

# 1 Profiles & Layout

## 1.1

## 1.2

## 1.3

# 2 Process Procedures

## 2.1

## 2.2

## 2.3

# 3 Calculations

a) Film Thickness

Layer	Theoretical calculation (nm)	Experimental (nm)	% Error	Linewidths (photoresist) (nm)	Linewidths (after PR Strip) (nm)	% Overetch
Field Oxide	505.8	477.2	5.65	?	3000	?
Polysilicon	?	?	?	?	?	?
Gate Oxide	80.1	86.5	7.40	3628	4000	?
Intermed Oxide	386.3	320	17.2	?	?	?
Aluminum	?	?	?	2088	2520	?

b) Sheet Resistance

# 4 Questions

1. The lab uses positive photoresist. The lithography machine uses a light that has g line wavelength. The I and G lines refer to the wavelength of the light coming off the light bulb that reacts with photoresist. G line is roughly xx wavelength and I line is xx wavelength.

# 5 Appendix

Film thickness calculation for oxide:

$$X_{ox} = \frac{0.5B}{B/A} \left[ \sqrt{1 + \frac{4}{B} \left(\frac{B}{A}\right)^2 (t + \tau)} - 1 \right] \quad (1)$$

$$\tau = \frac{X_i^2}{B} + \frac{X_i}{B/A} \quad (2)$$

where

$$B/A = D_o e^{\frac{-E_a}{kT}} \text{ (Use table 3.1 [1] to find } E_a \text{ and } D_o \text{)}$$

$$B = D_o e^{\frac{-E_a}{kT}} \text{ (Use table 3.1 [1] to find } E_a \text{ and } D_o \text{)}$$

$t$  = Time of oxide growth

$\tau$  = Time of initial oxide growth already present

$X_i$  = length of initial oxide growth

Example: Calculated oxide thickness of Intermed Oxide:

Given: 5 min dry oxidation at 1050°C and 12 + 25 min wet oxidation and annealing at 1050°C, calculated oxide growth.

First we consider the 5 min dry oxidation. Using table 3.1 [1] for a  $< 100 >$  Silicon, and using dry oxidation, we see that for the linear rate constant (B/A),  $E_A = 2.00$  eV and  $D_o = 3.71 \times 10^6 \mu\text{m/hr}$ . For the parabolic rate constant (B),  $E_A = 1.23$  eV and  $D_o = 772 \mu\text{m/hr}$ .

Using an arrhenius equation where  $k$  = Boltzmann's constant, and  $T$  = temperature.

$$B/A = D_o e^{\frac{-E_A}{kT}} = 3.71 \times 10^6 e^{\frac{-2.00 \times 1.602 \times 10^{-19}}{1.38 \times 10^{-23} (1050^\circ \text{C} + 273)}} = 0.0887 \mu\text{m/hr}$$

$$B = D_o e^{\frac{-E_A}{kT}} = 772 e^{\frac{-1.23 \times 1.602 \times 10^{-19}}{1.38 \times 10^{-23} (1050^\circ \text{C} + 273)}} = 0.0159 \mu\text{m}^2/\text{hr}$$

Since there is no initial oxide here,  $\tau = 0$ ,

$$X_{ox} = \frac{0.5B}{B/A} \left[ \sqrt{1 + \frac{4}{B} \left( \frac{B}{A} \right)^2 (t + \tau)} - 1 \right] = \frac{0.5(0.0159)}{0.0887} \left[ \sqrt{1 + \frac{4}{0.0159} (0.0887)^2 \left( \frac{5\text{min}}{60\text{min/hr}} + 0 \right)} - 1 \right] \approx 7.11 \text{ nm}$$

Now after this dry oxidation, we have a 37 minute wet oxidation at 1050°C. Using table 3.1 [1] again, but this time using the constants that apply for wet oxidation,

$$B/A_{\text{wet}} = D_o e^{\frac{-E_A}{kT}} = 9.70 \times 10^7 e^{\frac{-2.05 \times 1.602 \times 10^{-19}}{1.38 \times 10^{-23} (1050^\circ \text{C} + 273)}} = 1.50 \mu\text{m/hr}$$

$$B_{\text{wet}} = D_o e^{\frac{-E_A}{kT}} = 386 e^{\frac{-0.78 \times 1.602 \times 10^{-19}}{1.38 \times 10^{-23} (1050^\circ \text{C} + 273)}} = 0.411 \mu\text{m}^2/\text{hr}$$

This time we do have an initial oxidation time  $\tau$  because of the dry oxidation we did. Here  $X_i$  is the oxide length we calculated for the dry oxidation growth,

$$\tau = \frac{X_i^2}{B_{\text{wet}}} + \frac{X_i}{B/A_{\text{wet}}} = \frac{0.00711^2}{0.411} + \frac{0.00711}{1.50} \approx 0.00488 \text{ hrs}$$

And finally our oxide growth is,

$$X_{ox} = \frac{0.5B}{B/A} \left[ \sqrt{1 + \frac{4}{B} \left( \frac{B}{A} \right)^2 (t + \tau)} - 1 \right] = \frac{0.5(0.411)}{1.50} \left[ \sqrt{1 + \frac{4}{0.411} (1.50)^2 \left( \frac{(12 + 25)\text{min}}{60\text{min/hr}} + 0.00488 \text{ hrs} \right)} - 1 \right] \approx 386.3 \text{ nm}$$