

CZECH TECHNICAL UNIVERSITY IN PRAGUE Faculty of Civil Engineering Department of mechanics Thákurova 7 166 29 Praha 6 Issue No. 1 Revision No. 0 Date 30.12.2023 Number of pages: 17

## User manual

StableTrussOpt-MATLAB: Program of 3D truss structure optimization with global stability constraints in MATLAB.

MATĚJ LEPŠ ŠIMON GLANC

# **Contents**

| REFERENCES |                                 |    |  |  |  |  |
|------------|---------------------------------|----|--|--|--|--|
| 0.3        | Example of usage - optimization | 16 |  |  |  |  |
| 0.2        | Example of usage - stability    | 15 |  |  |  |  |
| 0.1        | Functions                       | 5  |  |  |  |  |

StableTrussOpt-MATLAB is a program of 3D truss structure optimization with global stability constraints in MATLAB. For structural analysis, the frame elements are used to capture true 3D behavior. Then the problem is solved as a sizing optimization task formulated as a SDP program with polynomial constraints.

The software is available at https://github.com/lepsmate/StableTrussOpt-MATLAB. It is provided under LGPL-2.1 license.

## **Pre-requisites**

Software needed to run the following functions:

- MATLAB (tested on MATLAB R2021a)
- YALMIP toolbox for Matlab (https://yalmip.github.io/)
- SGLIB toolbox for Matlab (https://web.mat.bham.ac.uk/kocvara/penlab/)

## Acknowledgment

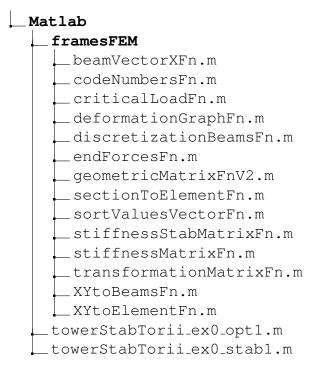
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## Introduction

StableTrussOpt-MATLAB software is focused on the optimization of truss structures with regard to global stability. Although there are mathematical approaches that enable simultaneous analysis of stability and optimization (SAND), we will separately describe both topics in the introduction part and in the description of the conducted work. First, we will clarify the complexity of stability calculation compared to classical linear analysis. Then, we will describe the nonlinearity of structural optimization including conditions for global stability.

## 0.1 Functions

In this paragraph, the functions of StableTrussOpt-MATLAB software are briefly described. Following file folder tree is considered



#### Torii\_ex0\_stab1.m

The file provides critical load scale factor calculations using linear stability, plots images of the deformed structure, and displays the critical load scale factor, normal force and stress values from the reference load.

Important parts that can be appropriately changed are following:

```
_ Lines 13-30 of the Torii_ex0_stab1.m file -
    %% Sections
13
14
15
        nSections = 6;
16
        r0 = 10*10^-3;
17
18
        sections.A = (15*pi*(ones(nSections,1)*r0).^2)/64;
19
20
        for j = 1:nSections
21
             sections.Iy(j,1) = sections.A(j)^2*113/(60*pi);
22
23
24
25
        sections.Iz = sections.Iy;
        sections.Ix = sections.Iy*2;
        sections.E = ones(nSections,1) * 210*10^9;
27
28
         sections.v = ones(nSections,1) * 0.3;
29
        ndisc = 8;
```

- Line 15: Number of cross-sections in the model.
- Line 17-28: Computation of cross-sectional characteristics for individual beams.
- Line 30: Definition of the number of FEM elements per beam

- Line 33-35: Definition of node coordinates.
- Line 36: Number of nodes in the model.

```
Lines 38-52 of the Torii_ex0_stab1.m file -
38
     %% Supports
        kinematic.x.nodes = [1;3];
39
40
        kinematic.y.nodes = [1;3];
        kinematic.z.nodes = [1;3];
41
        kinematic.rx.nodes = [];
42
        kinematic.rv.nodes = [];
43
44
        kinematic.rz.nodes = [1;3];
45
46
        nodes.dofs = true(nodes.nnodes,6);
47
        nodes.dofs(kinematic.x.nodes,1) = false;
        nodes.dofs(kinematic.y.nodes,2) = false;
48
        nodes.dofs(kinematic.z.nodes,3) = false;
49
        nodes.dofs(kinematic.rx.nodes,4) = false;
50
        nodes.dofs(kinematic.ry.nodes,5) = false;
51
52
        nodes.dofs(kinematic.rz.nodes,6) = false;
```

- Line 38-44: Nodes indices with restricted displacements/rotations.
- Line 46-52: Degrees of freedom according to boundary conditions.

```
Lines 54-60 of the Torii_ex0_stab1.m file

8% Beams

beams.nodesHead = [1;3;3;2;4;2];

beams.nodesEnd = [2;2;4;4;5;5];

beams.nbeams = numel(beams.nodesHead);

beams.disc = ones(beams.nbeams,1)*ndisc;

beams.sections = 1:nSections;
```

- Line 55: Index of head nodes of beams.
- Line 56: Index of end nodes of beams.
- Line 57: Number of beams in the model.
- Line 59-60: In this step, the discretization and section index on the beams are set.

```
_ Lines 62-73 of the <code>Torii_ex0_stab1.m</code> file .
     %% Ground structure
62
        plot3([nodes.x(beams.nodesHead) nodes.x(beams.nodesEnd)]', ...
63
              [nodes.y(beams.nodesHead) nodes.y(beams.nodesEnd)]', ...
              [nodes.z(beams.nodesHead) nodes.z(beams.nodesEnd)]', ...
65
66
              'k','LineWidth',3);
        hold on;
67
        scatter3(nodes.x, nodes.y, nodes.z, 'black', 'filled', 'o');
68
69
        axis equal;
        xlim([min(nodes.x)-0.1, max(nodes.x)+0.1]);
70
71
        ylim([min(nodes.y)-0.1, max(nodes.y)+0.1]);
        zlim([min(nodes.z)-0.1, max(nodes.z)+0.1]);
72
        grid on
```

• Line 63-73: These lines plot a graph showing the structure with nodes and beams.

```
_ Lines 75-88 of the Torii_ex0_stab1.m file -
    %% Loads
75
76
        loads.y.nodes = [];
77
        loads.y.value = [];
        loads.x.nodes = [];
78
        loads.x.value = [];
        loads.z.nodes = [5];
80
        loads.z.value = [-1000];
81
82
        loads.rx.nodes = [];
83
        loads.rx.value = [];
84
        loads.ry.nodes = [];
85
86
        loads.ry.value = [];
         loads.rz.nodes = [];
87
        loads.rz.value = [];
```

• Line 76-88: In this section load input is defined. *nodes* is the index of the node and *value* is the magnitude of the force for the specified load. In the same way the load moments are defined

```
Lines 90-95 of the Torii_ex0_stab1.m file

%% Force vector
forceVector = sparse([loads.x.nodes*6-5; loads.y.nodes*6-4; loads.z.nodes*6-3;...
loads.rx.nodes*3-2; loads.ry.nodes*3-1; loads.rz.nodes*3],...
1,[loads.x.value; loads.y.value; loads.z.value;loads.rx.value;...
loads.ry.value; loads.rz.value],nodes.nnodes*6, 1);
f = forceVector(reshape(reshape(nodes.dofs.',[],1).', 1, [])');
```

• Line 91-95: The force vector for finite element method is defined.

- Line 97: Number of unknown degrees of freedom.
- Line 99-101: In these lines, the direction vector is calculated, the code numbers from the degrees of freedom are plotted, and the vector in the XY plane is constructed.
- Line 103-106: In this part, the beams are divided into finite elements, assigned the cross-section, the vector in the XY plane and the new number of degrees of freedom is calculated.

```
_ Lines 108-115 of the Torii_ex0_stab1.m file
     % Linear analysis
108
109
         endForces.global = sparse(elements.ndofs,1);
110
         endForces.global(1:max(max(beams.codeNumbers))) = f;
111
         transformationMatrix = transformationMatrixFn(elements);
         stiffnesMatrix = stiffnessMatrixStabFn(elements,transformationMatrix);
112
113
         [endForces.local, displ] = endForcesFn(stiffnesMatrix,endForces,...
114
115
                                  transformationMatrix, elements);
```

- Line 109-110: Create a force vector for the FEM elements
- Line 111: Preparation of the transformation matrix and calculating the lengths of the FEM elements contained in the structure.
- Line 112: Creation of local and global stiffness matrices that are contained in the structure.
- Line 114: Solution of the linear static analysis equation  $\mathbf{K_e}\mathbf{u} = \mathbf{f}$ , which leads to the calculation of local end forces and element displacements.

```
Lines 117-124 of the Torii_ex0_stab1.m file

% Stability
geometricMatrix = geometricMatrixFnV2(elements,transformationMatrix,endForces);

119
120 volume = sum(elements.sections.A .* transformationMatrix.lengths);

121
122 Results = criticalLoadFn(stiffnesMatrix.global,geometricMatrix.global,100);

123
124 [sortedValues,sortedVectors] = sortValuesVectorFn(Results.values,Results.vectors);
```

- Line 118: Creation of geometric matrix  $K_{\sigma}$  with found end forces and element lengths.
- Line 120: Calculation of the volume of the structure, which is not important for stability.
- Line 122-124: Solving the eigenvalue problem, finding the critical load factors and ordering the positive eigenvalues from lowest to highest.

```
_ Lines 126-148 of the {	t Torii\_ex0\_stab1.m} file -
126
     %% Post-procesing
127
         disp('= Section areas =======')
         fprintf( 'A%d = %f\n', [(1:nSections)', sections.A]');
128
         fprintf( 'Volume: %f\n', value(volume));
129
130
131
         disp( '= Five smallest critical loads =======')
         fprintf( 'lambda%d = %f \ n', [(1:numel(sortedValues(1:5)))', value(sortedValues(1:5))]');
132
133
         for i = 1:beams.nbeams
134
             idR = 1:12;
135
             idC = (i-1)*ndisc + 1 : i*ndisc;
136
137
              endForces.beams{i} = endForces.local(idR, idC);
             N(1,i) = endForces.beams{i}(7,1);
138
139
140
         N = full(N'/1000);
141
         disp('= Normal forces ======')
142
         fprintf('N%d = %f kN \n', [(1:numel(N))', value(N)]');
143
         sigma = N./value(sections.A)/1000;
144
         disp('= Normal stresses ======')
145
         fprintf('sigma%d = %f MPa \n', [(1:numel(sigma))', value(sigma)]');
146
147
     % Graph of deformed structure
148
         graphValueId = 1;
         graphScale = 3;
149
150
         graph = deformationGraphFn(nodes, beams, sortedVectors(:, graphValueId), graphScale);
```

- Line 127-146: The critical load scale factors, normal forces and stresses on the beams are displayed.
- Line 148-150: A graph of the deformed structure corresponding to the coefficient of the lowest critical load scale factor is displayed. If you want to display a different value, you can change the index, or if you want to change the scale, this is also possible.

### Torii\_ex0\_opt1.m

The procedure used in this file is almost identical to the file Torii\_ex0\_stab1.m, therefore only the parts different to this file are listed here.

```
— Lines 16-27 of the Torii_ex0_opt1.m file -
16
     %% Sections
17
        nSections = 6; % number of cross-sections
18
19
        r0 = 10 * 10^{-3}
20
21
        startingA = (15*pi*(ones(nSections,1)*r0).^2)/64; % cross section area
22
23
        outA = sdpvar(nSections,1);
24
25
        assign(outA, startingA);
26
        sections.A = outA ;
27
        for j = 1:nSections
28
            sections.Iy(j,1) = outA(j)^2*113/(60*pi);
29
30
31
        sections.Iz = sections.Iy;
32
33
        sections.Ix = sections.Iy*2;
        sections.E = ones(nSections,1) * 210*10^9;
34
        sections.v = ones(nSections,1) * 0.3;
35
```

• Line 20: Initial radius on beams

• Line 22-35: Define the radius as a *sdpvar* variable (from YALMIP library) and calculate the cross-sectional characteristics for each beam. *sdpvar* variable overloads the original one by its symbolic representation, but the object itself can contain a real value.

```
Lines 118-128 of the Torii_ex0_opt1.m file -
     % Linear analysis
118
         endForces.global = sparse(elements.ndofs,1);
119
         endForces.global(1:max(max(beams.codeNumbers))) = f;
120
         transformationMatrix = transformationMatrixFn(elements);
121
         stiffnesMatrix = stiffnessMatrixFn(elements,transformationMatrix);
122
123
         assign(outA, startingA);
124
         realMatrix.global = value(stiffnesMatrix.global) ;
125
         for i=1:size(stiffnesMatrix.local,2)
126
127
             realMatrix.local{i} = value(stiffnesMatrix.local{i});
128
```

- Line 122: Creation of local and global stiffness matrices with *sdpvar* variables that are contained in the structure.
- Line 124: Assign the *sdpvar* variables with starting radius.
- Line 125-128: Since the *stiffnesMatrix* is dependent on *outA*, the Line 124 fills the current values of areas into *outA* and Lines 125-128 recomputes current real values of *stiffnesMatrix* and stores these numbers in *realMatrix*.

```
- Lines 132-144 of the {	t Torii\_ex0\_opt1.m} file -
132
     %% Optimization
         geometricMatrix = geometricMatrixFnV2(elements, transformationMatrix, endForces);
133
134
135
         nonnegativeCrossSections = outA>=0.00001;
136
137
         Lambda = 10.0;
         LMIconstraint = stiffnesMatrix.global+Lambda*geometricMatrix.global >= 0;
138
139
140
         volume = sum(elements.sections.A .* transformationMatrix.lengths);
141
         ops = sdpsettings('solver', 'penlab', 'verbose', 1, 'debug', 1);
142
143
         optimize([nonnegativeCrossSections, LMIconstraint], ...
                    volume, ops);
```

- Line 133: Creation of geometric matrix  $K_{\sigma}$  with found end forces and element lengths.
- Line 135: Setting of minimal (non-zero) areas  $A_i \geq A_{min}, \forall i$
- Line 137: Setting of target value of critical multiplier  $\bar{\lambda}$
- Line 138: SDP condition  $(\mathbf{K_e} + \bar{\lambda}\mathbf{K_g}) \succeq \mathbf{0}$
- Line 140: Calculate the volume of the structure.
- Line 142: Select the optimization method, solver and settings.
- Line 143: Optimize with a defined objective function and constraints.

```
Lines 146-154 of the Torii_ex0_opt1.m file

%% Post-procesing
fprintf('Optimized objective: %f\n', value(volume));
disp('= Section areas =======')
fprintf('A%d = %f\n', [(1:numel(outA))', value(outA)]');

realMatrix.global = value(stiffnesMatrix.global);
Results = criticalLoadFn(realMatrix.global,geometricMatrix.global,100);

[sortedValues,sortedVectors] = sortValuesVectorFn(Results.values,Results.vectors);
```

- Line 147-149: The optimized objective and optimized cross-section areas are displayed.
- Line 151-154: Solving the eigenvalue problem, finding the critical load factors and ordering the positive eigenvalues from lowest to highest.

#### framesFEM/

#### **function** [vector] = beamVectorXFn (beams, nodes)

#### InputVar:

beams.nbeams (number of beams), beams.nodesHead (indexes of initial nodes), beams.nodesEnd (indexes of ending nodes), nodes.x (x node coordinates), nodes.y (y node coordinates), nodes.z (z node coordinates)

#### OutVar:

vector (directional vector for individual beams).

#### function [codes] = codeNumbersFn ( beams, nodes )

#### InputVar:

beams.nbeams (number of beams), beams.nodesHead (indexes of initial nodes), beams.nodesEnd (indexes of ending nodes), nodes.dofs (degrees of freedom) *OutVar*:

codes (code numbers of beams).

### function [Results] = criticalLoadFn ( stiffnesMatrix, geometricMatrix, n )

#### InputVar:

beams.nbeams (number of beams), beams.nodesHead (indexes of initial nodes), beams.nodesEnd (indexes of ending nodes), nodes.dofs (degrees of freedom) OutVar:

Results.values (critical load scale factor), Results.vectors (buckling shape vector)

#### graph [graph] = deformationGraphFn ( nodes, beams, eigenVector, scale )

#### InputVar:

beams.nbeams (number of beams), beams.nodesHead (indexes of initial nodes), beams.nodesEnd (indexes of ending nodes), beams.disc (number of elements per beam),

nodes.x (x node coordinates), nodes.y (y node coordinates), nodes.z (z node coordinates), nodes.dofs (degrees of freedom), eigenVector (eigenmode vector), scale (deformation scale parameter)

#### OutVar:

graph (buckling shape of the structure in graph).

#### **function** [elements] = discretizationBeamsFn (beams, nodes)

#### InputVar:

beams.nodesHead (indexes of initial nodes), beams.nodesEnd (indexes of ending nodes), beams.disc (number of elements per beam), beams.codeNumbers (code numbers of beams), beams.vectorX (directional vector of beams), beams.nbeams (number of beams), nodes.dofs (degrees of freedom)

#### OutVar:

elements (elements with code numbers, directional vector and number of elements).

### function [ localEndForces, displacements ] = endForcesFn ( stiffnesMatrix, endForces, transformationMatrix, elements )

#### InputVar:

stiffnesMatrix.global (global stiffness matrix), stiffnesMatrix.local (local stiffness matrix), endForces.global (global loads at nodes), transformationMatrix.matrices (transformation matrices for individual elements), elements.codeNumbers (code numbers of elements), elements.vectorX (directional vector of elements), elements.nelement (number of elements), elements.ndofs (number of unknown DoFs)

#### OutVar:

localEndForces (local end forces on elements), displacements.local (local displacements on elements).

## function [geometricMatrix] = geometricMatrixFnV2 ( elements, transformationMatrix, endForces )

#### InputVar:

elements.codeNumbers (code numbers of elements), elements.vectorX (directional vector for individual elements), elements.nelement (number of elements), elements.ndofs (number of unknown DoFs), elements.sections.E (Young's modulus of the element),

elements.sections.v (Poisson's ratio of the element)

#### OutVar:

geometricMatrix.local (local matrixes of initial stresses), geometricMatrix.global (global matrix of initial stresses).

#### function [elemSections] = sectionToElementFn ( sections, beams )

#### InputVar:

beams.sections (section id from variable sections), beams.disc (number of elements per

beam), sections.A (cross-sectional area), sections.Iy (moment of inertia about Y axis), sections.Iz (moment of inertia about Z axis), sections.Ix (torsional moment of inertia), sections.E (Young's modulus of the material), sections.v (Poisson's ratio of the material) OutVar:

elemSections.A (cross-sectional area), elemSections.Iy (moment of inertia about Y axis), elemSections.Iz (moment of inertia about Z axis), elemSections.Ix (moment of inertia about X axis), elemSections.E (Young's modulus of the material), elemSections.v (Poisson's ratio of the material),

#### **function** [sorted\_values, sorted\_vectors] = sortValuesVectorFn (values, vectors)

#### InputVar:

values (eigenvalues), vectors (eigenvectors)

#### OutVar:

sorted\_values (sorted positive eigenvalues), sorted\_vectors (sorted eigenvectors according to the eigenvalues)

### function [stiffnesMatrix] = stiffnessMatrixStabFn ( elements, transformationMatrix )

#### InputVar:

elements.sections.A (cross-sectional area), elements.sections.Iy (moment of inertia about Y axis), elements.sections.Iz (moment of inertia about Z axis),

elements.sections.Ix (torsional moment of inertia), elements.sections.v (Poisson's ratio), elements.sections.E (Young's modulus), elements.nelement (number of elements), elements.ndofs (number of unknown DoFs), elements.codeNumbers (element code numbers), transformationMatrix.matrices (transformation matrices for individual elements), transformationMatrix.lengths (lengths of elements)

#### OutVar:

stiffnesMatrix.local (local stiffness matrices), stiffnesMatrix.global (global stiffness matrix)

### function [stiffnesMatrix] = stiffnessMatrixFn ( elements, transformationMatrix )

#### InputVar:

elements.sections.A (cross-sectional area), elements.sections.Iy (moment of inertia about Y axis), elements.sections.Iz (moment of inertia about Z axis),

elements.sections.Ix (torsional moment of inertia), elements.sections.v (Poisson's ratio), elements.sections.E (Young's modulus), elements.nelement (number of elements), elements.ndofs (number of unknown DoFs), elements.codeNumbers (element code numbers), transformationMatrix.matrices (transformation matrices for individual elements), transformationMatrix.lengths (lengths of elements)

#### OutVar:

stiffnesMatrix.local (local stiffness matrices for optimization), stiffnesMatrix.global (global stiffness matrix for optimization)

#### function [transformationMatrix] = transformationMatrixFn ( elements )

#### InputVar:

elements.vectorX (directional vector of individual elements), elements.XY (vector determining the XY plane of the element), elements.nelement (number of elements)

OutVar:

transformationMatrix.matrices (transformation matrices for individual elements), transformationMatrix.lengths (lengths of elements)

#### **function** [XY] = XYtoBeamsFn (beams)

#### InputVar:

beams.vectorX (directional vector of individual beams), beams.nbeams (number of beams)

OutVar:

XY (vector determining the XY plane of the beams)

#### **function** [XY] = XYtoElementFn (beams)

#### InputVar:

beams.XY (vector determining the XY plane of the beams), beams.nbeams (number of beams), beams.disc (number of elements per beam)

#### OutVar:

XY (vector determining the XY plane of the elements)

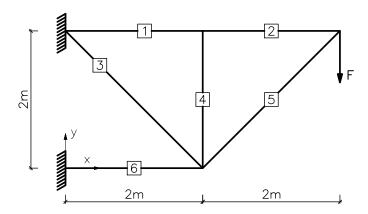


Figure 1: Example Setup.

## 0.2 Example of usage - stability

The studied example is taken from the introduction of the article [1]. The cross-section of the structure in Figure 1 is a tubular section with an outer radius of  $r_o=4$  cm and an inner radius of  $r_i=3.5$  cm. The material parameters are the modulus of elasticity E=210 GPa and Poisson's ratio  $\nu=0.3$ . Each member is divided into 16 frame elements. Running the file Torii\_ex0\_stab1.m with the implementation of this example yields  $P_{crit}=83.22$  kN. For comparison and validation, results from the OOFEM software package (http://oofem.org) are provided. The plot of the corresponding first mode shape is shown in Figure 2.

| $\lambda_i$ | OOFEM   | StableTrussOpt-MATLAB | [%]  |
|-------------|---------|-----------------------|------|
| 1           | 83.21   | 83.22                 | 0.01 |
| 2           | 288.91  | 288.95                | 0.01 |
| 3           | 344.47  | 344.52                | 0.01 |
| 4           | 471.79  | 471.93                | 0.03 |
| 5           | 521.11  | 521.18                | 0.01 |
| 6           | 814.43  | 814.95                | 0.06 |
| 7           | 942.06  | 943.18                | 0.12 |
| 8           | 1208.39 | 1209.99               | 0.13 |
| 9           | 1276.09 | 1278.20               | 0.16 |
| 10          | 1729.81 | 1735.48               | 0.33 |

Table 1: Comparison of critical load factors for the first 10 eigenmodes.

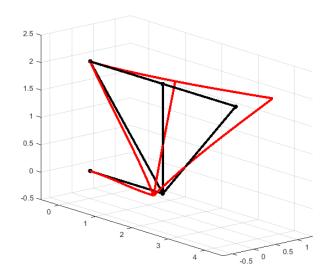


Figure 2: First eigenmode shape, showing deflection out of plane.

## 0.3 Example of usage - optimization

By running the file Torii\_ex0\_opt1.m, the optimization of the example is performed, yielding the targeted  $P_{crit} = 10.00$  kN. For comparison and validation, the results from the OOFEM software package (http://oofem.org) are provided in the following table.

| $\lambda_i$ | OOFEM  | StableTrussOpt-MATLAB | [%]   |
|-------------|--------|-----------------------|-------|
| 1           | 10.00  | 10.00                 | 0.04  |
| 2           | 37.53  | 37.50                 | 0.06  |
| 3           | 41.95  | 41.95                 | 0.02  |
| 4           | 76.01  | 76.02                 | 0.01  |
| 5           | 84.42  | 84.34                 | 0.09  |
| 6           | 119.62 | 119.38                | 0.20  |
| 7           | 143.41 | 143.45                | 0.03  |
| 8           | 229.50 | 216.41                | 5.70  |
| 9           | 283.64 | 229.80                | 18.98 |
| 10          | 314.50 | 283.08                | 9.99  |

Table 2: Comparison of critical load factors

# **REFERENCES**

[1] André Torii, Rafael Lopez, and Leandro Miguel. Modeling of global and local stability in optimization of truss-like structures using frame elements. *Structural and Multidisciplinary Optimization*, 51, 12 2014.