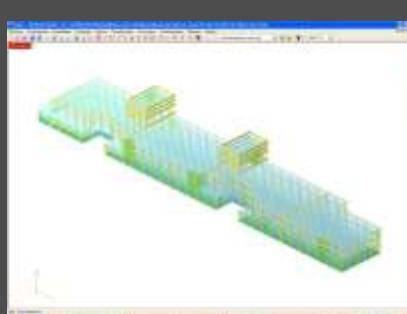
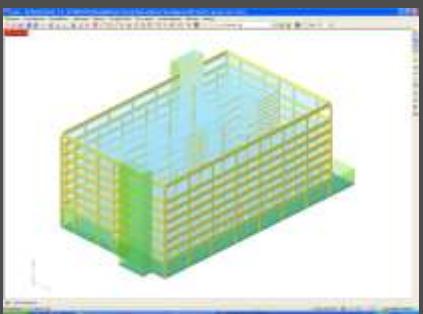




MOSKVA - RŽANJ

STAMBENO POSLOVNI OBJEKAT

objekat visine preko 50m





MOST PREKO REKE LEPENICA NA AUTOPUTU BATOČINA-KRAGUJEVAC

most na autoputu





NADVOŽNJAK PREKO PRUGE NA AUTOPUTU BATOČINA-KRAGUJEVAC most na autoputu

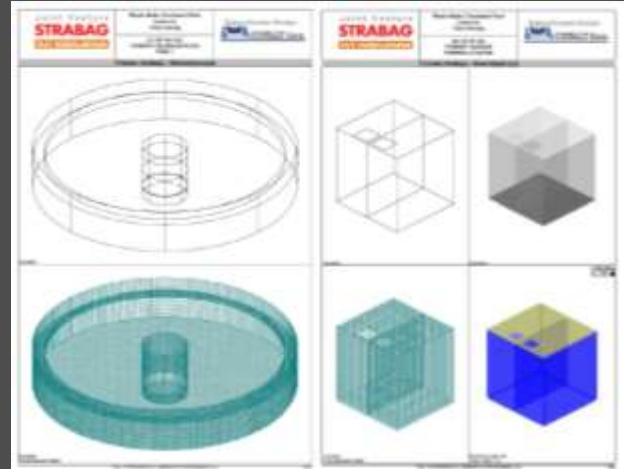




LESKOVAC

POSTROJENJE ZA PREČIŠĆAVANJE OTPADNIH VODA

kategorija - hidrotehničke konstrukcije





NOVI SAD
POSTROJENJE ZA PIJAĆU VODU „ŠTRAND“
kategorija - hidrotehničke konstrukcije





ZAKLJUČCI

- Različitost tehničke regulative;
- Lokalne karakteristike intenziteta dejstava;
 - Intenzitet seizmičkih dejstava
 - Intenzitet uticaja vетра
 - Lokalni temperaturni uslovi
- Tehnološka ograničenja;
- Softverska ograničenja (obavezujući sertifikati);
- Sastav projektne dokumentacije;
- Različite obaveze projektanta u toku izvođenja objekat;





6 ZAKLJUČAK

Na osnovu rezultata u projektovanju 38 objekata u ovom postrojenju za prečišćavanje otpadnih voda i nekoliko sličnih postrojenja manjih kapaciteta iskustva su sledeća:

- Merodavni kriterijum za dimenzionisanje armiranobetonskih preseka je granično stanje upotrebljivosti a ne granično stanje nosivosti;
- Kombinacije opterećenja sa seizmičkim dejstvima nisu merodavne ni u jednom slučaju;
- Posebno analizirati delove konstrukcije koji se nalaze iznad tečnosti (ne potpoljeni), potopljeni a ne zatrpani, potopljeni i zatrpani do dobine od 100 cm i potopljeni i zatrpani na većim dubinala od 100 cm;
- Za temperature vazduha usvojiti prosečne mesečne temperature (posebno za letnji i zimski period);
- Za temeprature tčnosti koristiti vrednosti dobijene od tehnologa i potvrđene merenjem na objektu koji je u ekspolataciji;
- Referentnu temperaturu usvojiti u skladu sa dinamikom građenja ili u skladu sa predlogom Pravilnika za opteećenje mostova;
- Prsline u armiranobetonskim konstrukcijskim elementima nisu smetnja ako im širina ne premašuje dopuštenu graničnu vrednost, odnosno pojava prsline je dozvoljena;
- Prsline koje su se pojavile i posle toga sanirane ne predstavljaju opasnost u daljoj fazi eksploatacije objekta. Ovo se dokazuje ne curenjem tečnosti koja se nalazi u objektu (prethodne probe). Sanirane prsline ne umanjuju kvalitet konstrukcijskih elemenata i objekta u celini;
- Na cenu koštanja direktno utiče izloženost objekta temperaturnim uticajima što navodi na zaključak da je poželjno objekte (kada je to moguće) zatrpati – zasuti zemljom ili termički izolovati.

