# 1 Measurements & Parameter Extraction

### 1.1 Line Width/Misalignment

### 1.1.1 Measured line widths

Nominal	ACTV	POLY	CONT	METAL
Linewidth	(dark field)	(clear field)	(dark field)	(clear field)
$2\mu\mathrm{m}$	3	4	1.869	2.520

### 1.1.2 Misalignment

### 1.2 Four-Point Resistors [2a, 2b]

### 1.2.1 Measurement Setup

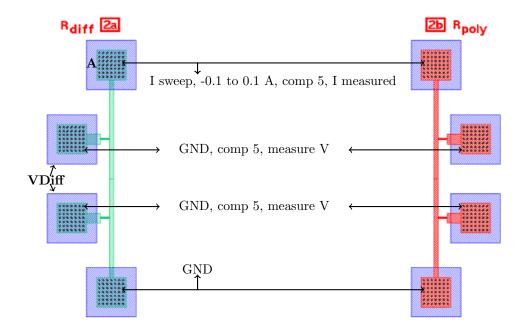


Figure 1: Device 2a is a diffusion resistor and 2b is a poly resistor.

#### 1.2.2 I-V plot for the diffusion resistor, 2a

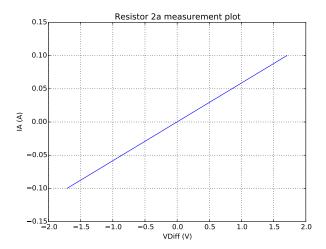


Figure 2: A plot of the measurement data taken for resistor 2a. The plot is based off of 2 data points.

From the plot above we can calculate our resistance. Note that the slope of the above plot will be equal to 1/R. Since I = V/R, where I is our dependent variable (y axis) and V is our independent variable (X axis). A resistance of  $R = 17 \Omega$  was calculated. Our width and length values are  $10 \mu m$  and  $200 \mu m$ . However our final  $2 \mu m$  line after the ACTV mask was  $3 \mu m$  which means that we had a overetch of about 50%. This means that

$$R_s = \frac{W}{L}R_{\text{diff}} = \frac{10(1.50)}{200}17 = 1.28\,\Omega$$

From the previous lab report we have a junction depth of  $1 \mu m$ . This means that our Resistivity is  $\rho = R_s x_j = 1.07 \times 10^{-4}$   $\Omega$ -cm. Using the Irvin curves in Jaeger [1], we can estimate the surface concentration  $N_0 \approx 10^{21}$ . Now the mobility can be calculated using a table of values from Appendix xx.

$$\mu_e = \mu_{\min} + \frac{\mu_0}{1 + (N/N_{\text{ref}})^{\alpha}} = 92 + \frac{1268}{1 + (10^{21}/1.3 \times 10^{17})^{0.91}} = 92.4 \,\text{cm}^2/V - s$$

### 1.2.3 I-V plot for the poly resistor, 2b

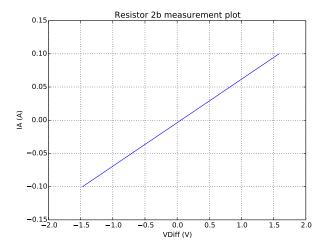


Figure 3: A plot of the measurement data taken for resistor 2b. The plot is based off of 2 data points.

From the plot above we calculate a 1/slope value of 15. Hense  $R = 15 \Omega$ . This means that

$$R_s = \frac{W}{L}R_{\text{poly}} = \frac{10(1.26)}{200}15 = 0.945\,\Omega$$

Our Resistivity is then  $\rho = R_s t_{\text{poly}}$  where  $t_{\text{poly}}$  is the polysilicon thickness which is 0.4  $\mu m$ , Hense  $\rho = 0.378 \,\Omega$ - $\mu m$ .

# 1.3 Four-Point Contact Resistor [17a, 17b]

### 1.3.1 Measurement Setup

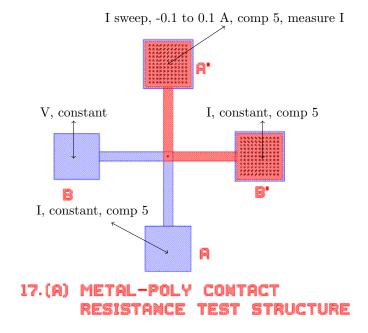


Figure 4: Measurement setup for 17a poly contact resistor. The same setup is used for the diffusion contact resistor, 17b.

### 1.3.2 I-V plot for 17a, poly reisistor

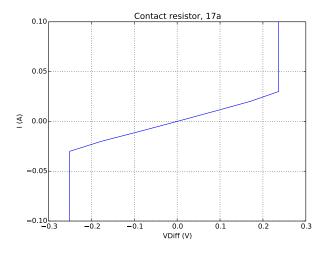


Figure 5: A plot of the measurement data taken for resistor 17a.

From the above plot we calculated a resistance of  $R=8.54\Omega$ . Note that the slope above gives us 1/R so we need to take the inverse to find the resistance.

### 1.3.3 I-V plot for 17b, diffusion resistor

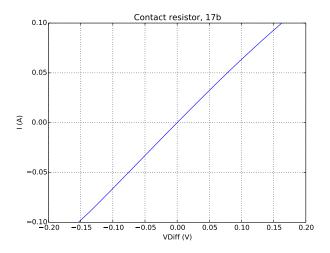


Figure 6: A plot of the measurement data taken for resistor 17b.

Similarly, from the above plot we calculated a resistance of  $R = 1.46\Omega$ .

# 1.4 Four-Point Contact-Chain Resistor [2c, 2d]

### 1.4.1 Measurement Setup

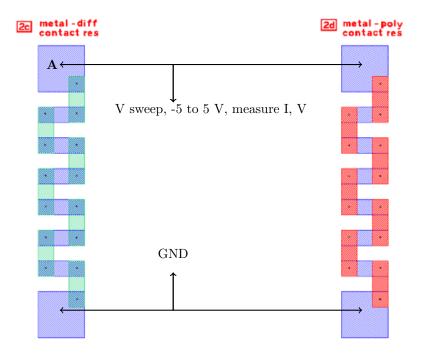


Figure 7: Chain resistor setup for diffusion and poly resistors.

### 1.4.2 b. I-V plot for diffusion resistor, 2c

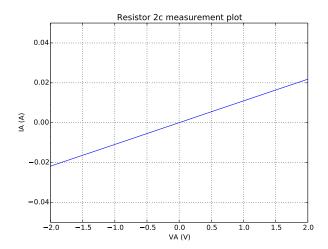


Figure 8: A plot of the measurement data taken for resistor 2c. The plot is based off of 2 data points.

The resistance calculated from the graph here is  $R = 91.2\Omega$ . Using sheet resistance from 2a/b and the total resistance from the slope above, we can solve for the contact resistance

$$R_{\rm total~diff} = 7(\eta R_{\rm S~diff} + R_{\rm C~diff}) \Rightarrow R_{\rm C~diff} = \frac{1}{7} R_{\rm total~diff} - \eta R_{\rm S~diff} = \frac{1}{7} (91.2\Omega) - 2.3 (1.07\Omega) = 10.6\Omega$$

### .4.3 b. I-V plot for poly resistor, 2d

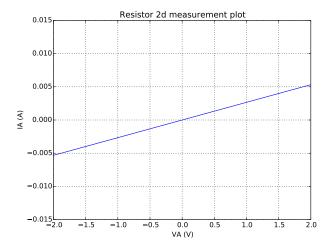


Figure 9: A plot of the measurement data taken for resistor 2d. The plot is based off of 2 data points.

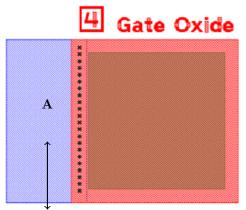
The resistance calculated from the graph here is  $R = 370\Omega$ . Using sheet resistance from 2a/b and the total resistance from the slope above, we can solve for the contact resistance

$$R_{\rm total~poly} = 7(\eta R_{\rm S~poly} + R_{\rm C~poly}) \Rightarrow R_{\rm C~poly} = \frac{1}{7} R_{\rm total~poly} - \eta R_{\rm S~poly} = \frac{1}{7} (370\Omega) - 2.3(0.945\Omega) = 50.7\Omega$$

### 1.5 Gate Oxide Capacitor, 4

### 1.5.1 Measurement Setup

Stage connector set to GND



V sweep, -10 to 10 V, step 0.2 V, oscillation 0.02Hz, integration medium

Figure 10: Gate capacitor setup.

### 1.5.2 C-V plot of gate oxide capacitor w/ lights ON

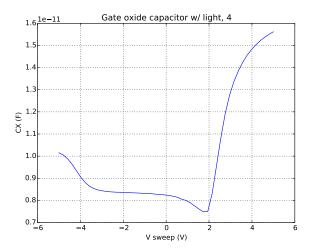


Figure 11: A plot of the measurement data taken for the gate capacitor, 4. Lights on.

The minimum capacitance from the plot above is 7.48 pF. The accumulation region capacitance at about 5 V is 15.7 pF. The active area is 200  $\mu m$  by 200  $\mu m$  while the pad+ring area is 240  $\mu m$  by 335  $\mu m$ . Also note the gate oxide thickness calculated below for the field oxide capacitors is 1.15  $\mu m$ .

$$C_{\rm measured} = A_{\rm active} \frac{\epsilon_{\rm ox}}{t_{\rm gox}} + A_{\rm pad\text{-}ring} \frac{\epsilon_{\rm ox}}{t_{\rm fox}}$$

$$t_{\rm gox} = [\frac{1}{A_{\rm active}}(\frac{C_{\rm measured}}{\epsilon_{\rm ox}} - \frac{A_{\rm pad\text{-}ring}}{t_{\rm fox}})]^{-1} = [\frac{1}{4\times10^{-8}}(\frac{15.7\times10^{-12}}{(3.9)8.85\times10^{-12}} - \frac{8.04\times10^{-8}}{1.15\times10^{-6}})]^{-1} = 0.104\,\mu{\rm m}$$

The capacitance per unit area in this case would be 15.7 pF /  $(240\mu m \times 335\mu m)$ . C/area = 1.95 pF/ $\mu$ m or 1.95 F/ $\mu$ m. Now in order to calculate the maximum depletion region we use an equation from lecture notes. Note the max and min capacitance we calculated earlier,

$$\frac{1}{C_{\min}} = \frac{1}{C_{\max}} + \frac{1}{A_{\text{pad-ring}}C_{\text{Dmin}}}, \text{ where } C_{\text{Dmin}} = \frac{\epsilon_{\text{si}}}{x_{\text{dmax}}}$$
(1)

Solving for the maximum depletion region we get,

$$x_{\rm dmax} = A_{\rm pad\text{-}ring} \epsilon_{\rm si} (\frac{1}{C_{\rm min}} - \frac{1}{C_{\rm max}}) = (8.04 \times 10^{-8}) (11.7 \times 8.85 \times 10^{-12}) (\frac{1}{7.48 \times 10^{-12}} - \frac{1}{15.7 \times 10^{-12}}) = 0.583 \mu m$$

Another equation from lecture will help us solve for the substrate doping concentration,

$$x_d = \sqrt{\frac{2\epsilon_{\rm si}}{q} \frac{1}{N_A} |\psi_s|} \tag{2}$$

where  $\psi_s$  is the potential drop and has a typical value of 0.3, q is the charge of an electron 1.602×10<sup>-19</sup> C, and  $N_A$  is the doping concentration.

$$N_A = \frac{2\epsilon_{\rm si}|\psi_s|}{qx_d{}^2} = \frac{2(11.7\times8.85\times10^{-12})(0.3)}{1.602\times10^{-19}(0.583\times10^{-6})^2} = 1.14\times10^{21}\,{\rm cm}^{-3} = 1.14\times10^{27}\,{\rm m}^{-3}$$

From the curve above (Figure 11) we can see that the flatband voltage is  $V_{FB} \approx 5.5$  and the corresponding  $C_{FB} \approx 15.5 \text{pF}$ . To find the charge per unit area at the oxide silicon interface we can use the Q = CV equation.

$$\frac{Q_{ss}}{A} = \frac{C_{FB}V_{FB}}{A_{\text{pad-ring}}} = \frac{(5.5)(15.5 \times 10^{-12})}{8.04 \times 10^{-8}} = 1.06 \,\text{mF/m}^2$$

To calculate the threshold voltage we will assume that  $V_{SB} = 0$ . First we must also calculate  $Q_{BO}$  which is the charge stored in the depletion region,

$$Q_{BO} = \sqrt{2q\epsilon_{si}N_B 2\phi_F} = \sqrt{2(1.602 \times 10^{-19})(11.7 \times 8.85 \times 10^{-12})(1.14 \times 10^{27})(2 \times 0.3)} = 1.51 \times 10^{-1} \, C/m^2$$

Now to calculate/estimate threshold voltage. Note that the work function  $\phi_{ms}$  is zero for n+ doped poly gate.

$$V_t = \phi_{ms} + 2\phi_f - \frac{Q_{ss}}{C_{\text{max}}} + \frac{Q_{BO}}{C_{\text{max}}} = 0 + 0.6 - \frac{1.06 \times 10^{-3}}{1.95} + \frac{1.51 \times 10^{-1}}{1.95} = 0.677V$$

### 1.5.3 C-V plot of gate oxide capacitor w/ lights OFF

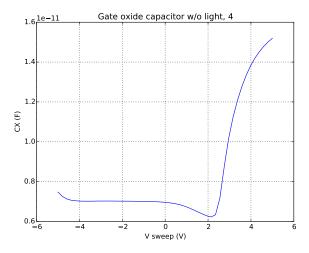


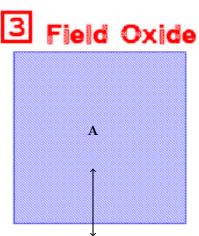
Figure 12: A plot of the measurement data taken for the gate capacitor, 4. Lights off.

minimum capacitance ...

### 1.6 Field Oxide Capacitor, 3

### 1.6.1 Measurement Setup

Stage connector set to GND



V sweep, -5 to 5 V, step 0.2 V, oscillation 0.02Hz, integration medium

Figure 13: Field oxide capacitor setup.

### 1.6.2 C-V plot of field oxide capacitor

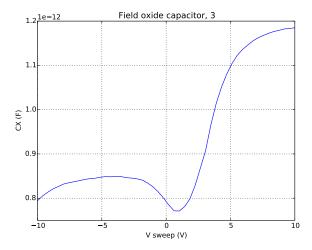


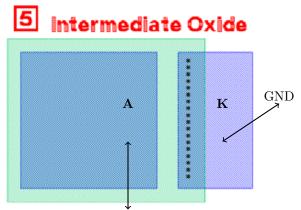
Figure 14: A plot of the measurement data taken for the field oxide capacitor, 3

From the plot above we see that at the accumulation region of  $\approx 10$  volts we have a corresponding capacitance of  $C \approx 1.2 \mathrm{pF}$ . Noting that the area of the capacitor plate is 200  $\mu m$  by 200  $\mu m$ , we can now solve for the dieletric (oxide) thickness.

$$C = \frac{A\epsilon_{\rm ox}}{t_{\rm fox}} \Rightarrow t_{\rm fox} = \frac{3.9A\epsilon_0}{C} = \frac{3.9(4\times 10^{-8})(8.85\times 10^{-12})}{1.2\times 10^{-12}} = 1.15\,\mu{\rm m}$$

# 1.7 Intermediate Oxide Capacitors, 5

### 1.7.1 Measurement Setup



V sweep, -5 to 0 V, step 0.2 V, oscillation 0.02Hz, integration medium

Figure 15: Intermediate oxide capacitor setup.

### 1.7.2 C-V plot of intermediate oxide capacitor

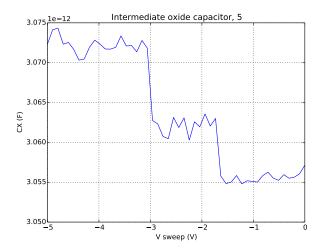


Figure 16: A plot of the measurement data taken for the Intermediate oxide, 5

The capacitance at the accumulation region of  $\approx 5$  V is about 3.0725 pF.

### 1.8 Diode, 7

### 1.8.1 Measurement setups for forward and reverse operations

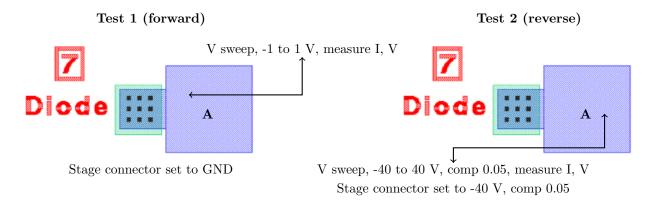


Figure 17: Two tests were performed on this diode; both measurement setups are shown above.

#### 1.8.2 I-V plots for forward and reverse operation

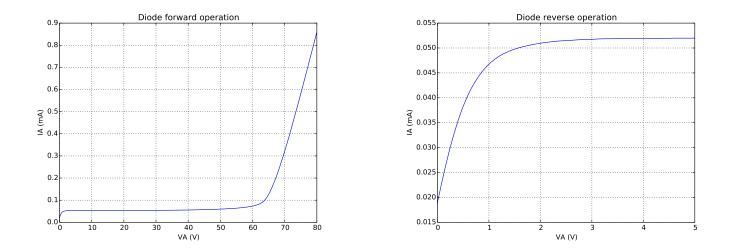


Figure 18: Plots of forward and reverse operation of Diode 7.

Looking at the plots above, the forward turn on voltage is  $V_F \approx 70V$  while the reverse bias turn off voltage is about  $V_{RB} \approx 0.5V$ . To calculate the series resistance in the forward bias we look at the region of the curve where V is greater than 65 V. The inverse of the slope there results in  $R = 17.8 \, k\Omega$ . Similarly for the reverse bias plot, looking at the region below 0.5 Volts, we find that the inverse of the slope is  $R = -22.1 \, k\Omega$ .

### 1.9 MOSFETs of Varying Length, [8a-d]

### 1.9.1 Measurement setups

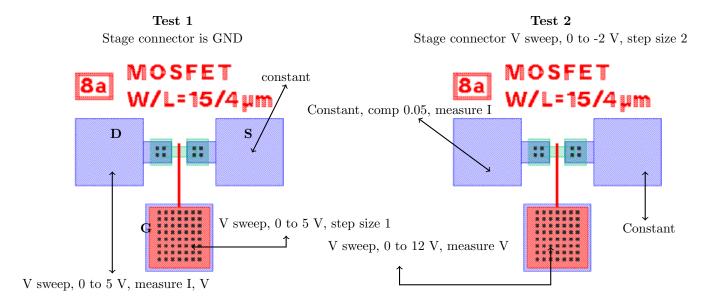


Figure 19: Measurement setup for Mosfet 8a. The same setup is used for Mosfets 8a-d. The only difference is the channel length which changes from 4 (8a) to 6 (8b) to 8 (8c) to 10 (8d) microns.

### 1.9.2 Plots of $I_D$ - $V_D$ , sweeping $V_G$

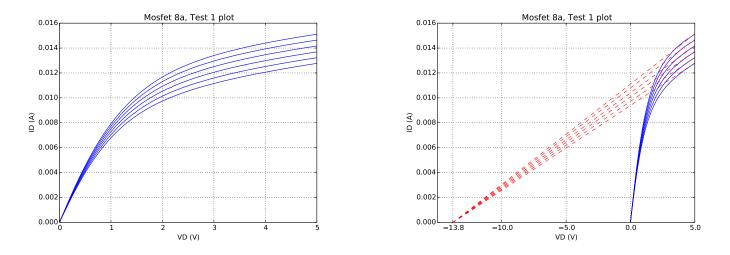
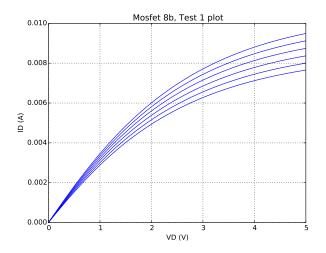


Figure 20: Test 1 for Mosfet 8a with extended x axis range in order to calculate lambda.

We see that everything intersects at about -13.8 V. This corresponds to  $\lambda = \frac{1}{-13.8} = -0.0725$ .



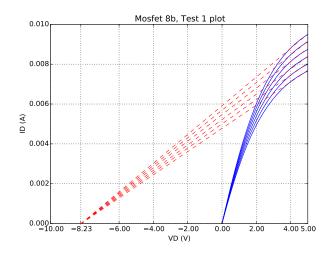
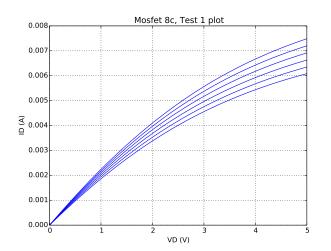


Figure 21: Test 1 for Mosfet 8b with extended x axis range in order to calculate lambda.

We see that everything intersects at about -8.23 V. This corresponds to  $\lambda = \frac{1}{-8.23} = -0.122$ .



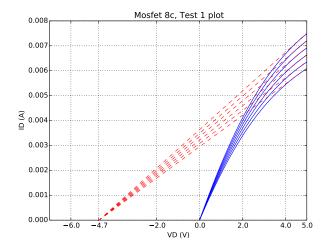
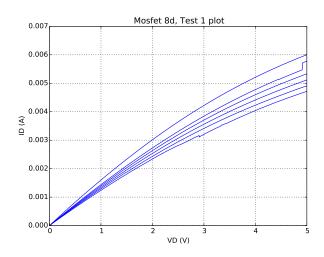


Figure 22: Test 1 for Mosfet 8c with extended x axis range in order to calculate lambda.

We see that everything intersects at about -4.70 V. This corresponds to  $\lambda = \frac{1}{-4.70} = -0.213$ .



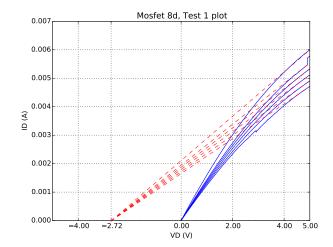


Figure 23: Test 1 for Mosfet 8d with extended x axis range in order to calculate lambda.

We see that everything intersects at about -2.72 V. This corresponds to  $\lambda = \frac{1}{-2.72} = -0.368$ .

### 1.9.3 $\lambda$ vs $L_{Drawn}$

To summarize, here is a table of all  $\lambda$  values calculated,

MOSFET device	$\lambda$ $(V^{-1})$	$L_{\text{drawn}} (\mu m)$	Fig #
8a	-0.0725	4	20
8b	-0.122	6	21
8c	-0.213	8	22
8d	-0.368	10	23

Figure 24: all  $\lambda$  values for mosfets 9a-d along with gate lengths.

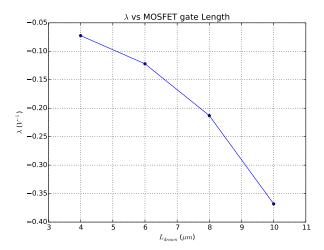
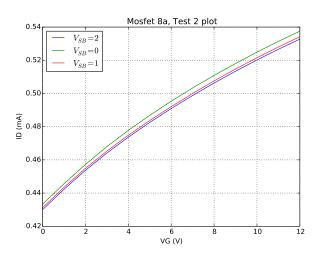


Figure 25:  $\lambda$  for each 8a-d device vs the gate length.

### 1.9.4 Plots of $I_D$ - $V_G$ , sweeping $V_B$



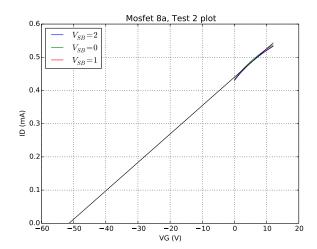
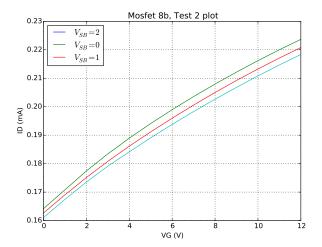


Figure 26: Test 2 for Mosfet 8a. On the right side we did a linear regression on the  $V_{SB} = 0$  line in order to get a estimate of the threshold voltage.

Since it is quite difficult to see where a slope change occurs in order to find the threshold voltage, we can do a linear regression using the  $V_{SB}=0$  line. With linear regression,  $V_t=-51.4V$ . One reason why there is no slope change might have to do with the fact that most of our MOSFETS show characteristics of junction leakage.



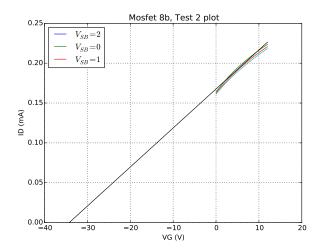
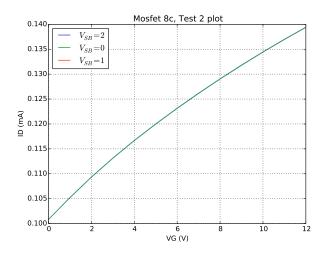


Figure 27: Test 2 for Mosfet 8b. On the right side we did a linear regression on the  $V_{SB} = 0$  line in order to get a estimate of the threshold voltage.

Similarly, the threshold voltage is not clear in the figure above. Using linear regression again with  $V_{SB} = 0$  we get  $V_t = -34.2$ .



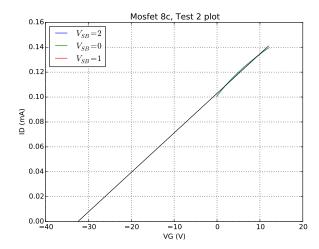
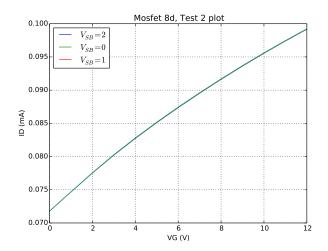


Figure 28: Test 2 for Mosfet 8c. On the right side we did a linear regression on the  $V_{SB} = 0$  line in order to get a estimate of the threshold voltage.

Similarly, the threshold voltage is not clear in the figure above. Using linear regression again with  $V_{SB} = 0$  we get  $V_t = -32.4$ .



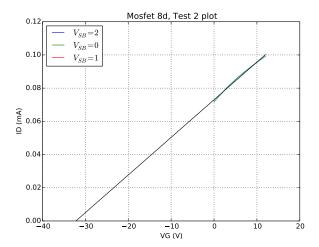


Figure 29: Test 2 for Mosfet 8d. On the right side we did a linear regression on the  $V_{SB} = 0$  line in order to get a estimate of the threshold voltage.

Similarly, the threshold voltage is not clear in the figure above. Using linear regression again with  $V_{SB} = 0$  we get  $V_t = -32.2$ .

### 1.9.5 Estimate of $\Delta L$

To summarize the threshold voltages calculated in the last section,

MOSFET device	$V_t(V)$	$L_{\text{drawn}} (\mu m)$	Fig #
8a	-51.4	4	26
8b	-34.2	6	27
8c	-32.4	8	28
8d	-32.2	10	29

Figure 30: Threshold voltages for all MOSFET 8 devices.

Now the first step in calculating  $\Delta L$  is to find the extended Resistance. We can do this by plotting the measured resistance vs gate Length at various voltages (from lecture). This plot looks like the following:

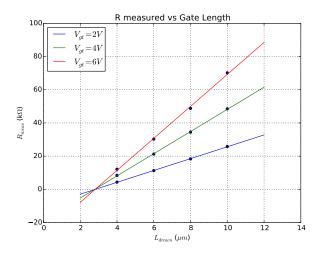


Figure 31: Measured Resistance vs Gate length for various lengths and voltages

The Y value from the origin (0) to the point of intersection would be the extended Resistance value. However in our case the lines intersect at just about 0; this means that  $R_{\rm ext} \approx 0$ . Now we can solve for  $\Delta L$  by using the following equation from lecture:

$$R_{\text{meas}} = \frac{L_{\text{drawn}} - \Delta L}{\mu W C_{\text{gox}}(V_{\text{gs}} - V_t)} + R_{\text{ext}}$$
(3)

Solving for  $\Delta L$  and noting that from earlier that  $C_{\rm gox}=1.95 {\rm pF}/\mu m^2$  and  $\mu_n=92.4 {\rm cm}^2/{\rm V}$ -s. We will also choose  $V_{gs}-V_t=2V$ ,  $L_{\rm drawn}=4\mu m$ , and  $R_{\rm meas}=8.368 k\Omega$ . Note that W = 15  $\mu m$  and  $R_{ext}=0$ .

$$\Delta L = L_{\rm drawn} - R_{\rm meas} \mu_n C_{\rm gox} (V_{\rm gs} - V_t) = (8.368 \times 10^3 \Omega) (92.4 {\rm cm}^2 / {\rm V \cdot s}) (15 \times 10^{-6} {\rm m}) (1.95 \times 10^{-7} {\rm F/cm}^2) (2 {\rm V}) = 1.59 \, \mu m^2 / {\rm V \cdot s}$$

# 1.10 MOSFETs of varying width [9a-c]

### 1.10.1 Measurement setup

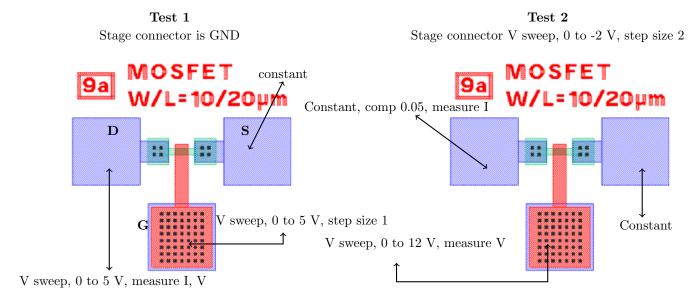


Figure 32: Measurement setup for Mosfet 9a. The same setup is used for Mosfets 9a-c. The only difference is the channel widths which changes from 10 (9a) to 15 (9b) to 20 (9c) microns.

# 1.10.2 Plots of $I_D$ - $V_D$ , sweeping $V_G$

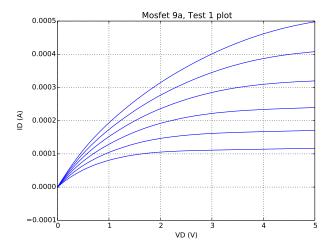


Figure 33: Test 1 for Mosfet 9a

### Calculate stuff here...

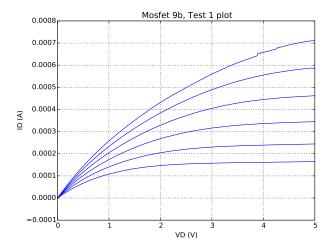


Figure 34: Test 1 for Mosfet 9b

Calculate stuff here...

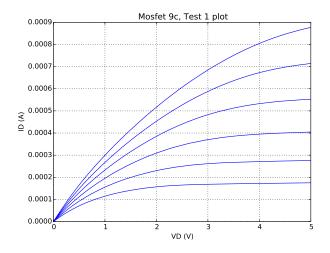
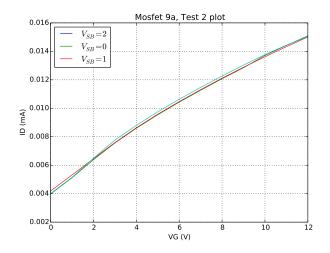


Figure 35: Test 1 for Mosfet 9c

Calculate stuff here...

# 1.10.3 Plots of $I_D$ - $V_G$ , sweeping $V_B$



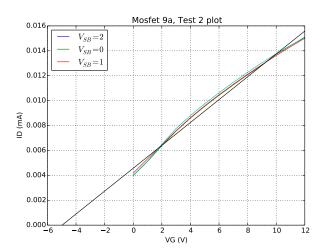
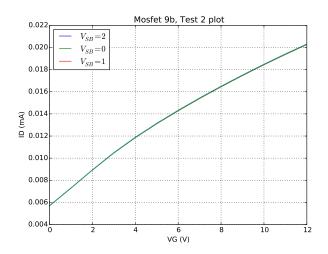


Figure 36: Test 2 for Mosfet 9a. On the right side we did a linear regression on the  $V_{\rm SB}=0$  line in order to get a estimate of the threshold voltage.

Using linear regression, we calculated a threshold voltage of  $V_t = -4.98$ .



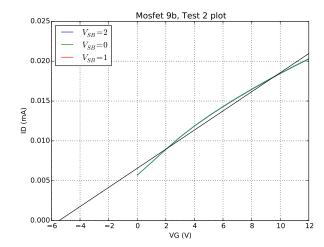
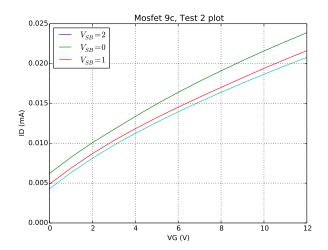


Figure 37: Test 2 for Mosfet 9b. On the right side we did a linear regression on the  $V_{\rm SB}=0$  line in order to get a estimate of the threshold voltage.

Using linear regression, we calculated a threshold voltage of  $V_t = -5.46$ .



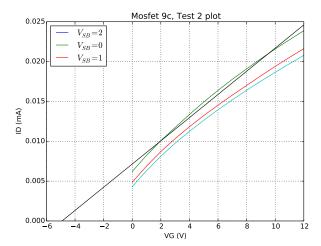


Figure 38: Test 2 for Mosfet 9c. On the right side we did a linear regression on the  $V_{\rm SB}=0$  line in order to get a estimate of the threshold voltage.

Using linear regression, we calculated a threshold voltage of  $V_t = -4.91$ .

### 1.10.4 W calculation and plot

To summarize the threshold voltages calculated in the last section,

MOSFET device	$V_t(V)$	$W_{\rm drawn} \ (\mu m)$	Fig #
9a	-4.98	10	36
9b	-5.46	15	37
9c	-4.91	20	38

Figure 39: Threshold voltages for all MOSFET 8 devices.

Now to calculate the channel width we first plot the reciprocal of the measured resistance vs channel width (from lecture).

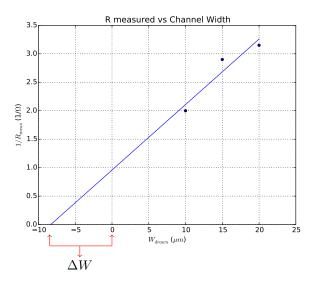


Figure 40: 1/R vs the channel Width. A linear regression was used to fit the data points. Note that it intersects zero at a negative length.

The line above intercepts the x axis at -8.33  $\mu$ . Hense our  $\Delta W = -8.33 \mu m$ . Now to plot the threshold voltage vs the effective channel width we can use Figure 39. Note that  $W_{\rm eff} = W_{\rm drawn} - \Delta W$ .

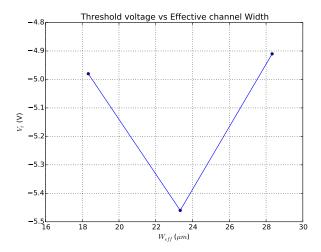


Figure 41: Channel threshold voltage vs the channel width. Note the odd V shape which appears because of the calculated threshold voltages.

### 1.11 Large MOSFET, 10

### 1.11.1 Measurement setup

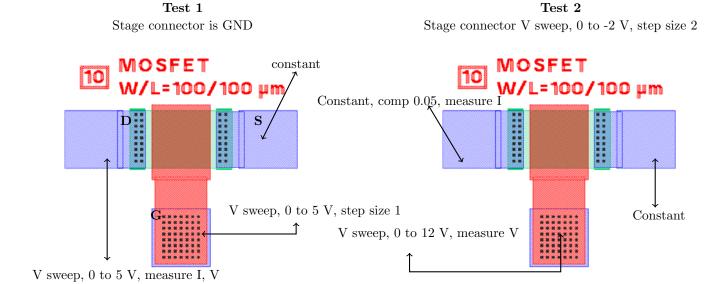


Figure 42: Measurement setup for Mosfet 10. This mosfet has very large dimensions compared to others.

### 1.11.2 Plots of $I_D$ - $V_D$ , sweeping $V_G$

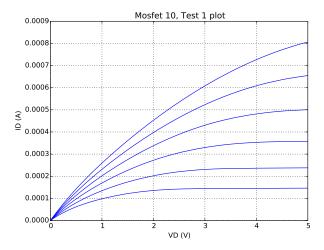
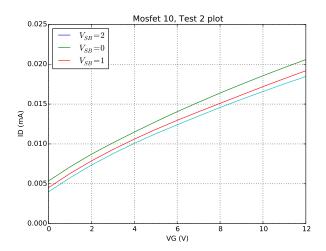


Figure 43: Test 1 for Mosfet 10

### 1.11.3 Plots of $I_D$ - $V_G$ , sweeping $V_B$



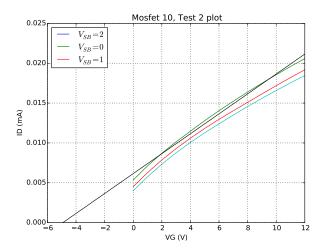


Figure 44: Test 2 for Mosfet 10. On the right side we did a linear regression on the  $V_{\rm SB} = 0$  line in order to get a estimate of the threshold voltage.

The threshold voltage here is  $V_t = -4.92V$ .

#### 1.11.4 Calculating mobility, threshold, and other parameters

To calculate the effective electron mobility we will use the following equation,

$$\mu_{\text{eff}}(V_G) = \frac{I_D}{\frac{W_{\text{eff}}}{L_{\text{eff}}} C_{\text{gox}}(V_{GS} - V_t) V_{DS}} \tag{4}$$

Note that  $I_D$  depends on  $V_G$  from the previous plot. For  $\Delta W$  and  $\Delta L$  we will use values calculated earlier (-8.33 and 1.59  $\mu m$ ). MOSFET 10 has a W and L value of 100  $\mu m$ . Threshold voltage was calculated as  $V_t = -4.92V$  and  $V_{DS} = 0.05V$ .  $C_{\rm gox}$  was also calculated earlier as  $1.95 {\rm pF}/\mu {\rm m}^2$ .

$$\mu_{\rm eff}(V_G) = \frac{I_D}{\frac{W_{\rm eff}}{L_{\rm eff}}C_{\rm gox}(V_{GS}-V_t)V_{DS}} = \frac{I_D(V_G)}{\frac{(100+8.33)\times 10^{-6}}{(100-1.59)\times 10^{-6}}(1.95\times 10^{-15})(V_{GS}+4.92)(0.05)} = \frac{I_D(V_G)}{1.07\times 10^{-8}(V_{GS}+4.92)} {\rm cm}^2/{\rm V-s}$$

Now we plot  $\mu_{\text{eff}}(V_G)$  vs  $V_G$  using the values for  $I_D(V_G)$  from the previous graph (Figure 44).

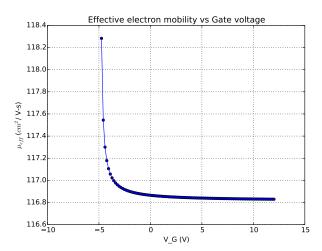


Figure 45: Note how the graph levels off almost immediately. The first few data points are right above the threshold voltage.

Now if we do a linear fit to each line in Figure 44 we get the following results,

$V_{SB}$ (V)	$V_t$ (V)
0	-4.92
1	-4.55
2	-4.18

Figure 46: Results from doing a linear fit to each line in Figure 44 above.

With this data we can now make a  $V_t(V_{SB})$  vs  $\sqrt{V_{SB}+0.7}$  plot in order to estimate our body effect parameter  $\gamma$ .

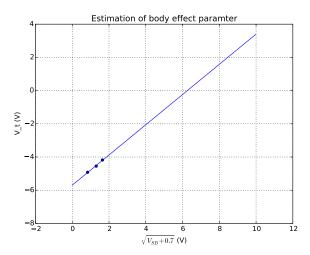


Figure 47: The slope of the above plot is our body effect parameter

Since we only have 3 data points for  $V_{SB}$  our plot is not very accurate and does not show the change of slope as would be present in the theoretical case. Nonetheless, the slope for the above plot is  $\gamma = 0.910$ . The equation for  $\gamma$ , the body effect parameter, is:

$$\gamma = \frac{\sqrt{2\epsilon_{\rm si}qN_A}}{C_{\rm gox}} = \tag{5}$$

Solving for the surface concentration and using previous values of  $C_{\text{gox}} = 0.195 \mu \text{F/cm}^2$ .

$$N_A = \frac{(\gamma C_{\rm gox})^2}{2q\epsilon_{\rm si}} = \frac{(0.910*0.195\times10^{-6})^2}{2(1.602\times10^{-19})(11.7\times8.85\times10^{-12})} = 9.49\times10^{14} {\rm cm}^{-3}$$

Finally, we plot a log plot of the data in Figure 44.

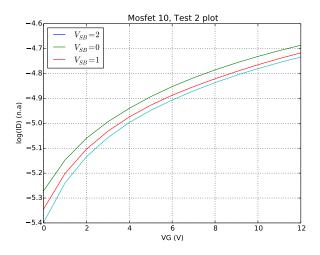


Figure 48: Log plot of Figure 44.

The subthreshold slope was calculate between  $V_G = 0$  and  $V_G = 1$ . This slope was calculated to be 0.12  $(V^{-1})$ .

### 1.12 Inverter, 14

### 1.12.1 Measurement setup

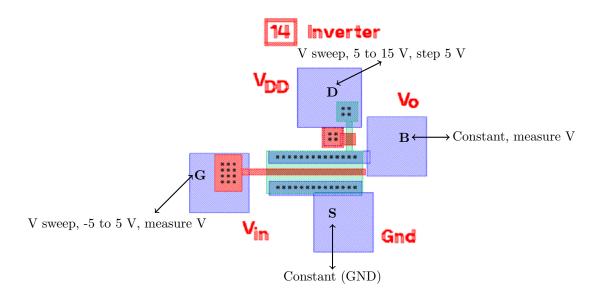


Figure 49: Setup for the inverter. Note that the source is connected to a GND and not the stage connector.

### 1.12.2 b. $V_{in} - V_{out}$ plot

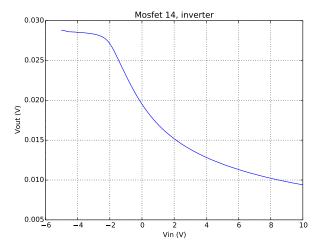


Figure 50: Plot for Inverter. Note both axis are in units of Volts.

To find the point where  $V_{IN} = V_{OUT}$  we ran a simple loop to find the closest point. We calculated  $V_M = 0.025V$ . At that voltage  $|V_{OUT} - V_{IN}|$  is minimized.

### 2 Theoretical Calculations

### 2.1 Measured Physical Dimensions and Parameters

Parameter	Measured Value
Field $t_{ox}$	477.2 nm
Gate $t_{\rm ox}$	86.5 nm
Intermediate $t_{ox}$	320 nm
$X_{j}$	1000 nm
$X_{j, \text{lateral}}$	880 nm
$N_D$	$10^{21}\mathrm{cm}^{-3}$

### 2.2 Resistors [2a,2b]

### 2.3 Contact Resistances [17a,17b]

From jaeger Figure 7.6 [1] we that the specific contact resistivity  $10^{-2} \mu\Omega$ -cm<sup>2</sup>. The contact area of resistors 17a and 17b is  $5\mu m$  by  $5\mu m$ . This means the theoretical contact resistance for our contact resistors is

$$R_c = \frac{\rho_c}{A} = \frac{10^{-2}\mu\Omega - \text{cm}^2}{25\mu m} = \frac{10}{25} = 0.4\Omega$$

### 2.4 Contact-Chain Resistors [2c, 2d]

#### 2.4.1 Diffusion chain resistor, 2c

 $R_c$  is the contact resistance calculated earlier and  $R_s$  is the sheet resistance calculate for the diffused resistor.  $\eta$  is a geometrical constant that has a value of 2.3

$$R_{\text{total}} = 7(\eta R_s + R_c) = 7((2.3)(R_s) + (0.4)) = ?$$

#### 2.4.2 Poly chain resistor, 2d

 $R_c$  is the contact resistance calculated earlier and  $R_s$  is the sheet resistance calculate for the poly resistor.  $\eta$  is a geometrical constant that has a value of 2.3

$$R_{\text{total}} = 7(\eta R_s + R_c) = 7((2.3)(R_s) + (0.4)) = ?$$

### 2.5 Gate/Field Oxide Capacitors[3,4]

### 2.6 Diode

We make the assumption that the junction is a step junction and that the concentrations of dopants are constant across respective regions of the device. Built-in potential for a p-n diode is given by the function:

$$\phi = \frac{kT}{q} \ln \frac{N_A N_d}{n_i^2} \tag{6}$$

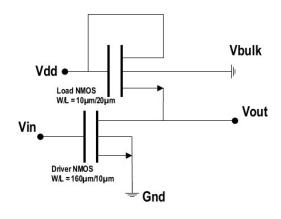
Where T is room temperature,  $N_A$  is the p-sub dopant concentration (8×10<sup>14</sup>cm<sup>-3</sup>),  $N_d$  is the n+ dopant concentration (10<sup>21</sup>cm<sup>-3</sup>), and  $n_i$  is the instrinsic carrier concentration for silicon (10<sup>10</sup>).

$$\phi = \frac{kT}{q} \ln \frac{N_A N_d}{{n_i}^2} = \frac{1.38 \times 10^{-23} (298)}{1.602 \times 10^{-19}} \ln \frac{(8 \times 10^{14})(10^{21})}{10^{20}} = 0.92V$$

### 2.7 MOSFETs

- 2.7.1 MOSFETs of varying length [8] and width [9]
- 2.7.2 Large MOSFET

### 2.8 Inverter



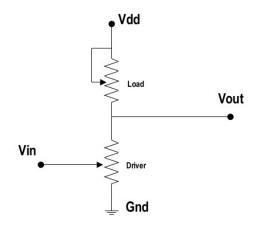


Figure 51: Setup for inverters.

The load resistor has Vdd connected to the drain and the gate. Since

$$V_{DS} = V_{dd} - Vout$$
$$V_{GS} = V_{dd} - V_{out}$$

Then

$$V_{DS} = V_{dd} - V_{out} > = V_{dd} - V_{out} - V_{tnl} = V_{GS} - V_{tnl}$$

So the load transistor is always in the saturation region, regardless of Vdd. It therefore acts as a variable resistor dependent on Vdd. The threshold voltage for both NMOS transistors is:

$$V_{TN} = V_{FB} + 2|\Phi_F| + (1/C_0)\sqrt{2\epsilon_s q N_B(2|\Phi_F| + V_{sb})}$$

They differ in  $V_{sb}$  so

$$V_{tnl}=V_{TN0}+(1/C_0)\sqrt{2\epsilon_sqN_B}(\sqrt{2|\Phi_F|}+V_{out}-\sqrt{2|\Phi_F|})$$
 
$$V_{tnd}=V_{TN0}$$
 Where  $V_{TN0}=V_{TND}=0.03$ 

Since  $V_{tnl}$  is dependent on  $V_{out}$  and vice versa,  $V_{out}$  can only be determined by iteration. For the purposes of graphing, we will make the simplifying assumption that the effect of substrate bias is small, and thus that  $V_{tnl}$  can be estimated to be  $V_{TN0}$ . This is not the case in reality, but should serve the purpose of illustrating the expected curves.

For the drive transistor: In the cutoff region  $(V_{in} < V_{tnd})$ , no current flows through the driver transistor, therefore the drain currents are zero for both transistors.

$$I_{Dl} = K_L (V_{dd} - V_{out} - V_{tnl})^2 = 0$$

Therefore  $V_{out} = V_{dd} - V_{tnl}$ . In the saturated region  $(V_{out} > V_{in} - V_{tnd} > 0)$ , both transistors are saturated. Their drain currents must be equal.

$$I_{dl} = K_L (V_{dd} - V_{out} - V_{tnl})^2 = K_D (V_{in} - V_{tnd})^2 = I_{Dd}$$

$$V_{out} = V_{dd} - V_{tnl} - \sqrt{K_D / K_L} (V_{in} - V_{tnd})$$

In the linear region  $(V_{in} - V_{tnd} > V_{out} > 0)$ , the driver transistor is in the linear region and the load transistor is in the saturated region. Since their drain currents must again be equal:

$$I_{dl} = K_L (V_{dd} - V_{out} - V_{tnl})^2 = 2K_D (V_{in} - V_{tnd} - 0.5V_{out})V_{out} = I_{Dd}$$

Here the dependence of Vin on Vout is becomes non-linear.

$$V_{in} = \frac{(K_L/K_D)(V_{dd} - V_{out} - V_{tnl})^2 + V_{out}^2 + V_{tnd}V_{out}}{2V_{out}}$$

Also note that for our transistor, the aspect ratio should be

$$\frac{K_D}{K_L} = \frac{W_D L_L}{L_D W_L} = \frac{160 * 20}{10 * 10} = 16$$

For  $V_{tnl}$  and  $V_{tnd}$  we will use a value of 0.3 as mentioned above.  $V_{dd}$  will range from 0 to 5 volts.

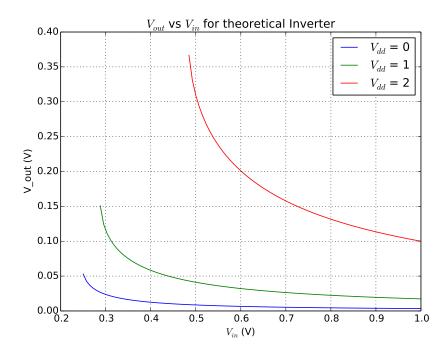


Figure 52: Theoretical inverter plot.

- 3 Discussion
- 4 Optional Questions
- 5 Appendix
- 6 References

1. Jaeger, Richard. Introduction to microelectronic fabrication. New Jersey: Prentice Hall, 2002. Print.