

## TLV61220 采用薄型 SOT-23 封装的低输入电压升压转换器

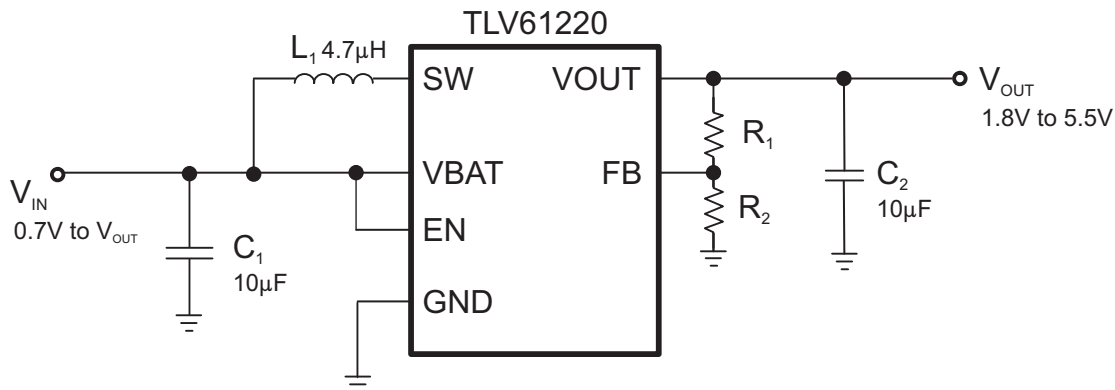
### 1 特性

- 在典型工作条件下效率高达 95%
- 5.5 $\mu$ A 静态电流
- 负载的启动输入电压为 0.7V
- 运行输入电压范围为 0.7V 至 5.5V
- 停机期间具有导通功能
- 最小开关电流为 200mA
- 保护特性：
  - 输出过压
  - 过热
  - 输入欠压闭锁
- 可调节输出电压范围为 1.8V 至 5.5V
- 小型 6 引脚超薄小外形尺寸晶体管 (SOT)-23 封装

### 2 应用范围

- 电池供电类 应用
  - 1 至 3 节碱性电池、镍镉电池 (NiCd) 或者镍氢电池 (NiMH)
  - 1 节锂离子或者锂离子一次性电池
- 太阳能或燃料电池供电 应用
- 消费类及便携式医疗产品
- 个人护理产品
- 白色或者状态发光二极管 (LED)
- 智能电话

### 4 典型应用电路原理图



### 3 说明

TLV61220 器件可以为由单节、2 节或 3 节碱性、镍镉或镍氢电池或单节锂离子或锂聚合物电池供电的产品提供电源解决方案。可实现的输出电流取决于输入输出电压比。升压转换器建立在采用同步整流的磁滞控制器拓扑基础之上，能够以最少的静态电流实现最高的效率。可通过一个外部电阻分压器对此可调版本的输出电压进行设定，或者可将此电压内部设定为一个固定值。此转换器可由一个特定的使能引脚关闭。关闭时，电池消耗降至最低。此器件采用一个 6 引脚超薄 SOT-23 封装 (DBV)。

器件信息<sup>(1)</sup>

器件型号	封装	封装尺寸 (标称值)
TLV61220	SOT (6)	2.90mm x 1.60mm

(1) 如需了解所有可用封装，请见数据表末尾的可订购产品附录。



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## 5 修订历史记录

### Changes from Original (May 2012) to Revision A

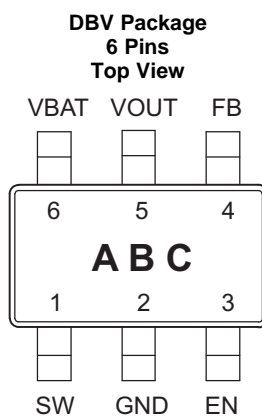
### Page

• 已添加 <b>ESD</b> 额定值表, 特性 描述部分, 器件功能模式, 应用和 实施部分, 电源相关建议部分, 布局部分, 器件和文 档支持部分以及 机械、封装和可订购信息部分 .....	1
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## 6 Device Options

T <sub>A</sub>	OUTPUT VOLTAGE DC/DC	PACKAGE	PART NUMBER
–40°C to 85°C	Adjustable	6-Pin SOT-23	TLV61220DBV

## 7 Pin Configuration and Functions



### Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
EN	3	I	Enable input (VBAT enabled, GND disabled)
FB	4	I	Voltage feedback for programming the output voltage
GND	2	—	IC ground connection for logic and power
SW	1	I	Boost and rectifying switch input
VBAT	6	I	Supply voltage
VOUT	5	O	Boost converter output

## 8 Specifications

### 8.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) <sup>(1)</sup>

		MIN	MAX	UNIT
V <sub>IN</sub>	Input voltage on VBAT, SW, VOUT, EN, FB	−0.3	7.5	V
T <sub>J</sub>	Operating junction temperature	−40	150	°C
T <sub>stg</sub>	Storage temperature	−65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### 8.2 ESD Ratings

		VALUE	UNIT
V <sub>(ESD)</sub> Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	V
	Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	±1500	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 8.3 Recommended Operating Conditions

		MIN	NOM	MAX	UNIT
V <sub>IN</sub>	Supply voltage at VIN	0.7		5.5	V
T <sub>A</sub>	Operating free air temperature range	−40		85	°C
T <sub>J</sub>	Operating virtual junction temperature range	−40		125	°C

### 8.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		TLV61220	UNIT
		DBV	
		6 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	185.7	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	124.3	
R <sub>θJB</sub>	Junction-to-board thermal resistance	31.3	
ψ <sub>JT</sub>	Junction-to-top characterization parameter	22.9	
ψ <sub>JB</sub>	Junction-to-board characterization parameter	30.8	
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	N/A	

- (1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](#).

## 8.5 Electrical Characteristics

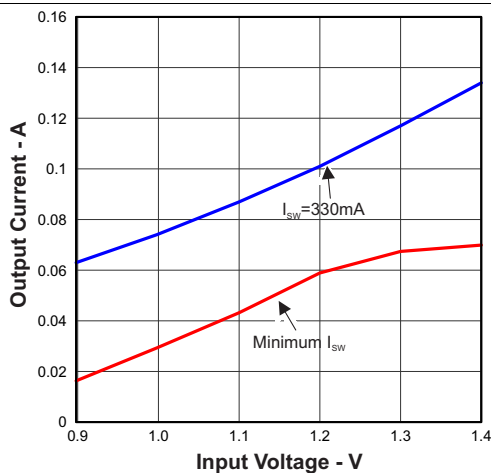
over recommended free-air temperature range and over recommended input voltage range (typical at an ambient temperature range of 25°C) (unless otherwise noted)

PARAMETER			TEST CONDITIONS	MIN	TYP	MAX	UNIT
DC/DC STAGE							
V <sub>IN</sub>	Input voltage range			0.7		5.5	V
V <sub>IN</sub>	Minimum input voltage at startup		R <sub>Load</sub> ≥ 150 Ω			0.7	V
V <sub>OUT</sub>	TLV61220 output voltage range		V <sub>IN</sub> < V <sub>OUT</sub>	1.8		5.5	V
V <sub>FB</sub>	TLV61220 feedback voltage			483	500	513	mV
I <sub>LH</sub>	Inductor current ripple			200			mA
I <sub>SW</sub>	switch current limit		V <sub>OUT</sub> = 3.3 V, V <sub>IN</sub> = 1.2 V, T <sub>A</sub> = 25 °C	220	400		mA
			V <sub>OUT</sub> = 3.3 V, T <sub>A</sub> = -40°C to 85 °C	180	400		mA
			V <sub>OUT</sub> = 3.3 V, T <sub>A</sub> = 0°C to 85 °C	200	400		mA
R <sub>DS(on)</sub>	Rectifying switch on resistance, HSD	V <sub>OUT</sub> = 3.3 V	1000			mΩ	
		V <sub>OUT</sub> = 5 V	700			mΩ	
	Main switch on resistance, LSD	V <sub>OUT</sub> = 3.3 V	600			mΩ	
		V <sub>OUT</sub> = 5 V	550			mΩ	
	Line regulation		V <sub>IN</sub> < V <sub>OUT</sub>	0.5%			
	Load regulation		V <sub>IN</sub> < V <sub>OUT</sub>	0.5%			
I <sub>Q</sub>	Quiescent current	V <sub>IN</sub>	I <sub>O</sub> = 0 mA, V <sub>EN</sub> = V <sub>IN</sub> = 1.2 V, V <sub>OUT</sub> = 3.3 V	0.5		0.9	μA
		V <sub>OUT</sub>		5		7.5	μA
I <sub>SD</sub>	Shutdown current	V <sub>IN</sub>	V <sub>EN</sub> = 0 V, V <sub>IN</sub> = 1.2 V, V <sub>OUT</sub> ≥ V <sub>IN</sub>	0.2		0.5	μA
I <sub>LKG</sub>	Leakage current into VOUT		V <sub>EN</sub> = 0 V, V <sub>IN</sub> = 1.2 V, V <sub>OUT</sub> = 3.3 V	1			μA
	Leakage current into SW		V <sub>EN</sub> = 0 V, V <sub>IN</sub> = 1.2 V, V <sub>SW</sub> = 1.2 V, V <sub>OUT</sub> ≥ V <sub>IN</sub>	0.01		0.2	μA
I <sub>FB</sub>	TLV61220 Feedback input current		V <sub>FB</sub> = 0.5 V	0.01			μA
I <sub>EN</sub>	EN input current		Clamped on GND or V <sub>IN</sub> (V <sub>IN</sub> < 1.5 V)	0.005		0.1	μA
CONTROL STAGE							
V <sub>IL</sub>	EN input low voltage		V <sub>IN</sub> ≤ 1.5 V			0.2 × V <sub>IN</sub>	V
V <sub>IH</sub>	EN input high voltage		V <sub>IN</sub> ≤ 1.5 V	0.8 × V <sub>IN</sub>			V
V <sub>IL</sub>	EN input low voltage		5 V > V <sub>IN</sub> > 1.5 V			0.4	V
V <sub>IH</sub>	EN input high voltage		5 V > V <sub>IN</sub> > 1.5 V	1.2			V
V <sub>UVLO</sub>	Undervoltage lockout threshold for turn off		V <sub>IN</sub> decreasing	0.5		0.7	V
Overvoltage protection threshold				5.5		7.5	V
Overtemperature protection				140			°C
Overtemperature hysteresis				20			°C

## 8.6 Typical Characteristics

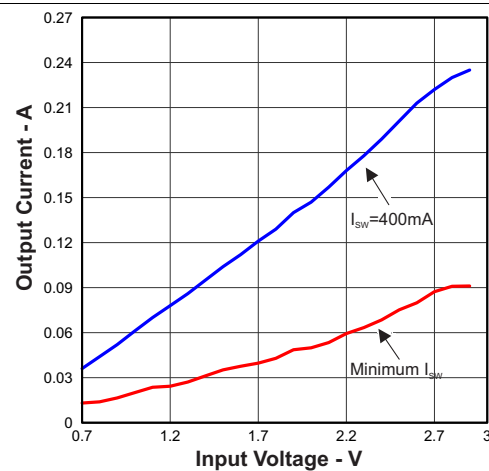
Table 1. Table of Graphs

		FIGURE
Output Current	Input Voltage, $I_{SW} = 330\text{ mA}$ , Minimum $I_{SW} = 200\text{ mA}$ , $V_O = 1.8\text{ V}$	Figure 1
	Input Voltage, $I_{SW} = 400\text{ mA}$ , Minimum $I_{SW} = 200\text{ mA}$ , $V_O = 3.3\text{ V}$	Figure 2
	Input Voltage, $I_{SW} = 380\text{ mA}$ , Minimum $I_{SW} = 200\text{ mA}$ , $V_O = 5\text{ V}$	Figure 3
Efficiency	vs Output Current, $V_O = 1.8\text{ V}$ , $V_I = [0.7\text{ V}; 1.2\text{ V}; 1.5\text{ V}]$	Figure 4
	vs Output Current, $V_O = 3.3\text{ V}$ , $V_I = [0.7\text{ V}; 1.2\text{ V}; 2.4\text{ V}; 3\text{ V}]$	Figure 5
	vs Output Current, $V_O = 5\text{ V}$ , $V_I = [0.7\text{ V}; 1.2\text{ V}; 3.6\text{ V}; 4.2\text{ V}]$	Figure 6
Efficiency	vs Input Voltage, $V_O = 1.8\text{ V}$ , $I_O = [100\mu\text{A}; 1\text{ mA}; 10\text{ mA}; 50\text{ mA}]$	Figure 7
	vs Input Voltage, $V_O = 3.3\text{ V}$ , $I_O = [100\mu\text{A}; 1\text{ mA}; 10\text{ mA}; 50\text{ mA}]$	Figure 8
	vs Input Voltage, $V_O = 5\text{ V}$ , $I_O = [100\mu\text{A}; 1\text{ mA}; 10\text{ mA}; 50\text{ mA}]$	Figure 9
Output Voltage	vs Output Current, $V_O = 1.8\text{ V}$ , $V_I = [0.7\text{ V}; 1.2\text{ V}]$	Figure 10
	vs Output Current, $V_O = 3.3\text{ V}$ , $V_I = [0.7\text{ V}; 1.2\text{ V}; 2.4\text{ V}]$	Figure 11



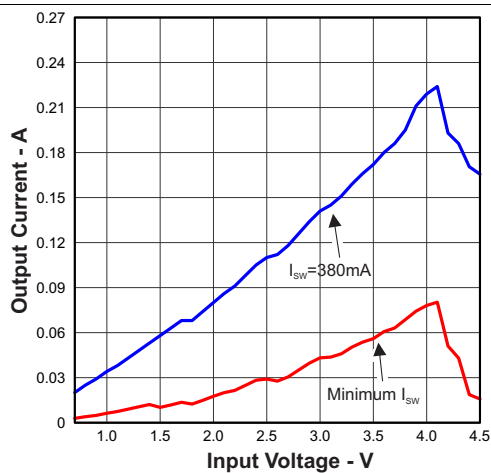
$V_O = 1.8\text{ V}$

Figure 1. Maximum Output Current vs Input Voltage



$V_O = 3.3\text{ V}$

Figure 2. Maximum Output Current vs Input Voltage



$V_O = 5\text{ V}$

Figure 3. Maximum Output Current vs Input Voltage

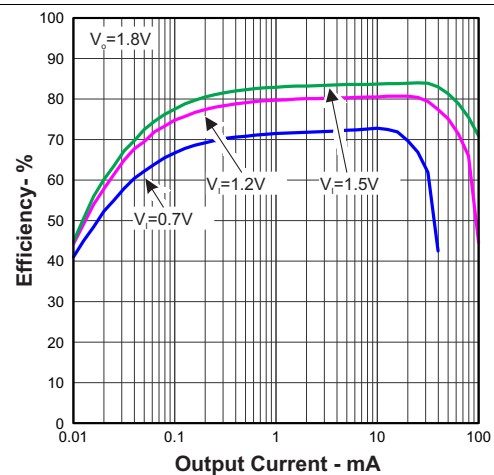
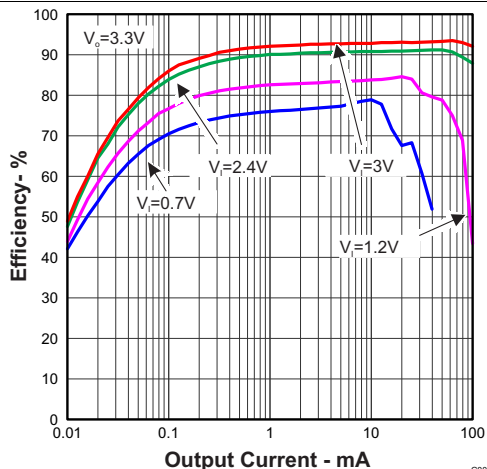
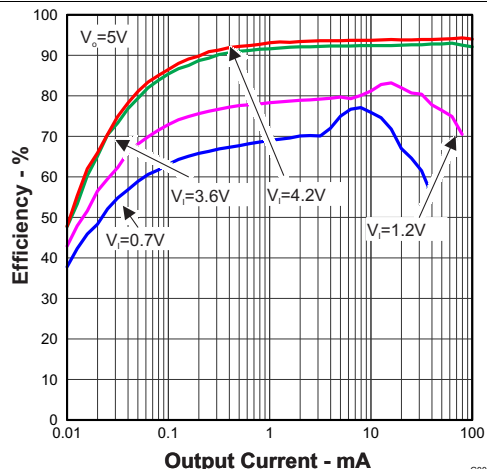


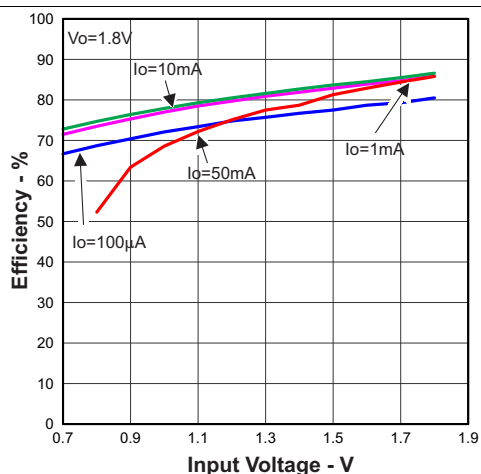
Figure 4. Efficiency vs Output Current and Input Voltage



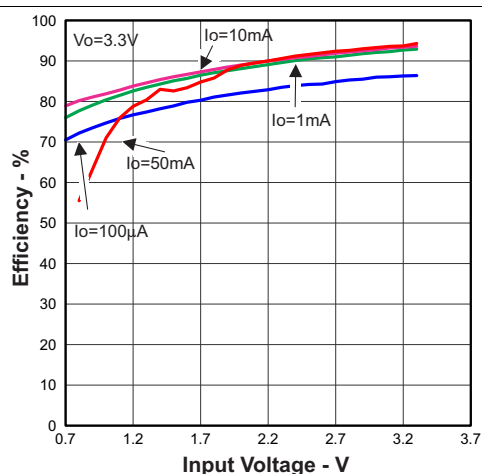
**Figure 5. Efficiency vs Output Current and Input Voltage**



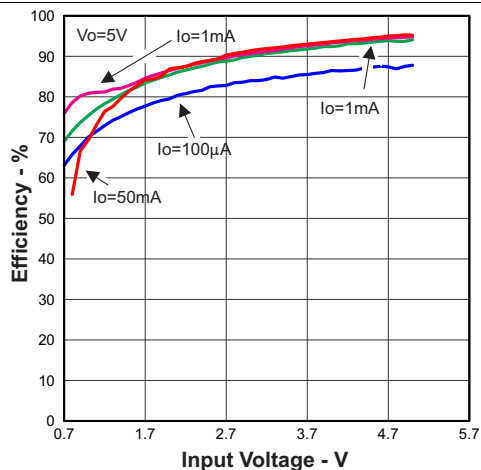
**Figure 6. Efficiency vs Input Voltage and Output Current**



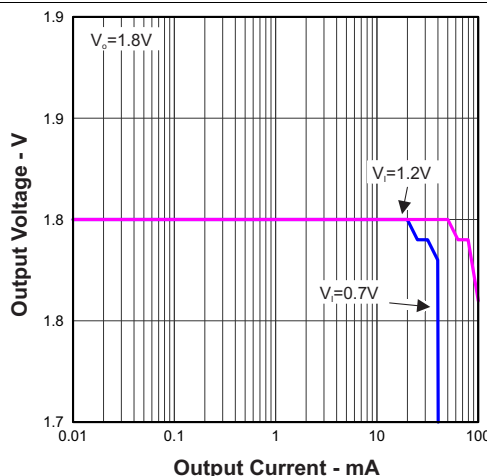
**Figure 7. Efficiency vs Input Voltage and Output Current**



**Figure 8. Efficiency vs Input Voltage and Output Current**



**Figure 9. Efficiency vs Input Voltage and Output Current**

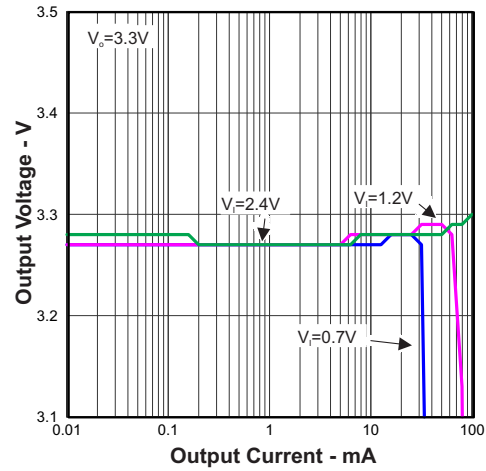


**Figure 10. Output Voltage vs Output Current and Input Voltage**

**TLV61220**

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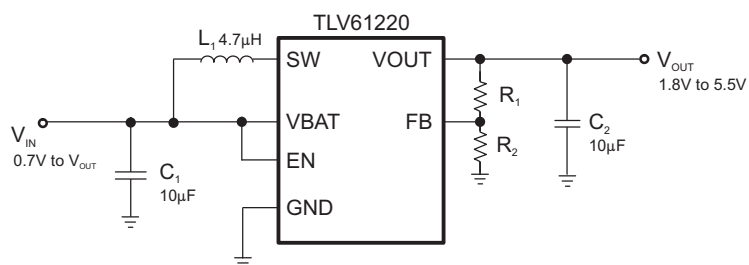
[www.ti.com.cn](http://www.ti.com.cn)



**Figure 11. Output Voltage vs Output Current and Input Voltage**



## 9 Parameter Measurement Information



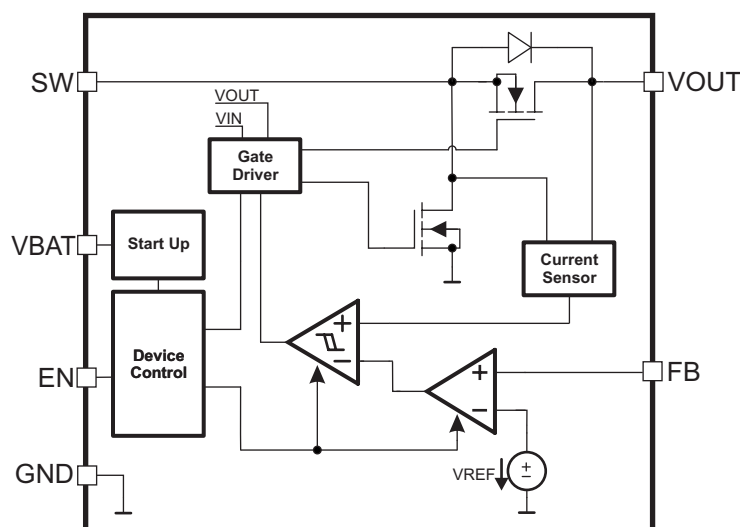
**Figure 12. Parameter Measurement Schematic**

## 10 Detailed Description

### 10.1 Overview

The TLV61220 is a high performance, highly efficient boost converter. To achieve high efficiency the power stage is realized as a synchronous boost topology. For the power switching two actively controlled low  $R_{DS(on)}$  power MOSFETs are implemented.

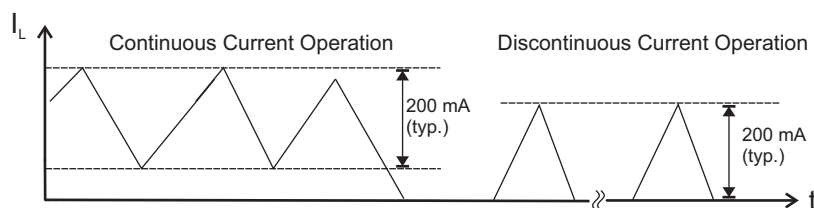
### 10.2 Functional Block Diagram



### 10.3 Feature Description

#### 10.3.1 Controller Circuit

The device is controlled by a hysteretic current mode controller. This controller regulates the output voltage by keeping the inductor ripple current constant in the range of 200 mA and adjusting the offset of this inductor current depending on the output load. In case the required average input current is lower than the average inductor current defined by this constant ripple the inductor current gets discontinuous to keep the efficiency high at low load conditions.



**Figure 13. Hysteretic Current Operation**

The output voltage  $V_{OUT}$  is monitored via the feedback network which is connected to the voltage error amplifier. To regulate the output voltage, the voltage error amplifier compares this feedback voltage to the internal voltage reference and adjusts the required offset of the inductor current accordingly. An external resistor divider needs to be connected.

The self oscillating hysteretic current mode architecture is inherently stable and allows fast response to load variations. It also allows using inductors and capacitors over a wide value range.

## **Feature Description (continued)**

### **10.3.1.1 Startup**

After the EN pin is tied high, the device starts to operate. In case the input voltage is not high enough to supply the control circuit properly a startup oscillator starts to operate the switches. During this phase the switching frequency is controlled by the oscillator and the maximum switch current is limited. As soon as the device has built up the output voltage to about 1.8 V, high enough for supplying the control circuit, the device switches to its normal hysteretic current mode operation. The startup time depends on input voltage and load current.

### **10.3.1.2 Operation at Output Overload**

If in normal boost operation the inductor current reaches the internal switch current limit threshold the main switch is turned off to stop further increase of the input current.

In this case the output voltage will decrease since the device can not provide sufficient power to maintain the set output voltage.

If the output voltage drops below the input voltage the backgate diode of the rectifying switch gets forward biased and current starts flow through it. This diode cannot be turned off, so the current finally is only limited by the remaining DC resistances. As soon as the overload condition is removed, the converter resumes providing the set output voltage.

### **10.3.1.3 Undervoltage Lockout**

An implemented undervoltage lockout function stops the operation of the converter if the input voltage drops below the typical undervoltage lockout threshold. This function is implemented in order to prevent malfunctioning of the converter.

### **10.3.1.4 Overvoltage Protection**

If, for any reason, the output voltage is not fed back properly to the input of the voltage amplifier, control of the output voltage will not work anymore. Therefore an overvoltage protection is implemented to avoid the output voltage exceeding critical values for the device and possibly for the system it is supplying. For this protection the TLV61220 output voltage is also monitored internally. In case it reaches the internally programmed threshold of 6.5 V typically the voltage amplifier regulates the output voltage to this value.

If the TLV61220 is used to drive LEDs, this feature protects the circuit if the LED fails.

### **10.3.1.5 Overtemperature Protection**

The device has a built-in temperature sensor which monitors the internal IC junction temperature. If the temperature exceeds the programmed threshold (see electrical characteristics table), the device stops operating. As soon as the IC temperature has decreased below the programmed threshold, it starts operating again. To prevent unstable operation close to the region of overtemperature threshold, a built-in hysteresis is implemented.

## **10.4 Device Functional Modes**

### **10.4.1 Device Enable and Shutdown Mode**

The device is enabled when EN is set high and shut down when EN is low. During shutdown, the converter stops switching and all internal control circuitry is turned off. In this case the input voltage is connected to the output through the back-gate diode of the rectifying MOSFET. This means that there always will be voltage at the output which can be as high as the input voltage or lower depending on the load.

## 11 Application and Implementation

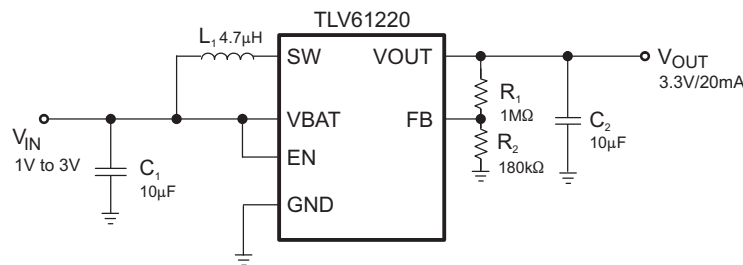
### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 11.1 Application Information

The TLV61220 is intended for systems powered by a single cell battery to up to three Alkaline, NiCd or NiMH cells with a typical terminal voltage between 0.7 V and 5.5 V. It can also be used in systems powered by one-cell Li-Ion or Li-Polymer batteries with a typical voltage between 2.5 V and 4.2 V. Additionally, any other voltage source with a typical output voltage between 0.7 V and 5.5 V can be used with the TLV61220.

### 11.2 Typical Application



**Figure 14. Typical Application Circuit for Adjustable Output Voltage Option**

#### 11.2.1 Design Requirements

In this example, TLV61220 is used to design a 3.3-V power supply with up to 50-mA output current capability. The TLV61220 can be powered by a single-cell battery to up to three Alkaline, NiCd or NiMH cells with a typical terminal voltage between 0.7 V and 5.5 V. It can also be used in systems powered by one-cell Li-Ion or Li-Polymer batteries with a typical voltage between 2.5 V and 4.2 V. In this example, the input voltage range is from 2 V to 3 V for one-cell coin cell battery input design.

**Table 2. TLV61220 3.3 V Output Design Requirements**

PARAMETERS	VALUES
Input Voltage	2 V to 3 V
Output Voltage	3.3 V
Output Current	50 mA

#### 11.2.2 Detailed Design Procedure

**Table 3. List of Components**

COMPONENT REFERENCE	PART NUMBER	MANUFACTURER	VALUE
C <sub>1</sub>	GRM188R60J106ME84D	Murata	10 µF, 6.3V. X5R Ceramic
C <sub>2</sub>	GRM188R60J106ME84D	Murata	10 µF, 6.3V. X5R Ceramic
L <sub>1</sub>	1269AS-H-4ZR7N	Toko	4.7 µH
R <sub>1</sub> , R <sub>2</sub>			R <sub>1</sub> = 1MΩ, R <sub>2</sub> = Values depending on the programmed output voltage

### 11.2.2.1 Adjustable Output Voltage Version

An external resistor divider is used to adjust the output voltage. The resistor divider needs to be connected between VOUT, FB and GND as shown in [Figure 14](#). When the output voltage is regulated properly, the typical voltage value at the FB pin is 500 mV. The maximum recommended value for the output voltage is 5.5 V. The current through the resistive divider should be about 100 times greater than the current into the FB pin. The typical current into the FB pin is 0.01  $\mu$ A, and the voltage across the resistor between FB and GND,  $R_2$ , is typically 500 mV. Based on those two values, the recommended value for  $R_2$  should be lower than 500 k $\Omega$ , in order to set the divider current to 1  $\mu$ A or higher. The value of the resistor connected between VOUT and FB,  $R_1$ , depending on the needed output voltage ( $V_{OUT}$ ), can be calculated using [Equation 1](#):

$$R_1 = R_2 \times \left( \frac{V_{OUT}}{V_{FB}} - 1 \right) \quad (1)$$

As an example, if an output voltage of 3.3 V is needed, a 1-M $\Omega$  resistor is calculated for  $R_1$  when for  $R_2$  a 180-k $\Omega$  has been selected.

### 11.2.2.2 Inductor Selection

To make sure that the TLV61220 can operate, a suitable inductor must be connected between pin VBAT and pin SW. Inductor values of 4.7  $\mu$ H show good performance over the whole input and output voltage range .

Choosing other inductance values affects the switching frequency  $f$  proportional to  $1/L$  as shown in [Equation 2](#).

$$L = \frac{1}{f \times 200 \text{ mA}} \times \frac{V_{IN} \times (V_{OUT} - V_{IN})}{V_{OUT}} \quad (2)$$

Choosing inductor values higher than 4.7  $\mu$ H can improve efficiency due to reduced switching frequency and, therefore, with reduced switching losses. Using inductor values below 2.2  $\mu$ H is not recommended.

Having selected an inductance value, the peak current for the inductor in steady state operation can be calculated. [Equation 3](#) gives the peak current estimate.

$$I_{L,MAX} = \begin{cases} \frac{V_{OUT} \times I_{OUT}}{0.8 \times V_{IN}} + 100 \text{ mA}; & \text{continuous current operation} \\ 200 \text{ mA}; & \text{discontinuous current operation} \end{cases} \quad (3)$$

For selecting the inductor this would be the suitable value for the current rating. It also needs to be taken into account that load transients and error conditions may cause higher inductor currents.

[Equation 4](#) helps to estimate whether the device will work in continuous or discontinuous operation depending on the operating points. As long as the inequation is true, continuous operation is typically established. If the inequation becomes false, discontinuous operation is typically established.

$$\frac{V_{OUT} \times I_{OUT}}{V_{IN}} > 0.8 \times 100 \text{ mA} \quad (4)$$

The following inductor series from different suppliers have been used with TLV61220 converters:

**Table 4. List of Inductors**

VENDOR	INDUCTOR SERIES
Toko	DFE252010C
Coilcraft	EPL3015
	EPL2010
Murata	LQH3NP
Taiyo Yuden	NR3015
Würth Elektronik	WE-TPC Typ S

### 11.2.2.3 Capacitor Selection

#### 11.2.2.3.1 Input Capacitor

At least a 10-μF input capacitor is recommended to improve transient behavior of the regulator and EMI behavior of the total power supply circuit. A ceramic capacitor placed as close as possible to the VBAT and GND pins of the IC is recommended.

#### 11.2.2.3.2 Output Capacitor

For the output capacitor  $C_2$ , it is recommended to use small ceramic capacitors placed as close as possible to the VOUT and GND pins of the IC. If, for any reason, the application requires the use of large capacitors which can not be placed close to the IC, the use of a small ceramic capacitor with an capacitance value of around 2.2μF in parallel to the large one is recommended. This small capacitor should be placed as close as possible to the VOUT and GND pins of the IC.

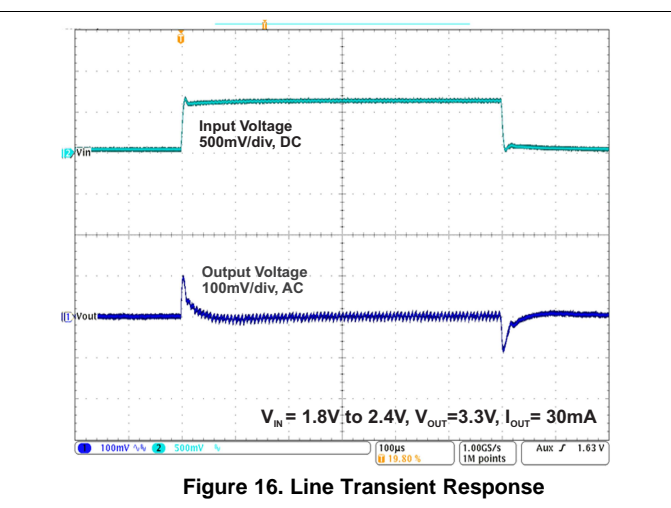
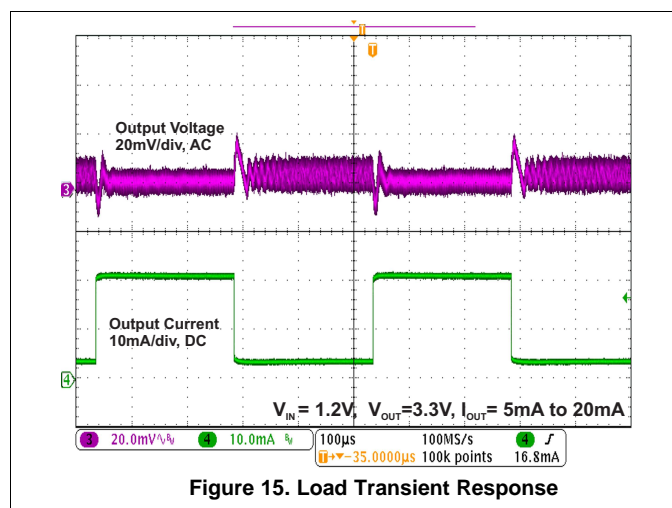
A minimum capacitance value of 4.7 μF should be used, 10 μF are recommended. If the inductor value exceeds 4.7 μH, the value of the output capacitance value needs to be half the inductance value or higher for stability reasons, see [Equation 5](#).

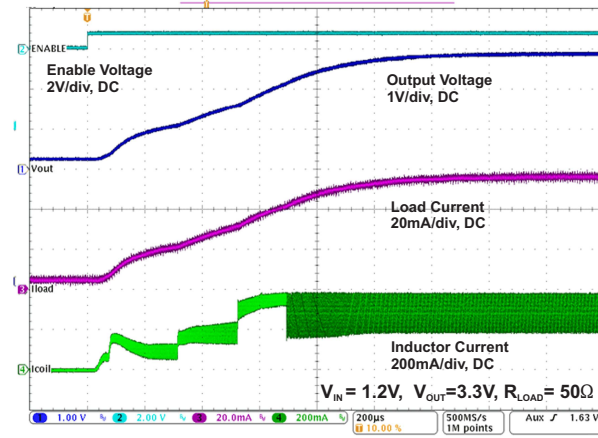
$$C_2 \geq \frac{L}{2} \times \frac{\mu F}{\mu H} \quad (5)$$

The TLV61220 is not sensitive to the ESR in terms of stability. Using low ESR capacitors, such as ceramic capacitors, is recommended anyway to minimize output voltage ripple. If heavy load changes are expected, the output capacitor value should be increased to avoid output voltage drops during fast load transients.

### 11.2.3 Application Curves

	FIGURE
Load transient, $V_I = 1.2\text{ V}$ , $V_O = 3.3\text{ V}$ , $I_O = 5\text{ mA}$ to $20\text{ mA}$	<a href="#">Figure 15</a>
Line transient, $V_I = 1.8\text{ V}$ to $2.4\text{ V}$ , $V_O = 3.3\text{ V}$ , $I_O = 30\text{ mA}$	<a href="#">Figure 16</a>
Startup after Enable, $V_I = 1.2\text{ V}$ , $V_O = 3.3\text{ V}$ , $R_{LOAD} = 50\ \Omega$	<a href="#">Figure 17</a>





**Figure 17. Start Up After Enable**

## 12 Power Supply Recommendations

The power supply can be single-cell, two-cell, or three-cell alkaline, NiCd or NiMH, or one-cell Li-Ion or Li-polymer battery.

The input supply should be well regulated with the rating of TLV61220. If the input supply is located more than a few inches from the device, additional bulk capacitance may be required in addition to the ceramic bypass capacitors. An electrolytic or tantalum capacitor with a value of 47  $\mu\text{F}$  is a typical choice.

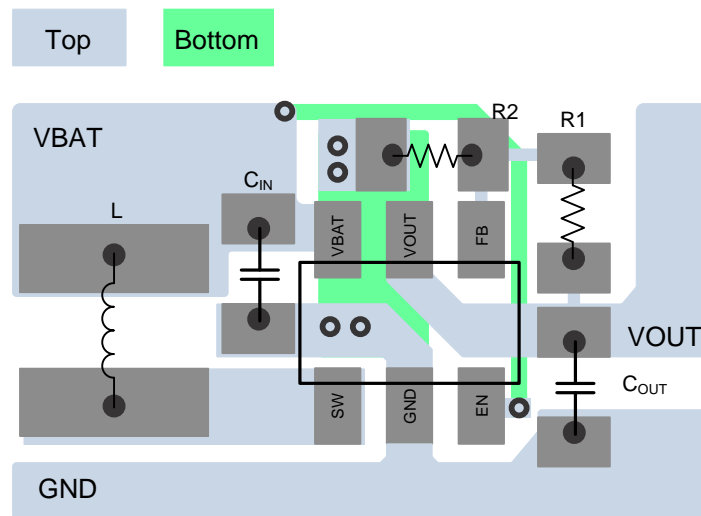
## 13 Layout

### 13.1 Layout Guidelines

As for all switching power supplies, the layout is an important step in the design, especially at high peak currents and high switching frequencies. If the layout is not carefully done, the regulator could show stability problems as well as EMI problems. Therefore, use wide and short traces for the main current path and for the power ground paths. The input and output capacitor, as well as the inductor should be placed as close as possible to the IC.

The feedback divider should be placed as close as possible to the control ground pin of the IC. To lay out the ground, it is recommended to use short traces as well, separated from the power ground traces. This avoids ground shift problems, which can occur due to superimposition of power ground current and control ground current. Assure that the ground traces are connected close to the device GND pin.

### 13.2 Layout Example



**Figure 18. PCB Layout Recommendation**

### 13.3 Thermal Considerations

Implementation of integrated circuits in low-profile and fine-pitch surface-mount packages typically requires special attention to power dissipation. Many system-dependent issues such as thermal coupling, airflow, added heat sinks and convection surfaces, and the presence of other heat-generating components affect the power-dissipation limits of a given component.

Three basic approaches for enhancing thermal performance are listed below.

- Improving the power-dissipation capability of the PCB design
- Improving the thermal coupling of the component to the PCB
- Introducing airflow in the system

For more details on how to use the thermal parameters in the dissipation ratings table please check the [Thermal Characteristics Application Note \(SZZA017\)](#) and the [IC Package Thermal Metrics Application Note \(SPRA953\)](#).



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### 14.2 文档支持

#### 14.2.1 相关文档

相关文档请参见以下部分：

- 《散热特性数据应用手册》，[SZZA017](#)
- 应用手册《IC 封装热指标》（文献编号：[SPRA953](#)）

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### 14.5 术语表

[SLYZ022](#) — TI 术语表。

这份术语表列出并解释术语、首字母缩略词和定义。

## 15 机械、封装和可订购信息

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接口	<a href="http://www.ti.com.cn/interface">www.ti.com.cn/interface</a>	安防应用	<a href="http://www.ti.com.cn/security">www.ti.com.cn/security</a>
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Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TLV61220DBVR	ACTIVE	SOT-23	DBV	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM	-40 to 85	VUAI	<a href="#">Samples</a>
TLV61220DBVT	ACTIVE	SOT-23	DBV	6	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM	-40 to 85	VUAI	<a href="#">Samples</a>

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**TBD:** The Pb-Free/Green conversion plan has not been defined.

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**TAPE AND REEL INFORMATION**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TLV61220DBVR	SOT-23	DBV	6	3000	178.0	9.0	3.23	3.17	1.37	4.0	8.0	Q3
TLV61220DBVT	SOT-23	DBV	6	250	178.0	9.0	3.23	3.17	1.37	4.0	8.0	Q3

## TAPE AND REEL BOX DIMENSIONS



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TLV61220DBVR	SOT-23	DBV	6	3000	180.0	180.0	18.0
TLV61220DBVT	SOT-23	DBV	6	250	180.0	180.0	18.0

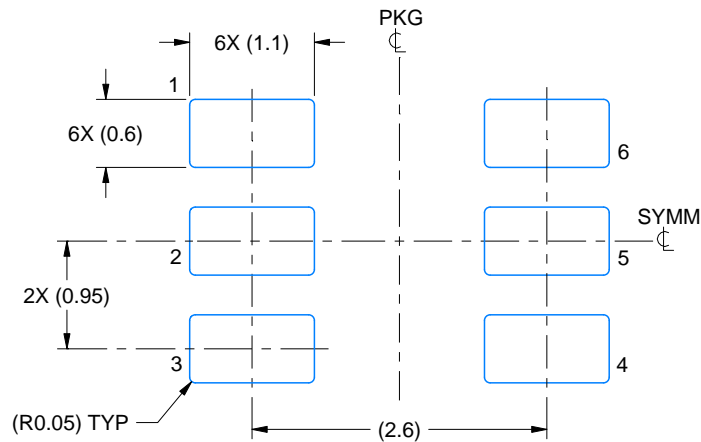


# EXAMPLE BOARD LAYOUT

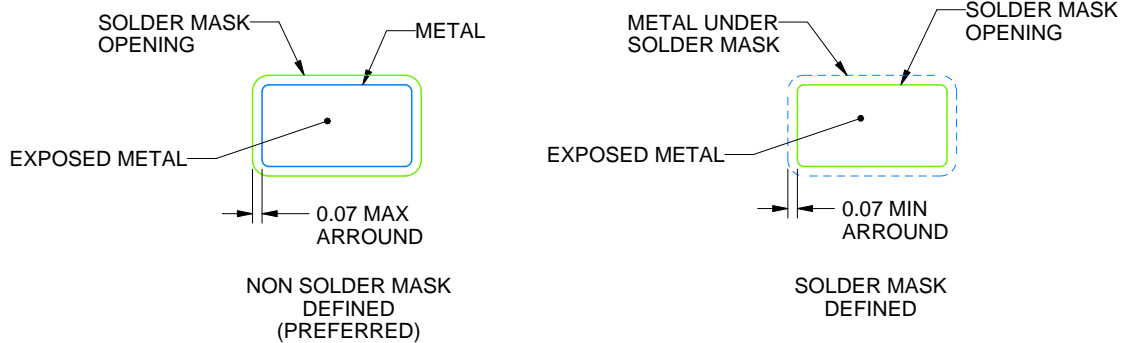
DBV0006A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

4214840/B 03/2018

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

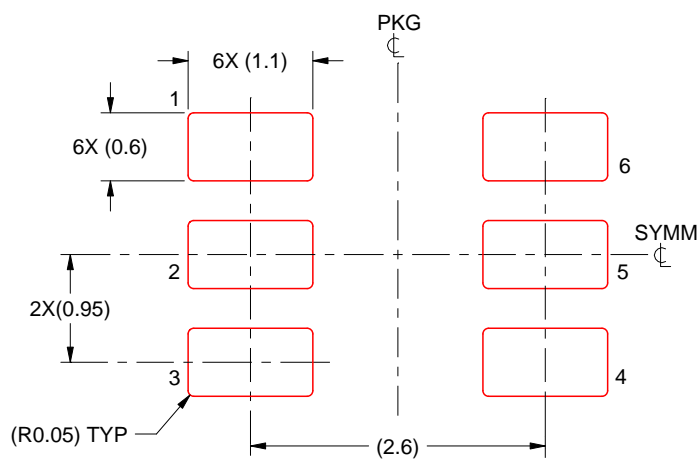


## EXAMPLE STENCIL DESIGN

DBV0006A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

4214840/B 03/2018

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

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