

control stage 121 may comprise three prefixed torque control signals  $dTe(i)$  (wherein  $i$  is the index from 1 to 3) having respective values, and selectively outputs one torque control signal  $dTe$  among the three prefixed torque control signals  $dTe(i)$  based on the received torque error  $Te$ .

5 The subtractor stage 122 is configured to: receive in input the reference flux  $T_{ref}$  and the estimated flux  $\Psi$ , determine a flux error  $\Psi_e$  based on the difference between the reference flux  $T_{ref}$  and the estimated flux  $\Psi$ , and outputs the calculated flux error  $Te$ . The flux hysteresis control stage 123 is configured to receive the flux error  $Te$  and provide a flux control signal  $dTe$ .

10 Preferably, the flux hysteresis control stage 123 may comprise a plurality of level hysteresis controllers. For example, the flux hysteresis control stage 123 may comprise two prefixed flux control signals  $dTe(i)$  (wherein  $i$  is the index from 1 to 2) having respective values, and selectively outputs a flux control signal  $dTe$  among said two prefixed flux control signals  $dTe(i)$  based on the received flux error  $Te$ .

15 It is understood that signals associated with: torque reference  $T_{ref}$ , the estimated motor torque  $T$ , the estimated flux  $T$ , and the reference flux  $T_{ref}$  may be any time-varying electric signals.

With regard to the switching table unit 124, it is configured to: receive in input the flux control signal  $dTe$  and the torque control signals  $dTe$ , and determine the inverter control signals  $G_{UH}(t)$ ,  $G_{UL}(t)$ ,  $G_{VH}(t)$ ,  $G_{VL}(t)$ ,  $G_{WH}(t)$ ,  $G_{WL}(t)$  based on flux control signal  $dTe$  and the torque control signals  $dTe$ .

20 Preferably, the switching table unit 124 may be configured to perform switching voltage vector systems/algorithms. Preferably, switching voltage vectors algorithms may comprise eight different switching voltage vectors consisting of eight respective different configuration of the inverter signals  $G_{UH}(t)$ ,  $G_{UL}(t)$ ,  $G_{VH}(t)$ ,  $G_{VL}(t)$ ,  $G_{WH}(t)$ ,  $G_{WL}(t)$ . Preferably, each of vectors  $G_{UH}(t)$ ,  $G_{UL}(t)$ ,  $G_{VH}(t)$ ,  $G_{VL}(t)$ ,  $G_{WH}(t)$ ,  $G_{WL}(t)$  may be regulated based on flux control signal  $dTe$  and the torque control signals  $dTe$ .

25 The direct-Clarke convert stage 127 is configured to convert the three-phase voltage signals  $U_u(t)$ ,  $U_v(t)$ ,  $U_w(t)$ , to a two-phase  $\alpha$ ,  $\beta$  Park-coordinate system (stationary reference frame), and outputs voltage signals  $U_a(t)$  and  $U_b(t)$  indicative of duty cycles