# \chapter{Optimize}

## %introduction

## This chapter aims to discuss the optimization methods to improve the Fiber-to-Chip coupling efficiency. Five proposals will be obtained in this chapter. One is to relocate the waveguide. Another is to replace the round condition of the simulation setup with oil. In the third proposal we will consider to change the composed material of the waveguide. The application of a taper interface at the beginning of the waveguide is involved in the next consideration. At last we are going to mount a lens at the waveguide end face.

## \section{Coupling by location shifting}

As a 3D model the waveguide can be shifted in transversal (Fig. \ref{fig:shift\_x\_axis} and Fig. \ref{fig:shift\_y\_axis}) or longitudinal (Fig. \ref{fig:shift\_z\_axis}) direction.

\begin{itemize}

\item Shift the waveguide along X-Axis: Relocate the waveguide from $-0.5\mu$m to $0.5\mu$m:

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/shift\_x\_axis}

\caption{Displacing the waveguide along x-axis}

\label{fig:shift\_x\_axis}

\end{figure}

\item Shift the waveguide along Y-Axis: Relocate the waveguide from $-0.5\mu$m to $0.5\mu$m:

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/shift\_y\_axis}

\caption{Displacing the waveguide along y-axis}

\label{fig:shift\_y\_axis}

\end{figure}

\item Shift the waveguide along Z-Axis: Relocate the waveguide from $-0.5\mu$m to $0.5\mu$m:

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/shift\_z\_axis}

\caption{Displacing the waveguide along z-axis}

\label{fig:shift\_z\_axis}

\end{figure}

\end{itemize}

\begin{table}

\caption{Coupling efficiency by shifting the waveguide along X,Y and Z-Axis}

\centering

\begin{tabular}{c|ccc}

\hline

Shift distance & X-Asis & Y-Axis & Z-Axis \\

\hline

$-0.5\mu$m &$32.4\%$ &$32.4\%$&$46.6\%$ \\

$-0.4\mu$m &$37.3\%$ &$36.5\%$&$47\%$ \\

$-0.3\mu$m &$41.9\%$ &$41.3\%$&$48.2\%$ \\

$-0.2\mu$m &$45.5\%$ &$45.2\%$&$49.1\%$ \\

$-0.1\mu$m &$48\%$ &$47.8\%$&$49.1\%$ \\

$0\mu$m &$48.9\%$ &$48.9\%$&$48.9\%$ \\

$0.1\mu$m &$47.8\%$ &$48.4\%$&$48.9\%$ \\

$0.2\mu$m &$45.5\%$ &$46.4\%$&$49.4\%$ \\

$0.3\mu$m &$41.9\%$ &$42.9\%$&$49.7\%$ \\

$0.4\mu$m &$37.5\%$ &$38.5\%$&$49.5\%$ \\

$0.5\mu$m &$32.3\%$ &$33.1\%$&$48.8\%$ \\

\hline

\end{tabular}

\label{tab:shift\_result}

\end{table}

\begin{figure}[!ht]

\centering

\includegraphics[width=0.8\textwidth]{bilder/shift\_curve}

\caption{Coupling efficiency due to the displacement of the wavguide.}

\label{fig:shift\_curve}

\end{figure}

Tab. \ref{tab:shift\_result} contains the results of above simulations. According these results we can draw coupling-efficiency curves due to shifting waveguide in Fig. \ref{fig:shift\_curve}. It is obvious that the coupling efficiency falls very quickly for vertical or horizontal shifting, while it stays relative stable for longitudinal displacement. From this Figure we can also reveal that coupling efficiencies are symmetric due to positive and negative X-Axis shifting. While the coupling efficiencies due to negative and positive Y-Axis shifting is not symmetric. This trend can be explained by the geometric characters of the waveguide, which is same in X-direction and different in Y-direction. The highest coupling efficiency due to shifting along Z-Axis lies not exactly at working distance of $4\mu$m but of $4.3\mu$m, which agree with the estimation of minimum spot location about $4.26\mu$m at section \ref{sect:model\_model\_model\_TLF}. Alought the minimum spot location lies not on the working distance $4\mu$m, displacement of the waveguide cannot greatly improve the coupling efficiency. Thus the waveguide will stay at the working distance of $4\mu$m in following simulations.

## \section{Simulation in oil environment}

% coupling\_oil

In default condition the simulation models are surrounded by vacuum background in CST MWS.

In this section we will run the coupling simulation in a different background. For the practical experiment there are not many options for changing the environment. Here the coupling configuration will be placed in an environment full of oil, $n=1.526$ or $\emps=2.33$. Changing around conditions of the simulation may greatly affect the working distance of the TLF. Therefore determining the new working distance is necessary before coupling the TLF to the waveguide. Similar as in section \ref{sect:model\_model\_model\_TLF} the spot size curve Fig. \ref{fig:oil\_spot\_curve} can be drawn by loading data of TLF beam propagation in oil from CST MWS. Here we can tell from the spot size cure that the minimum spot in oil lies at the position of about $19\mu$m from the TLF, farer than the original minimum spot location in vacuum.\\

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/spot\_curve\_oil}

\caption{Spot size curve of TLF in oil.}

\label{fig:oil\_spot\_curve}

\end{figure}

We simulate the coupling setup at the new working distance of $19\mu$m. Fig. \ref{fig:oil\_coupling\_curve} shows the coupling efficiency in frequency domain of this configuration. The coupling efficiency at working frequency $282$THz achieves about $34.5\%$, which is lower than that of the original configuration in section \ref{sect:model\_model\_model\_TLF}.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/s21\_oil\_curve}

\caption{Coupling efficiency between TLF and the rib waveguide due to frequency domain in oil background.}

\label{fig:oil\_coupling\_curve}

\end{figure}

## \section{Different refract indexes}

It is obvious that the refractive index of the waveguide affects the coupling ability. In this section the effect of varying refractive index for coupling will be discussed.

We will keep the substrate setup and test the guide in refractive indexes form $1.6$ to $2.5$ in this section.\\

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/s21\_refractive\_index}

\caption{Coupling efficiency between TLF and the rib waveguide due to refractive index.}

\label{fig: refractive\_index}

\end{figure}

Simulation results are mapped into Fig. \ref{fig:refractive\_index}. It can be told from the figure that the coupling ability rise sharply within $n=1.6$ to $1.8$ then decline softly due to the increasing of refractive indexes. The highest value of the coupling efficiency among the arrangements in this section is about $62.6\%$ when the guide is composed of material of $n=1.8$.\\

Surely, it is not possible to find the material of any refractive index. If we want to improve the coupling ability by this means, we can only choose a material with a refractive index close to $n=1.8$.

## \section{Tapered waveguide}

## Tapered waveguide is composed of a regular waveguide and a taper interface, whose dimensions in the tapered section changes slightly along the longitudinal dirccetion\cite{linear\_tapered\_waveguides}. Tapered structure enables the waveguide to receive more light so that this structure can improve the coupling efficiency between beam source and waveguide.\\

## Nathaniel in \cite{design\_fabrication\_tapered\_waveguide} has presented two general types of tapered waveguide: conventional taper like Fig. \ref{fig:conventional\_taper} and inverse taper like top view Fig. \ref{fig:inverse\_taper}. For a conventional taper the entry is wider than the exit while for an inverse taper the entry is narrower than the exit. Because the entry of the inverse taper has smaller dimensions than that of beam spots in this work, only the conventional taper will be discussed in this section.

## \begin{figure}[!ht]

## \centering

## \includegraphics[width=0.7\textwidth]{bilder/convernational\_taper}

## \caption{Schema of a conventional taper.}

## \label{fig:conventional\_taper}

## \end{figure}

## \begin{figure}[!ht]

## \centering

## \includegraphics[width=0.7\textwidth]{bilder/inverse\_taper}

## \caption{Schema of a inverse taper.}

## \label{fig:inverse\_taper}

## \end{figure}

## Two taper properties, the width $d\_{1}$ of a taper interface and the divergence angle $\theta$ of the taper, may strongly affect the coupling efficiency. For convenient calculations our simulations will be arranged respectively due to variations of taper width and taper length $L\_{taper}$.

## \subsection{Tapered waveguide due to interface width}

The taper width affects the acceptable scale of the waveguide. The beam spot diameter at the working distance is about $\1.5\mu$m, while the regular waveguide has smaller dimensions (w=$1\mu$m and h=$0.5\mu$m). In order to catch a complete view we discuss the tapered width starting with $1.2\mu$m to match the beam spot. Fig. \ref{fig:tapered\_waveguide\_wxx} presents the coupling behavior of the tapered waveguide along the variation of the interface width. From the figure it can be told that the coupling efficiency of this arrangement rise firstly with the width increasing and achieve its peak value at the width $d\_{1}=2\mu$m and $2.2\mu$m. Then the efficiency falls as the interface width increasing. This tendency can be explained that a wider interface can confine more incident rays into the propagation tunnel but if the interface expands continually, other aspects, such as the divergence angle, may cause the decline of the coupling ability over the effect of the interface width.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/tapered\_waveguide\_wxx}

\caption{Coupling efficiency between TLF and tapered waveguide with constant taper length $= 5.5\mu$m due to the variations of the interface width.}

\label{fig:tapered\_waveguide\_wxx}

\end{figure}

## \subsection{Tapered waveguide due to taper length}

The value of the divergence angle is also a important character of the tapered waveguide to determine the coupling ability. The author of \cite{study\_linear\_tapered\_waveguides} has presented that the smaller the divergence angle is, the more power of fundamental mode propagates in the taper. In order to simplify the modeling process the variation of taper length will be performed in the following coupling simulations to discuss the effect of the divergence angle.

We will keep the taper interface width of the waveguide as a constant of $2\mu$m and change the taper length from $2\mu$m to $5.5\mu$m in following simulations.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/tapered\_waveguide\_dxx}

\caption{Coupling efficiency between TLF and tapered waveguide due to taper length and taper width $= 2\mu$m}

\label{fig:tapered\_waveguide\_dxx}

\end{figure}

The coupling behavior of the arrangement, the taper length vary from $2\mu$m to $5.5\mu$m, is shown in Fig. \ref{fig:tapered\_waveguide\_dxx}. The figure illustrate that the coupling efficiency increase monotonously with the taper length expanding. After taper length $4.5\mu$m of the coupling efficiency rise more and more gently, close approximately to a constant $54\%$.

Therefore for an efficient coupling the optimal divergence angle of the taper in this arrangement is less than:

\begin{equation}

\theta=atan\frac{d\_{1}-d\_{0}}{L\_{taper}}=actan\frac{2-1}{5.5}=10.3^{o}

\label{eq:divergence\_angle}

\end{equation}

## \subsection{Extension}

%tapered\_extension

Moreover, there are other optional designs of tapered waveguide can be involved to improve the Fiber-to-Chip coupling ability. In this section we will only deliver other possibilities of tapered structures for reference and most of them will not be verified in this work. \\

\textbf{Hybrid tapered waveguides}\\

In the other simulations of coupling between TLF and tapered waveguide there is another interesting result. If the taper is made from a proper material different from both guide and substrate, a more efficient coupling can be achieved in compare with our previous designs.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/tapered\_waveguide\_others}

\caption{Schema of a tapered waveguide combined with two different materials.}

\label{fig:tapered\_waveguide\_others}

\end{figure}

For example, for a taper chosen for $n=2.0$, $d\_{1}=2\mu$m, $L\_{taper}=5.5\mu$m and other configurations maintain as that of the original simulation models. In this case the coupling efficiency reaches $|S\_{21}|=63\%$ according the simulation result Fig. \ref{fig:tapered\_waveguide\_others\_coupling}. Because this design is not easy for fabrication, no more attention will be paid on it in this section.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/s21\_tapered\_waveguide\_others}

\caption{Coupling efficiency between TLF and the tapered waveguide combined with two different materials.}

\label{fig:tapered\_waveguide\_others\_coupling}

\end{figure}

\textbf{Tapered plasmonic waveguides}\\

Verhagen mentions in \cite{tapered\_plasmonic\_waveguides} a tapered plasmonic waveguide, which is composed of a thin tapered metal film, on the surface of which lies many small holes like Fig. \ref{fig:tapered\_waveguide\_plasmonic}. For transmission input beams excite the surface plasmon polariton (SPP) wave, which is explained by quantum emission, provided by the metal/dielectric interfaces of the plasmonic waveguides. By means of this arrangement the coupling efficiency can even achieve a value greater than $100\%$.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/tapered\_waveguide\_plasmonic}

\caption{Schema of a taperd plasmonic waveguide.}

\label{fig:tapered\_waveguide\_plasmonic}

\end{figure}

\textbf{Grating tapered waveguides}\\

Alonso-Ramos has provided in \cite{fiber\_to\_chip\_grating\_waveguides} an inversely tapered waveguide with gratings like Fig. \ref{fig:tapered\_waveguide\_grating}. The gratings of this waveguide are delicately designed to match the work mode: bloch mode. In \cite{fiber\_to\_chip\_grating\_waveguides} the author presented his achievement of $65.6\%$ coupling efficiency.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/tapered\_waveguide\_grating}

\caption{Schema of a taperd waveguide with grating.}

\label{fig:tapered\_waveguide\_grating}

\end{figure}

## \section{Lensed waveguide}

In this section we will discuss another important waveguide structure for efficient coupling. In many articles it has been well discussed about the coupling between laser source and lensed fiber\cite{microlensese\_to\_fiber\_coupling} and \cite{integrated\_coupling \_between\_LD\_SMF}. Edward in \cite{microlensese\_to\_fiber\_coupling} provided a microlens design for coupling lasers to fibers. The coupling efficiency in his work reaches maximum about $56\%$. SHIRAISHI has also presented in \cite{integrated\_coupling \_between\_LD\_SMF} some lensed fiber designs and has gained a minimum coupling loss less than $2$dB with those microlens designs. It brings us a idea, by means of mounting a microlens on the waveguide interface we could gain higher performance by the use of a microlens at the interface of the waveguide. For the fabrication it may be not easy to mount a microlens on a stript rib waveguide. But in \cite{lens\_end\_manufacture} the process sequence for fabricating the lens on the fiber end brings us the possibility to create a lens on a buried waveguide. In this section the coupling efficiency between TLF and the lensed buried waveguide (or lensed waveguide) Fig. \ref{fig:lensed\_waveguide} will be discussed. In the first subsection we will calculate the coupling efficiency between TLF and regular buried waveguide as the reference for further discussing. Then we can continue to talk about the lensed waveguide and the effect of varying the lens geometric ($h$ and $R$) parameters of the lensed waveguide.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/lensed\_waveguide}

\caption{Schema of a lensed buried waveguide.}

\label{fig:lensed\_waveguide}

\end{figure}

### \subsection{Coupling between TLF and basic buried waveguide}

In agreement with the waveguide in the experiment, the buried waveguide model like Fig. \ref{fig:buried\_waveguide} in this section obtains the identical dimensions ($w$ and $h$) and refractive indexes (n$\_{1}$ and n$\_{2}$) with the original waveguide.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.6\textwidth]{bilder/buried\_waveguide}

\caption{Schema of a basic buried waveguide}

\label{fig:buried\_waveguide}

\end{figure}

Fig. \ref{fig:curve\_coupling\_basic\_buried\_waveguide} shows the coupling efficiency between TLF and the regular buried waveguide due to the frequencies. The coupling efficiency at the working frequency $282$THZ reaches about $51.3\%$, which is relative higher than that of the stripped rib waveguide. We will refer this value for further discussion about coupling between TLF and the lensed waveguide.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.8\textwidth]{bilder/s21\_sym\_waveguide}

\caption{Coupling efficiency curve between TLF and the basic buried waveguide due to frequency domain.}

\label{fig:curve\_coupling\_basic\_buried\_waveguide}

\end{figure}

### \subsection{Effect of lens height}

In this section we aim to find out the effect of the lens geometric to the coupling, while the lensed interface is made from the same material with the substrate. Here we are going to maintain the guide end at the distance of $4\mu$m from the the TLF and lens radius as a constant. Meanwhile the lens height $h$ is varying from $0.4\mu$m to $3\mu$m. Tab. \ref{tab:coupling\_lensed\_waveguide\_height} obtains the coupling efficiency for these arrangements. It is apparently, the coupling efficiency in this case has greatly be improved in compare with that of the coupling for regular buried waveguide in section \ref{sect:optim\_lensed\_regular}. These simulation results can also be presented as Fig. \ref{fig:coupling\_lenses\_curve\_hxx}, from which the coupling behaviors between TLF and lensed waveguide.

\begin{table}

\caption{Cupling efficiency between TLF and lensed waveguide due to changing the lens height}

\centering

\begin{tabular}{|c|c|c|c|}

\hline

\multirow{2}{\*}{Height($\mu$m)}&\multicolumn{3}{c|}{Radius($\mu$m)}\\

\cline{2-4}

& 2& 2.5& 3\\

\hline

$0.4$&$54\%$&$53.4\%$&$52.9\%$\\

$0.6$&$58.35\%$&$57.4\%$&$56.9\%$\\

$0.8$&$57.3\%$&$56.7\%$&$56.3\%$\\

$1.0$&$60\%$&$58.8\%$&$57.8\%$\\

$1.2$&$60.7\%$&$59.1\%$&$57.9\%$\\

$1.4$&$61.7\%$&$59.9\%$&$58.8\%$\\

$1.6$&$65.1\%$&$62.7\%$&$60.7\%$\\

$1.8$&$62.9\%$&$60.9\%$&$59.9\%$\\

$2.0$&$69\%$ & $66\%$&$63\%$\\

$2.2$&--------&$62.5\%$&$61.6\%$\\

$2.4$&--------&$68.8\%$&$64.4\%$\\

$2.6$&--------&--------&$66.7\%$\\

$2.8$&--------&--------&$64.8\%$\\

$3.0$&--------&--------&$68.9\%$\\

\hline

\end{tabular}

\label{tab:coupling\_lensed\_waveguide\_height}

\end{table}

It can also be found from Fig. \ref{fig:coupling\_lenses\_curve\_hxx} that the most efficient lens configuration exist at the highest lens height when the radius of the lens is fixed. In another word a hemisphere lens is the best coupling configuration. But an exact hemisphere structure (height$=2\mu$m,Radius$=2\mu$m) may be not so easy for fabrication. Therefore the second efficient configuration (height$=1.6\mu$m,Radius$=2\mu$m) must be an optimal option among simulations.\\

\begin{figure}[!ht]

\centering

\includegraphics[width=0.8\textwidth]{bilder/s21\_fix\_lens\_radius\_hxx}

\caption{Coupling efficiency due to the variation of the lens height.}

\label{fig:coupling\_lenses\_curve\_hxx}

\end{figure}

The reason of the efficiency change can be explained by lens theory with Fig. \ref{fig:matlab\_coupling\_lenses\_rxx}-\ref{fig:matlab\_coupling\_lenses\_rxx2}. From Fig. \ref{fig:matlab\_coupling\_lenses\_rxx} we can tell that beam spot size at the working distance is bigger than the dimensions of the waveguide interface and from Fig. \ref{fig:matlab\_coupling\_lenses\_rxx2} we understand the reason because rays near margin are penetrating mostly into substrate. In Fig. \ref{fig:matlab\_coupling\_lenses\_rxx} rays near margin are refracted and focused to axis, so that the beam spot size is decreased and more rays are concentrated into waveguide to make the coupling become more efficient.\\

\begin{figure}[!ht]

\centering

\includegraphics[width=0.8\textwidth]{bilder/beam\_ray\_without\_refract}

\caption{The marginal rays propagate without refraction.}

\label{fig:matlab\_coupling\_lenses\_rxx}

\end{figure}

\begin{figure}[!ht]

\centering

\includegraphics[width=0.8\textwidth]{bilder/beam\_ray\_refract}

\caption{The marginal rays are concentrated by lens of the waveguide.}

\label{fig:matlab\_coupling\_lenses\_rxx2}

\end{figure}

\begin{figure}[!ht]

\centering

\includegraphics[width=0.8\textwidth]{bilder/spot\_fix\_lens\_radius\_hxx}

\caption{The spot size curve at lensed waveguide interface due to changing lens height}

\label{fig:lensed\_guide\_spot\_size\_curve}

\end{figure}

Meanwhile we can analyze the spot size of these arrangements due to the variation of lens heights and draw the Fig. \ref{fig:lensed\_guide\_spot\_size\_curve}. Curves in Fig. \ref{fig:lensed\_guide\_spot\_size\_curve} reveal that spot sizes changing agree well with the corresponding coupling efficiency inversely.

### \subsection{Effect of lens radius}

In this part the effect of the radius of the lens interface for the waveguide will be discussed. We are going to keep the height of the lens on the waveguide and change the lens radius. In Tab. \ref{tab:coupling\_lensed\_waveguide\_radius} the lens height is chosen for $1\mu$m, $1.5\mu$m and $2\mu$m respectively. We expand the lens radius from $2\mu$m to $3.6\mu$m and observe $|S21|$ as coupling efficiency.\\

\begin{table}

\caption{Cupling efficiency between TLF and lensed waveguide due to changing the lens radius}

\centering

\begin{tabular}{|c|c|c|c|}

\hline

\multirow{2}\*{Radius($\mu$m)}&\multicolumn{3}{c|}{Height($\mu$m)}\\

\cline{2-4}

& 1& 1.5&2\\

\hline

$2.0$& $59.5\%$ &$61.3\%$ &$69\%$\\

$2.2$& $59\%$ &$60.8\%$ &$68.3\%$\\

$2.4$&$59\%$ &$60.3\%$ &$66.8\%$\\

$2.6$&$58.6\%$ &$59.9\%$ &$65.3\%$\\

$2.8$&$58.2\%$ &$59.3\%$ &$64\%$\\

$3.0$&$57.8\%$ &$58.7\%$ &$63\%$\\

\hline

\end{tabular}

\label{tab:coupling\_lensed\_waveguide\_radius}

\end{table}

According the data in Tab. \ref{tab:coupling\_lensed\_waveguide\_radius} the coupling behavior curve can be mapped in Fig. \ref{fig:coupling\_lenses\_curve\_rxx}. Apparently, it can be told that the coupling efficiencies under different lens heights are monotonously declining due to the variation of the lens radius.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.8\textwidth]{bilder/s21\_fix\_lens\_height\_rxx}

\caption{Coupling efficiency due to changing the lens radius}

\label{fig:coupling\_lenses\_curve\_rxx}

\end{figure}

\begin{figure}[!ht]

\centering

\includegraphics[width=0.8\textwidth]{bilder/spot\_fix\_lens\_height\_rxx}

\caption{The spot size curve at lensed waveguide interface due to changing lens height}

\label{fig:lensed\_guide\_spot\_size\_curve\_rxx}

\end{figure}

At the mean time the spot size curve in Fig. \ref{fig:lensed\_guide\_spot\_size\_curve\_rxx} along the variation of the lens radius behave inversely in compare with the trends of coupling efficiency. These simulation results bring us the conclusion that the smallest lens radius gains the best coupling efficiency when the lens height is fixed.

### Subsection{Extension}

%lensed\_waveguide\_extension

Beside the previous discussion about the lensed waveguide, there are more operations we can resort to. From \cite{integrated\_coupling\_between\_LD\_SMF} we can come to more ideas to promote the coupling efficiency between TLF and lensed waveguide. The author at the end has presented a tapered core fiber like Fig.\ref{fig:tapered\_core\_fiber}, which is capable to confine more beam rays. From this we also get to know there is a small distance $h\_{1}$ between the lens end $H\_{1}$ and core interface $H\_{2}$ because the lens end is not the exact minimum spot location for a lensed waveguide. Thus it is possible to gain a higher coupling efficiency if we expand properly the distance between the lens and the core within the lensed waveguide as a 'neck' between the lens and the waveguide (see Fig. \ref{fig:lensed\_waveguide\_neck}). For a proper 'neck' length $h\_{1}$ higher coupling efficiency should be achieved. This setup will be considered at further development instead of in this work.

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/ tapered\_core\_fiber}

\caption {Schema of tapered core fiber\cite{ integrated\_coupling\_between\_LD\_SMF}.}

\label{fig:tapered\_core\_fiber}

\end{figure}

\begin{figure}[!ht]

\centering

\includegraphics[width=0.7\textwidth]{bilder/lensed\_waveguide\_neck}

\caption {Schema of a lensed buried waveguide with a 'neck'.}

\label{fig:lensed\_waveguide\_neck}

\end{figure}

## Conclusion

%description of the project and theory.

Coupling the light from optical fiber to photonic waveguide (fiber-to-chip) is a common topic for research and application in optical communication. As the light source the normal fiber has a generally an interface bigger than the dimension of the photonic waveguide. In order to promote the coupling efficiency the tapered lensed fibers (TLF) are usually applied as the light source. Thus the coupling between TLF and photonic waveguide become an attractive agenda of the optic research. \\

%purpose of this work

This work aims for the optimal solution for the effective coupling between TLF and photonic waveguide. In order to achieve this goal the coupling models have been constructed and simulated with the aid of CST MWS. In this work the modeling procedure and the analyses of the result are recounted.\\

%the content and the result of this work

%summary of each chapter,

In chapter\ref{chp:background} the basic knowledge about the geometric optic, fiber optic, Gaussian beam, finite integral method and S-Parameter is listed. The above knowledge could be helpful to understand some terms of this work. The chapter\ref{chp:model} gives readers of this work at first an impression about the technical detail of the experimental objects. Then the modeling procedure, how the model is simplified and how the properties of models look like, is introduced. Especially, two types of TLF models are compared and one is finally chosen for the further discussion. In chapter\ref{chp:optim} simulations about the effective coupling between TLF and the waveguide is divided into five parts. In the first part, the simulation aim at the effect of displacing the waveguide on the coupling efficiency. In the second part we try the same coupling configuration in oil environment instead of in air. In the third parts the effect of the refractive index is discussed. After that, the fourth and fifth parts provide two important techniques of waveguide interface, tapered and lensed interface, for promoting the coupling ability.\\

%compare and conclude the results, advice for experiment

According the results from all simulations in this work, a good designed waveguide interface can greatly affect the coupling ability of Fiber-to-Chip. The original coupling arrangement in this work achieve an efficiency $48.9\%$. The waveguide with $n=1.8$ in coupling leads to an attractive result $62.5\%$. The simply constructed tapered interface in this work gains maximally a value about $54\%$. In comparison to the tapered interface, lensed interface of the waveguide can catch the efficiency about $69\%$ in this work. From this view, the lensed interface is the most optimal option for Fiber-to-Chip coupling in this work. But coupling ability is not the exclusive aspect for the practical application. The fabrication cost must be considered. The method of using simple tapered interface or using another guide material is easier for the fabrication than the lensed interface. Thus the simple tapered interface is a more economical solution. \\

% the extensions of this work.

Techniques advance every day. There are more interesting designs for the effective Fiber-to-Chip coupling. The tapered plasmonic waveguide in \cite{tapered\_plasmonic\_waveguides} is the application of SPP mode wave provided by metal/dielectric interface. This design may achieves coupling efficiency over $100\%$. Alonso-Ramos involve grating as coupler in \cite{fiber\_to\_chip\_grating\_waveguides} to extract beams into another planner waveguide. In his developments he reaches the coupling efficiency of $65.6\%$. Beside above two designs section \ref{sect:optim\_tapered\_ext} and section \ref{sect:optim\_lensed\_ext} of this work also mension two extension for further development. The hybrid tapered interface and lensed interface with a neck are properly uneasy for fabrication, but as a simulation project they can still engage our attentions.