

Seaglider Quality Control Manual

SCHOOL OF OCEANOGRAPHY
and
APPLIED PHYSICS LABORATORY
UNIVERSITY OF WASHINGTON

Version 1.11 October 2012

Corresponding to Seaglider basestation version 2.08

Revision History

08/12/2011	Initial version.
10/20/2011	Change interpolation and suggestion policies; handle warm trapped water at apogee; document speed QC.
03/21/2012	Remove discussion of CTD data decimation.
04/19/2012	Update discussion of conductivity and salinity checks and bounds; removed stalled from directives lists.
06/05/2012	Broaden handling warm trapped water to dives; improve discussion of oxygen corrections.
10/06/2012	Improve description of oxygen corrections and QC.
07/29/2013	Clarify pressure to depth interpolation; SBE43 flow-related effects now corrected.

Introduction

This document describes the data processing and quality-control procedures for profile data received from Seaglider (and Deepglider) deployments.

The overall data quality control process is patterned after the Argo data processing scheme (Schmid, *et al*, 2007 and Argo, 2010). In particular, an initial fully-automated quality control process, described in this manual, produces a NetCDF-format file for each profile sufficient for deposit to any national repository, such as the National Oceanographic Data Repository. This process corresponds to Argo's 'real-time' quality control procedure.

This is followed, at some date, by a manual review of each profile by one or more trained oceanographers, leading to possible adjustments to the automated results and hence resubmission. This process corresponds to the Argo 'delayed-mode' quality control procedure. A preliminary manual adjustment mechanism is presented in this document.

Additional information about oceanographic data quality control may be found in the references. The basic seawater property calculations used throughout rely upon formulas taken from UNESCO's joint panel on oceanographic tables and standards, described in UNESCO, 1981 and Fofonoff, *et al*, 1983.

Known limitations

With few exceptions due to minor parameter renaming, glider data files written after May, 2006 (Seaglider code version 65.03) can be processed. Files written prior to this date must be converted to a more recent format; contact the Seaglider Fabrication Center at the University of Washington for software and assistance with this procedure.

The conversion and quality-control tests assume that the data was collected during a normal profile cycle comprising a dive, apogee, climb, and possible surface maneuver. So-called 'yo-yo' dives (a series of multiple apogee and perigee maneuvers before surfacing) are supported but depth-averaged current calculations are not performed. Dives under ice or using RAFOS navigation are not supported.

No quality control checks are performed between profiles on a deployment. For example, checks for possible sensor drift or conductivity anomalies occurring between adjacent profiles are not performed.

Files required and produced during data processing

During a deployment, the glider transmits a log file and one or more engineering data files for each profile; additional engineering data files may be produced by other instruments not part of the basic glider sensor package. (Separate Seaglider documents describe the on-board file formats, how the data is collected, and how it is transmitted by the vehicle.)

To control data conversion and checking during and after the deployment, the scientist supplies a **sg_calib_constants.m** file containing a set of calibration constants and other control parameter values that apply to all profiles in the deployment. A partial list of these control variables is given in Appendix B. In addition, the scientist may supply a **sg_directives.txt** file containing per-deployment or per-dive directives describing manual quality-control corrections and review notations. The form and processing of this file is described in the 'Manual Quality Control' Chapter below. While the basestation as a whole handles many different files, the dive profile processing code initially requires only a log and engineering file for each profile, and a **sg_calib_constants.m** file for the deployment. Other glider control files, such as the **cmdfile**, **science** or **targets** files, are ignored.

After processing the log and engineering files, all recorded data and any derived results, with associated quality control values, as well as the **sg_calib_constants** values are written to a NetCDF-format file (the so-called '.nc' file), one per profile. The .nc file also records the level of quality control procedures, various control parameters, the review state, and a record of processing history, documenting how the results were obtained. A list of the main output variables in an .nc file is given in Appendix C. Each profile .nc file, regardless of review level, should be sufficient for national repositories. The .nc files follow CF 1.6 Metadata Conventions and NODC guidelines for trajectory files.

As each .nc file contains all the uncorrected data from the original data files, they are sufficient to support subsequent processing in the absence of those original files. The basestation inspects the time-stamps of the various files, if they are present, to determine if any further processing need occur. If any original file is found to be more recent than the .nc file (for example, the scientist updates the `sg_calib_constants.m` or `sg_directives.txt` file or a transmission from the glider updates a data file), the calculations will be recomputed and the .nc file will be updated. Indeed, it is typical to manually review and adjust the data in the .nc file in the absence of any of the original files using the directives mechanism (or, in the future, via a GUI-based system). Reprocessing of any profile can be ensured by providing the `--force` option to the `MakeDiveProfiles.py` basestation script.

Automated Quality Control

This section describes the main data processing for a single dive/climb profile and the automated quality control checks currently implemented. As these checks and corrections are performed, their quality is assessed and reported in the .nc file. In this document quality assessments are referred to symbolically, e.g., 'QC_GOOD' indicates the associated data or test is trustworthy, 'QC_BAD' indicates uncorrectable data or a problem with a calculation, etc. The equivalent numeric values recorded in the .nc file are given in Appendix A.

Processing overview

Seaglider data observations are taken on a regular time interval that can be varied by vehicle depth. Typical sample rates range from 4-15 seconds (every 0.4 to 1.5 meters) near the surface and 15-60 seconds (every 1.5 to 6.0 meters) near the bottom of the dive. During each observation, different installed instruments may be sampled. The vehicle pressure sensor and compass heading and pitch are always recorded. Other instruments (including the unpumped CT) may be configured to record or not every n th vehicle observation. Historically data was recorded exclusively during these sampling intervals. However, newer instruments, including the pumped CTD, may sample data at different times and frequencies. These are described, as appropriate, below.

Overall the processing code is responsible for converting these raw measurements into common oceanographic units, validating and possibly adjusting their values for known vehicle and instrument issues, and then deriving other interesting quantities from this data. The primary computations performed involve determining accurate temperature and salinity of the water column, based on possibly corrected temperature and conductivity measures, deriving the vehicle buoyancy and flight speeds, directions and displacements, and finally inferring a depth-averaged current by comparing predicted surfacing location from the flight model with the actual surfacing positions reported by the GPS instrument. Each of these steps is described in the following sections.

Validating GPS locations and times

Proper calculation of vehicle depth, surface drift and depth-averaged currents requires three accurate GPS fixes, recorded in the log file: the position when initially surfaced (GPS1), the position just before leaving the surface on the dive (GPS2), and the position when surfaced subsequently (GPS, which is GPS1 of the next profile). GPS positions and times from the unit are assumed to be well-formed (valid dates and times) and accurate (valid locations) unless the unit timed out and was unable to acquire a fix, or the reported horizontal displacement of

precision (HDOP) is greater than 10, which suggests an error in the fix greater than 35 meters. Unlike the Argo system, GPS positions are not tested whether they are on land.

To determine surface drift, the GPS2 time must be strictly greater than the GPS1 time. To determine depth-averaged current, the final GPS time must be strictly greater than the GPS2 time. If either (or both) of these tests fail, the associated quality control variable is marked as QC_BAD and the calculation is not performed.

Correcting depth and pressure

The vehicle measures pressure in dbar at every sample but converts it on-board (using a linear factor of 0.685 m/psi) to an estimated depth, which is reported in the engineering file. The basestation inverts this calculation to recover pressure. The seawater depth routine then determines accurate vehicle depth given measured pressure and the average latitude between the GPS2 and GPS fixes (or GPS1 and GPS2 if the GPS fix is bad). If required, the glider pressure readings are linearly interpolated to the CT sampling grid before the conversion to depth.

For an unpumped CT, the vehicle pressure and corrected depth, measured vehicle pitch, and known installation geometry of the CT instrument with respect to the pressure sensor are used to compute the depth and pressure at the thermistor of CT instrument. This 'CT depth' is used in the temperature and salinity corrections discussed below. A pumped CTD reports its own pressure, which is converted to depth as above and used directly as the 'CT depth'.

Warnings are emitted (and conductivity points are marked QC_BAD) for any depths where the CT is apparently out of the water (CT depth < 0 meters). This can occur during high sea state, when the vehicle breaches during surface maneuver, if the sensor drifts over a deployment, or if the pressure sensor was not zeroed properly before deployment. In the latter case, it may be advisable to adjust the values by setting the `depth_bias` variable. No check is made whether the measured pressures are monotonically increasing on the dive or decreasing on the climb.

Computing initial vehicle velocity and glide angle

An initial estimate of vehicle velocity and glide angle is determined using the glide-slope model ('gsm'), a version of the glider's hydrodynamic flight equations discussed in Eriksen, *et al*, 2001. Speed and glide angle are determined from the measured vertical velocity (w , the rate of change of vehicle depth), compass-measured pitch and heading and an assumed in-situ seawater density (1020). The gsm estimate does not account for vehicle buoyancy forcing; see the full hydrodynamic speed calculation ('hdm') discussion below.

Generally, the vehicle compass is calibrated prior to deployment such that heading and pitch measurements are accurate to within +/-1.2 degrees. Compass inaccuracies are typically due either to the installation of an incorrect calibration file or to a change to the vehicle hard or soft iron signature after the calibration; both of these conditions can be addressed by changing the calibration file during deployment, which should be annotated using a manual directive. The compass calibrations have been tested at latitudes between 70 degrees North and 76 degrees South.

Computing temperature, conductivity and salinity

The computation of salinity from temperature and conductivity occurs first from uncorrected data and then from adjusted data. Corrections depend upon whether the CT sensor is pumped or unpumped.

Each vector of temperature, conductivity and salinity values, corrected or not, is accompanied by a separate, parallel vector of quality-control indicators. All sampled data points are initially considered QC_GOOD; unsampled points are marked QC_UNSAMPLED. As checks and computations are performed individual points are marked as QC_BAD (uncorrectable for various reasons) or, for corrected data, QC_INTERPOLATED if any interpolation occurs.

In the unpumped CT case, the measured temperature and conductivity frequencies are converted to uncorrected temperature and conductivity values using instrument-specific calibration constants. Temperature and conductivity frequency bounds, if provided by the scientist, are used to mark points exceeding these values as QC_BAD.

An uncorrected salinity (expressed in practical salinity units, PSU) is derived using the seawater routines based on the uncorrected temperature and conductivity values and the pressure at the CT. These salinity values are independent of any thermal-inertia effects.

As with Argo, the uncorrected temperature, conductivity, and salinity values are checked against global bounds. Temperature and conductivity are checked for individual spikes that suggest electrical noise in the CT sensor. Unlike Argo, there are no checks for excessive gradients.

Any value that exceeds the specified global bounds, regardless of CT depth, is marked QC_BAD.

A spike test value $(|(v_2 - (v_3 + v_1)/2| - |(v_3 - v_1)/2|) / (|(d_3 - d_1)/2|)$ is computed for a measurement value v_2 , where v_1 and v_3 are the data points before and after v_2 respectively, and d_1 and d_3 are the CT depths associated with v_1 and v_3 . The spike test value may not exceed the bounds given below, otherwise the point is marked QC_INTERPOLATED. These tests have a shallow and deep bound: If the CT depth corresponding to v_2 is deeper than the specified depth, the test value must not exceed the deep bound, otherwise (the point is shallower) the test value must not exceed the shallow bound (Schmid, *et al*, 2007 uses pressure (dbar); Carnes, 2008 uses depth).

The default allowable bounds for each test are taken from Schmid, *et al*, 2007 (and IOC Manual and Guides #22) or Carnes, 2008. These bounds are *not* adjusted to reflect regional climatology. All depth and parameter bounds may be overridden by the scientist on a per-deployment basis.

Temperature bounds:

Temperature values must fall between -2.5 and 43 °C. These bounds correspond to Carnes, 2008 and are higher than Schmid, *et al*, 2007 (40 °C).

Temperature spikes:

For temperature spike test values deeper than 500 meters, the (deep) bound is 0.01 °C/m, otherwise the (shallow) bound is 0.05 °C/m. Compare with Schmid, *et al*, 2007 of 2.0/50 (0.04) °C/m deep and 6.0/50 (0.12) °C/m shallow, assuming a nominal Argo sampling interval of 25 meters..

Conductivity spikes:

For conductivity spike test values deeper than 500 meters, the (deep) bound is 0.001 mS/m/m, otherwise the (shallow) bound is 0.006 mS/m/m. These values are roughly 10 times smaller than the temperature spike values, as expected.

Salinity bounds:

Salinity values must fall between 19 and 45 PSU. The upper bound corresponds to Carnes, 2008 and is higher than Schmid, *et al*, 2007 (41 PSU). The lower bound is higher than Carnes or Schmid. Seagliders typically cannot operate in waters fresher than 19 PSU. However, the CT might sample a fresh surface cap from river runoff or intense rain events. Salinity bound errors, not explained by temperature issues, are assumed to be conductivity issues.

If any temperature or conductivity value is marked QC_BAD, the corresponding salinity value is marked QC_BAD. Uncorrected CT data is never interpolated or changed, even if marked QC_BAD.

Adjusting temperature, conductivity, and salinity

The uncorrected CT data and their quality control indices are reported to the .nc file. Copies of temperature, conductivity, salinity and their associated quality control indicators are made and additional adjustments and corrections, described below, apply to these copies, which are then reported separately in the .nc file.

Any *adjusted* temperature, conductivity, or salinity data value marked QC_BAD is replaced with NaN. Interpolated values are marked QC_INTERPOLATED. Interpolation is linear between two or more trustworthy 'anchor' points. For temperature and conductivity the anchors are always those points immediately adjacent to each contiguous set of QC_INTERPOLATED points, if they are not 'bad'. Points are considered bad if they are marked QC_BAD, QC_PROBABLY_BAD, or QC_UNSAMPLED. For salinity, the interpolation anchors are computed as described below and may be modified by the `trust_salinity directive`. If interpolation fails (due to insufficient anchor points), values are left unchanged and they are marked QC_PROBABLY_BAD.

Adjusting temperature

The temperature is adjusted for a first-order thermistor-response lag that depends on the thermal gradient encountered by the instrument.

Correcting trapped water temperature anomalies during apogee

On dives, the Seaglider forward fairing can trap and transport water from the upper part of the water column to depth, where it can be expelled when the glider pitches up because of a stall or to begin its climb. If the surrounding water is relatively still and the glider is trimmed heavy so the vehicle continues to sink during apogee, it is possible for the trapped warmer water to waft up to the thermistor on the CT sail. This temperature anomaly appears as a strong multi-point fresh spike on a typical temperature salinity diagram with a size proportional to the overlying thermal stratification.

To account for this effect, temperature points from the start of the second pump (and pitch up) until the glider is deemed flying (0.1 m/s) are marked QC_BAD unless the measured change of pressure indicates the glider is ascending by at least 0.04 m/s vertically. Vehicles employing an interstitial compressesee, such as the Deepglider, are not affected.

Detecting conductivity anomalies

All CTDs on gliders are subject to bubbles on the surface (either because of high sea state or breaching) and biofouling at depth. These conductivity anomalies, in which the sensor is not measuring seawater, are often transient and must be accounted for when correcting salinity. Anomalies typically extend over several data points and thus escape the simple bound and spike tests outlined above.

Most conductivity anomalies appear as sharp drops in measured conductivity compared to what is expected in seawater at that temperature based on the seawater conductivity routines. This fact is exploited to detect and track the growth and clearance of anomalies, including warning of unexpected anomalies (e.g., sudden unexpected increases in conductivity, possible but weak anomalies, etc.).

Bubbles near the surface are considered uncorrectable, and marked QC_BAD, from the start of dive to the deepest bubble clearance and, on climbs, from deepest bubble start to the end of climb. Deeper conductivity anomalies, when detected, trigger directive suggestions, which the scientist may elect to employ. A heuristic policy recommends interpolation for anomalies with vertical extents is less than 50 meters, otherwise they should be considered uncorrectable.

The detector is unable to handle anomalies that straddle two or more profiles, although it may detect their start and finish in the different profiles. Further, anomalies that begin or end in strong thermoclines are difficult to detect. These situations require manual intervention.

Correcting salinity for thermal-inertia effects

The conductivity measured in all CTDs depends on the temperature of the sampled water in the tube. This in turn depends on the thermal-inertia and thermal flux in the conductivity tube itself, which depends on the construction of the instrument and speed of the water through the tube. In the unpumped case, the vehicle propulsion

provides the sensor fluid flow. The thermal-inertia effects change as the speed of the vehicle fluctuates and the sensor encounters thermoclines. See Eriksen, forthcoming, and Lueck, 1990 for detailed discussions of this effect.

Thermal-inertia effects are corrected for measurements taken by an unpumped Seabird CT41 as described in Eriksen, forthcoming. An effective water temperature inside the conductivity tube is computed based on the tube's thermal response to the changes in measured temperature outside the tube and the estimated flow through the tube, yielding a corrected salinity derived from the associated conductivity measurement. The corrections assume relatively steady flow through the conductivity tube. Measurements where the vehicle is rapidly accelerating (during flare, apogee, or surface maneuvers) are marked QC_BAD in conductivity. Measurements where the vehicle is stalled (low or no CT flow) are removed from these computations; the scientist may elect to interpolate these points against surrounding corrected points (see below).

In the unpumped CT case, determining the vehicle speed (and hence flow speed through the sensor tube) depends on knowing the buoyancy of the vehicle, which requires knowing the in-situ density, hence salinity of the seawater. An iterative scheme is employed to find a mutually-consistent solution of corrected salinity and vehicle speed, if possible. The speed and glide angle of the vehicle are determined using the full hydrodynamic equations in Eriksen, *et al*, 2001 and are based on the measured pitch and computed buoyancy of the vehicle. Vehicle buoyancy is based on the maximum volume of the vehicle, its measured mass, the state of the variable buoyancy device (VBD), thermal and pressure effects on the hull, interstitial seawater, and any compressesee, and the in-situ corrected density of the water. The final, converged, speed and glide angle results are referred to as the hydrodynamic model results or 'hdm'. As with the gsm, speeds and glide angles during stalls are set to zero but marked QC_GOOD. Speeds and glide angles are marked QC_BAD and set to NaN (unknown) where buoyancy cannot be determined because salinity is QC_BAD.

In the case of restarting flow after stalls or during steep thermoclines that are insufficiently sampled, the thermal-inertia estimates may not completely correct the salinity values. A simple temperature-correction heuristic discovers these locations, which, along with vehicle stall points for unpumped CTs, may be interpolated. Another heuristic estimates where the salinity of the surrounding water masses is stable, hence trustworthy, to anchor these salinity interpolations. If any suspect points require interpolation between a pair of stable points, all points in that segment are recommended to be interpolated, since it is often unclear where the flow and thermal-inertia effects begin and end in these locations. Both heuristics can fail; the points to interpolate and the points to trust can be adjusted manually.

Correcting pumped CTD data

The pumped Seabird GPCTD instrument reports temperature and conductivity values directly, along with an associated pressure; no frequency data is reported. The CT pressure is used directly to determine the CT depth corrected for the latitude of the vehicle.

Thermal-inertia corrections assume a constant tube flow velocity (corresponding to the normal pump speed) and ignore the vehicle speed, including stalls. Thus, unlike the unpumped CT, points during the entire dive, apogee, climb, and surface phases of the profile are retained. Conductivity anomaly detection is performed. Since the thermal-inertia correction (and possible salinity interpolation) is independent of vehicle speed, the buoyancy and hydrodynamic speed results are computed once rather than iteratively.

Derived seawater properties

In the case of a pumped CTD or an unpumped CTD running on a separate science controller, the sampling rate and timing can differ from the glider sampling rate. In these cases the CTD data sampled during glider operation is employed to determine salinity, vehicle speeds, and quantities based on that data. Relevant glider data required for the salinity and speed corrections, such as vehicle pitch, VBD state, and depth are interpolated to the CTD sample grid.

Assuming computations converge on a consistent speed and salinity, the final adjusted salinity values are evaluated again against the salinity bound and spike tests described above. The resultant QC_GOOD salinity values are accurate to 0.01 PSU, 0.03 PSU in regions of high thermocline. Adjusted temperatures are accurate to 0.001 °C. Vehicle speeds are accurate to 0.01 m/s. The CTD readings are considered overall trustworthy (CTD qc) if more than 70% of the adjusted points are QC_GOOD, otherwise the data are considered QC_BAD.

Seawater potential temperature, potential density, and sound velocity are computed from the adjusted temperatures and salinities.

At present no attempt is made to detect deployment sensor drift, density inversions, turbulent mixing, etc.

For reference, Appendix C lists the results of these calculations and, where applicable, their corresponding Argo variable counterparts.

Computing depth-average and surface-drift current

Given the accurate flight model for the vehicle in still water, the expected surfacing position can be predicted by computing the displacements of the vehicle at each data point based on the hydrodynamic speed and direction of the vehicle. Any vector deviation in actual (GPS) surfacing position from predicted implies a current encountered somewhere at depth while the vehicle was flying, stalled, or drifting (e.g., during apogee or surface maneuver). The depth-average current is assumed to apply uniformly over the entire profile. Rough latitude and longitude for each data point are computed using adjusted displacements reflecting any depth-average current. Points where the vehicle appears stuck on the bottom or the speed is unknown are removed from the current and displacement calculations.

A depth-average current and associated quantities is computed for both the gsm and the hdm velocity results unless the speed estimation was inconsistent. The depth-average current is only computed if the GPS2 and GPS fixes and times are trustworthy, if the vehicle reported data over the entire profile, and there was no apparent significant up- or down-welling. The latter is detected by finding differences between the measured vertical velocity and predicted vertical velocity larger than 0.05 m/s. The depth-average current is accurate to 0.01 m/s.

Surface-drift current is computed using the differences in position and time between valid GPS1 and GPS2 fixes.

Correcting oxygen sensor data

There are three oxygen sensors available on a Seaglider: the Seabird 43, and the Aanderaa 3830 and 4330 optodes. Direct measurements from all instruments are reported. All sampled data points are assumed to be QC_GOOD; unsampled points are marked as QC_UNSAMPLED. Negative raw data values are marked as QC_BAD. Corrections and conversions, always to micromoles/kg, are performed for all instruments following both manufacturer's recommended procedure (and current Argo processing adjustments [Swift, personal communication]) using associated calibration constants with the following differences.

The Seabird 43 reports a frequency measurement that is converted to a dissolved oxygen value using supplied instrument calibration constants, the CT pressure, and an estimate of the expected oxygen saturation based on the corrected CT temperature and salinity. Following Nicholson 2009, oxygen is then corrected for speed-related boundary-layer effects in the measurement tube.

The Aanderaa 3380 and 4330 O₂ and dphase measurements are converted to a dissolved oxygen value using instrument calibration constants, CT depth, and the corrected CT temperature (to eliminate possible instrument self-heating), salinity, and potential density.

The calculation of oxygen saturation for fresh water and seawater salinity correction used in these corrections follow Garcia and Gordon 1992 except the corrections employ the 'Benson and Krause 1984' coefficients in Table 1 rather than the 'Combined fit' values, per their recommendation.

Correcting WETLabs sensor data

All direct measurements from the instrument are reported; NaN indicates unsampled points. No corrections or quality-control tests are applied to the data.

Manual Quality Control

To handle situations where automated checks and corrections are insufficient or incorrect, the scientist may provide directives in a simple language to direct whether and where various corrections should be applied or overridden. Profile-specific directives and comments are placed in an optional `sg_directives.txt` file associated with each deployment, which is interpreted for each profile. Comments follow MATLAB convention: Blank lines and characters after '%' are ignored. Applicable directives with their associated comments are preserved in the .nc file for future reference and use.

Directives have the following format:

profile_spec function [location]

where *profile_spec* is a profile number, e.g., '149', a range of profile numbers, e.g., '84:90', or '*' for all profiles in the deployment.

The *functions* currently available are:

<code>skip_profile</code>	Do no processing for this profile. (False)
<code>reviewed</code>	Mark the .nc file as reviewed; comments should indicate reviewer and date. (False)
<code>interp_gc_temperatures</code>	Interpolate temperatures during GC maneuvers. A consistent temperature increase during guidance-and-control (GC) maneuvers has been observed on one vehicle. Declaring this directive will interpolate temperature readings during GC with points just before and after each GC, unless the glider was in a sharp thermocline. (False)
<code>correct_thermal_inertia_effects</code>	Apply the thermal-inertia corrections. (True)
<code>interp_suspect_thermal_inertia_salinities</code>	Interpolate points where thermal-inertia corrections are suspect. (False)

The functions above set booleans and direct processing; the default values of the booleans are enclosed in (). The prefix 'no_' may be added to the function to set the associated boolean to False, e.g., 'no_correct_thermal_inertia_effects' defeats the thermal-inertia corrections.

The following functions apply to the *adjusted*, not uncorrected, temperature, conductivity and salinity values. These directives change (add or remove) the marks in the quality-control variables; these marks then direct modification of the data. As mentioned above, any adjusted data value marked QC_BAD is replaced with NaN; any value marked QC_INTERPOLATED will be interpolated.

<code>bad_temperature</code>	Mark as QC_BAD
<code>interp_temperature</code>	Mark as QC_INTERPOLATED
<code>bad_conductivity</code>	Mark as QC_BAD
<code>interp_conductivity</code>	Mark as QC_INTERPOLATED
<code>bad_salinity</code>	Mark as QC_BAD
<code>interp_salinity</code>	Mark as QC_INTERPOLATED

As with the boolean functions, for the `bad_` and `interp_` functions the prefix 'no_' may be added to the function, e.g., `no_bad_temperature` or `no_interp_salinity`. Those points will be removed from the points

automatically determined to be bad or interpolated respectively. This allows the scientist to override which points are marked uncorrectable or interpolated.

These functions may be followed by an option, which can be a named list (e.g., **depth**, **time** (see below)) or, more typically, a user-specified list of points in terms of actual data point number. Locations typically restrict the set of values desired. For example:

```
* bad_salinity depth below 10 % all salinities strictly less than 10
meters are considered QC_BAD

346 interp_salinity data_points at 120 121 122 % ensure these points
are interpolated on dive 346 only

346 interp_salinity data_points between 120 122 % equivalent to the
above
```

The modifier 'at' lists specific values that must match exactly. The modifiers 'below' and 'above' test that values are strictly less than or strictly greater than the given value, respectively. The synonyms 'less_than', 'before', 'greater_than' and 'after' are also recognized. The modifier 'between' is inclusive of the range. The modifier 'in_between' includes all points the range except the end points. If no location is specified, the function applies to all the available data points. At present boolean combinations of locations on a single directive are not supported.

If there are several directives for a function (or its negation) they are combined, first by forming a union of all the included points and then removing the union of any negated points. Thus negation trumps inclusion, which is often what is desired. The order of the directives does not matter.

Several lists of data point indices and values are computed and made available for directives. They are:

depth	Vehicle depth, in meters, over the entire profile
dive_depth	Vehicle depth, in meters, before start of apogee
climb_depth	Vehicle depths, in meters, after end of apogee
time	The elapsed time, in seconds, of each glider data point
data_points	The index, starting at 1, of each CTD data point
glider_data_points	The index, starting at 1, of each vehicle data point

Application of directives

The **skip_profile** directive is honored after all the data is read but before any processing occurs. The **reviewed** directive is honored after all corrections are made.

The **bad_temperature**, **interp_temperature**, **bad_conductivity**, and **interp_conductivity** directives are honored once, just before the salinity corrections and hdm speed computations are performed. The **bad_salinity** directive is also honored once just before the (possibly iterative) speed computations are performed, to eliminate these points from participating in the buoyancy computations. Any **interp_salinity** directives are honored after each thermal-inertia correction is made and before the buoyancy and hdm speed computation is performed; for the iterative, unpumped CT case, these directives may be applied several times.

There are cases where thermal inertia corrections do not permit the speeds and salinities to converge to an acceptable solution (often the vehicle is on the verge of stalling in many places). Rather than completely abandoning the profile (by employing **skip_profile**), the scientist might try **no_correct_thermal_inertia_effects**. This will compute salinities and speeds but will not iterate. If the results are still unacceptable for whatever reason, employ **skip_profile**.

Appendices

A. Quality control values

These are the available quality control names and their numeric equivalents. They are taken from Argo, 2010 with the addition of QC_UNSAMPLED. Not all values are currently used.

QC_NO_CHANGE	0 - No QC was performed
QC_GOOD	1 - Value is ok
QC_PROBABLY_GOOD	2 - Value is likely good
QC_PROBABLY_BAD	3 - Potentially correctable
QC_BAD	4 - Untrustworthy and uncorrectable
QC_CHANGED	5 - Explicit manual change
QC_UNSAMPLED	6 - Explicitly not sampled (vs. expected but QC_MISSING)
QC_INTERPOLATED	8 - Interpolated value
QC_MISSING	9 - Value missing; instrument timed out

B. Selected parameters controlling processing

The following is a partial list of the variables and parameters that the scientist can set in the `sg_calib_constants.m` file to control the corrections and the quality-control processing. Instrument-specific calibration constants are not listed. All values should be scalars, either real numbers, integers, or strings. MATLAB conventions apply: comments follow '%', and ';' should terminate lines to silence output from MATLAB. Setting a variable applies that value to all the profiles in a deployment.

Vehicle parameters: All but `sg_configuration` are required.

The general configuration of the glider

<code>sg_configuration</code>	<ol style="list-style-type: none"> 1. Seaglider with original SBE41 CT 2. Seaglider with gun-style SBE41 CT 3. Deepglider with gun-style SB41 CT 4. Seaglider with pumped GPCTD
<code>hd_a</code>	Hydrodynamic lift factor for given hull shape [$1/^\circ$ of attack angle]
<code>hd_b</code>	Hydrodynamic drag factor for given hull shape [$\text{Pa}^{-1/4}$]
<code>hd_c</code>	Hydrodynamic induced drag factor for given hull shape [$1/\text{radians}^2$ of attack angle]
<code>rho0</code>	Typical expected density of seawater for this deployment [kg/m^3]
<code>volmax</code>	Maximum displaced volume of the glider [m^3]
<code>mass</code>	Mass of the glider [kg]

Instrument biases: All are optional; default values are 0.

<code>pitchbias</code>	Pitch sensor bias [$^\circ$]
<code>depth_bias</code>	Depth bias of pressure sensor [m]
<code>vbdbias</code>	VBD bias [cc]

General CTD parameters: All are optional. Default bias values are 0.

<code>sbe_temp_freq_min</code>	SBE41 minimum permitted temperature frequency [Hz]
<code>sbe_temp_freq_max</code>	SBE41 maximum permitted temperature frequency [Hz]
<code>sbe_temp_freq_offset</code>	Temperature frequency offset [Hz]
<code>temp_bias</code>	Temperature bias [$^\circ\text{C}$]
<code>sbe_cond_freq_min</code>	SBE41 minimum permitted conductivity frequency [Hz]
<code>sbe_cond_freq_max</code>	SBE41 maximum permitted conductivity frequency [Hz]
<code>sbe_cond_freq_offset</code>	Conductivity frequency offset [Hz]
<code>cond_bias</code>	Conductivity bias [mS/cm]

Quality control test parameters: See above for default values.

<code>QC_temp_min</code>	Minimum allowable temperature [°C]
<code>QC_temp_max</code>	Maximum allowable temperature [°C]
<code>QC_temp_spike_depth</code>	Depth for deep temperature spike test [m]
<code>QC_temp_spike_shallow</code>	Allowable temperature spike in shallow deep water [°C/m]
<code>QC_temp_spike_deep</code>	Allowable temperature spike in deep water [°C/m]
<code>QC_cond_spike_depth</code>	Depth for deep conductivity spike test [m]
<code>QC_cond_spike_shallow</code>	Allowable conductivity spike in shallow deep water [mS/cm/m]
<code>QC_cond_spike_deep</code>	Allowable conductivity spike in deep water [mS/cm/m]
<code>QC_salin_min</code>	Minimum salinity value [PSU]
<code>QC_salin_max</code>	Maximum salinity value [PSU]
<code>QC_salin_spike_depth</code>	Depth for deep salinity spike test [m]
<code>QC_salin_spike_shallow</code>	Allowable salinity spike in shallow deep water [PSU/m]
<code>QC_salin_spike_deep</code>	Allowable salinity spike in deep water [PSU/m]
<code>QC_overall_ctd_percentage</code>	Maximum fraction of CTD data that can be QC_BAD

C. Main output variables in an .nc file

Within the .nc file the original data variables and vectors are tagged with a prefix that indicates their origin:

<code>sg_cal_</code>	Variables from <code>sg_calib_constants.m</code>
<code>log_</code>	Parameters from the log file
<code>log_gps_</code>	Selected values from the \$GPS lines in the log file
<code>gc_</code>	Selected values from the \$GC lines in the log file
<code>eng_</code>	Original data vectors from the engineering (eng) file

String constants are written as string arrays with dimensions appropriate to their length; these dimensions are named '`string_n`', where *n* is the length of the string. Other dimensions are as follows:

sg_data_point	Number of vehicle data points
gc_event	Number of \$GC events in the log
gps_info	Number of GPS readings (3)

Result variables are listed below. Units, if any, are enclosed in []. Quality control variables use the **_qc** suffix; values are listed in Appendix A. For reference, Argo-equivalent variable names, if appropriate, are enclosed in {}.

Information about the processing of the profile:

processing_history	Collected processing output
reviewed	Whether a scientist has reviewed and approved this profile
directives	The control directives supplied by the scientist for this profile

Information about the location of the profile Argo reports the date and time (**JULD**), and position (**LATITUDE** and **LONGITUDE**) of float surfacing. Equivalent times and locations for Seaglider missions may be found in the **log_gps_time**, **log_gps_lat** and **log_gps_lon** arrays; Seaglider surfacing is recorded under index 3. Seaglider output variables **time**, **latitude** and **longitude** are estimated times and positions of *each* vehicle sample during a profile. :

magnetic_variation	The magnetic variance from true north [°]
avg_latitude	The average latitude of the dive [° North]
GPS1_qc	Whether to trust the GPS1 information
GPS2_qc	Whether to trust the GPS2 information
GPSE_qc	Whether to trust the final GPS information

General information about the vehicle and event times:

time	Time in GMT epoch format [seconds from 00:00Z 1 January 1970]
depth	Depth below the surface, corrected for average latitude [m] { DEPTH }
start_of_climb_time	Seconds after dive start when the second apogee pump starts [s]

Results based on CTD measurements:

<code>ctd_time</code>	CTD sample time in GMT epoch format [seconds from 00:00Z 1 January 1970]
<code>ctd_depth</code>	CTD thermistor depth corrected for average latitude [m]
<code>CTD_qc</code>	Whether to trust the corrected CTD values
<code>temperature</code>	Temperature corrected for thermistor first-order lag [°C] { <code>TEMP_ADJUSTED</code> }
<code>temperature_qc</code>	Whether to trust each <code>temperature</code> value { <code>TEMP_ADJUSTED_QC</code> }
<code>conductivity</code>	Conductivity corrected for anomalies [mS/cm] { <code>CNDC_ADJUSTED</code> }
<code>conductivity_qc</code>	Whether to trust each <code>conductivity</code> value { <code>CNDC_ADJUSTED_QC</code> }
<code>salinity</code>	Salinity corrected for thermal-inertia effects [PSU] { <code>PSAL_ADJUSTED</code> }
<code>salinity_qc</code>	Whether to trust each <code>salinity</code> value { <code>PSAL_ADJUSTED_QC</code> }
<code>buoyancy</code>	Buoyancy of vehicle, corrected for compression effects [g]
<code>density</code>	Potential density based <code>temperature</code> and <code>salinity</code> at 0 pressure [g/m ³]
<code>sigma_t</code>	Sigma based on <code>density</code> [g/m ³]
<code>theta</code>	Potential temperature based on measured pressure, <code>temperature</code> , and <code>salinity</code> [°C]
<code>sigma_theta</code>	Potential density based on <code>theta</code> at 0 pressure [g/m ³]
<code>sound_velocity</code>	Sound velocity based on <code>temperature</code> and <code>salinity</code> [m/s]
<code>temperature_raw</code>	Uncorrected temperature (in situ) [°C] { <code>TEMP</code> }
<code>temperature_raw_qc</code>	Whether to trust each raw temperature value { <code>TEMP_QC</code> }
<code>conductivity_raw</code>	Uncorrected conductivity [mS/cm] { <code>CNDC</code> }
<code>conductivity_raw_qc</code>	Whether to trust each raw conductivity value { <code>CNDC_QC</code> }
<code>salinity_raw</code>	Uncorrected salinity derived from <code>temperature_raw</code> and <code>conductivity_raw</code> [PSU] { <code>PSAL</code> }
<code>salinity_raw_qc</code>	Whether to trust each raw salinity value { <code>PSAL_QC</code> }

Vehicle velocities and displacements:

hdm_qc	Whether corrected temperatures, salinities, and hdm velocities converged
speed	Vehicle speed based on hdm [cm/s]
speed_qc	Whether to trust each vehicle speed based on hdm
glide_angle	Glide angle based on hdm [°]
horz_speed	Vehicle horizontal speed based on hdm [cm/s]
vert_speed	Vehicle vertical speed based on hdm [cm/s]
flight_avg_speed_east	Eastward component of flight average speed based on hdm [m/s]
flight_avg_speed_north	Northward component of flight average speed based on hdm [m/s]
north_displacement	Northward displacement from hdm [m]
east_displacement	Eastward displacement from hdm [m]
speed_gsm	Vehicle speed based on gsm [cm/s]
glide_angle_gsm	Glide angle based on gsm [°]
horz_speed_gsm	Vehicle horizontal speed based on gsm [cm/s]
vert_speed_gsm	Vehicle vertical speed based on gsm [cm/s]
flight_avg_speed_east_gsm	Eastward component of flight average speed based on gsm [m/s]
flight_avg_speed_north_gsm	Northward component of flight average speed based on gsm [m/s]
north_displacement_gsm	Northward displacement from gsm [m]
east_displacement_gsm	Eastward displacement from gsm [m]

Positions based on displacements and computed depth-average current (DAC):

depth_avg_curr_qc	Whether to trust the DAC values and displacements
depth_avg_curr_east	Eastward component of DAC based on hdm [m/s]
depth_avg_curr_north	Northward component of DAC based on hdm [m/s]
latitude	Latitude based on hdm DAC [° North]
longitude	Longitude based on hdm DAC [° East]

<code>depth_avg_curr_east_gsm</code>	Eastward component of DAC based on gsm [m/s]
<code>depth_avg_curr_north_gsm</code>	Northward component of DAC based on gsm [m/s]
<code>latitude_gsm</code>	Latitude based on gsm DAC [° North]
<code>longitude_gsm</code>	Longitude based on gsm DAC [° East]

Computed surface current:

<code>surface_curr_qc</code>	Whether to trust the surface current values
<code>surface_curr_east</code>	Eastward component of surface current [cm/s]
<code>surface_curr_north</code>	Northward component of surface current [cm/s]

Dissolved oxygen from various instruments, if present:

<code>dissolved_oxygen_sat</code>	Dissolved oxygen saturation in based on salinity and temperature [micromoles/kg]
<code>SBE43_qc</code>	Whether to trust the SBE43 results
<code>sbe43_dissolved_oxygen</code>	Oxygen concentration corrected for salinity [micromoles/kg] {DOXY}
<code>sbe43_dissolved_oxygen_qc</code>	Whether to trust each SBE43 dissolved oxygen value
<code>aanderaa3830_qc</code>	Whether to trust the Aanderaa 3830 results
<code>aanderaa3830_dissolved_oxygen</code>	Oxygen concentration calculated from optode dphase corrected for salinity [micromoles/kg] {DOXY_ADJUSTED}
<code>aanderaa3830_dissolved_oxygen_qc</code>	Whether to trust each optode dissolved oxygen value
<code>aanderaa3830_instrument_dissolved_oxygen</code>	Oxygen concentration reported from optode corrected for salinity [micromoles/kg] {DOXY_ADJUSTED}
<code>aanderaa4330_qc</code>	Whether to trust the Aanderaa 4330 results
<code>aanderaa4330_dissolved_oxygen</code>	Oxygen concentration calculated from optode tcphase for salinity and depth [micromoles/kg] {DOXY_ADJUSTED}
<code>aanderaa4330_dissolved_oxygen_qc</code>	Whether to trust each optode dissolved oxygen value

aanderaa4330_instrument_dissolved_oxygen

Oxygen concentration reported from optode corrected
for salinity [micromoles/kg] {DOXY_ADJUSTED}

D. References

"Argo quality control manual, version 2.6", November, 2010.

Carnes, M. R., 2008: "LAGER Manual, version 1.0", Naval Research Laboratory.

Eriksen, C. C., Osse, T. J., Light, R. D., Wen, T., Lehman, T. W., Sabin, P.L., Ballard, J.W., and Chiodi, A. M., 2001: "Seaglider: A long-range autonomous underwater vehicle for oceanographic research", IEEE Journal of Oceanic Engineering, 26(4), 424-436.

Eriksen, C. C., forthcoming: "Thermal inertia in unpumped conductivity cells".

Garcia and Gordon, 1992: "Oxygen solubility in seawater: Better fitting equations", Limnol. Oceanog. 37(6), 1992, 1307-1312.

IOC Manual and Guides #22.

Nicholson, Richard: "Nitrogen, oxygen and the noble gases as tracers of upper-ocean productivity and air-sea gas fluxes", Appendix A, Ph.D. dissertation, University of Washington, 2009

Lueck, R. G., 1990: "Thermal inertia of conductivity cells", Theory J. Atmos. Ocean. Tech., 7, 741-755.

Schmid, C., Molinari, R. L., Sabina, R., Daneshzadeh, Y., Xia, X., Forteza, E., and Yang, H., 2007: "The real-time data management system for Argo profiling float operations", J. Atmos. Ocean. Tech., 24, 1608-1628.

UNESCO, 1981: "Tenth report of the joint panel on oceanographic tables and standards", UNESCO Technical Papers in Marine Science, 36.

Fofonoff, N.P. and Millard, R.C. Jr., 1983: "Algorithms for computation of fundamental properties of seawater", UNESCO Technical Papers in Marine Science, 44.