

MASTER OF SCIENCE THESIS

Hybrid Eulerian-Lagrangian Vortex Particle Method

A fast and accurate numerical method for 2D Vertical-Axis
Wind Turbine

L. Manickathan B.Sc.

Date TBD

Faculty of Aerospace Engineering · Delft University of Technology

Hybrid Eulerian-Lagrangian Vortex Particle Method

**A fast and accurate numerical method for 2D Vertical-Axis
Wind Turbine**

MASTER OF SCIENCE THESIS

For obtaining the degree of Master of Science in Aerospace
Engineering at Delft University of Technology

L. Manickathan B.Sc.

Date TBD



Copyright © L. Manickathan B.Sc.
All rights reserved.

DELFT UNIVERSITY OF TECHNOLOGY
DEPARTMENT OF
AERODYNAMICS AND WIND ENERGY

The undersigned hereby certify that they have read and recommend to the Faculty of Aerospace Engineering for acceptance a thesis entitled **“Hybrid Eulerian-Lagrangian Vortex Particle Method”** by **L. Manickathan B.Sc.** in partial fulfillment of the requirements for the degree of **Master of Science**.

Dated: Date TBD

Head of department:

prof.dr.ir. G.J.W. van Bussel

Academic Supervisor:

dr.ir. C.J. Simao Ferreira

Academic Supervisor:

dr.ir. A. Palha da Silva Clerigo

Industrial Supervisor:

prof.dr.ir. I. Bennett

Summary

This is the summary of the thesis.

Acknowledgements

I wish to thank the following persons...

Delft, The Netherlands
Date TBD

L. Manickathan B.Sc.

Contents

Summary	v
Acknowledgements	vii
List of Figures	xiii
List of Tables	xv
1 Introduction	1
1.1 Motivation and Goal	1
1.2 Research Aim and Plan	2
1.3 Introduction to Hybrid Eulerian-Lagrangian Vortex Particle Method . . .	2
1.3.1 Advantage of domain decomposition	2
1.3.2 Methodology	3
1.4 Thesis Outline	3
Nomenclature	1
2 Lagrangian Domain: Vortex Particle Method	5
2.1 Introduction to Vortex Method	5
2.1.1 Vorticity	5
2.1.2 Velocity-vorticity formulation of navier-stokes equations	6
2.1.3 Viscous splitting algorithm	6
2.2 Spatial Discretization: Generation of Vortex Blobs	7
2.2.1 Discrete form of vorticity field	7
2.2.2 Mollified vortex kernels	7
2.2.3 Beale's correction: Iterative circulation processing scheme	8
2.2.4 Error in blob initialization	8

2.3	Convection of vortex blobs	8
2.3.1	Biot-savart law	8
2.3.2	Remeshing scheme: Treating lagrangian grid distortion	9
2.4	Diffusion of Vortex Methods	9
2.4.1	Vorticity diffusion techniques	9
2.4.2	Modified remeshing for treating diffusion	9
2.5	Boundary conditions at solid boundary	9
2.5.1	Boundary integral equations	9
2.5.2	Panel method for treating no-slip boundary condition	9
2.5.3	Convergence study of panel method	9
2.6	Simulation acceleration techniques	9
2.6.1	Fast multi-pole Method	9
2.6.2	Parallel computation in GPU	9
2.7	Validation of lagrangian method	9
2.7.1	Lamb-oseen vortex at $Re = 100$	9
2.7.2	Convection of Clercx-Bruneau dipole at $Re = 625$	9
2.8	Summary	9
3	Eulerian Domain: Finite Element Method	11
3.1	Introduction to Finite Element Method	12
3.1.1	Finite element discretization	12
3.1.2	Finite element function and function space	12
3.2	Solving the Finite Element problem	12
3.2.1	Introduction to FEniCS Project	12
3.2.2	Mesh generation using GMSH	12
3.3	Solving Incompressible Navier-Stokes Equations	12
3.3.1	Velocity-pressure formulation	12
3.3.2	Incremental pressure correction scheme	12
3.3.3	Determining the vorticity field	12
3.3.4	Determining the body forces	12
3.4	Validation of eulerian method	12
3.4.1	Clercx-Bruneau dipole collison at $Re = 625$	12
3.4.2	Impulsively started cylinder at $Re = 550$	12
3.5	Summary	12

4	Hybrid Eulerian-Lagrangian Vortex Particle Method	13
4.1	Theory of Domain Decomposition Method	13
4.1.1	Advantage of domain decomposition	13
4.1.2	Assumptions and Limitations	13
4.1.3	Modified coupling strategy	13
4.2	Eulerian-Lagrangian coupling algorithm	13
4.2.1	Eulerian dirichlet boundary condition	13
4.2.2	Vorticity interpolation algorithm	13
4.3	Introduction to pHyFlow: Hybrid solver	13
4.3.1	Program structure	13
4.4	Summary	13
5	Verification and Validation of Hybrid Method	15
5.1	Error in coupling: Verification with Lamb-Ossen vortex	16
5.1.1	Generation of artificial vorticity	16
5.2	Clercx-Bruneau dipole convection at $Re = 625$	16
5.2.1	Comparison of vorticity contours	16
5.2.2	Variation in maximum vorticity	16
5.2.3	Variation in kinetic energy	16
5.2.4	Variation in enstrophy	16
5.3	Clercx-Bruneau dipole collision at $Re = 625$	16
5.3.1	Comparison of vorticity contours	16
5.3.2	Variation in maximum vorticity	16
5.3.3	Variation in kinetic energy	16
5.3.4	Variation in enstrophy	16
5.3.5	Variation in palinstrophy	16
5.4	Impulsively started cylinder problem at $Re = 550$	16
5.4.1	Evolution of the wake	16
5.4.2	Evolution of pressure and friction drag	16
5.4.3	Evolution of lift	16
5.5	Moving body	16
5.5.1	Error due to pertubation lag	16
5.6	Proof of concepts	16
5.6.1	Multiple cylinder case	16
5.6.2	Stalled airfoil at $Re = 5000$	16
5.7	Summary	16

6	Conclusion and Recommendation	17
6.1	Conclusion	17
6.1.1	Lagrangian domain	17
6.1.2	Eulerian domain	17
6.1.3	Hybrid method	17
6.2	Recommendations	17
6.2.1	Lagrangian domain	17
6.2.2	Eulerian domain	17
6.2.3	Hybrid method	17
	References	19

List of Figures

2.1	Circulation of the fluid	6
2.2	Vortex blob with Gaussian distribution: $[k = 2, \sigma = 1.0]$	8

List of Tables

Chapter 1

Introduction

Conventional energy resources such as fossil fuels and nuclear energy are not only limited supply but also pose adverse effects on the environment. Therefore, we are striving to find a cheap and renewable source of energy. Wind energy is such source of energy and is therefore getting more popular and also become more affordable and novel renewable technologies such as Vertical-Axis Wind Turbine (VAWT) is now an interested research field.

Vertical-Axis Wind turbines are unlike the normal wind turbine. Typical wind turbines are mounted on a mast away from the ground and generates energy by spinning normal to the ground. However, a VAWT spins parallel to the ground with its hub located at the ground [9]. The advantages of the vertical axis wind turbine are what makes them ideal for a source of renewable energy. As the turbine is located at the ground (unlike the Horizontal-Axis Wind Turbine), it is easily accessible and can be easily maintained. The second main advantage of the VAWT is the way it dissipates its wake [4] [7]. As the fluid past the turbine is more turbulent, the flow is able to smooth out much earlier. This means that it possible to places VAWTs much closer to each other is so in future this means that a VAWT farm can potentially give more power per area. Furthermore, operate independent of the flow direction and can operate at low wind speeds (low tip-speed ratios).

1.1 Motivation and Goal

However, with these advantages also comes drawbacks. As the blades passes through its own dirty air (the wake), complex wake-body interactions take places. These have adverse effect on the blade structure and therefore is more susceptible to fatigue. This happens because the blades are constantly pitching in front the free-stream flow and complex flow behaviour such as dynamic stall and constant vortex shedding occurs [6]. This complex fluid behaviours makes it hard to predict the performance of a VAWT and this is one of the reasons why VAWTs are not mainstream. In addition, as the VAWT operates at

large Reynolds number, accurate numerical methods are computationally very expensive. Therefore, it is vital to have a good understanding of the flow structure evolution and the wake generation of the VAWT using not only an efficient method, but also an accurate one.

To summarize, we are now able to formulate a research goal. The key interest of this project is to develop an efficient, reliable, and an accurate numerical method for modelling the flow around a 2D VAWT. For now, only 2D problems are considered because 3D method is build upon the methodology of the 2D. Thus, once the 2D methodology is made, a 3D numerical method should be a straightforward extension.

Furthermore, the numerical method efficient at capturing both the near-wake phenomenons such as the vortex shedding, dynamic stall, & the wake-body interaction, and should be able to capture the large scale flow structure such as the evolution of the VAWT wake. From this criterias, we are able to formulate the research question.

1.2 Research Aim and Plan

Research Question: *Is it possible to develop a numerical method that is both efficient at capturing the small-scale phenomenons and the large scale phenomenons? Is it possible to apply this to a 2D VAWT?*

Research aim and plan:

- Develop a numerical method for capturing small-scale phenomenons and large scale phenomenons.
- Ensure this tool is efficient, reliable, and accurate.
- Verify, Validate the tools with model problems.
- Apply the model to the 2D flow of VAWT.

With the above formulate research question, aim and plan we are able to thoroughly perform the literature study to determine whether the research goal stated here is feasible. Finally, this report will answer why a Hybrid Eulerian-Lagrangian Vortex Particle Method will be used to the achieved the goals.

1.3 Introduction to Hybrid Eulerian-Lagrangian Vortex Particle Method

1.3.1 Advantage of domain decomposition

!!! add picture here !!!

1.3.2 Methodology

1.4 Thesis Outline

Lagrangian Domain: Vortex Particle Method

2.1 Introduction to Vortex Method

Vortex Method (VM) is a branch of computational fluid dynamics that deals with the evolution of the vorticity of the fluid in a lagrangian description. Typically, the fluid is viewed at a fixed window where it is described as a function of space \mathbf{x} and time t . However, the lagrangian point of view regards the fluid as a collection of the particles carrying the propety of the fluid.

!!! Lagrangian vs. Eulerian fluid diagram !!!

Unlike the typical eulerian method that require discretization of all the fluid domain, vortex methods only needs fluid elements where there is vorticity. This means that the vortex method are inherently auto-adaptive method that only simulated the flow of interest. Furthermore, with the computational acceleration methods such as Fast-Multipole Method (FMM) and parallel computation on Graphics Processing Units (GPU), vortex method can be more efficient than typical eulerian methods.

2.1.1 Vorticity

Vorticity ω , the governing element of vortex method, is defined as

$$\omega = \nabla \times \mathbf{u}, \quad (2.1)$$

where \mathbf{u} is the velocity field. The circulation Γ is defined as

$$\Gamma = \int_L \mathbf{u} \cdot d\mathbf{r} = \int_S \omega \cdot \mathbf{n} dS, \quad (2.2)$$

by the stokes theorem, as represents the integral vorticity of the domain, figure 2.1

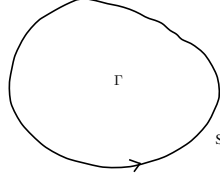


Figure 2.1: Circulation of the fluid

2.1.2 Velocity-vorticity formulation of navier-stokes equations

The governing equation of the vortex method is velocity-vorticity $\mathbf{u}-\omega$ formulation of the navier-stokes equations [2]. The 2-D incompressible navier-stokes momentum equation is given as

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{u}, \quad (2.3)$$

relating the velocity field $\mathbf{u}(\mathbf{x}, t)$ to the pressure field $p(\mathbf{x}, t)$, the kinematic viscosity ν and density ρ . Furthermore, we also have to satisfy the incompressibility constraint given as

$$\nabla \cdot \mathbf{u} = 0. \quad (2.4)$$

To attain the velocity-vorticity formulation, we should take the curl of the velocity-pressure $\mathbf{u}-p$ formulation of the navier-stokes equation. Taking the curl of the momentum equation 2.3, we get the vorticity transport equation

$$\frac{\partial \omega}{\partial t} + \mathbf{u} \cdot \nabla \omega = \nu \nabla^2 \omega, \quad (2.5)$$

which only relates the vorticity to the velocity enabling us to neglect the pressure field.

2.1.3 Viscous splitting algorithm

Vortex method is initially used to model the evolution of incompressible, inviscid flows. However, in order to simulate a real flow, we must also deal with the viscous component of the fluid. Chorin [1] has shown that using the viscous splitting algorithm, it is possible to simulate a viscous flow using vortex method.

The viscous splitting algorithm is basically a fractional step method, where the viscous and the inviscid part of the transport equation is dealt in two subsequent steps,

- Sub-step 1: convection

$$\frac{\partial \omega}{\partial t} + \mathbf{u} \cdot \nabla \omega = 0; \quad (2.6)$$

- Sub-step 2: diffusion:

$$\frac{\partial \omega}{\partial t} = \nu \nabla^2 \omega. \quad (2.7)$$

The first sub-step of the evolution deals with the convection of the vorticity. The second sub-step deals with the diffusion of the vorticity field.

There are several ways of dealing with the diffusion of the vorticity field. Chorin initially employed a random walk method, however this method suffers some limitations in accuracy and since then there are several methods that can be used to simulate the diffusion. Particle Strength Exchange (PSE) method [3], is an algorithm to treat diffusion by exchange of vortex element strengths. Vortex Redistribution Method (VRM) [5] models diffusion by distributing the fraction of circulation of the vortex elements to the neighbouring vortices. However, we use a modified interpolation [8] to simultaneously treat diffusion and remeshing through modified interpolation kernel.

2.2 Spatial Discretization: Generation of Vortex Blobs

Vortex blobs were first introduced by Chorin.

2.2.1 Discrete form of vorticity field

The spatial discretization of the fluid domain is done by representing the vorticity field in N Lagrangian vortex particles. This is done by dividing the fluid domains into cells where the circulation of the region is assigned to the particle. This gives

$$\omega(\mathbf{x}, t) \simeq \omega^h(\mathbf{x}, t) = \sum_p \Gamma_p(t) \zeta_\sigma[\mathbf{x} - \mathbf{x}_p(t)], \quad (2.8)$$

2.2.2 Mollified vortex kernels

where Γ_p is the estimate of the circulation around the particle \mathbf{x}_p with core size σ . We must not that ω^h is an approximation to ω of the fluid.

Due to the non-zero size of the vortex elements, it is referred to as vortex blobs. The advantage of the vortex blobs is that with a smooth distribution of the vorticity, the singularity disappears and so numerical instability does not happen when blobs get too close to each other.

An ideal choice for a cutoff function is a Gaussian distribution. Gaussian kernels satisfy the requirement for smooth distribution and decays quickly. The Gaussian kernel is defined as

$$\zeta_\sigma = \frac{1}{k\pi\sigma^2} \exp\left(\frac{-|\mathbf{x}|}{k\sigma^2}\right), \quad (2.9)$$

where k is 1, 2 or 4 and determines the width of the kernel.

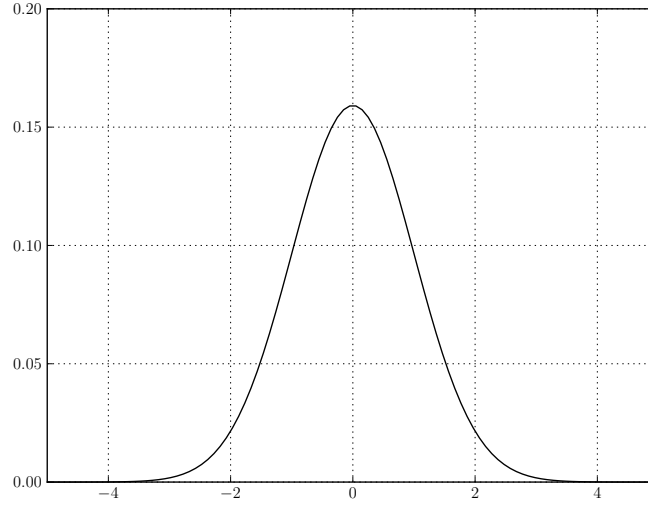


Figure 2.2: Vortex blob with Gaussian distribution: $[k = 2, \sigma = 1.0]$

2.2.3 Beale's correction: Iterative circulation processing scheme

2.2.4 Error in blob initialization

2.3 Convection of vortex blobs

2.3.1 Biot-savart law

The vortex transport equation evaluated using the viscous splitting algorithm. For vortex methods, it is ideal to express the equation 2.6 in Lagrangian form,

$$\frac{d\mathbf{x}_p}{dt} = \mathbf{u}(\mathbf{x}_p), \quad (2.10)$$

with

$$\frac{d\omega_p}{dt} = 0. \quad (2.11)$$

The velocity field can be decomposed using the Helmholtz decomposition,

$$\mathbf{u} = \mathbf{u}_\infty + \mathbf{u}_\omega \quad (2.12)$$

with \mathbf{u}_∞ as the free-stream velocity, \mathbf{u}_ω as the velocity of the vortical part of the flow.

The velocity can be related to the vorticity using the Biot-Savart law

$$\mathbf{u} = \mathbf{u}_\infty + \mathbf{K} \star \omega, \quad (2.13)$$

$$\mathbf{u} = \mathbf{u}_\infty + \mathbf{K} \star \omega, \quad (2.14)$$

where the \star represents convolution of the kernel \mathbf{K}_p given by

$$\mathbf{K}_p = \frac{1}{2\pi |\mathbf{x}|^2} (-x_2, x_1). \quad (2.15)$$

The advantage of discretizing and evaluating the vorticity field in this form is that vortex elements are only needed where the vorticity is nonzero. This means that the vortex elements inherently adapt to domain of interest and does not require simulation of region where nothing happens. From equation 2.15, we see that it has a singularity when the particles approach each other and so to overcome this we can mollify the kernel using a smooth cutoff function ζ . So the mollified kernel \mathbf{K}_ϵ is given as

$$\mathbf{K}_\epsilon = \mathbf{K} \star \zeta_\epsilon. \quad (2.16)$$

2.3.2 Remeshing scheme: Treating lagrangian grid distortion

2.4 Diffusion of Vortex Methods

2.4.1 Vorticity diffusion techniques

2.4.2 Modified remeshing for treating diffusion

2.5 Boundary conditions at solid boundary

2.5.1 Boundary integral equations

Linked boundary conditions

2.5.2 Panel method for treating no-slip boundary condition

2.5.3 Convergence study of panel method

2.6 Simulation acceleration techniques

2.6.1 Fast multi-pole Method

2.6.2 Parallel computation in GPU

2.7 Validation of lagrangian method

2.7.1 Lamb-oseen vortex at $Re = 100$

2.7.2 Convection of Clercx-Bruneau dipole at $Re = 625$

2.8 Summary

Chapter 3

Eulerian Domain: Finite Element Method

3.1 Introduction to Finite Element Method

3.1.1 Finite element discretization

3.1.2 Finite element function and function space

3.2 Solving the Finite Element problem

3.2.1 Introduction to FEniCS Project

3.2.2 Mesh generation using GMSH

3.3 Solving Incompressible Navier-Stokes Equations

3.3.1 Velocity-pressure formulation

3.3.2 Incremental pressure correction scheme

3.3.3 Determining the vorticity field

3.3.4 Determining the body forces

Frictional Forces

Pressure Forces

3.4 Validation of eulerian method

3.4.1 Clercx-Bruneau dipole collision at $Re = 625$

3.4.2 Impulsively started cylinder at $Re = 550$

3.5 Summary

Hybrid Eulerian-Lagrangian Vortex Particle Method

4.1 Theory of Domain Decomposition Method

4.1.1 Advantage of domain decomposition

4.1.2 Assumptions and Limitations

4.1.3 Modified coupling strategy

4.2 Eulerian-Lagrangian coupling algorithm

4.2.1 Eulerian dirichlet boundary condition

4.2.2 Vorticity interpolation algorithm

4.3 Introduction to pHyFlow: Hybrid solver

4.3.1 Program structure

4.4 Summary

Chapter 5

Verification and Validation of Hybrid Method

5.1 Error in coupling: Verification with Lamb-Ossen vortex

5.1.1 Generation of artificial vorticity

5.2 Clercx-Bruneau dipole convection at $Re = 625$

5.2.1 Comparison of vorticity contours

5.2.2 Variation in maximum vorticity

5.2.3 Variation in kinetic energy

5.2.4 Variation in enstrophy

5.3 Clercx-Bruneau dipole collision at $Re = 625$

5.3.1 Comparison of vorticity contours

5.3.2 Variation in maximum vorticity

5.3.3 Variation in kinetic energy

5.3.4 Variation in enstrophy

5.3.5 Variation in palinstrophy

5.4 Impulsively started cylinder problem at $Re = 550$

5.4.1 Evolution of the wake

5.4.2 Evolution of pressure and friction drag

5.4.3 Evolution of lift

5.5 Moving body

Conclusion and Recommendation

6.1 Conclusion

6.1.1 Lagrangian domain

6.1.2 Eulerian domain

6.1.3 Hybrid method

6.2 Recommendations

6.2.1 Lagrangian domain

6.2.2 Eulerian domain

6.2.3 Hybrid method

References

- [1] A.J. Chorin. Numerical study of slightly viscous flow. *Journal of Fluid Mechanics*, 1973.
- [2] G.H. Cottet and P.D. Koumoutsakos. *Vortex Methods: Theory and Practice*, volume 12. Cambridge University Press, 2000.
- [3] S. Degond, P.; Mas-Gallic, Pierre Degond, and S. Mas-Gallic. The weighted particle method for convection-diffusion equations. I. The case of an isotropic viscosity. *Mathematics of Computation*, 53(188):485–507, 1989.
- [4] C.J. Simão Ferreira. The near wake of the VAWT: 2D and 3D views of the VAWT aerodynamics. 2009.
- [5] S. Shankar and L. van Dommelen. A New Diffusion Procedure for Vortex Methods. *Journal of Computational Physics*, 127(1):88–109, August 1996.
- [6] Carlos Simão Ferreira, Gijs Kuik, Gerard Bussel, and Fulvio Scarano. Visualization by PIV of dynamic stall on a vertical axis wind turbine. *Experiments in Fluids*, 46(1):97–108, August 2008.
- [7] L.J. Vermeer, J.N. Sørensen, and a. Crespo. Wind turbine wake aerodynamics. *Progress in Aerospace Sciences*, 39(6-7):467–510, August 2003.
- [8] Daehyun Wee and Ahmed F. Ghoniem. Modified interpolation kernels for treating diffusion and remeshing in vortex methods. *Journal of Computational Physics*, 213(1):239–263, March 2006.
- [9] Wikipedia. Vertical-Axis Wind Turbine, July 2013.

