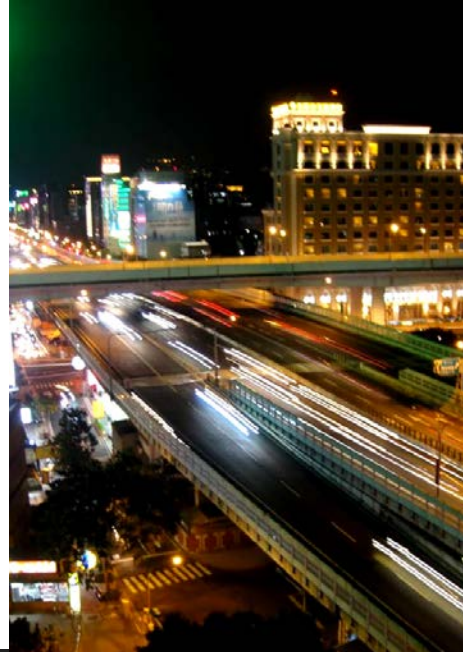




國立臺北科技大學



# 電路學 Circuit Theory

## Lecture 2

# **Advanced Techniques for Circuit Analysis**

Week 4, Fall 2019

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*Electronic Engineering, Taipei Tech*



# Contents

## Lecture 2:

### Advanced Techniques for Circuit Analysis

- 2.1 Nodal Analysis (Node-Voltage Method)
- 2.2 Mesh Analysis (Mesh-Current Method)
- 2.3 Superposition Theorem
- 2.4 Source Transformation
- 2.5 Thévenin and Norton Equivalents
- 2.6 Maximum Power Transfer Theorem







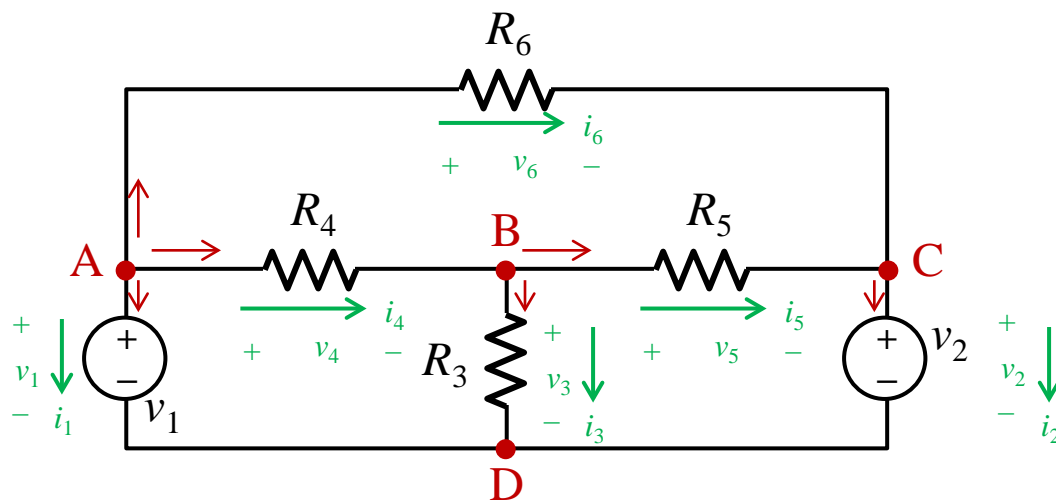
# Contents



## **2.1 Nodal Analysis (Node-Voltage Method)**



# Too Many Variables in 2B Method! (1/2)



2B method: a direct algebraic approach

 KCL:

- Node A:  $i_1 + i_4 + i_6 = 0$
- Node B:  $-i_4 + i_3 + i_5 = 0$
- Node C:  $i_2 - i_5 - i_6 = 0$
- Node D:  $-i_3 - i_2 - i_1 = 0$

3 KCL equations

 KVL:

- Loop ABDA:  $v_4 + v_3 - v_1 = 0$
- Loop BCDB:  $v_5 + v_2 - v_3 = 0$
- Loop ACBA:  $v_6 - v_5 - v_4 = 0$

3 KVL equations

 Component models:

- $v_1 = \text{Given } v_1$
- $v_2 = \text{Given } v_2$
- $v_3 = R_3 i_3$
- $v_4 = R_4 i_4$
- $v_5 = R_5 i_5$
- $v_6 = R_6 i_6$



# Too Many Variables in 2B Method! (2/2)

Objective of 2B method: find  $v_k$  and  $i_k$ ,  $k = 1, 2, 3, \dots, B$

- ❏ The number of unknown:  $2B$
- ❏ The number of KCL equations:  $N - 1$
- ❏ The number of KVL equations:  $B - (N - 1)$
- ❏ The number of component model:  $B$
- ❏ So there are  $2B$  equations for solving  $2B$  unknowns!

But it has serious problems:

- ❏ Too many variables
- ❏ Not efficient at all



We need better methods to reduce the complexity!



# Two IMPORTANT Methods in Midterm

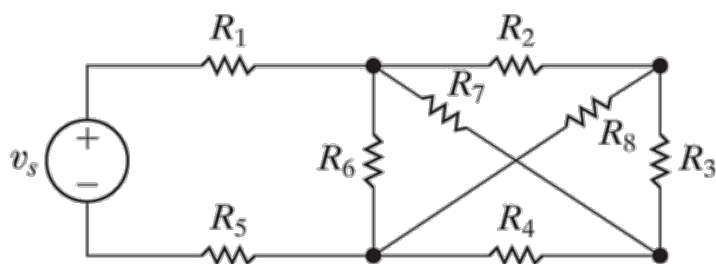
## Nodal analysis

- Based on KCL
- Suitable for general cases

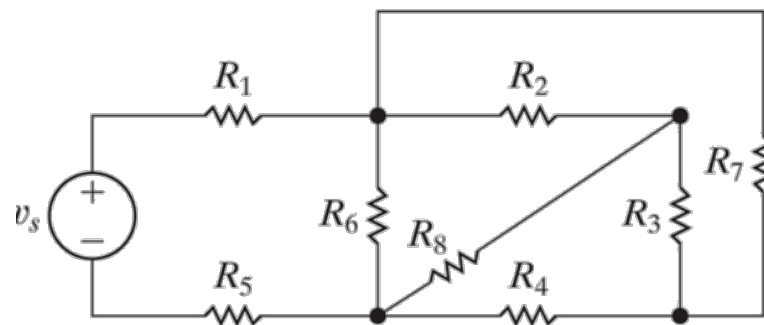
## Mesh analysis

- Based on KVL
- Only suitable for planar circuits

## Terminology: planar circuit



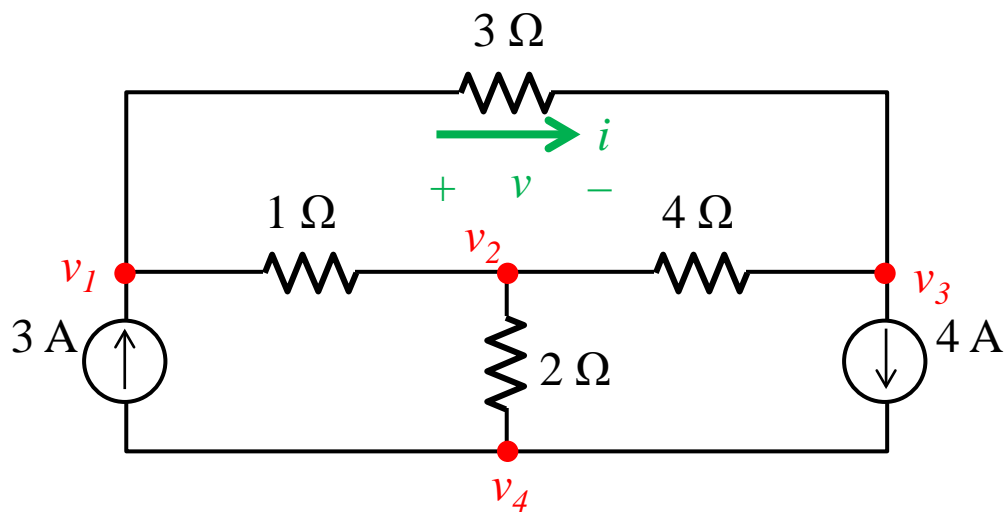
- Before putting it in order



- After rearrangement
- Definition: a circuit that can be drawn on a plane with no crossing branches



# The Idea of Nodal Analysis



Previous method: use **branch** currents as the variable

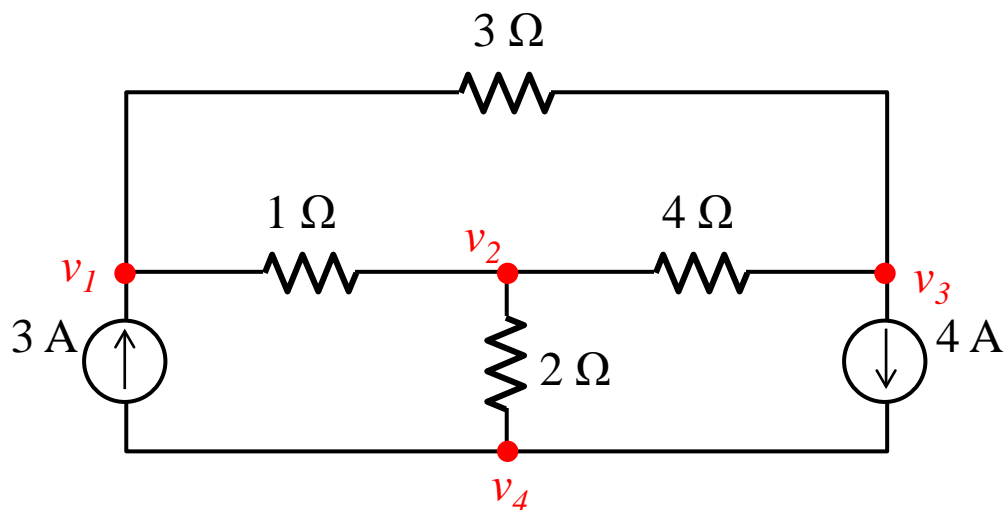
- But the number of branch is much larger than the number of node

New method: use **node** voltages as the variable

- Each branch voltage can be obtained from nodal voltages
- The corresponding branch current can be calculated by its component model
- 12 branch variables  $\rightarrow$  3 node variables



# Characteristics of Node-Voltage Method:



1. KVL is automatically satisfied in every loop (why?)
2. We only need to find the independent KCL equations
3. The component model is applied so that the branch current can be expressed

$$Gv = I$$





# Five Cases in the Following Analysis

## Only containing current sources

1. With independent current sources: basic case
2. With dependent current sources: expressing the controlling parameters in terms of nodal voltages

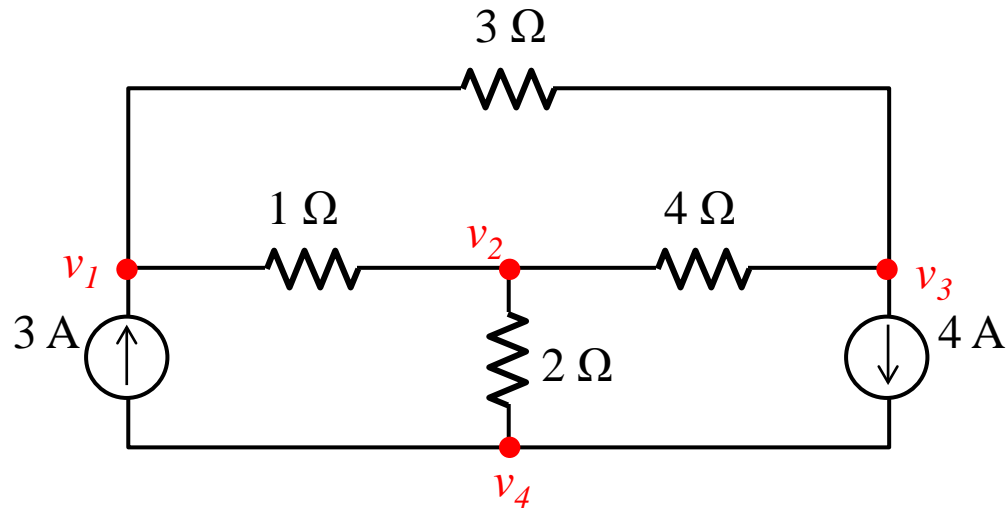
## Containing voltage sources

3. Voltage sources connect to the reference node: the easiest case
4. Voltage sources do not contain the reference node: by supernode concept
5. With dependent voltage sources: expressing the controlling parameters in terms of the nodal voltages

## Ex. 2.1

# With Independent Current Source

### CASE 1



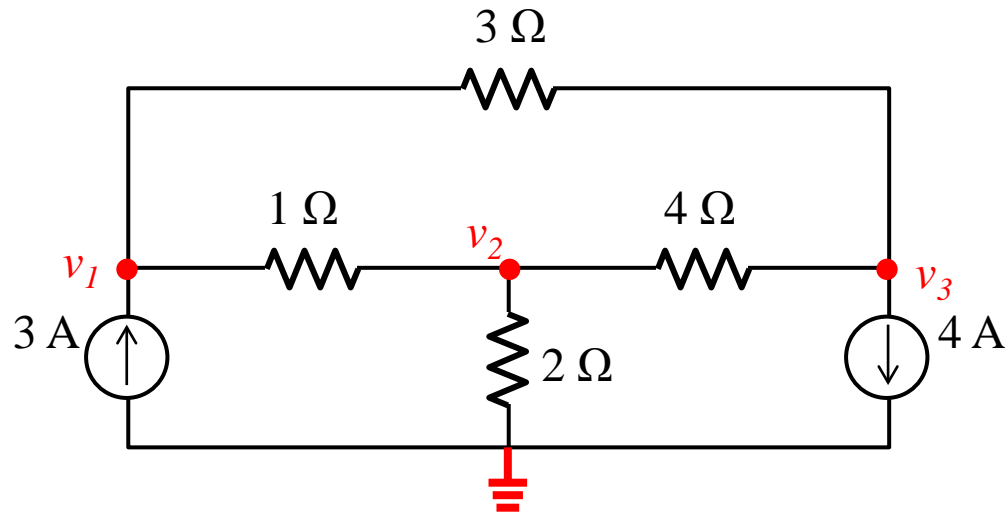
### Step 1

- Find 4 nodes
- Select a node as reference node. Which one?
- Set  $v_1$ ,  $v_2$ , and  $v_3$  as unknowns

## Ex. 2.1

# With Independent Current Source

### CASE 1



### Step 2

- Apply KCL to  $n - 1$  nodes and use the component model (Ohm's law) to express the branch currents in terms of nodal voltages

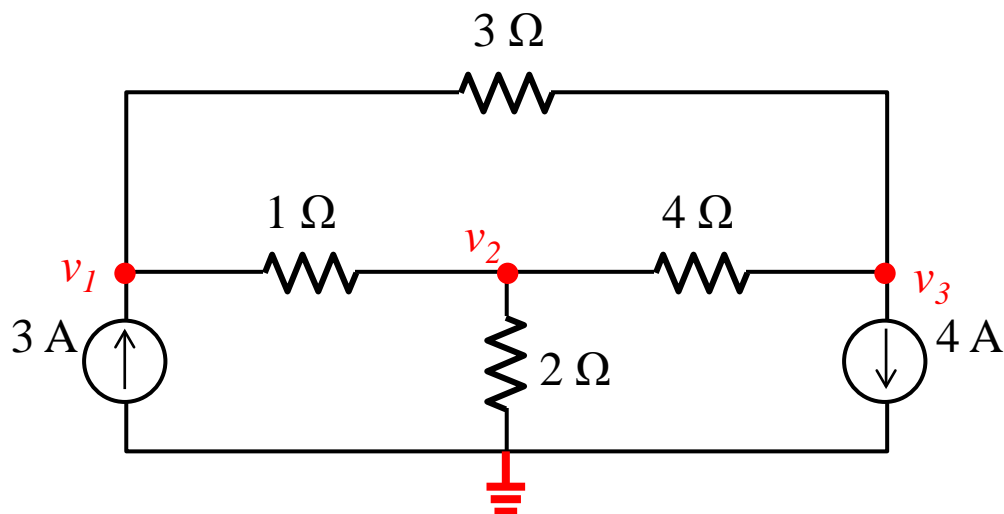
$$\sum_{\text{leaving}} i_k = 0 \quad \Rightarrow$$

$\forall \text{ node}$

## Ex. 2.1

# With Independent Current Source

### CASE 1



Step 3 (not necessary)

- Matrix expression

$$\begin{bmatrix} 1 + \frac{1}{3} & -1 & -\frac{1}{3} \\ -1 & 1 + \frac{1}{2} + \frac{1}{4} & -\frac{1}{4} \\ -\frac{1}{3} & -\frac{1}{4} & \frac{1}{3} + \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix} = \begin{bmatrix} 3A \\ 0 \\ -4A \end{bmatrix}$$

$$Gv = I$$

$G$

Conductance matrix

$G_{kk}$

Sum of the conductances connected to node  $k$

$G_{kj}$

Negative of the sum of conductances directly connecting nodes  $k$  and  $j$  ( $k \neq j$ )

$v_k$

Unknown; nodal voltage of the  $k^{\text{th}}$  node

$I_k$

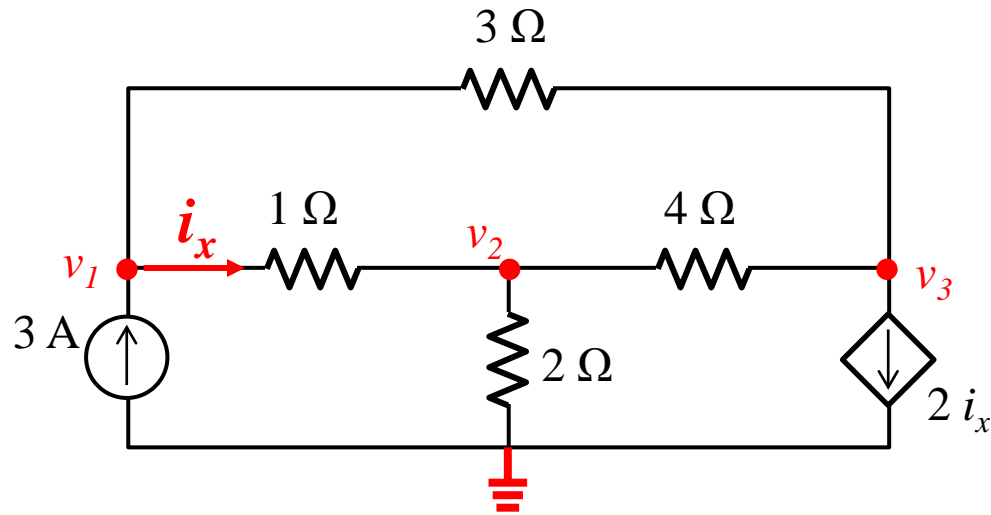
Sum of independent current sources **entering** to node  $k$



## Ex. 2.2

# With Dependent Current Source

### CASE 2



#### Step 1

- Set  $v_1$ ,  $v_2$ , and  $v_3$  as unknowns; set a reference node
- How to express  $i_x$ ?

→ Watch out the current direction!

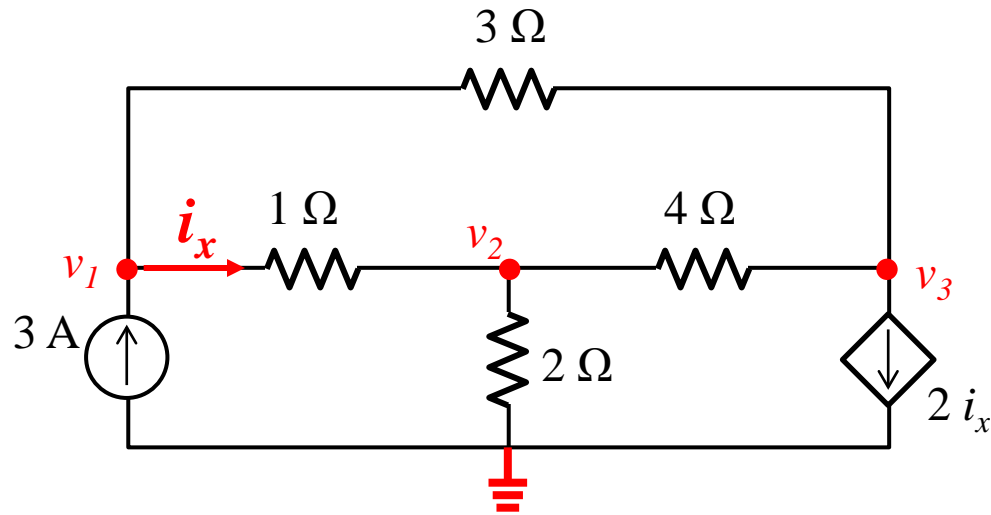
#### Step 2

- Apply KCL to  $n - 1$  nodes

## Ex. 2.2

# With Dependent Current Source

### CASE 2

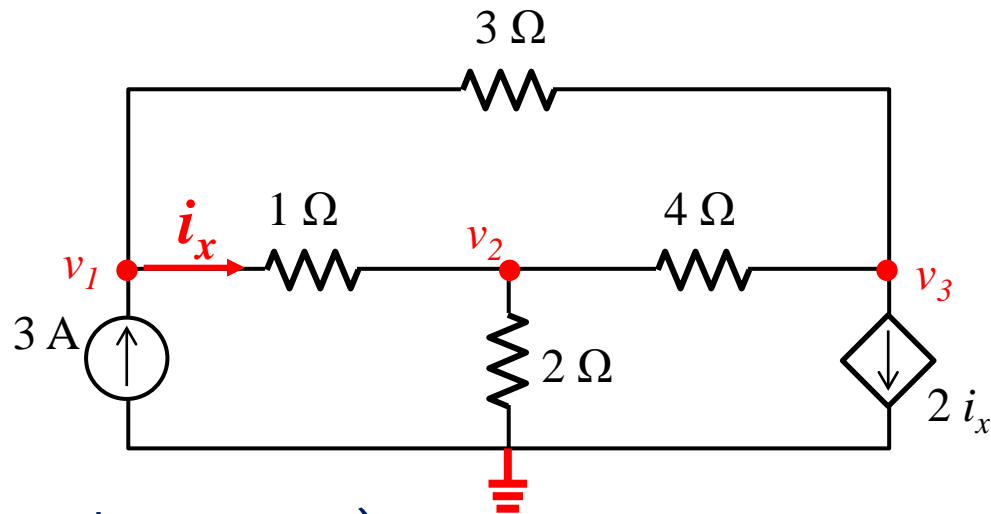


- Rearrange the equations and solve them!

## Ex. 2.2

# With Dependent Current Source

### CASE 2



Step 3 (again, not necessary)

- Step 3: Matrix expression

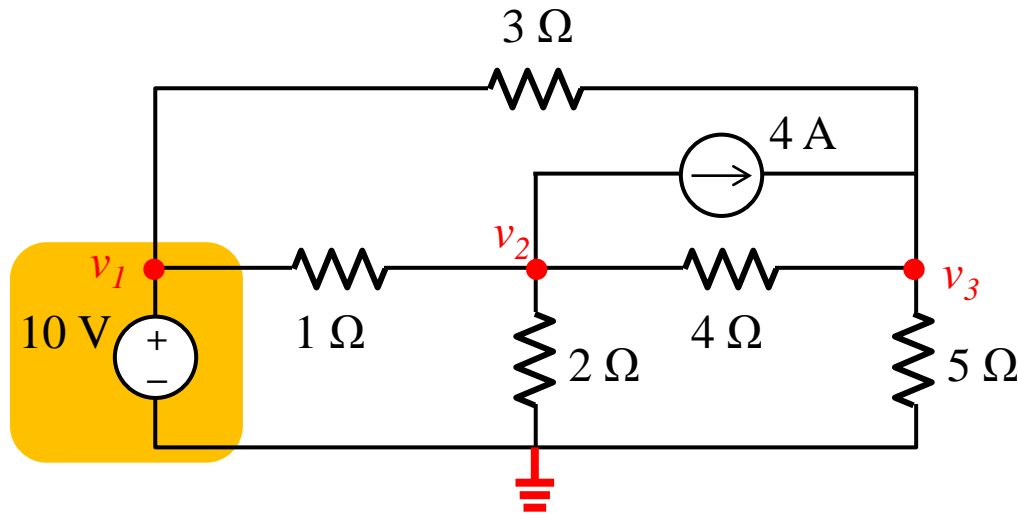
$$\begin{bmatrix} 1 + \frac{1}{3} & -1 & -\frac{1}{3} \\ -1 & 1 + \frac{1}{2} + \frac{1}{4} & -\frac{1}{4} \\ -\frac{1}{3} + 2 & -\frac{1}{4} - 2 & \frac{1}{3} + \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix} = \begin{bmatrix} 3A \\ 0 \\ 0 \end{bmatrix}$$

- No longer a symmetric matrix
- Off diagonal terms are not always negative

## Ex. 2.3

## With Voltage Source Connected to the Reference Node

### CASE 3



#### Step 1

- Set  $v_1$ ,  $v_2$ , and  $v_3$  as unknowns; set a reference node
- How to express  $v_1$ ?

#### Step 2

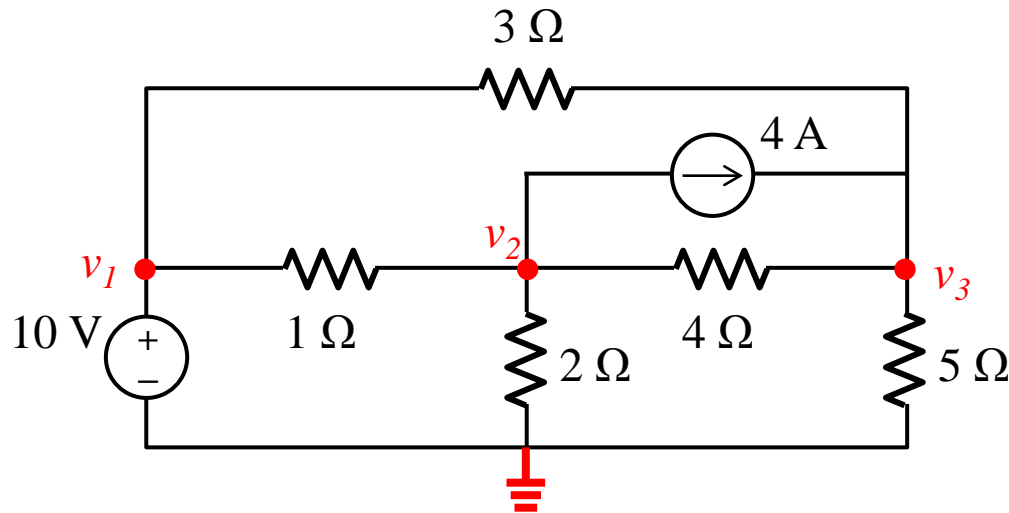
- Apply KCL to the 2<sup>nd</sup> and 3<sup>rd</sup> nodes



## Ex. 2.3

## With Voltage Source Connected to the Reference Node

### CASE 3



### Step 3 (not necessary)

- Matrix expression

$$\begin{bmatrix} 1 + \frac{1}{2} + \frac{1}{4} & -\frac{1}{4} \\ -\frac{1}{4} & \frac{1}{3} + \frac{1}{4} + \frac{1}{5} \end{bmatrix} \begin{bmatrix} v_2 \\ v_3 \end{bmatrix} = \begin{bmatrix} 10 - 4 \\ \frac{10}{3} + 4 \end{bmatrix}$$

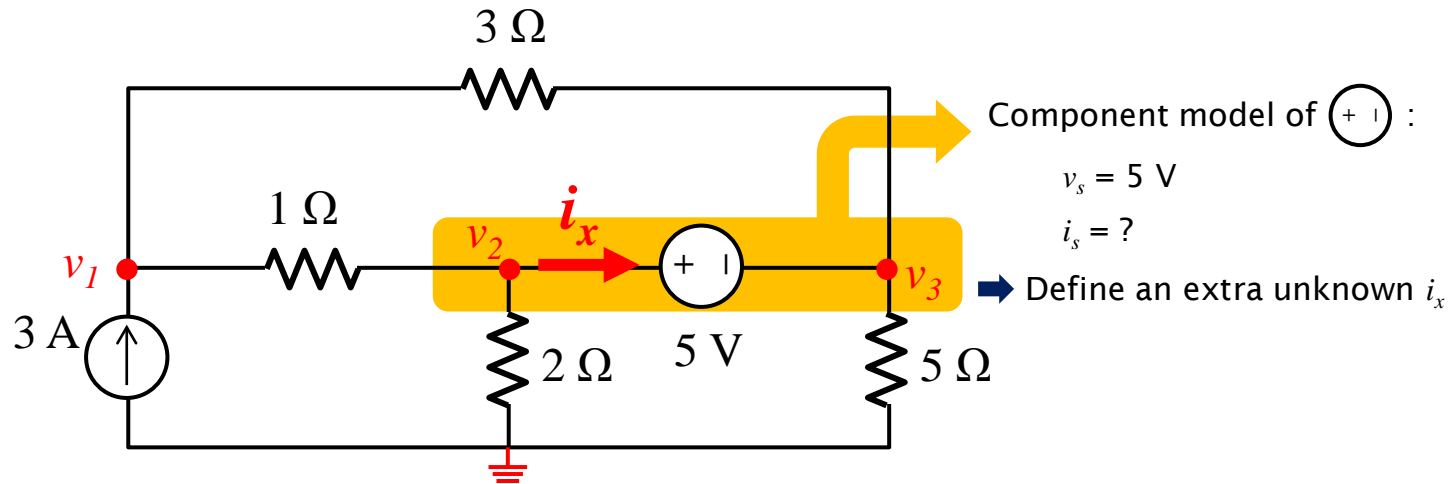
$$v_1 = 10 \text{ V}$$

- Only two unknowns!

## Ex. 2.4

## With Voltage Source **NOT** Connected to the Reference Node

### CASE 4



### Step 1

- Set  $v_1$ ,  $v_2$ , and  $v_3$  as unknowns; set a reference node
- What's the relation between  $v_2$  and  $v_3$ ?

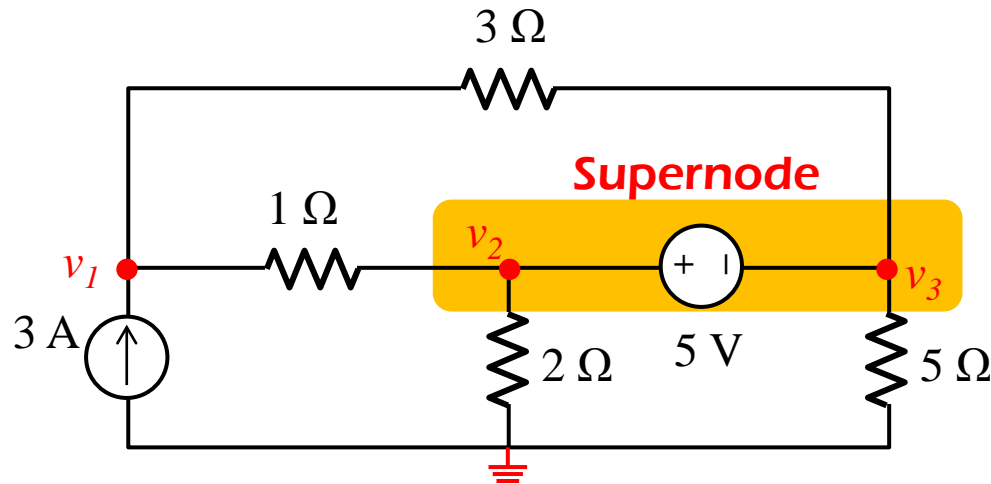
### Step 2

- Apply KCL to  $n - 1$  nodes

## Ex. 2.4

## With Voltage Source **NOT** Connected to the Reference Node

### CASE 4



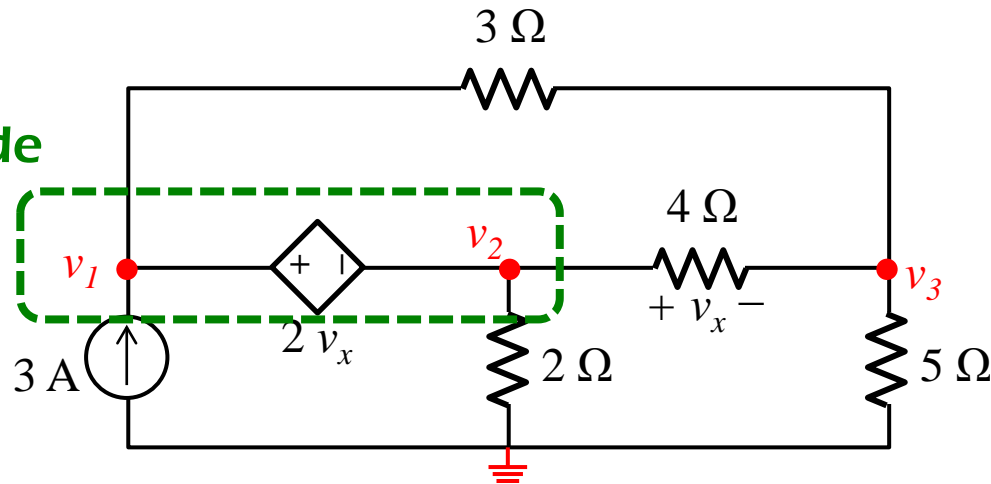
- And we already know that  $v_2 - v_3 = 5\text{ V}$ :

## Ex. 2.5

# With Dependent Voltage Source

### CASE 5

Supernode



### Step 1

- Set  $v_1$ ,  $v_2$ , and  $v_3$  as unknowns; set a reference node
- What's the relation between  $v_1$  and  $v_3$ ?
- How to express  $v_x$ ?

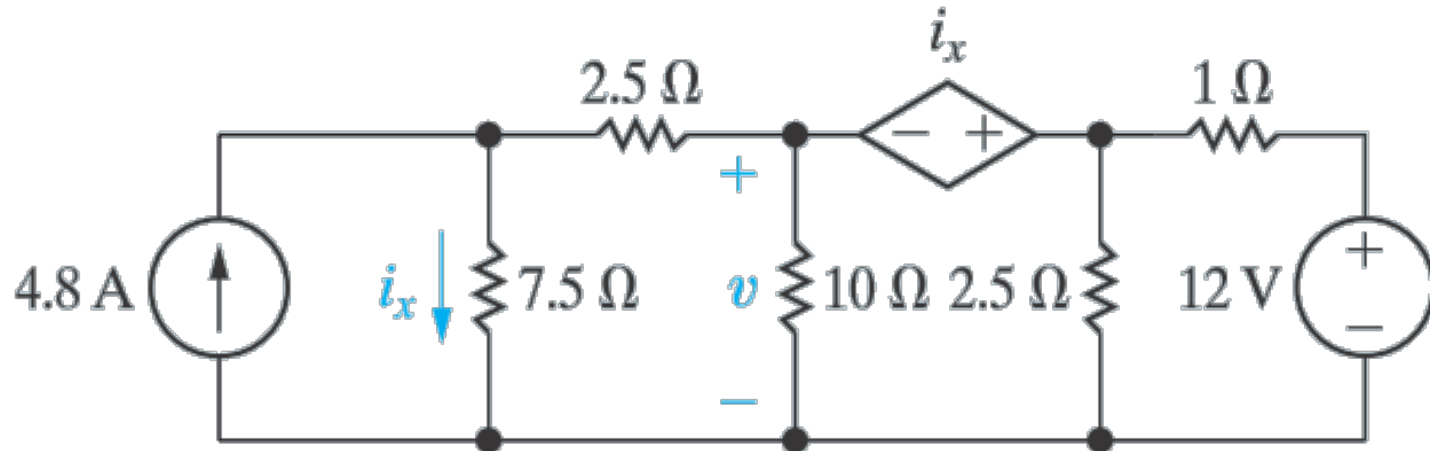
### Step 2

- Apply KCL to the 3<sup>rd</sup> node and the supernode



## Ex. 2.6

# Example of Nodal Analysis

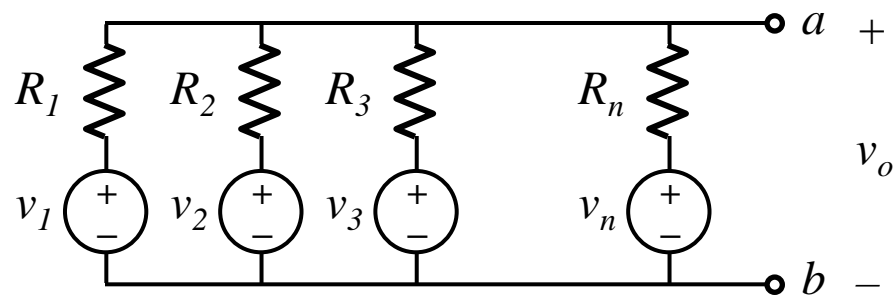


1. Find  $v$
2. Find the power consumed (or supplied) of the dependent voltage source



# Millman's Theorem

A.K.A. "Sharing bus method"



By using node-voltage method (choose b as the reference node):

$$\frac{v_o - v_1}{R_1} + \frac{v_o - v_2}{R_2} + \dots + \frac{v_o - v_n}{R_n} = 0$$

$$\Rightarrow v_o = \frac{\frac{v_1}{R_1} + \frac{v_2}{R_2} + \dots + \frac{v_n}{R_n}}{\frac{1}{R_1} + \frac{1}{R_2} + \dots + \frac{1}{R_n}}$$

If  $R_1 = R_2 = \dots = R_n = R$ ,  $v_o = \frac{1}{n} \sum_{k=1}^n v_k$



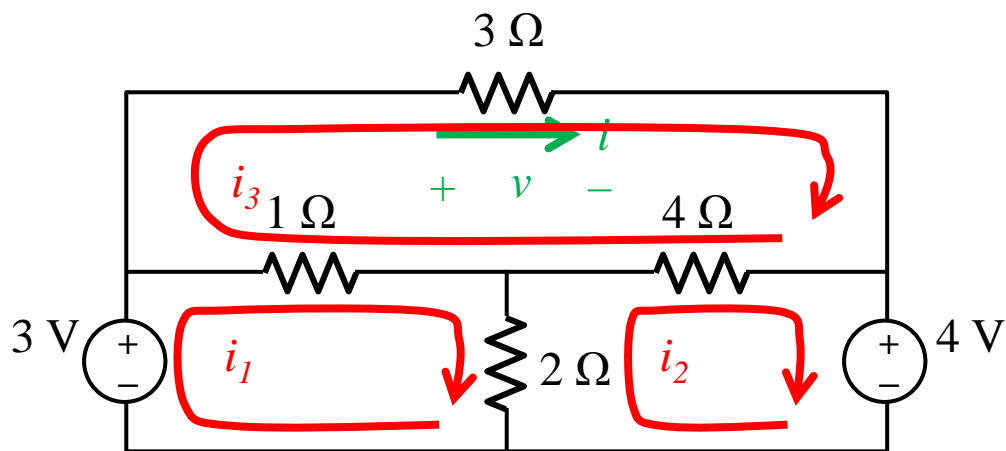
# Contents



## **2.2 Mesh Analysis (Mesh-Current Method)**



# The Idea of Mesh Analysis



Only valid for  
planar circuit

Previous method: use **branch** voltages as the variable

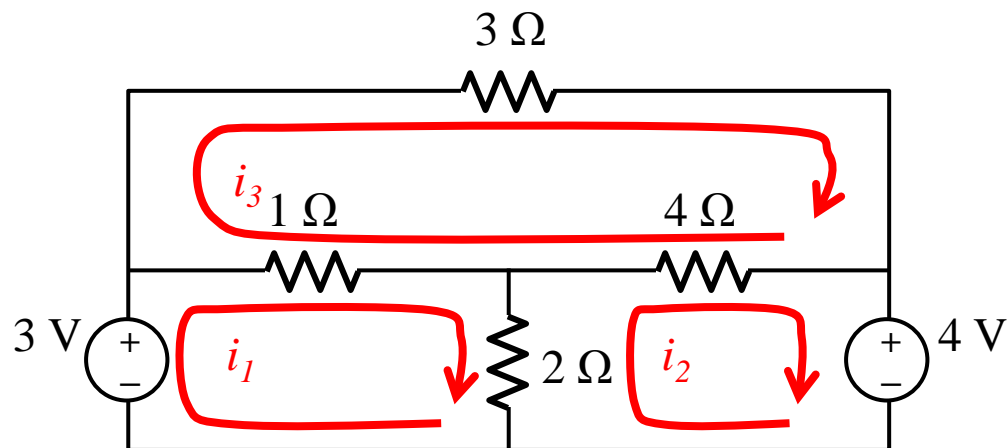
- But the number of branch is much larger than the number of mesh

New method: use **Mesh** currents as the variable

- Each branch current can be obtained from mesh currents
- The corresponding branch voltage can be calculated by its component model
- 12 branch variables  $\rightarrow$  3 mesh variables



# Characteristics of Mesh-Current Method



The current which runs through  $1\ \Omega$ :

$$i_1 - i_3$$

The current which runs through  $2\ \Omega$ :

$$i_1 - i_2$$

The current which runs through  $3\ \text{V}$ :

$$i_1$$

KVL on loop 1

$$(-3) + 1(i_1 - i_3) + 2(i_1 - i_2) = 0$$

1. KCL is automatically satisfied in every node (why?)
2. We only need to find the independent KVL equations
3. For a planar circuit consists of  $B$  branches and  $N$  nodes, one can have  $B - (N - 1)$  independent meshes
4. The direction of mesh current should be kept as the same orientation



# Five Cases in the Following Discussion

## Only containing voltage sources

1. Only with independent voltage sources: basic case
2. With dependent voltage sources: expressing the controlling parameter in terms of mesh currents

## Containing current sources

3. Independent current sources exist in single mesh: the easiest case
4. Independent current sources exist between two adjacent meshes: by supermesh concept
5. With dependent current sources: expressing the controlling parameters in terms of the mesh currents

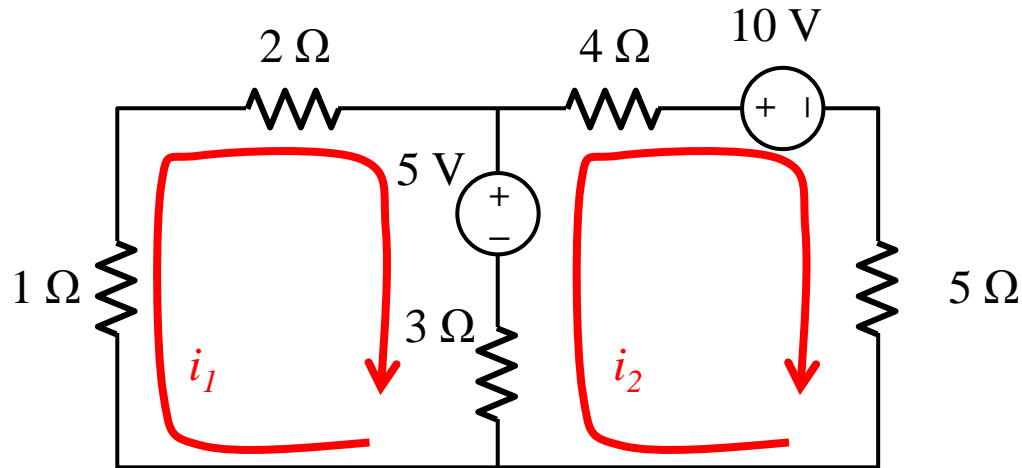
## Ex. 2.7

# With Independent Voltage Source

### CASE 1

$$b = 7, n = 6$$

$$b - (n - 1) = 2$$



- The number of branch:  $b = 7$
- The number of node:  $n = 6$
- So, there are  $b - (n - 1) = 7 - (6 - 1) = 2$  meshes

### Step 1

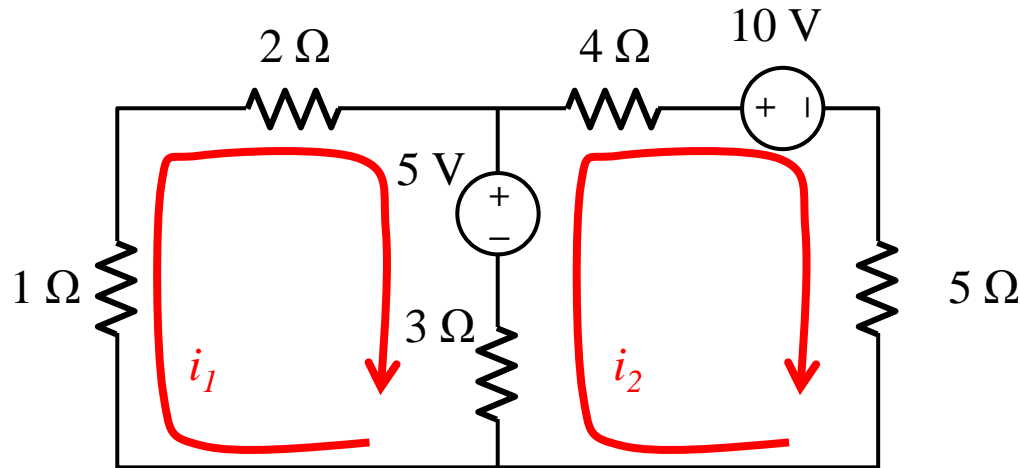
- Find 2 meshes and select  $i_1$  and  $i_2$  as mesh currents
- Choose the mesh currents as clockwise direction



## Ex. 2.7

# With Independent Voltage Source

### CASE 1



### Step 2

- Apply KVL to 2 meshes and use the component model (Ohm's law) to express the branch voltages in terms of mesh currents

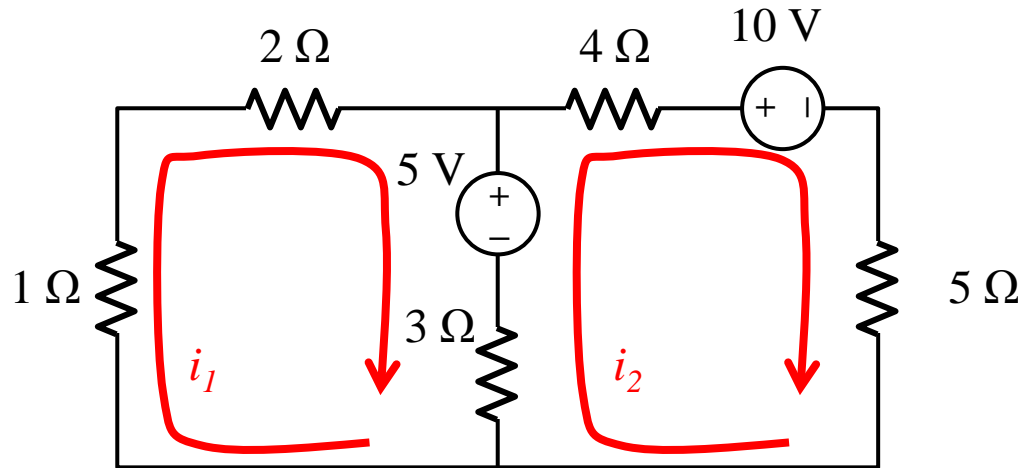
$$\sum_{\text{drop}} v_k = 0 \quad \Rightarrow$$

$\forall \text{ mesh}$

## Ex. 2.7

# With Independent Voltage Source

### CASE 1



### Step 3 (not necessary)

- Matrix expression

$$\begin{bmatrix} 1+2+3 & -3 \\ -3 & 3+4+5 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} -5 \\ 5-10 \end{bmatrix}$$

$$Ri = V$$

$R$  Resistance matrix

$R_{kk}$  Sum of the resistances in mesh  $k$

$R_{kj}$  Sum of the resistance between meshes  $i$  and  $k$  and the algebraic sign depends on the relative direction of meshes  $i$  and  $k$ , plus (minus) sign for same (opposite) direction

$V_k$  Sum of independent voltage **rises** at the  $k^{\text{th}}$  mesh

$i_k$  Unknown; mesh current at the  $k^{\text{th}}$  mesh

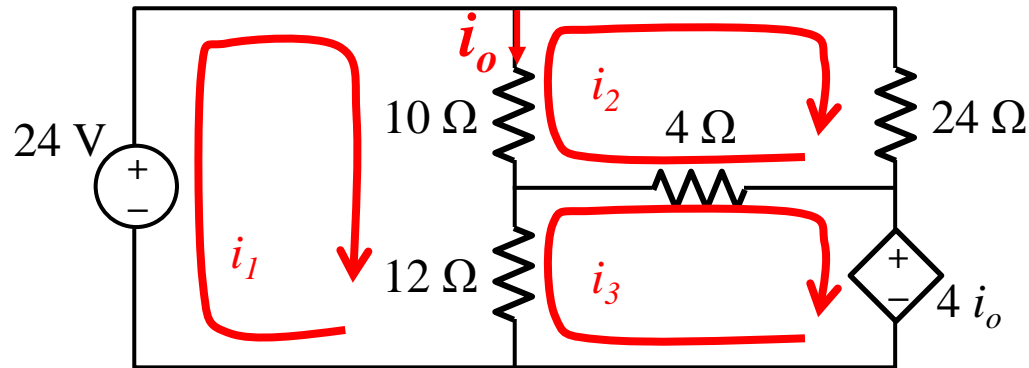
## Ex. 2.8

# With Dependent Voltage Source

### CASE 2

$$b = 6, n = 4$$

$$b - (n - 1) = 3$$



### Step 1

- Assign mesh currents:  $i_1$ ,  $i_2$ , and  $i_3$
- Express  $i_o$  in terms of the mesh currents ( $i_1$ ,  $i_2$ , and  $i_3$ )

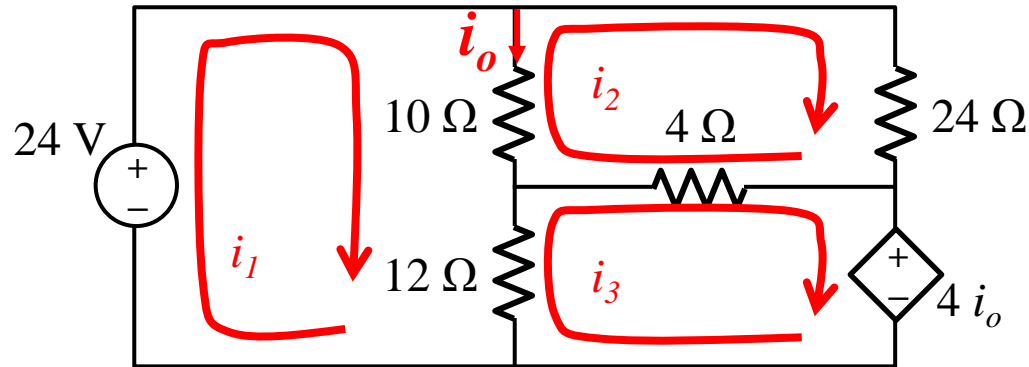
### Step 2

- Apply KVL to 3 meshes:

## Ex. 2.8

# With Dependent Voltage Source

### CASE 2



### Step 3

- Matrix expression (not necessary)

$$\begin{bmatrix} 10+12 & -10 & -12 \\ -10 & 10+4+24 & -4 \\ -12 \text{ } \textcolor{red}{+4} & -4 \text{ } \textcolor{red}{-4} & 4+12 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \\ i_3 \end{bmatrix} = \begin{bmatrix} 24 \\ 0 \\ 0 \end{bmatrix} \quad 4 i_o = 4 (i_1 - i_2)$$

➡  $i_1 = 2.25 \text{ A}, i_2 = 0.75 \text{ A}, i_3 = 1.5 \text{ A}$

How about the current, voltage and power through the 10-Ω resistor and the CCVS?

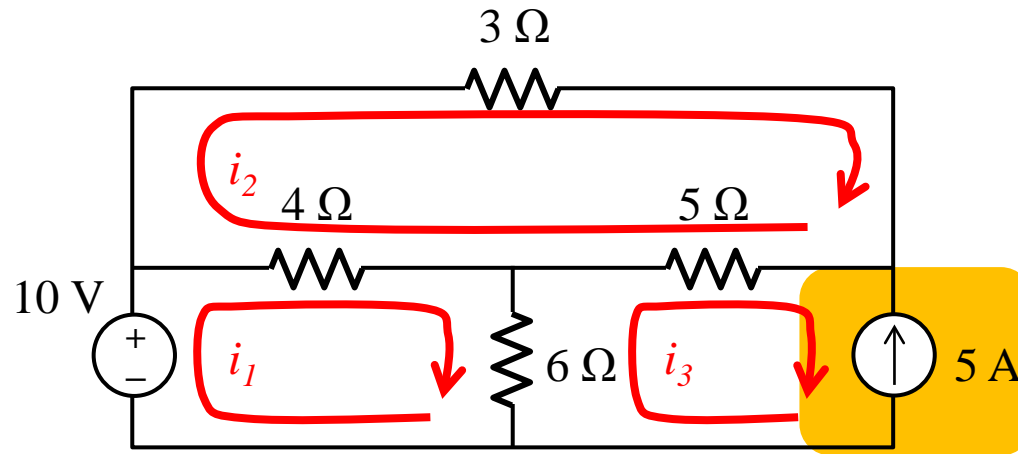
## Ex. 2.9

# With Current Source Existed in Only One Mesh

### CASE 3

$$b = 6, n = 4$$

$$b - (n - 1) = 3$$



### Step 1

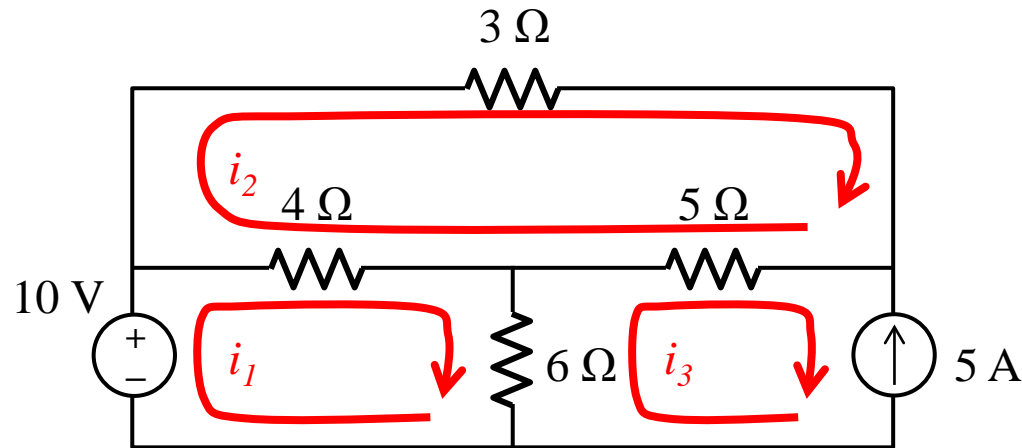
- Assign mesh currents:  $i_1$ ,  $i_2$ , and  $i_3$
- How to express  $i_3$ ?

### Step 2

- Apply KVL to 2 meshes:

## Ex. 2.9

# With Current Source Existed in Only One Mesh



- Rearrange the equations:

### Step 3

- Matrix expression (not necessary)

$$\begin{bmatrix} 4+6 & -4 \\ -4 & 3+5+4 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} 10-30 \\ -25 \end{bmatrix}$$

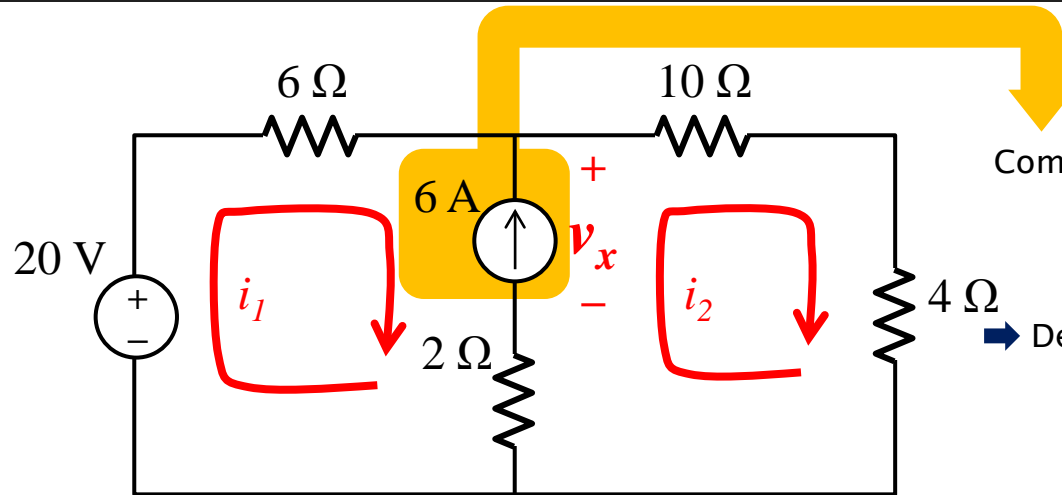
# Ex. 2.10

## With Current Source Existed Between Two Meshes

### CASE 4

$$b = 6, n = 5$$

$$b - (n - 1) = 2$$



Component model of  $\uparrow$  :

$$i_s = 6 \text{ A}$$

$$v_s = ?$$

➡ Define an extra unknown  $v_x$

### Step 1

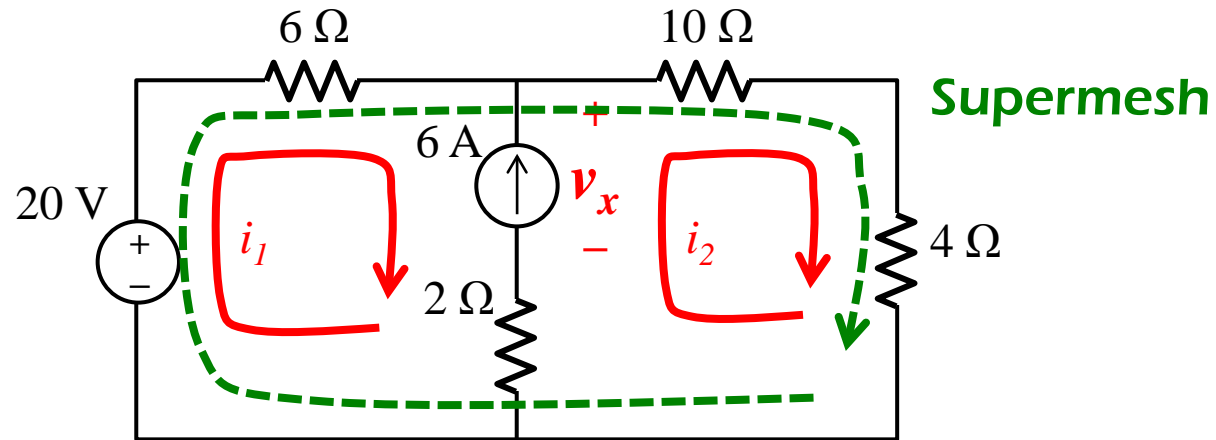
- Assign mesh currents:  $i_1$  and  $i_2$
- What's the relation between  $i_1$  and  $i_2$ ?

### Step 2

- Apply KVL to 2 meshes:

## Ex. 2.10

## With Current Source Existed Between Two Meshes



- And we already know that  $i_2 - i_1 = 6 \text{ A}$



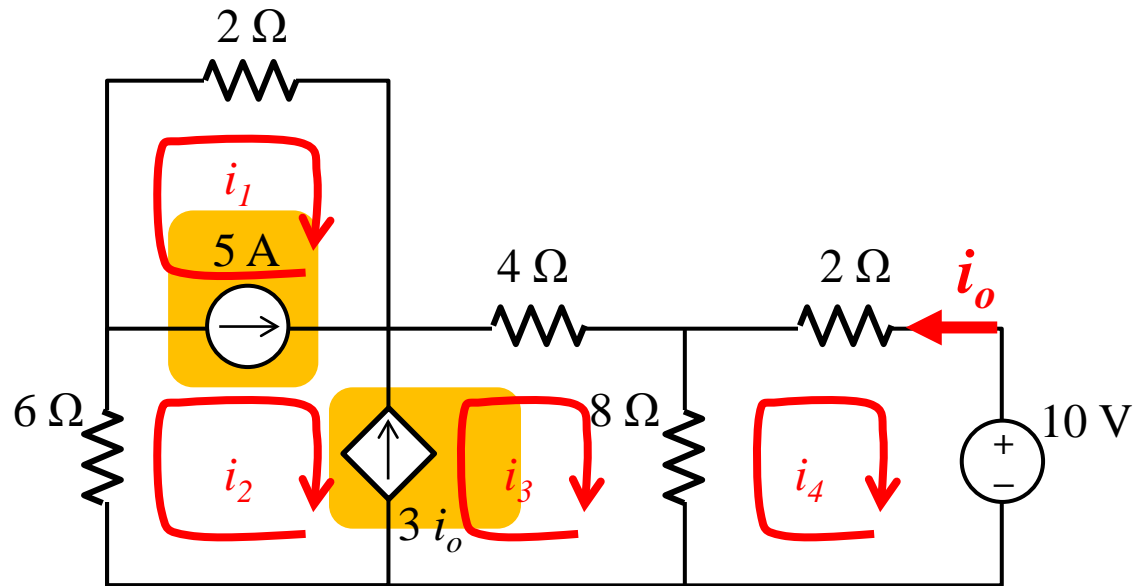
## Ex. 2.11

# With Dependent Current Source

### CASE 5

$$b = 8, n = 5$$

$$b - (n - 1) = 4$$

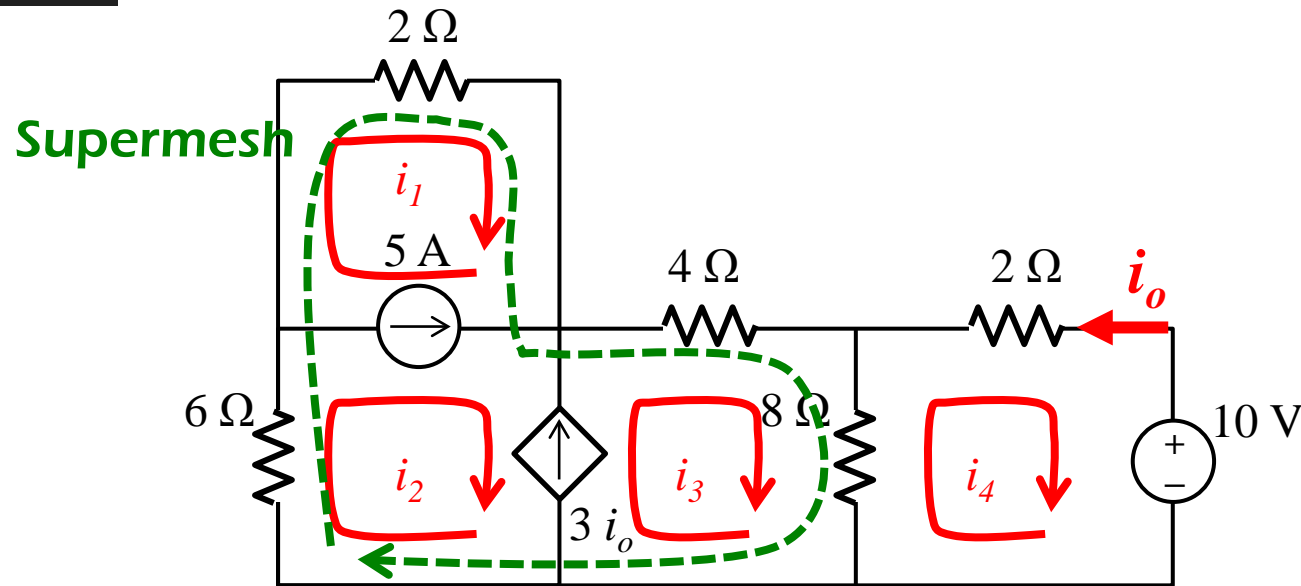


### Step 1

- Assign mesh currents:  $i_1$ ,  $i_2$ ,  $i_3$  and  $i_4$

## Ex. 2.11

# With Dependent Current Source



### Step 2

- We can find that both the  $5\text{ A}$  independent current source and the  $3i_o$  dependent current source lie between two meshes
- Apply the supermesh concept to the 1<sup>st</sup>, 2<sup>nd</sup>, and 3<sup>rd</sup> mesh
- Only two KVL equations are required



# Nodal Analysis vs. Mesh Analysis

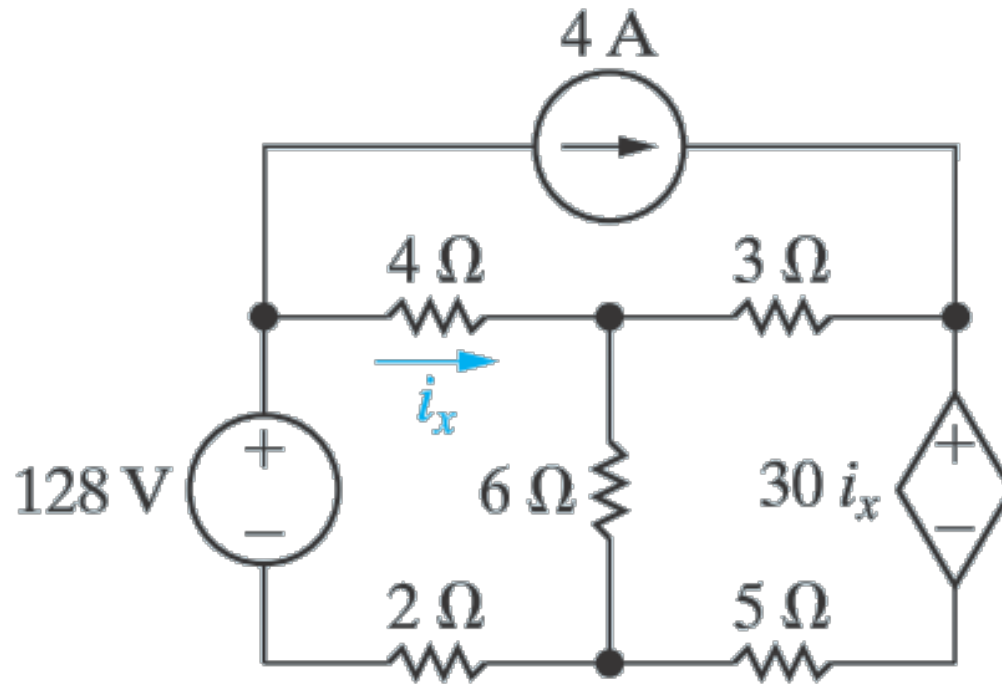
Advantage of nodal analysis and mesh analysis:

- Both methods provide a systematic way of analyzing a complex circuit
- The number of unknowns are much fewer than those of the 2B method

Nodal analysis		Mesh analysis
Node voltage	Unknown	Mesh current
$n - 1$	Number of unknowns	$b - (n - 1)$
$n - 1 - m_v$	Number of unknowns (including sources)	$b - (n - 1) - m_i$

( $m_v$ : number of voltage sources,  $m_i$ : number of current sources)

- Which method do we prefer? It depends on the solution required!



1. Find the power supplied of the 4 A independent current source (by nodal analysis and mesh analysis, respectively)



# Contents



## 2.3 Superposition Theorem



# Superposition Theorem in Circuits

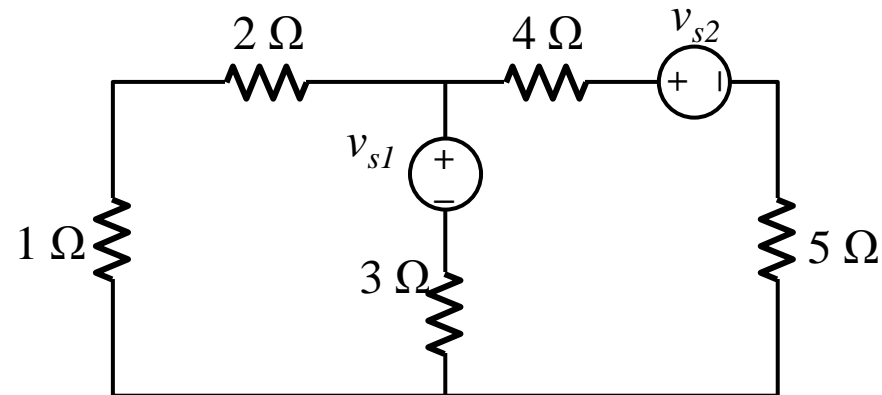
- The circuit theorem studied in this semester belongs to the area of “linear systems”
- So, we can apply some theorems of linearity to solve circuit problems

Two theorems are introduced in this section:

## 1. Homogeneous theorem

## 2. Superposition theorem

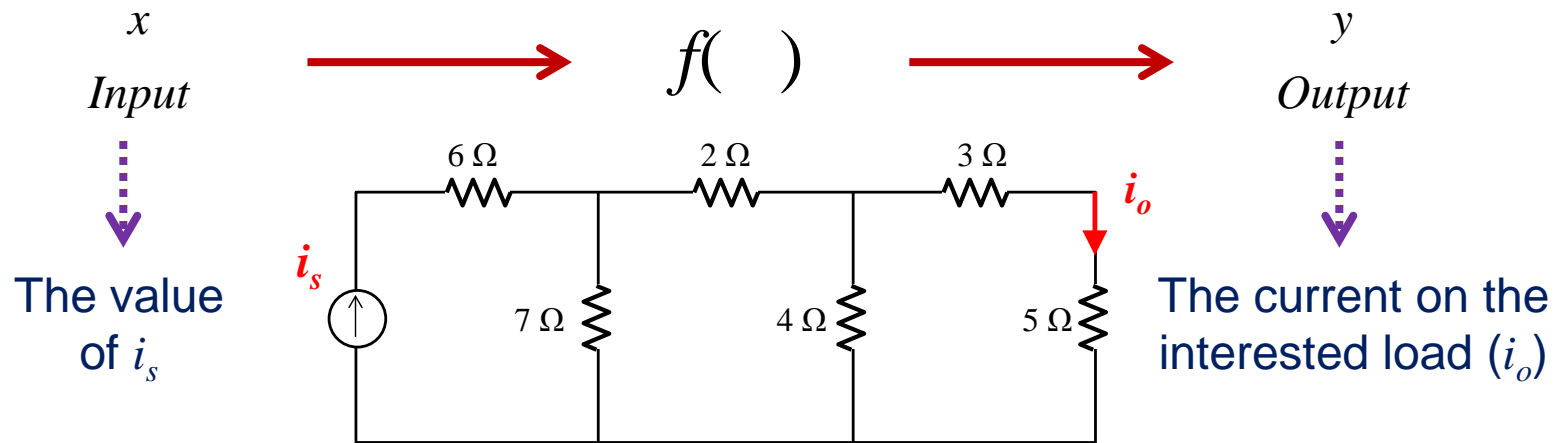
- Actually, these two theorems are not critical for dc independent sources
- However, they are important for the scenario that two independent sources are not of the same form, such as  $v_{s1} = v_1 e^{-2t}$  and  $v_{s2} = v_2 \cos \omega t$





# Linear Systems

A circuit can be considered as a linear system:



Properties of linear system (between output  $y$  and input  $x$ ):

Homogeneous property

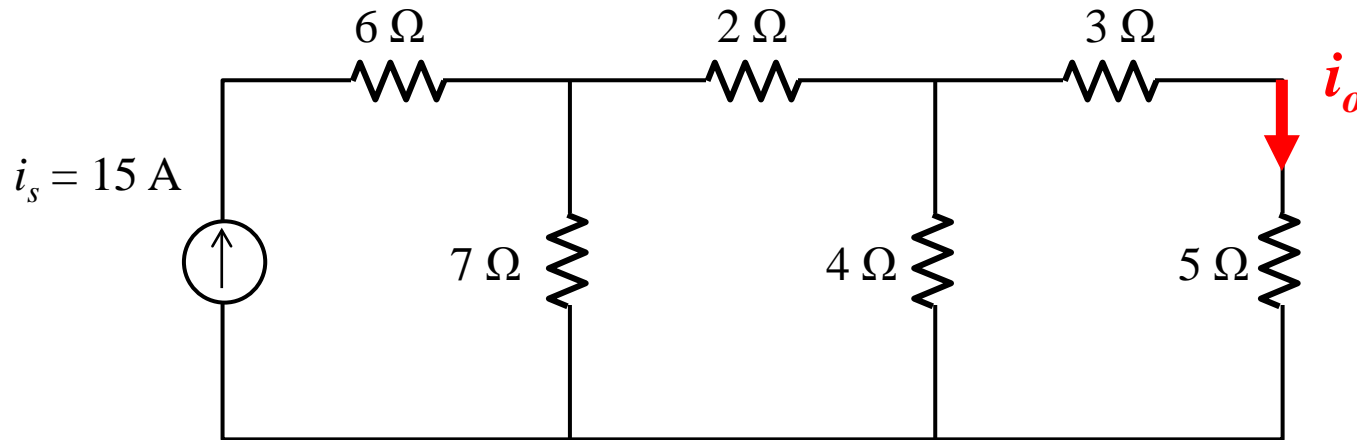
$$\text{If } f(x_1) = y_1, \text{ then } f(mx_1) = my_1$$

Additive property

$$\text{If } f(x_1) = y_1, f(x_2) = y_2, \text{ then } f(x_1 + x_2) = y_1 + y_2$$

## Ex. 2.13

# Homogeneous Property in Circuit



- Find  $i_o$  by assuming  $i_o = 1\text{ A}$  and use linear properties to find its actual value

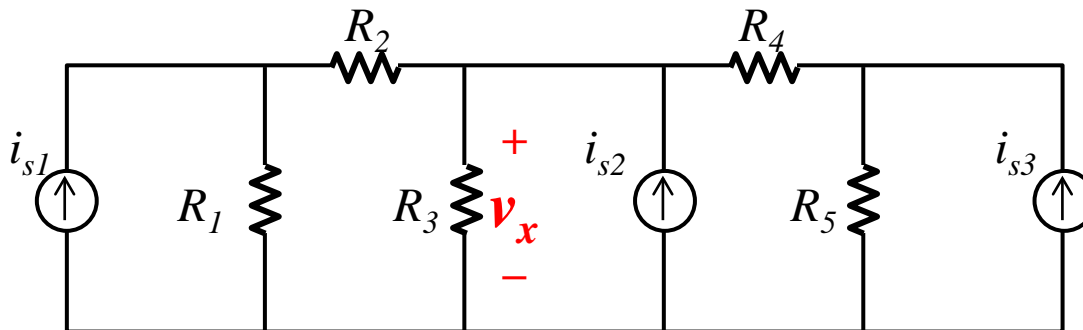
*Input:* The value of  $i_s$   $\longrightarrow f(\quad) \longrightarrow$  *Output:* The current on the interested load  $i_o$

Assumption	5	$\longleftarrow \cdots \cdots \cdots$	1
Real value	15	$\cdots \cdots \cdots \longrightarrow$	3





# Additive Property in Circuit (1/2)



- For a linear circuit consisting of  $n$  input source  $(u_1, u_2, u_3, \dots, u_n)$ , then the output response can be calculated as the sum of its components

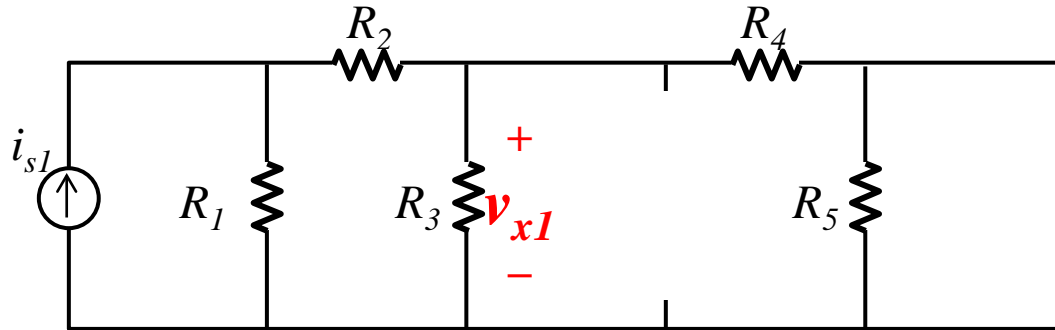
$$y = f(u_1) + f(u_2) + \dots + f(u_n)$$

- Input sources:  $i_{s1}$ ,  $i_{s2}$ , and  $i_{s3}$
- Interesting output response:  $v_x$
- We can activate one source at a time and sum the resultant output responses to determine the final result

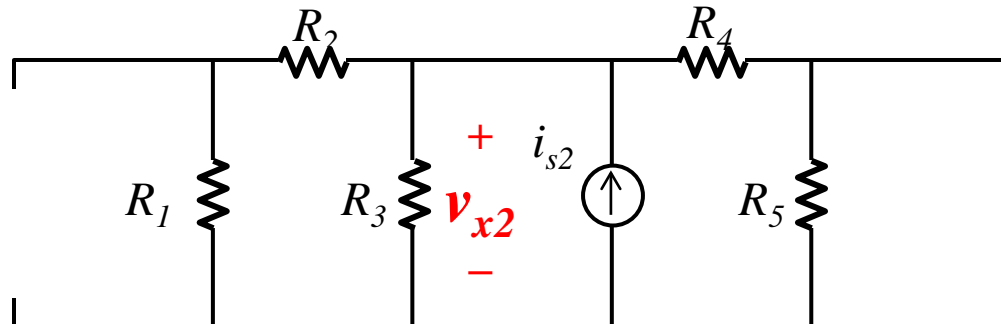


# Additive Property in Circuit (2/2)

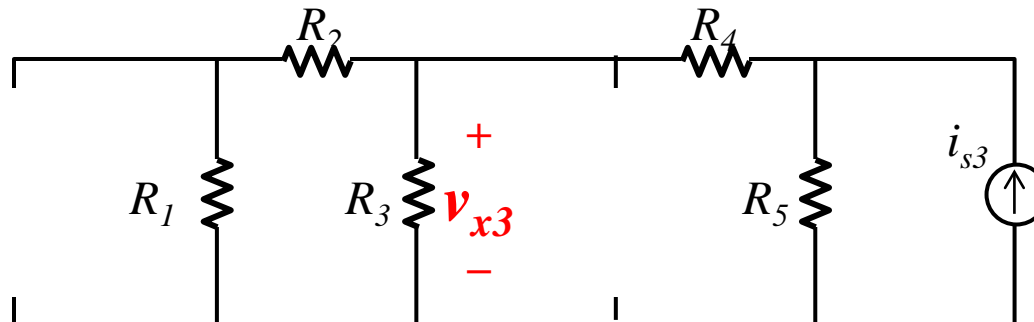
Source 1:



Source 2:



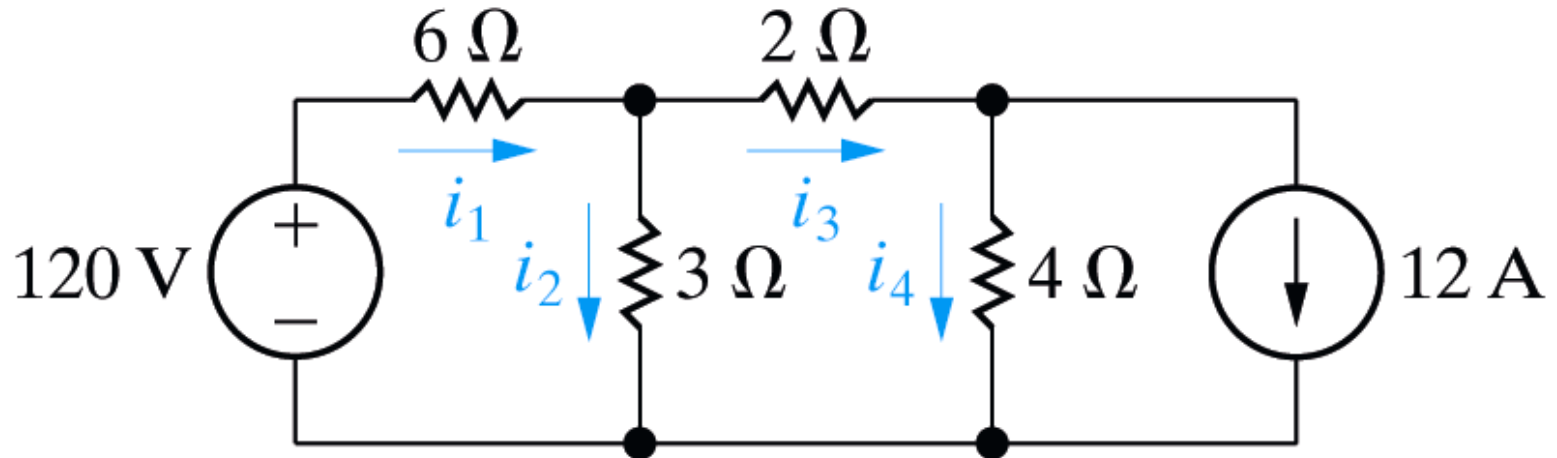
Source 3:



The final response  $v_x = v_{x1} + v_{x2} + v_{x3}$

## Ex. 2.14

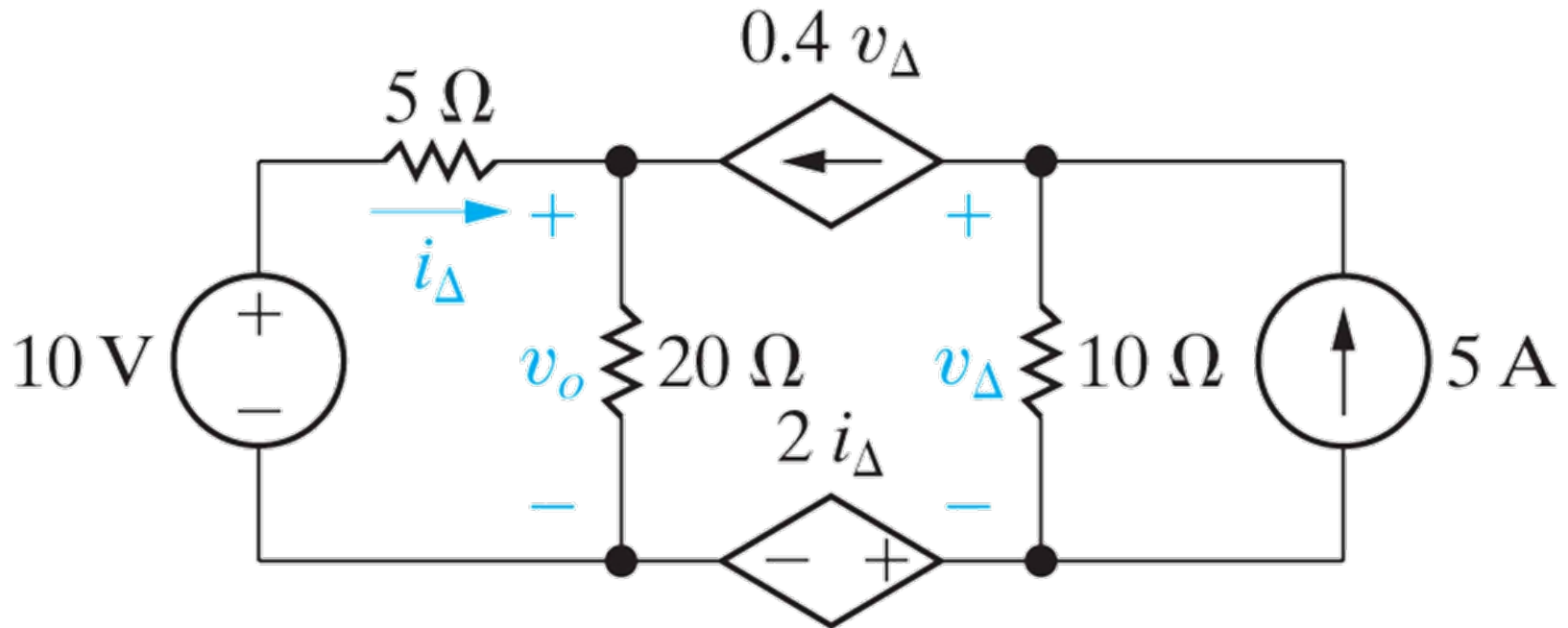
# Superposition Theorem



1. Calculate  $i_1$ ,  $i_2$ ,  $i_3$ , and  $i_4$  by superposition theorems

## Ex. 2.15

# Superposition Theorem



1. Use the principle of superposition to find  $v_o$  and the associated power delivered to it

(Note that dependent sources cannot be deactivate!!)



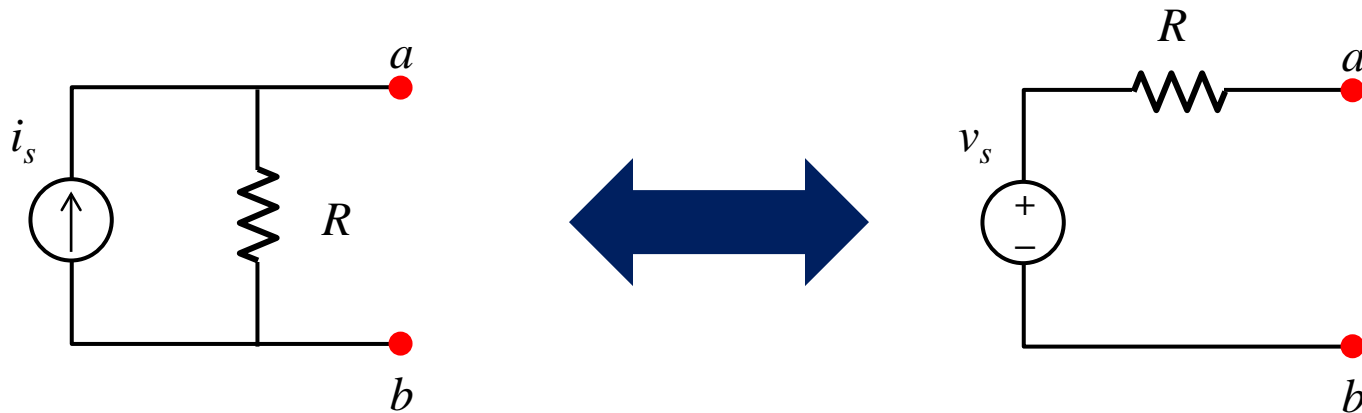
# Contents



## 2.4 Source Transformation



# Source Transformation

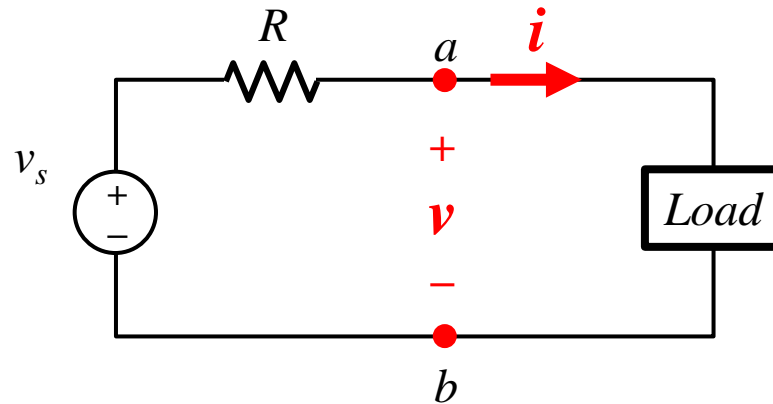


- It allows a voltage source in series with a resistor to be replaced by a current source in parallel with the same resistor
- Vice versa



# Voltage Source $\rightarrow$ Current Source

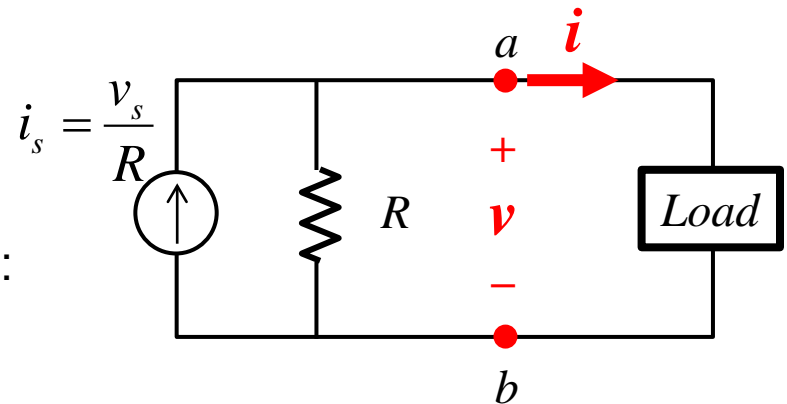
## Case 1:



■ The current run through the load:

$$i = \frac{v_s - v}{R} = \frac{v_s}{R} - \frac{v}{R}$$

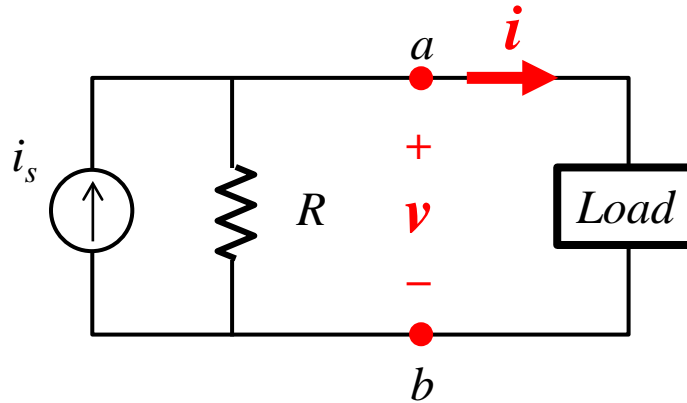
Let this term be  $i_s$  so it is equivalent to:





# Current Source $\rightarrow$ Voltage Source

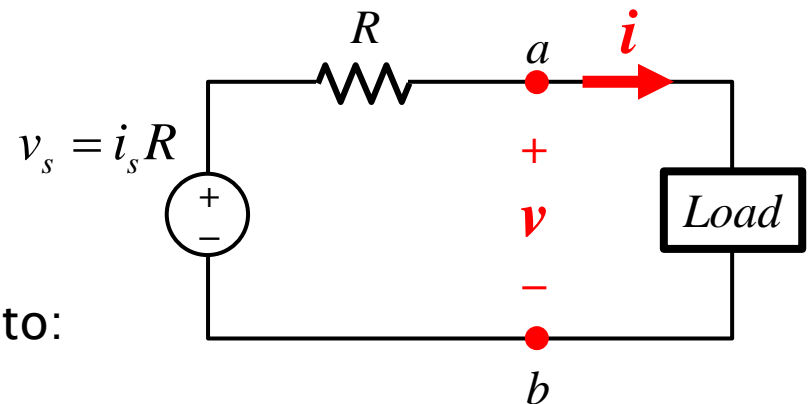
## Case 2:



■ The voltage across the load:

$$v = (i_s - i)R = \boxed{i_s R} - iR$$

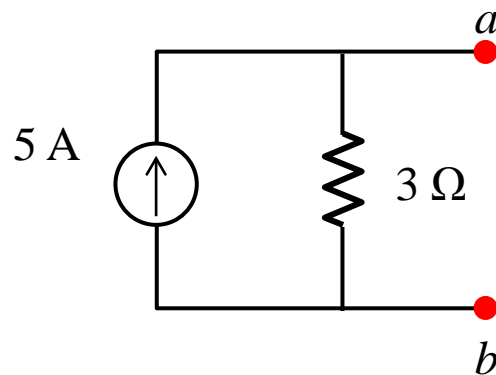
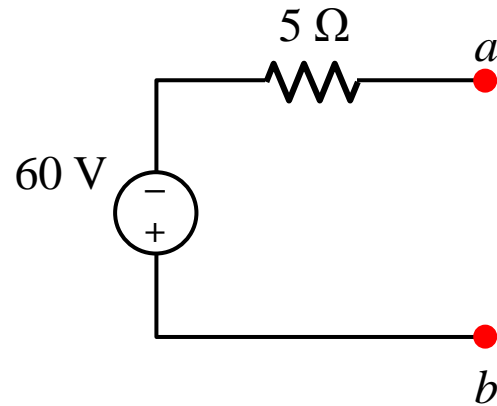
Let this term be  $\boxed{v_s}$ , so it is equivalent to:





## Ex. 2.16

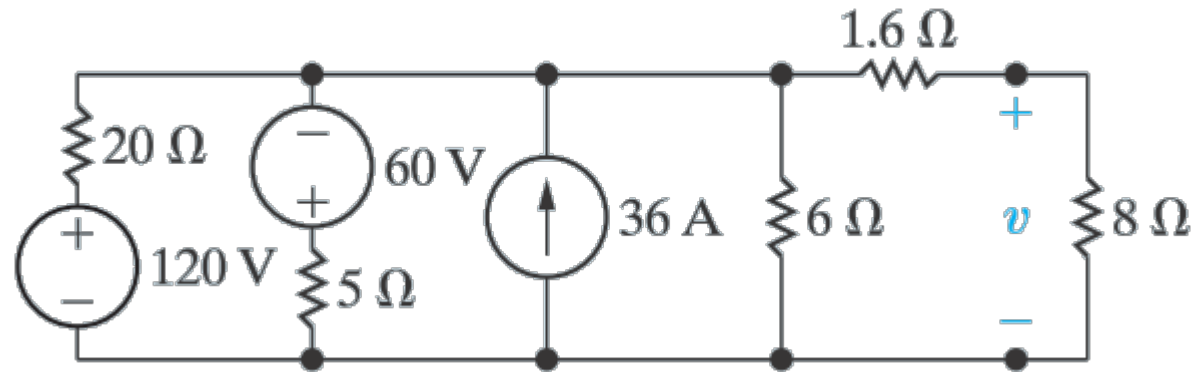
# Source Transformation



Both the source and resistor representations are equivalent for the load connected at *a-b* terminals

## Ex. 2.17

## Source Transformation



1. Use source transformations to find the voltage  $v$
2. Find the power developed by the 120-V voltage source



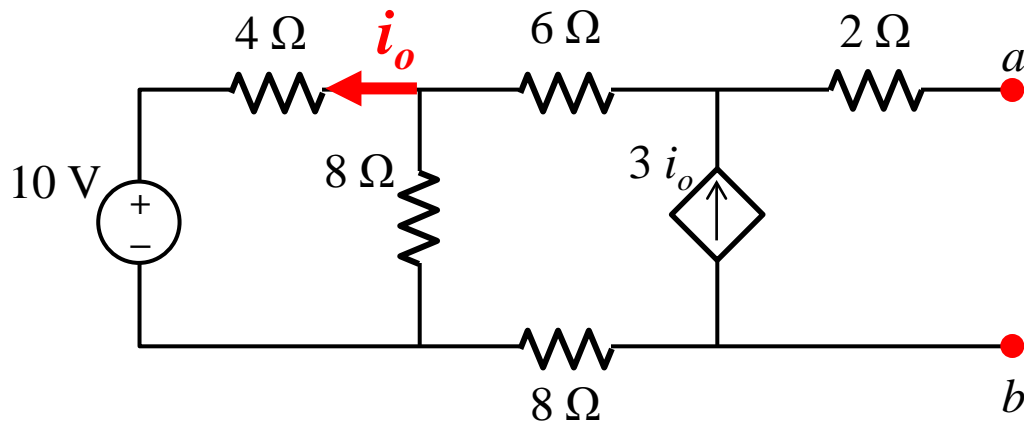
# Contents



## **2.5 Thévenin and Norton Equivalents**

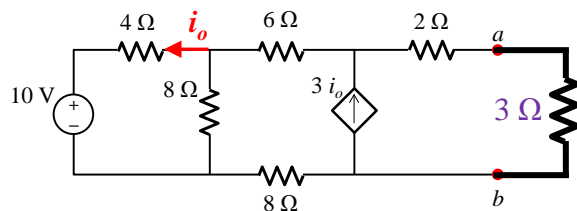


# Objective of Thévenin Equivalent Circuit (1/3)

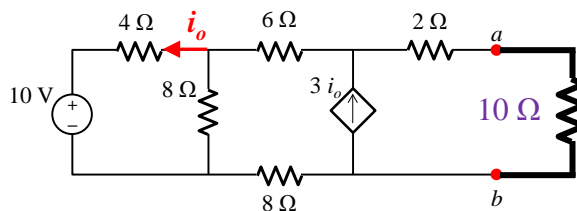


- Usually, we have a given circuit
- We connect a load to the a-b terminals; the load derives power from that given circuit
- The objective is to calculate the **voltage, current, or power on the load**

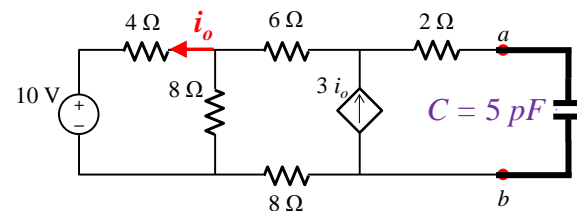
$$R_L = 3 \Omega$$



$$R_L = 10 \Omega$$

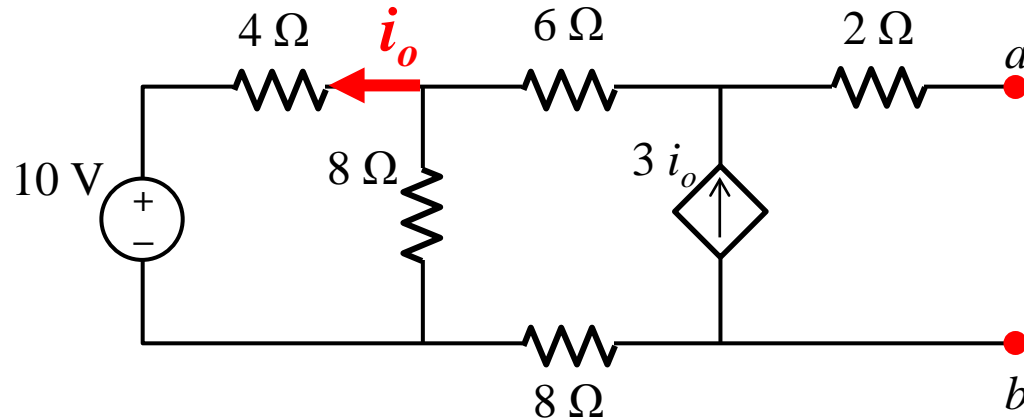


$$C_L = 5 \text{ pF}$$

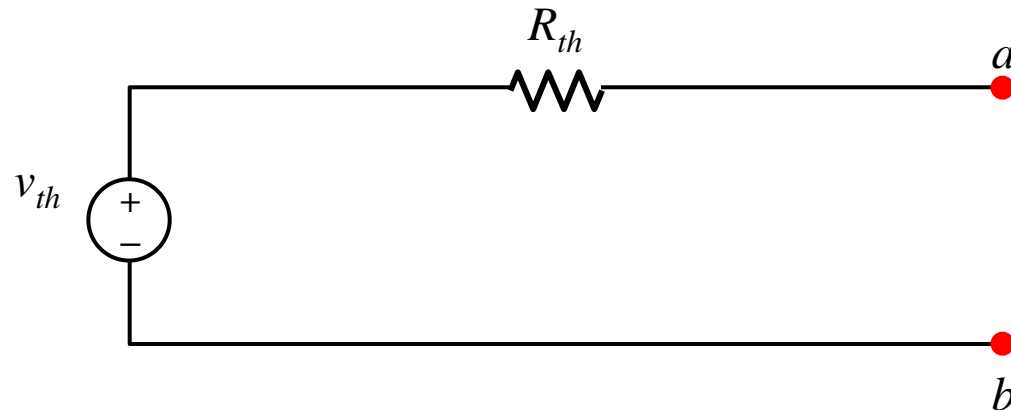




## Objective of Thévenin Equivalent Circuit (2/3)

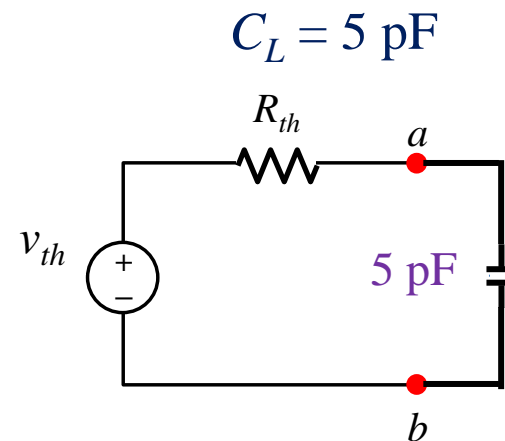
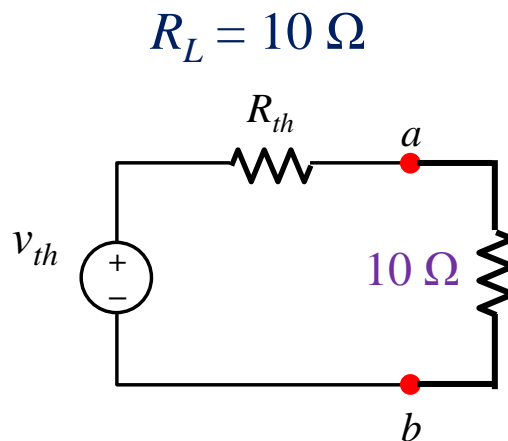
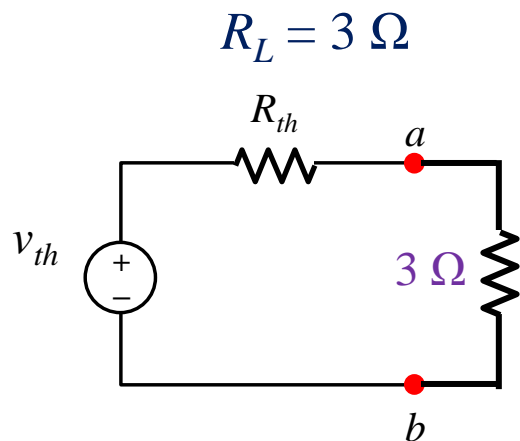


Instead of calculating  $v_L$  and  $i_L$  one at a time, the given two-terminal circuit can be replaced by:





## Objective of Thévenin Equivalent Circuit (3/3)

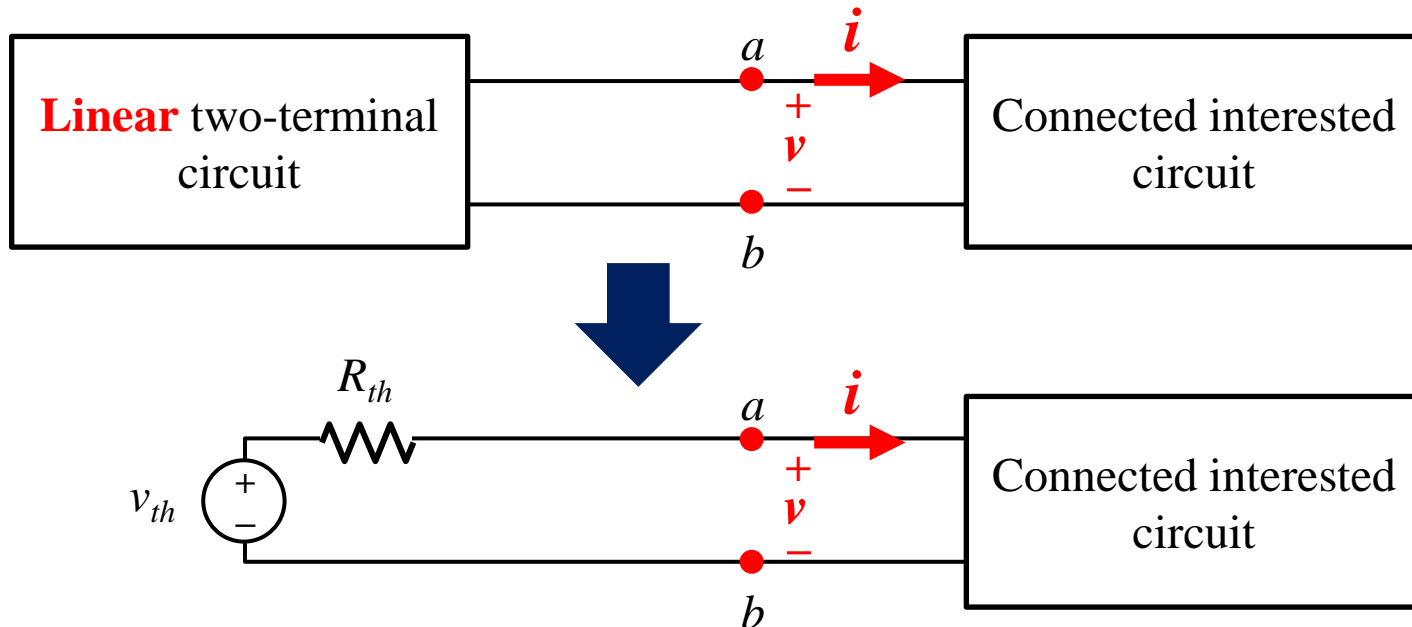


- ❏ To compute the voltage and current on the load becomes much easier
- ❏ **Voltage divider will do!**
- ❏ We don't have to reanalyze the entire circuit
- ❏ So, the most imperative task would be:
  - How to find  $v_{th}$ ?
  - How to find  $R_{th}$ ?



# Thévenin Theorem

- A linear two-terminal circuit can be replaced by an equivalent circuit consisting of a voltage source  $v_{th}$  in series with a resistor  $R_{th}$  where

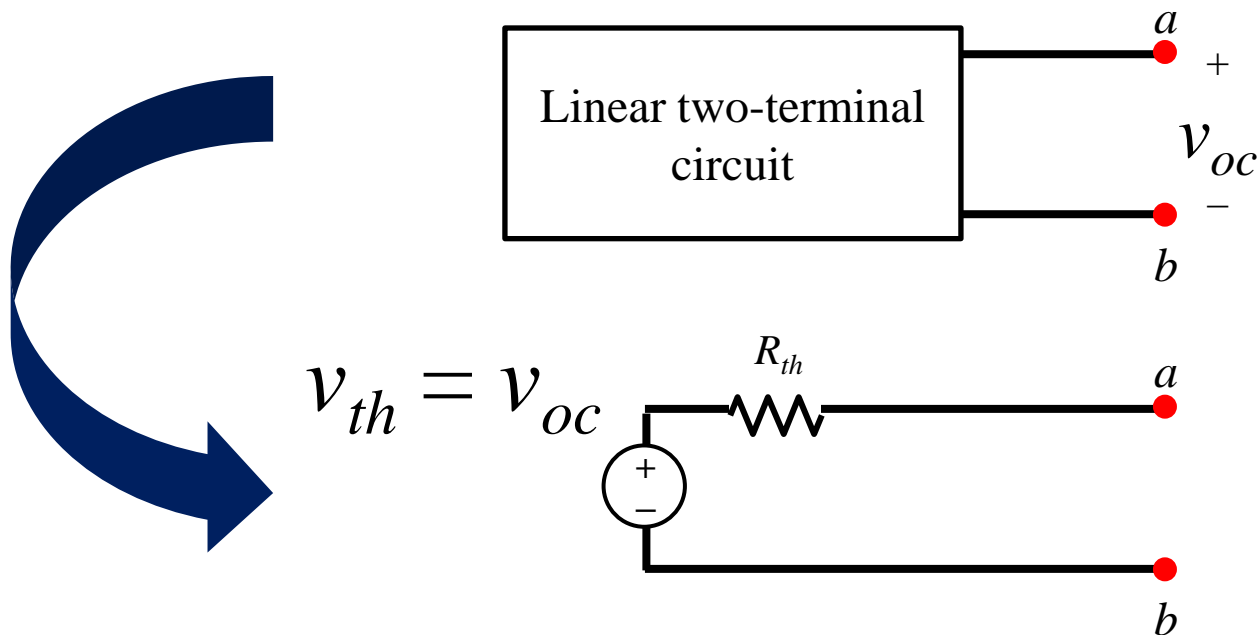


- $v_{th}$  : The open-circuit voltage at the terminals
- $R_{th}$  : The input resistance at the terminals when the **independent** sources are turned off



# $v_{th}$ : New Voltage Source

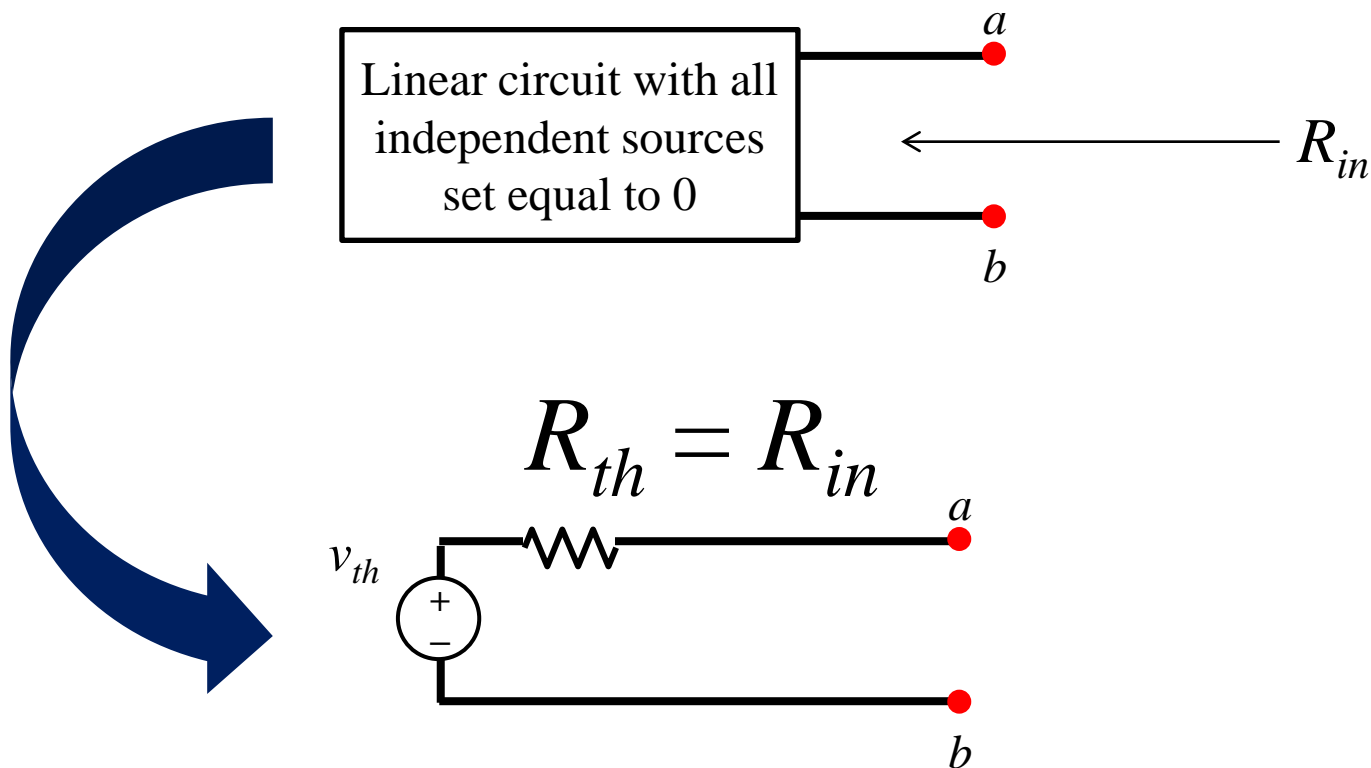
- Equivalent circuit: The same voltage-current relation at the terminals
- The equivalence is only valid for the viewpoint of the load
- However, if you concern about the voltage-current relation at some components of the source circuit, you can't find such information by using the equivalent circuit







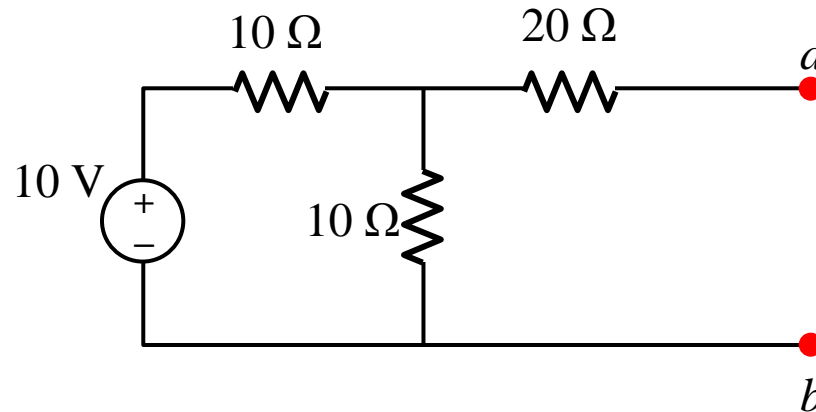
# $R_{th}$ : New Internal Resistance (Case 1)



- ❏ If dependent sources are included in the original circuit, we have to use another method for finding  $R_{th}$

## Ex. 2.18

### If the Original Circuit Only Has Independent Sources (1/2)



1. Derive the Thévenin equivalent circuit

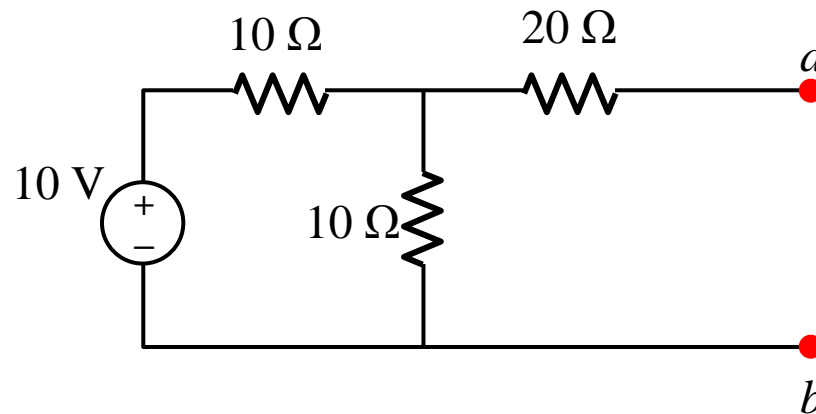


①  $v_{th}$  : By voltage divider principle:

②  $R_{th}$  :

## Ex. 2.18

### If the Original Circuit Only Has Independent Sources (2/2)



Thévenin equivalent circuit:



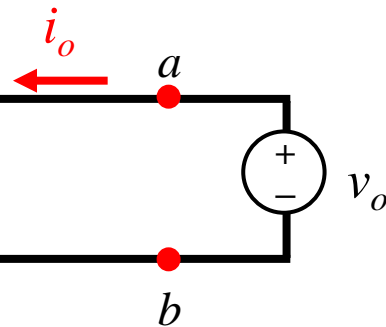
Verification: If  $R_L = 25 \Omega$ :

- Original circuit:  $i_L = 0.1 \text{ A}$ ,  $v_L = 2.5 \text{ V}$
- Thévenin equivalent circuit:  $i_L = 0.1 \text{ A}$ ,  $v_L = 2.5 \text{ V}$



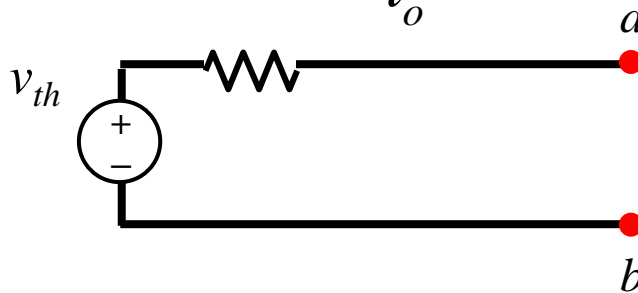
## $R_{th}$ : If the Original Network Has Dependent Sources (Case 2) (1/2)

Linear circuit with all independent sources set equal to 0



- Arbitrarily apply a testing voltage source  $v_o$
- And then find the associated  $i_o$

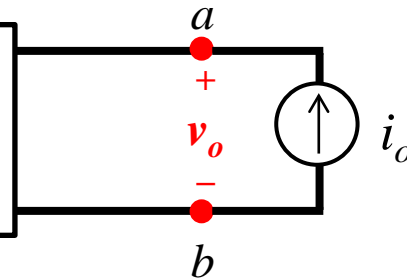
$$R_{th} = \frac{v_o}{i_o}$$





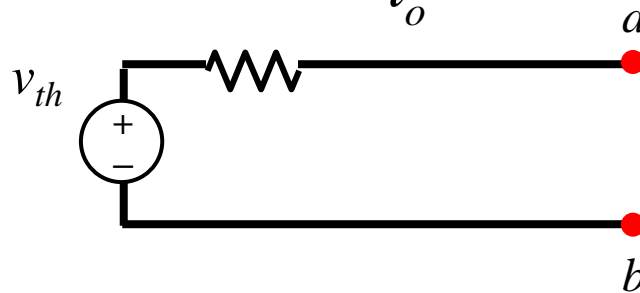
## $R_{th}$ : If the Original Network Has Dependent Sources (Case 2) (2/2)

Linear circuit with all independent sources set equal to 0



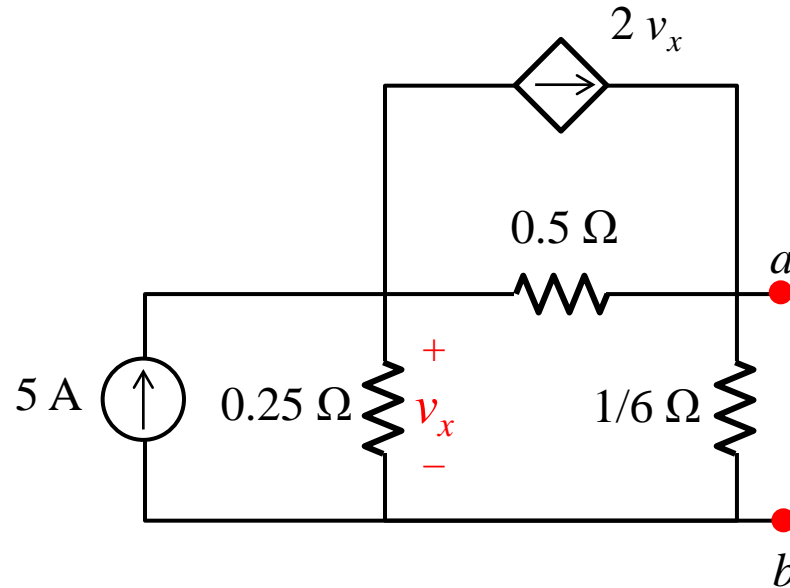
- Arbitrarily apply a testing current source  $i_o$
- And then find the associated  $v_o$

$$R_{th} = \frac{v_o}{i_o}$$



## Ex. 2.19

# If the Original Circuit Has Dependent Sources



1. Derive the Thévenin equivalent circuit

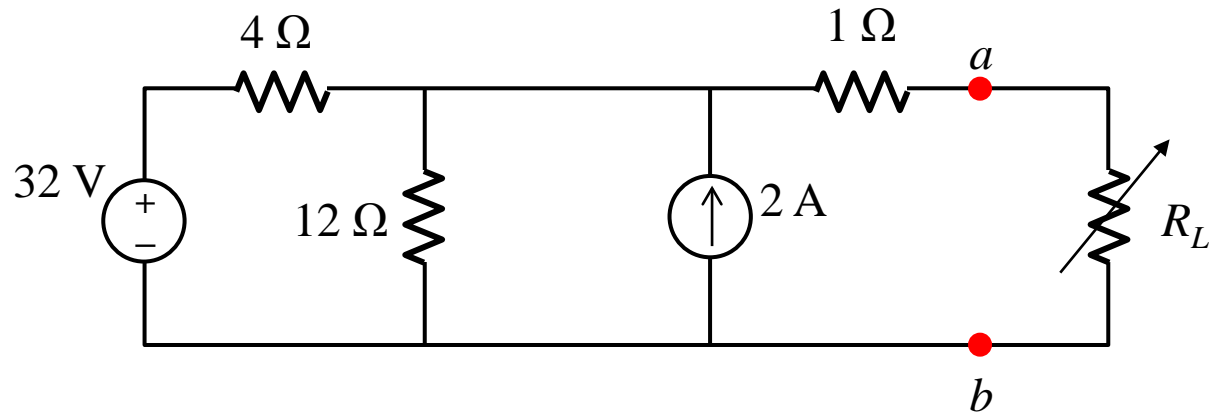


①  $v_{th}$  : By nodal analysis

②  $R_{th}$  :

## Ex. 2.20

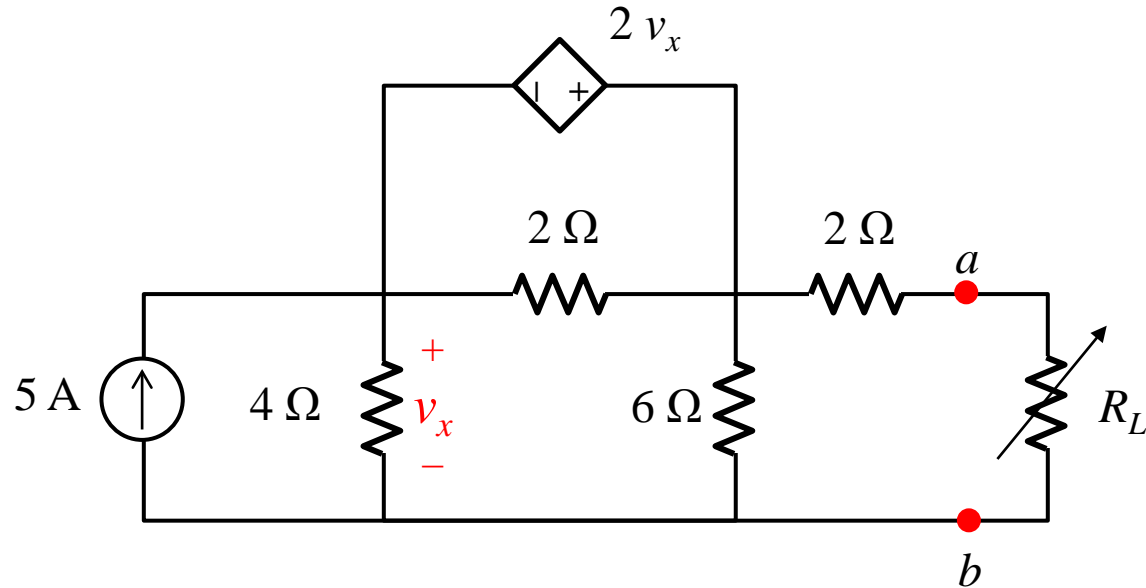
# Application of Thévenin Equivalent Circuit



1. Find the current through the adjustable resistor where  $R_L = 6$ , 16, and  $36\ \Omega$ , respectively

## Ex. 2.21

# A More Complicated Example



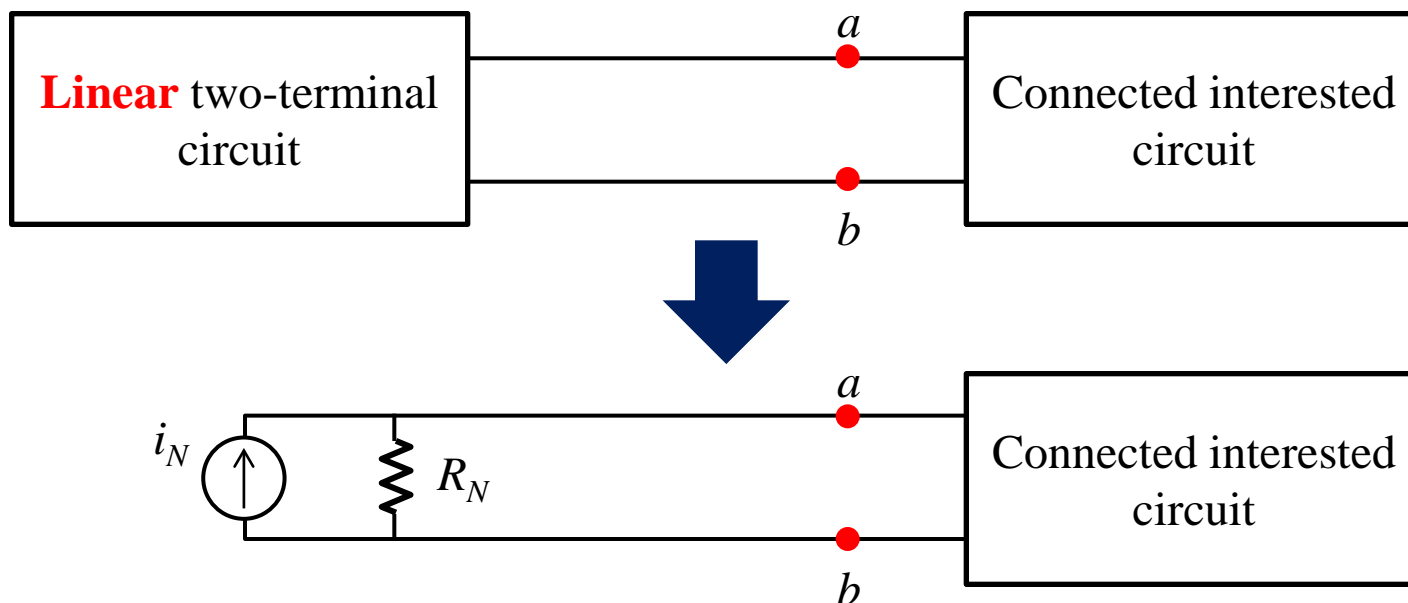
1. Find the consumed power on the adjustable resistor where  $R_L = 6, 16, \text{ and } 36\ \Omega$ , respectively
2. What value of  $R_L$  can derive maximum power from the original circuit?





# Norton Equivalent Circuit

- A linear two-terminal circuit can be replaced by an equivalent circuit consisting of a current source  $i_N$  in parallel with a resistor  $R_N$  where

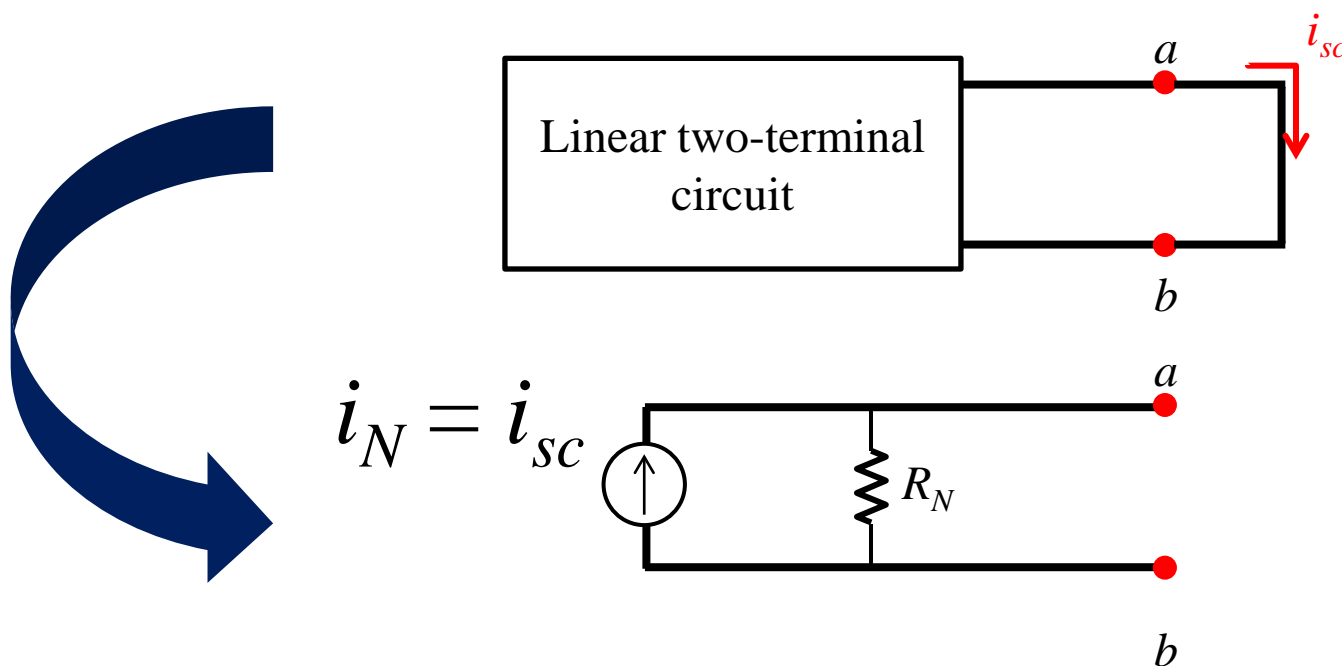


- $i_N$  : The short-circuit current through the terminals
- $R_N$  : The input resistance at the terminals when the independent sources are turned off



# Computation of $i_N$ and $R_N$

- $i_N$  : The short-circuit current run through the terminals

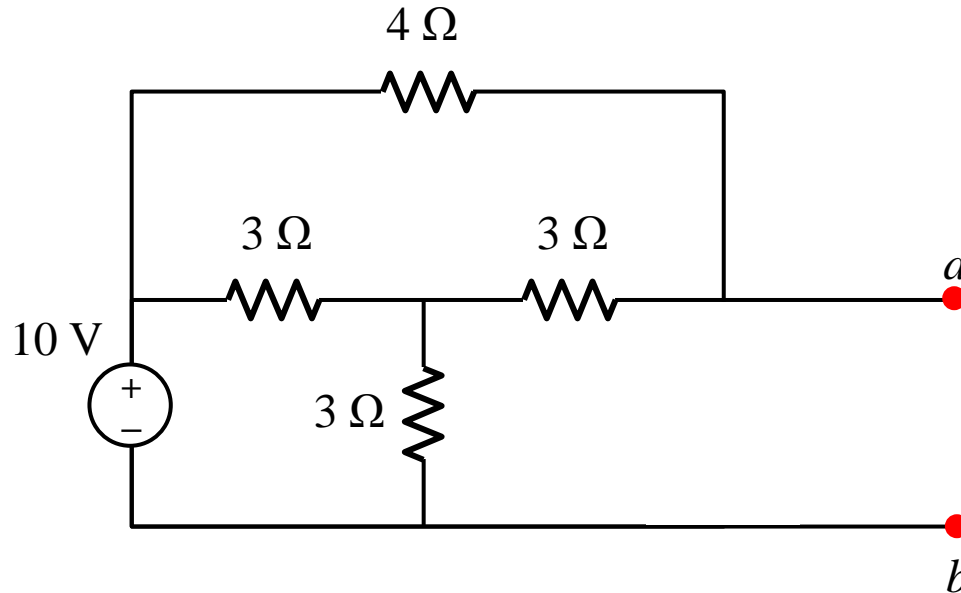


- $R_N$  : The computation of  $R_N$  is the same as that of  $R_{th}$

Norton equivalent circuit is the **source transformation** of Thévenin equivalent circuit

## Ex. 2.22

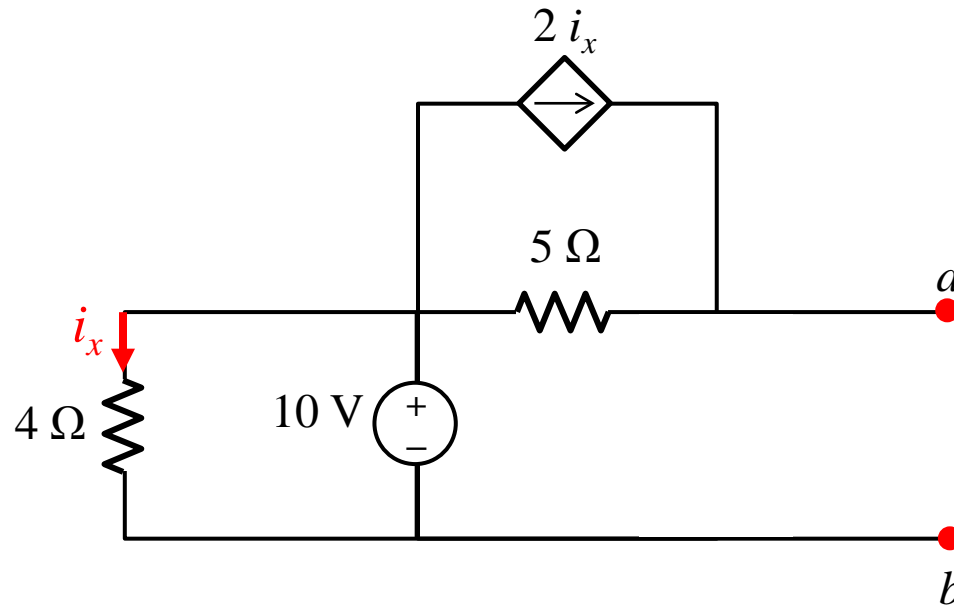
# Norton Equivalent Circuit



1. Derive the Norton equivalent circuit

## Ex. 2.23

# Norton Equivalent Circuit



1. Derive the Norton equivalent circuit



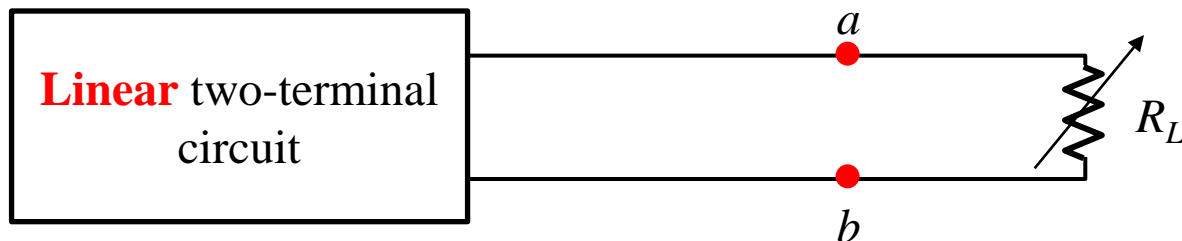
# Contents



## **2.6 Maximum Power Transfer Theorem**

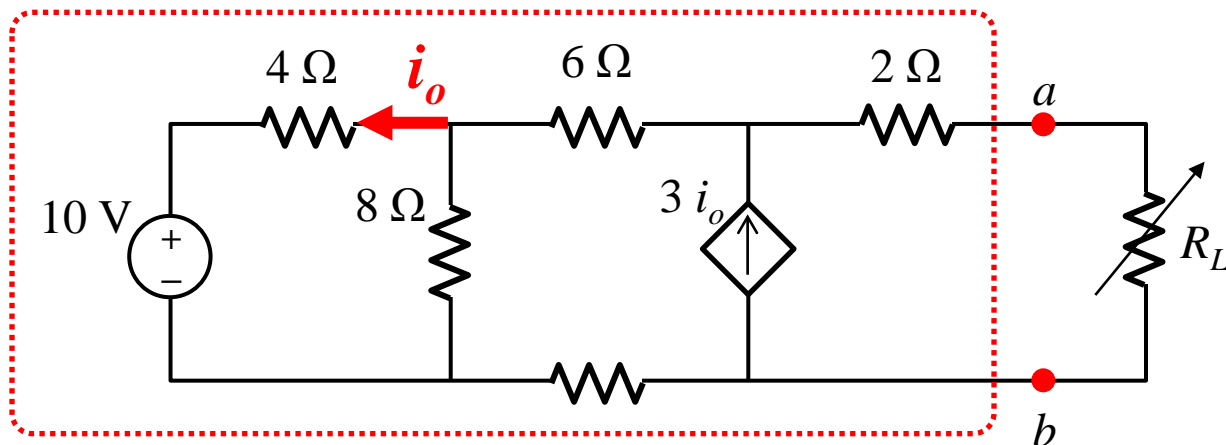


# Objective of This Section



Find the value of  $R_L$  that permits maximum power delivery to it

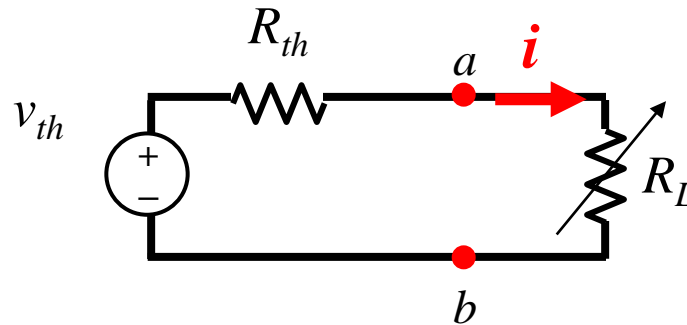
- The linear two-terminal circuit can be arbitrarily assigned, such as





# Solution to This Problem

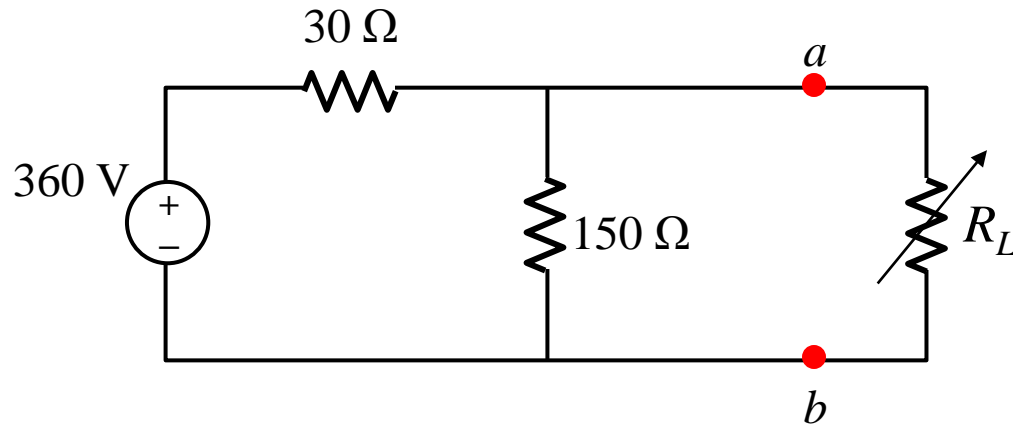
- To simplify the problem, we replace the two-terminal circuit with its Thévenin equivalent circuit



- The power on  $R_L$ :  $P = i^2 R_L = \left( \frac{v_{th}}{R_{th} + R_L} \right)^2 R_L$
- In order to have the maximum power transfer, let  $\frac{dP}{dR_L} = 0$
- Solution: when  $R_L = R_{th}$ ,  $P_{\max} = \left( \frac{v_{th}}{2R_L} \right)^2 R_L = \frac{v_{th}^2}{4R_L}$

## Ex. 2.24

# Maximum Power Transfer



1. Find the value of  $R_L$  that results in maximum power transferred to  $R_L$
2. Calculate the maximum power  $P_{max}$  that can be delivered to  $R_L$
3. When  $R_L$  is adjusted for maximum power transfer, what percentage of the power delivered by the 360 V source reaches  $R_L$ ?