

tance $R_{dc} = R_{beam} + R_0 = 794 \Omega$, bias and cable capacitances $C_0 = 54 \text{ nF}$ and $C_1 = 70 \text{ pF}$ were measured using an impedance analyser at 1.26 MHz. Terminals T3 and T4 are grounded. A 1 M Ω input impedance voltage buffer amplifier is used to minimize the effects of cables and spectrum analyser on the engine operation. In Fig. 3b DC resistive heating can lead to a temperature increase of the beam which opposes the refrigeration mechanism. It is estimated from the temperature dependence of the resistance and from FEM simulations that the maximum temperature of the engine beam is $370 \pm 20 \text{ K}$ at $I_{dc} = 3 \text{ mA}$ (see Supplementary Fig. C). This temperature increase of 17% by DC resistive heating is relatively small compared to the factor

5 decrease in T_{eff} as a result of the reduction of Q_{eff} . We thank J.J.M. Ruigrok, C.S. Vaucher, K. Reimann, R. Woltjer and E.P.A.M. Bakkers for discussions and suggestions and thank J. v. Wingerden for his assistance with the SEM measurements. The authors declare that they have no competing financial interests. Author Contributions: K.L.P., P.G.S., J.T.M.v.B. and M.J.G. invented and designed the device. P.G.S., K.L.P., M.J.G. and C.v.d.A. performed the experiments. P.G.S. developed the theory, analysed the experiments and wrote the article. J.T.M.v.B., G.E.J.K. and G.J.A.M.V. developed the process technology and manufactured the device. Correspondence and requests for materials should be addressed to P.G.S. (peter.steeneken@nxp.com).

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