



JOINT INSTITUTE  
交大密西根学院

# ECE2150J Introduction to Circuits

## Chapter 12. Three-Phase Circuits

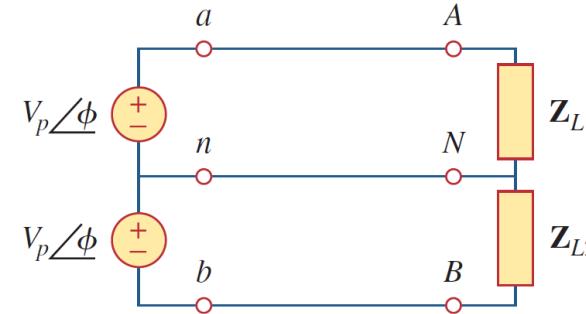
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## 12.1 Introduction



Single phase two wire

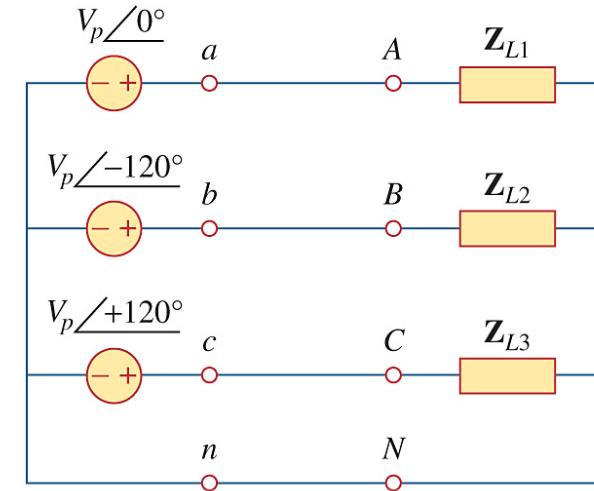
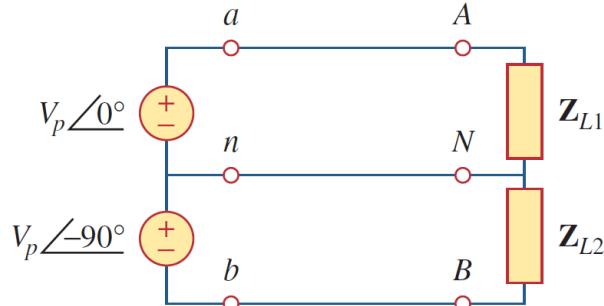


Single phase three wire

**A single-phase** ac power system: a generator connected through a pair of wires to a load.

**A single-phase** three wire system: two identical sources (equal magnitude and the same phase) connected to two loads by two outer wires and the neutral.

**Polyphase:** AC sources operate at the same frequency but different phases.



Two-phase three-wire system

Three-phase four-wire system

A three-phase system: Three sources having the same amplitude and frequency but out of phase with each other by  $120^\circ$ . The three-phase system is **by far the most prevalent and most economical polyphase system**.

## **Three-phase systems are important for at least three reasons.**

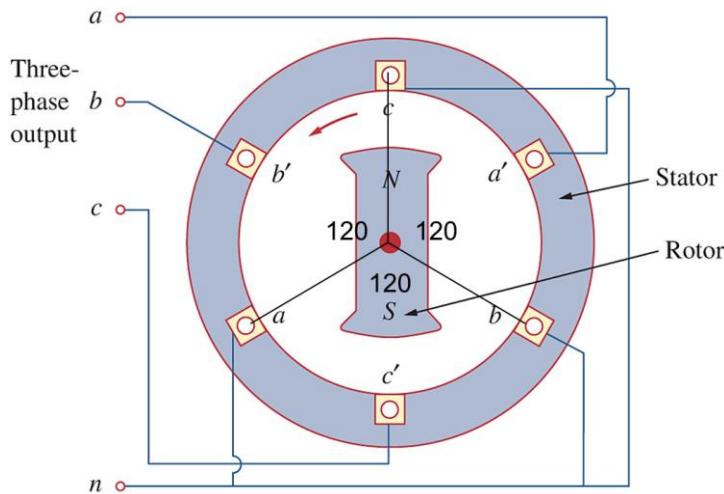
**First**, nearly all electric power is generated and distributed in three-phase, at the operating frequency of 50 or 60 Hz. **Multiphases** can be generated: from 1-2 to even 48 phases.

**Second**, the instantaneous power in a three-phase system can be **constant** (not pulsating). This results in uniform power transmission and less vibration of three-phase machines.

**Third**, for the same amount of power, the three-phase system is **more economical** than the single phase.

## 12.2 Balanced Three-Phase Voltages

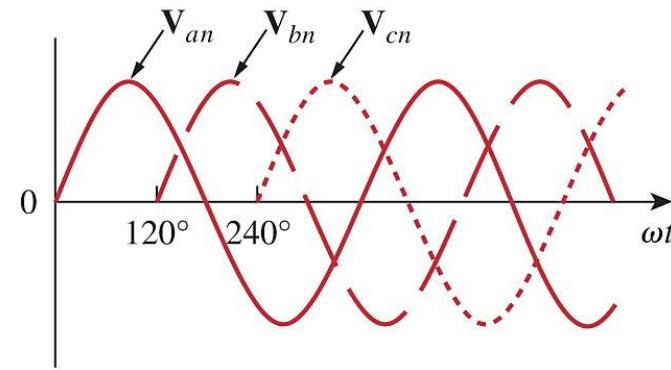
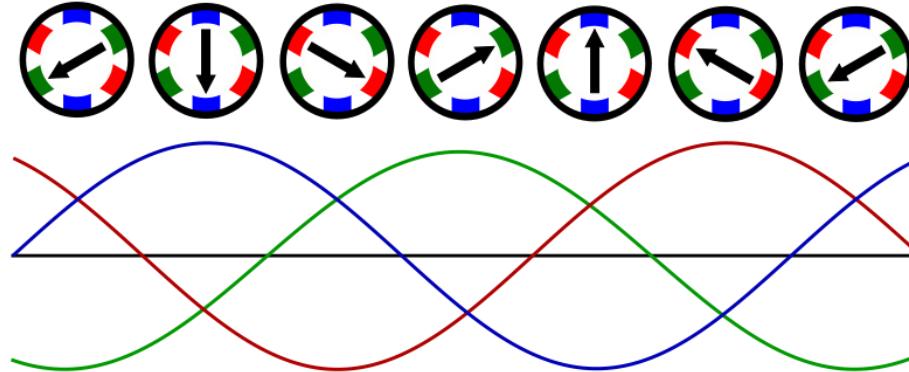
Three-phase voltages are often produced with a three-phase ac generator.



<https://www.tme.eu/>

Rotor: a rotating magnet

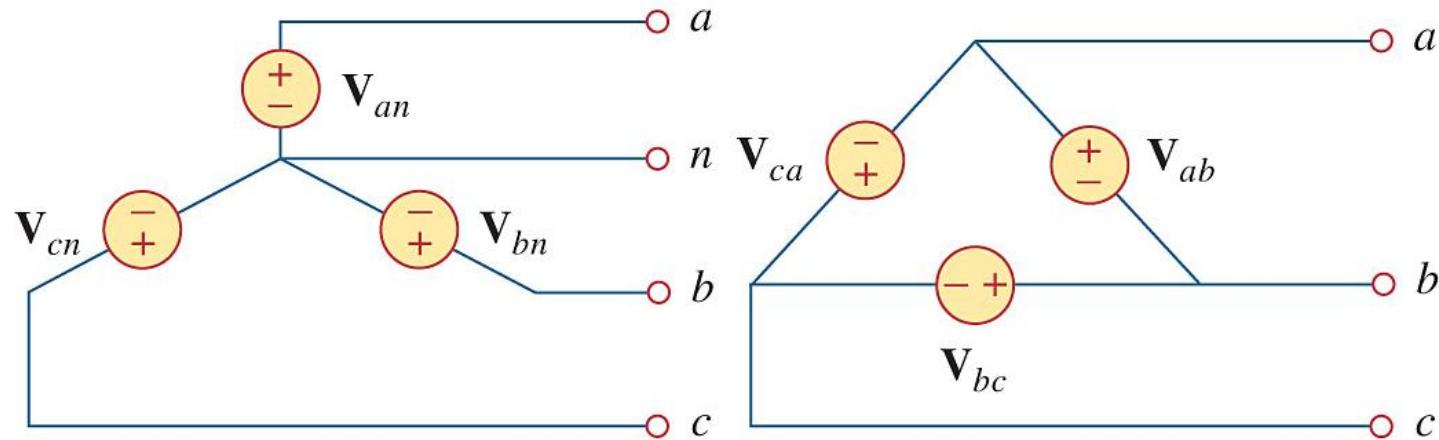
Stator: a stationary winding

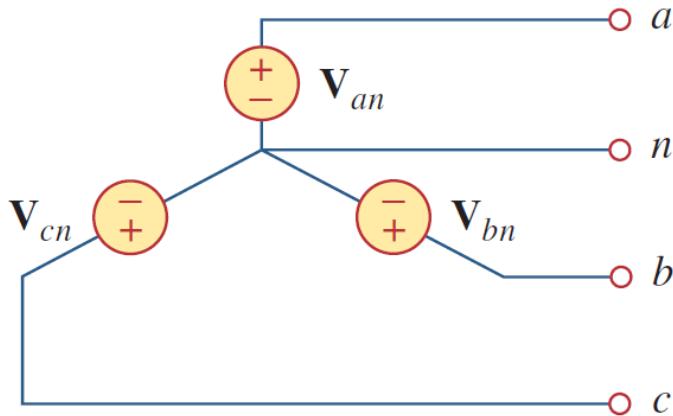


As the rotator rotates, the flux through each coil varies sinusoidally with time, inducing a sinusoidal voltage. Because the coils are placed **120°** apart, the induced voltages are out of phase by **120°**.

# Voltage sources

A typical **three-phase** system consists of three voltage sources connected to loads by three or four wires. A three-phase system is equivalent to three single-phase system. **The voltage sources** can be either **wye- or delta-connected**.





$V_{an}$ ,  $V_{bn}$ , and  $V_{cn}$  are phase voltages.

**Balanced phase voltages:** Equal in magnitude and frequency and are out of phase with each other by  $120^\circ$ . This implies that

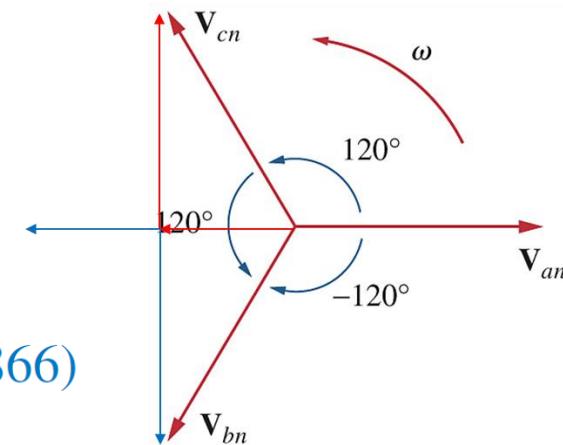
$$(i) |V_{an}| = |V_{bn}| = |V_{cn}|$$

$$(ii) V_{an} + V_{bn} + V_{cn} = 0$$

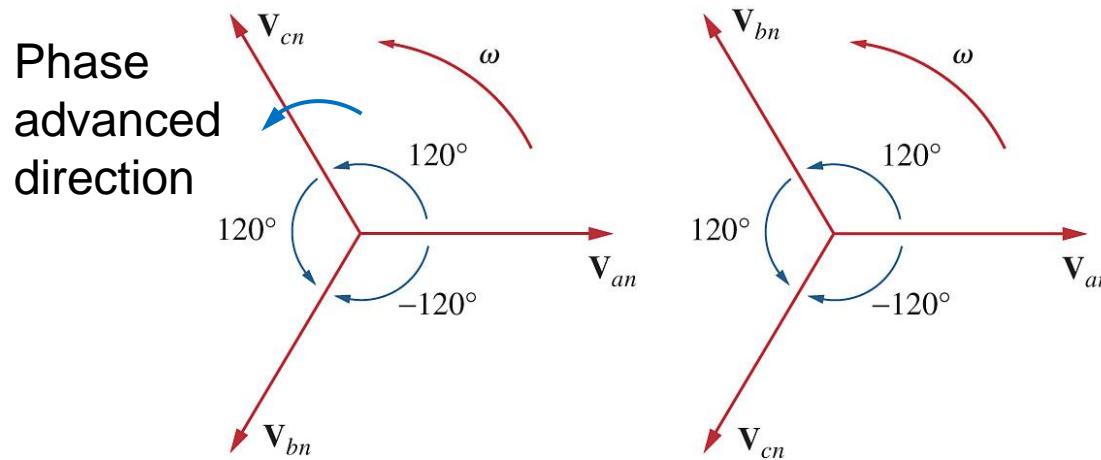
$$= V_p \angle 0^\circ + V_p \angle -120^\circ + V_p \angle +120^\circ$$

$$= V_p(1.0 - 0.5 - j0.866 - 0.5 + j0.866)$$

$$= 0$$



# Phase sequence



$$\mathbf{V}_{an} = V_p \angle 0^\circ$$

$$\mathbf{V}_{bn} = V_p \angle -120^\circ$$

$$\mathbf{V}_{cn} = V_p \angle -240^\circ = V_p \angle +120^\circ$$

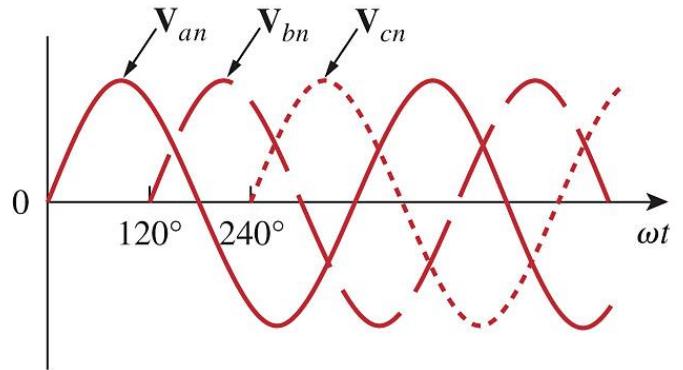
$$\mathbf{V}_{an} = V_p \angle 0^\circ$$

$$\mathbf{V}_{cn} = V_p \angle -120^\circ$$

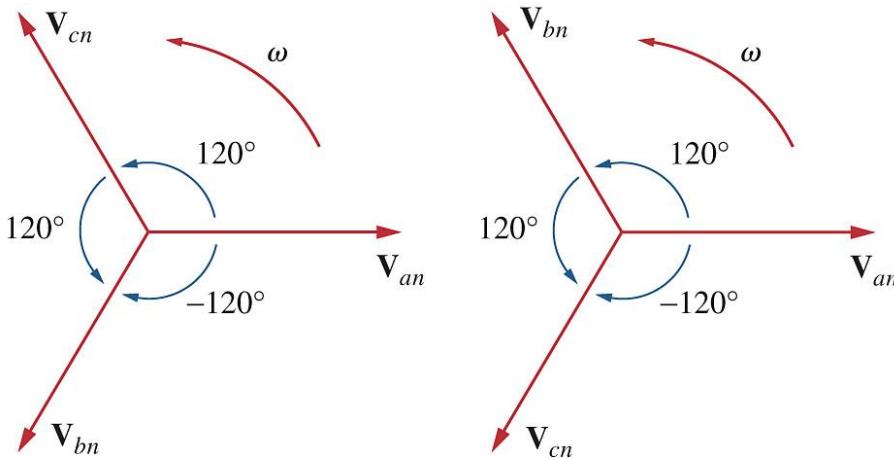
$$\mathbf{V}_{bn} = V_p \angle -240^\circ = V_p \angle +120^\circ$$

\* $V_p$  is the effective (rms) value of the phase voltage

The phase sequence is the time order in which the voltages pass through their respective maximum values.

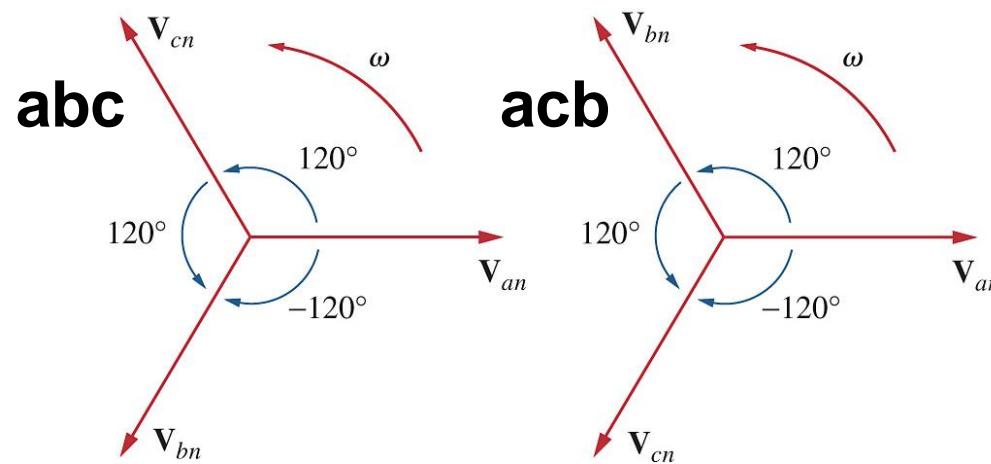


abc: a leads b, b leads c  
(i.e.,  $\angle a > \angle b > \angle c$ )



From which phase the voltage curve above is generated?  
abc or acb sequence?

The phase sequence is determined by the order in which the phasors pass through a fixed point in the phase diagram.



$$\mathbf{V}_{an} = V_p \angle 0^\circ$$

$$\mathbf{V}_{bn} = V_p \angle -120^\circ$$

$$\mathbf{V}_{cn} = V_p \angle -240^\circ = V_p \angle +120^\circ$$

$$\mathbf{V}_{an} = V_p \angle 0^\circ$$

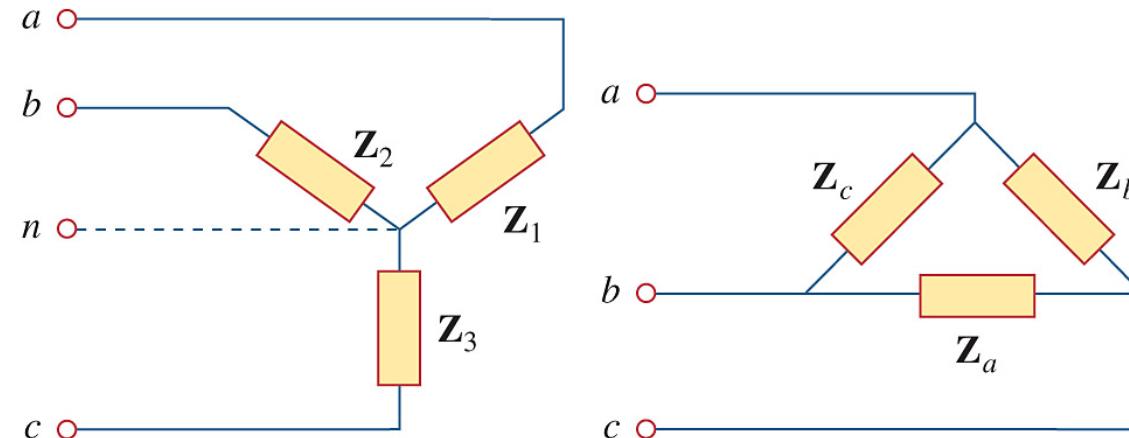
$$\mathbf{V}_{cn} = V_p \angle -120^\circ$$

$$\mathbf{V}_{bn} = V_p \angle -240^\circ = V_p \angle +120^\circ$$

\* $V_p$  is the effective (rms) value of the phase voltage

# Phase load connection

Similar to the source connections, a three-phase load can be either wye-connected or delta-connected



# Balanced Load

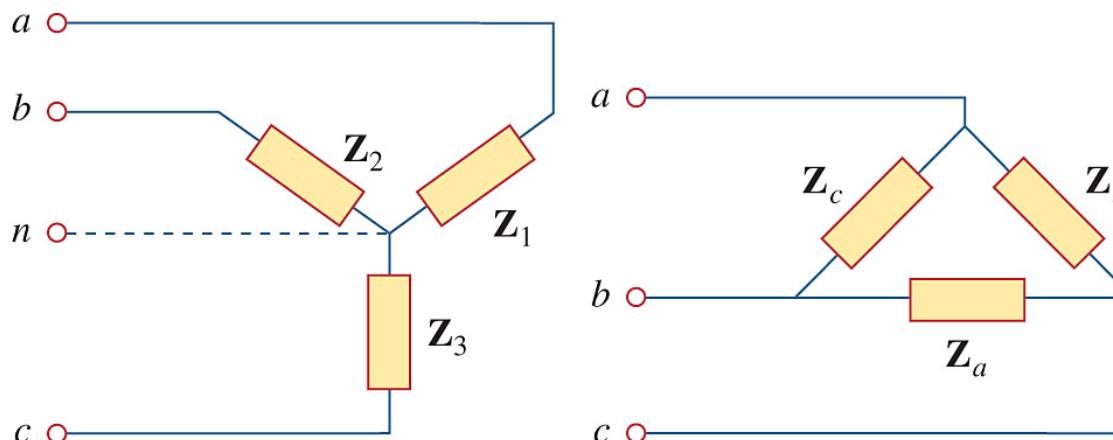
A balanced load is one in which the phase impedances are **equal in magnitude and in phase**.

(i) Balanced wye-connected load:

$$\mathbf{Z}_1 = \mathbf{Z}_2 = \mathbf{Z}_3 = \mathbf{Z}_Y$$

(i) Balanced delta-connected load:

$$\mathbf{Z}_a = \mathbf{Z}_b = \mathbf{Z}_c = \mathbf{Z}_\Delta$$



A wye-connected load can be transformed into a delta-connected load, or vice versa.

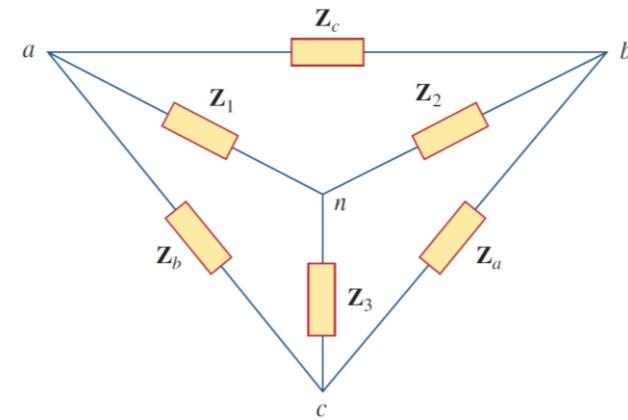
$$Z_{\Delta} = 3Z_Y \text{ or } Z_Y = \frac{1}{3}Z_{\Delta}$$

*Y- $\Delta$  Conversion:*

$$Z_a = \frac{Z_1Z_2 + Z_2Z_3 + Z_3Z_1}{Z_1}$$

$$Z_b = \frac{Z_1Z_2 + Z_2Z_3 + Z_3Z_1}{Z_2}$$

$$Z_c = \frac{Z_1Z_2 + Z_2Z_3 + Z_3Z_1}{Z_3}$$



*$\Delta$ -Y Conversion:*

$$Z_1 = \frac{Z_bZ_c}{Z_a + Z_b + Z_c}$$

$$Z_2 = \frac{Z_cZ_a}{Z_a + Z_b + Z_c}$$

$$Z_3 = \frac{Z_aZ_b}{Z_a + Z_b + Z_c}$$

$$\mathbf{Z}_1 = \mathbf{Z}_2 = \mathbf{Z}_3 = \mathbf{Z}_Y$$

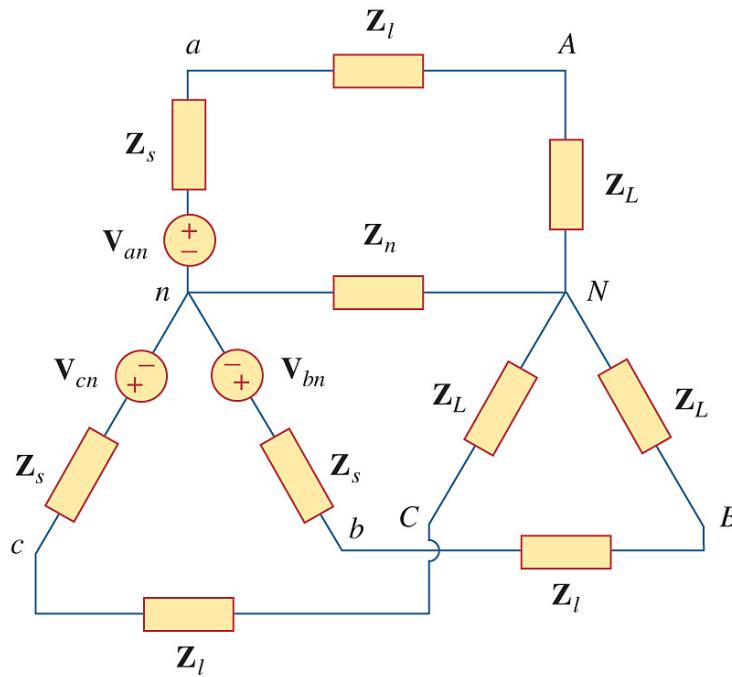
$$\mathbf{Z}_a = \mathbf{Z}_b = \mathbf{Z}_c = \mathbf{Z}_{\Delta}$$

Since both the three-phase source and the three-phase load can be either wye- or delta-connected, we have four possible connections:

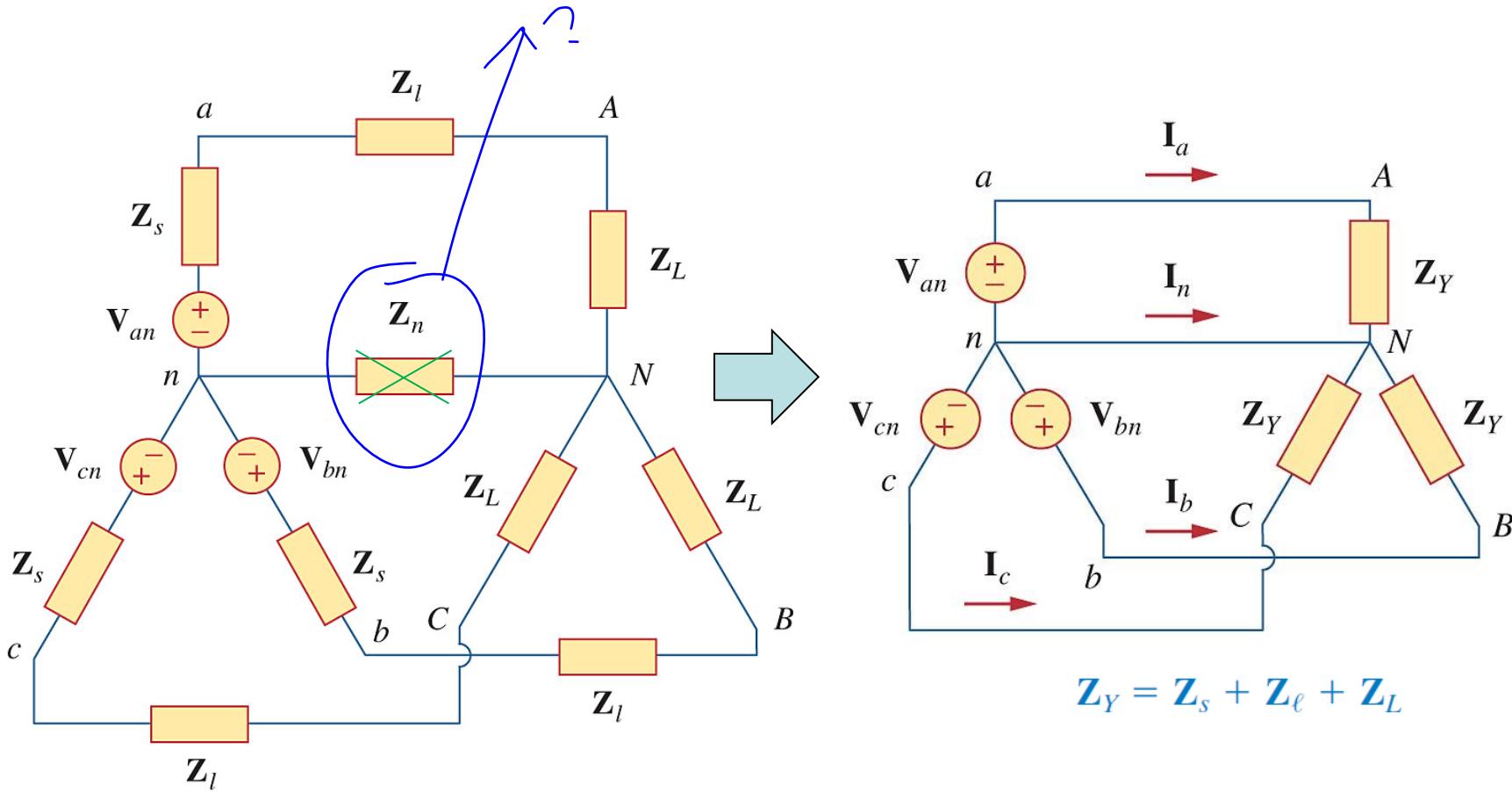
1. Y-Y connection (i.e., Y-connected source with a Y-connected load).
2. Y- $\Delta$  connection.
3.  $\Delta$ - $\Delta$  connection.
4.  $\Delta$ -Y connection.

## 12.3 Balanced Wye-Wye Connection

We begin with the Y-Y system, because any balanced three-phase system can be reduced to an equivalent Y-Y system. A balanced Y-Y system is a three-phase system with a balanced Y-connected source and a balanced Y-connected load.

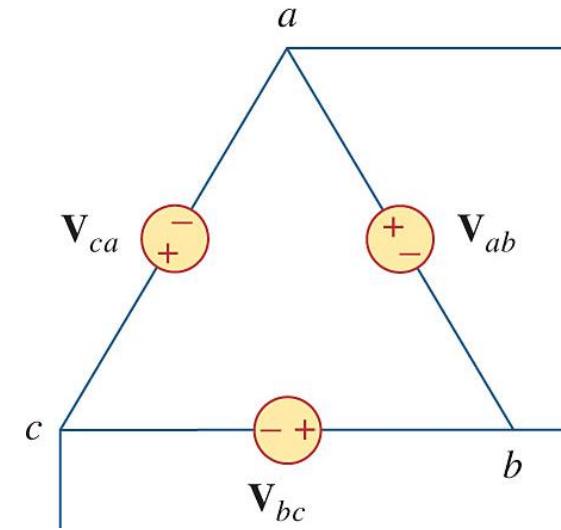
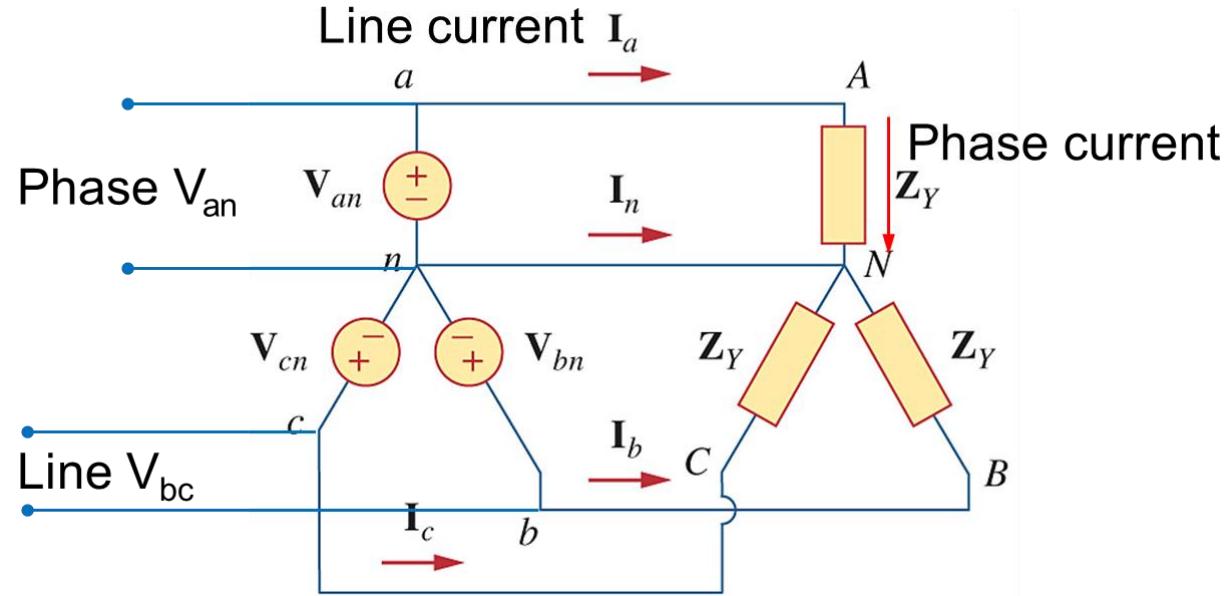


If balanced, the system can be simplified.



$$Z_Y = Z_s + Z_\ell + Z_L$$

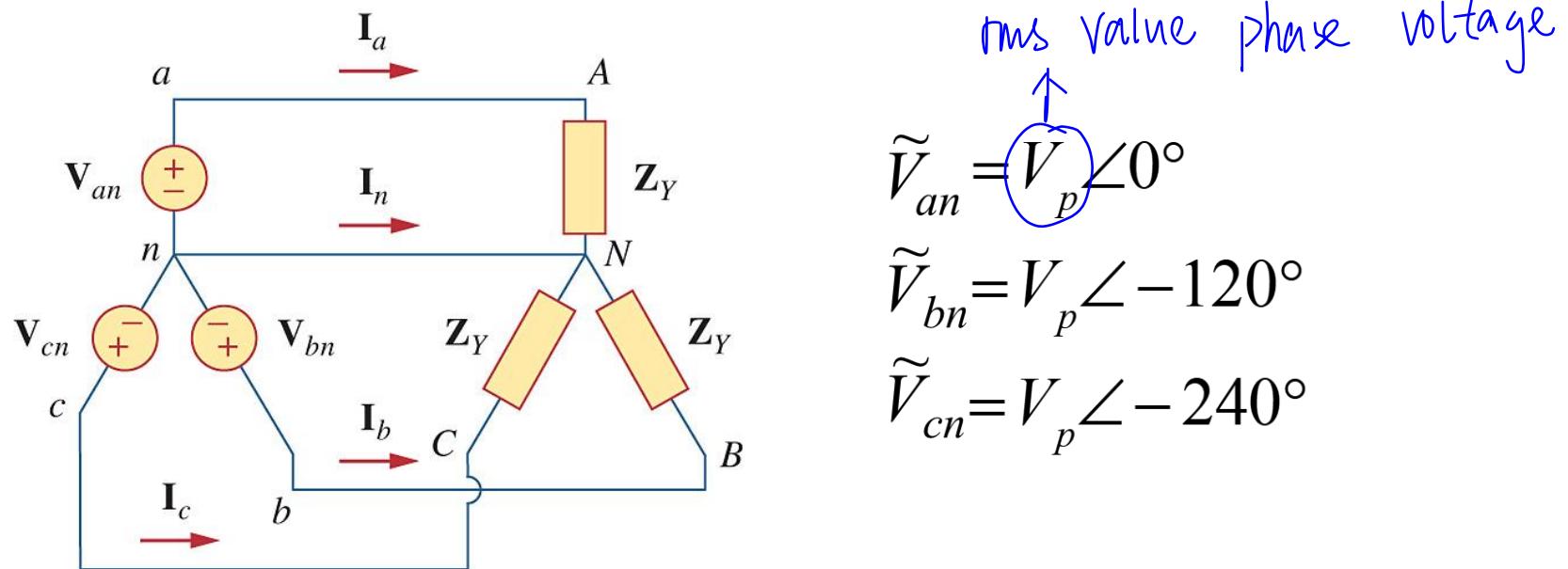
# Phases and Lines?



The **voltage** between any **two line** conductors are termed **line voltages** and the current that passes along **each line** conductor is termed a **line current**.

Phases are connected between any pair of line terminals. The voltage appearing across any phase is termed a **phase voltage**, and the current passing through any phase is termed a **phase current**.

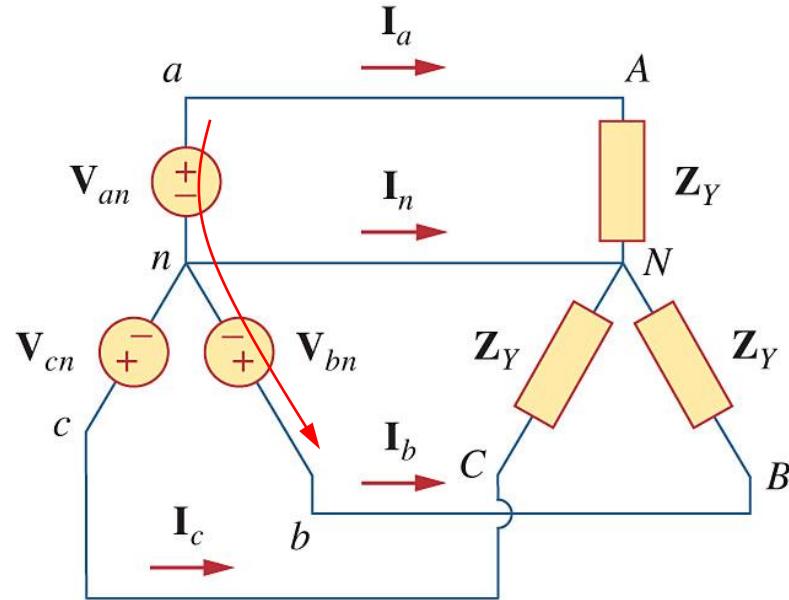
Assuming the positive sequence, **the phase voltages** (or line-to-neutral voltages) are



**Balanced source:**  
Same amplitude and frequency  
Out of phase with each other by  $120^\circ$

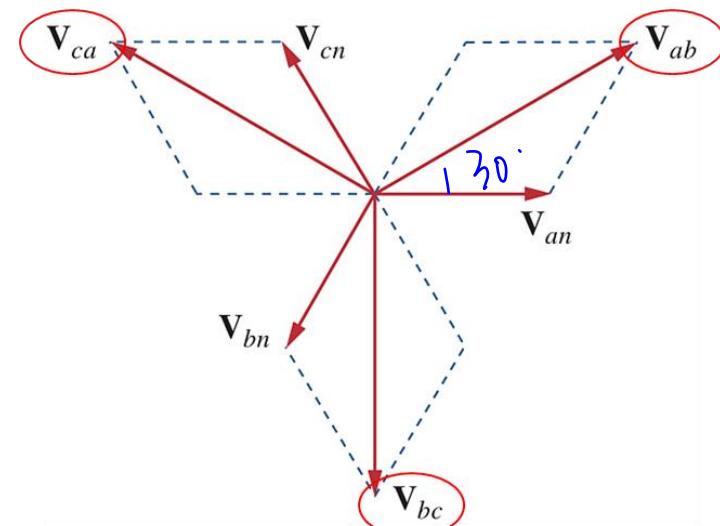
# Line voltages

The line voltages (or line-to-line voltages) are



$$\begin{aligned}\tilde{V}_{ab} &= \tilde{V}_{an} - \tilde{V}_{bn} = \sqrt{3}V_p \angle 30^\circ \\ \tilde{V}_{bc} &= \tilde{V}_{bn} - \tilde{V}_{cn} = \sqrt{3}V_p \angle -90^\circ = \tilde{V}_{ab} \angle -120^\circ \\ \tilde{V}_{ca} &= \tilde{V}_{cn} - \tilde{V}_{an} = \sqrt{3}V_p \angle -210^\circ = \tilde{V}_{ab} \angle -240^\circ \\ \tilde{V}_{ab} + \tilde{V}_{bc} + \tilde{V}_{ca} &= 0\end{aligned}$$

Line voltages are also balanced.

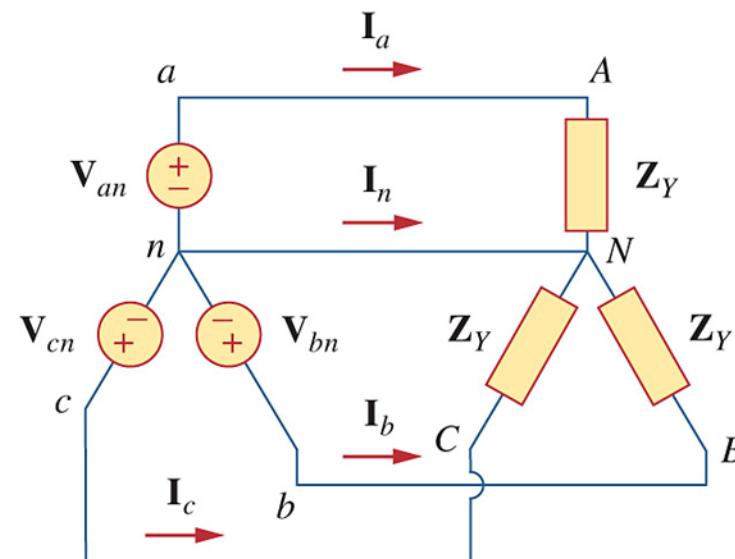


The magnitude of the line voltages is  $\sqrt{3}$  times the magnitude of the phase voltages.

$$V_L = \sqrt{3}V_p$$

$$V_p = |\tilde{V}_{an}| = |\tilde{V}_{bn}| = |\tilde{V}_{cn}|$$

$$V_L = |\tilde{V}_{ab}| = |\tilde{V}_{bc}| = |\tilde{V}_{ca}|$$



The line voltages lead their corresponding phase voltages by  $30^\circ$

$$\tilde{V}_{an} = V_p \angle 0^\circ$$

$$\tilde{V}_{bn} = V_p \angle -120^\circ$$

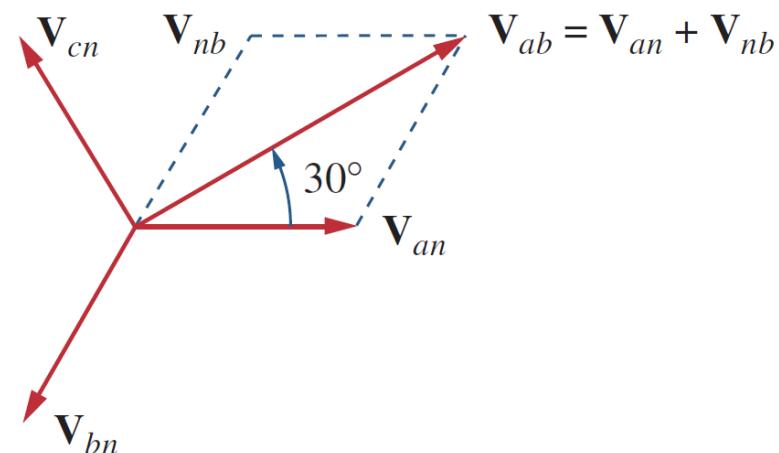
$$\tilde{V}_{cn} = V_p \angle -240^\circ$$

$$\tilde{V}_{ab} = \tilde{V}_{an} - \tilde{V}_{bn} = \sqrt{3}V_p \angle 30^\circ$$

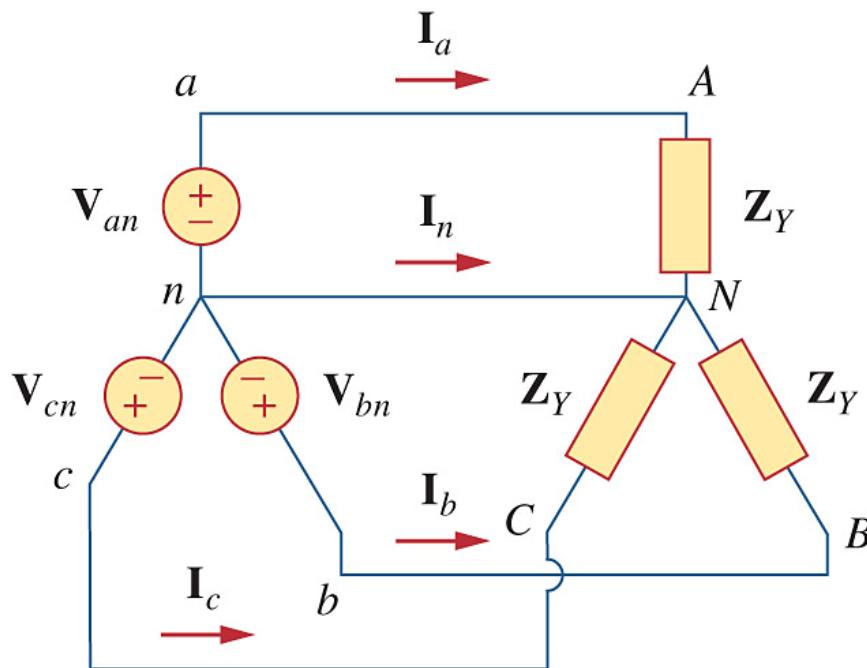
$$\tilde{V}_{bc} = \tilde{V}_{bn} - \tilde{V}_{cn} = \sqrt{3}V_p \angle -90^\circ$$

$$\tilde{V}_{ca} = \tilde{V}_{cn} - \tilde{V}_{an} = \sqrt{3}V_p \angle -210^\circ$$

$$\begin{array}{lcl} \angle \tilde{V}_{ab} & = & \angle \tilde{V}_{an} + \angle 30^\circ \\ \rightarrow \quad \angle \tilde{V}_{bc} & = & \angle \tilde{V}_{bn} + \angle 30^\circ \\ \angle \tilde{V}_{ca} & = & \angle \tilde{V}_{cn} + \angle 30^\circ \end{array}$$



# Line currents



By KVL at each phase

$$\mathbf{I}_a = \frac{\mathbf{V}_{an}}{\mathbf{Z}_Y},$$

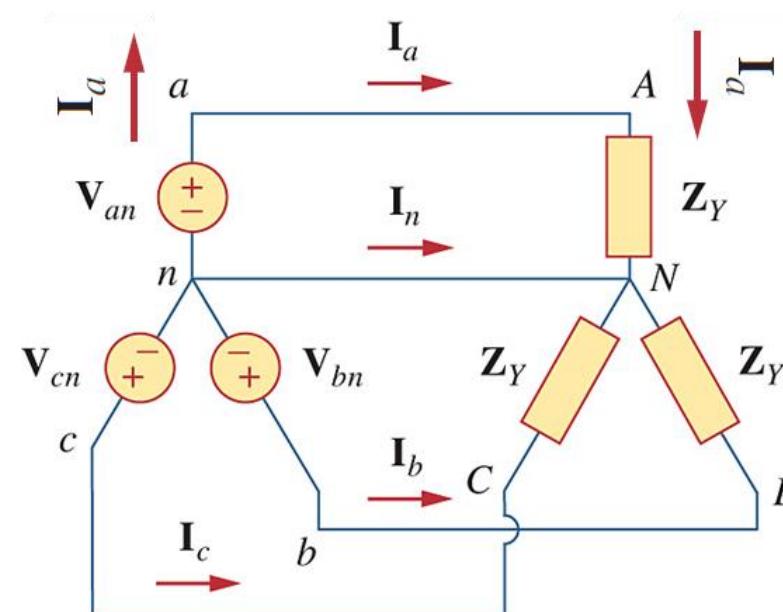
$$\mathbf{I}_b = \frac{\mathbf{V}_{bn}}{\mathbf{Z}_Y} = \frac{\mathbf{V}_{an} \angle -120^\circ}{\mathbf{Z}_Y} = \mathbf{I}_a \angle -120^\circ$$

$$\mathbf{I}_c = \frac{\mathbf{V}_{cn}}{\mathbf{Z}_Y} = \frac{\mathbf{V}_{an} \angle -240^\circ}{\mathbf{Z}_Y} = \mathbf{I}_a \angle -240^\circ$$

Line currents add up to zero:  $\mathbf{I}_a + \mathbf{I}_b + \mathbf{I}_c = 0$

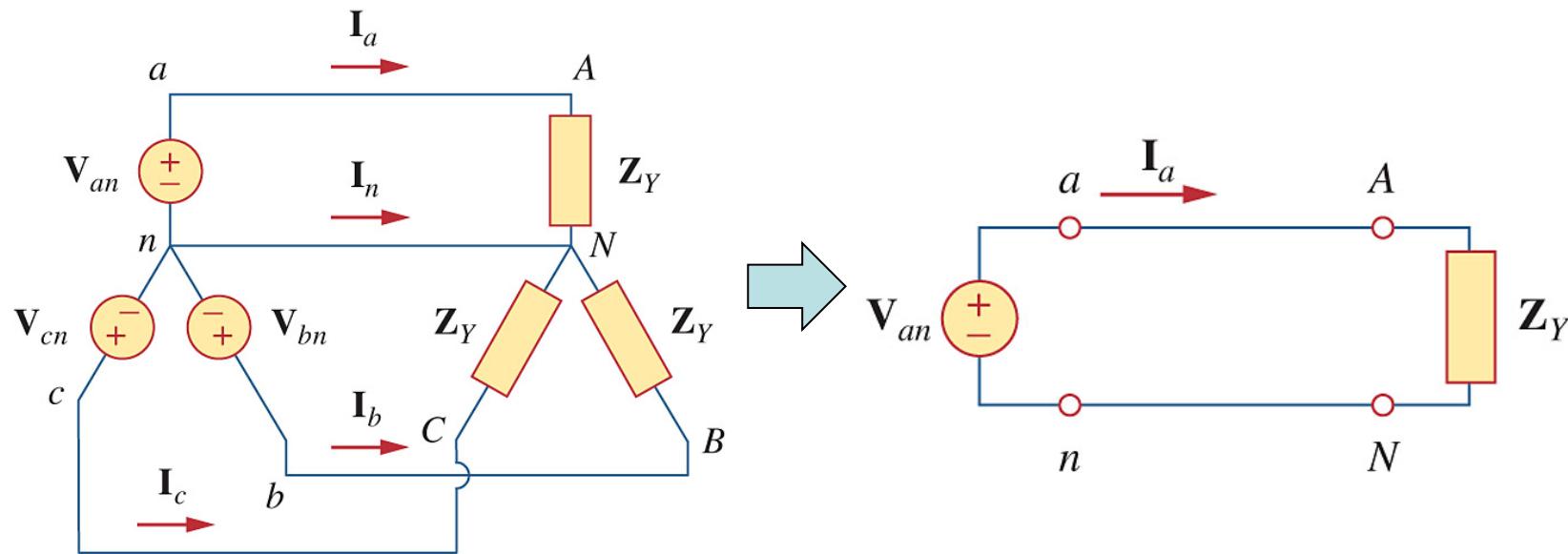
Thus,  $\mathbf{I}_n = -(\mathbf{I}_a + \mathbf{I}_b + \mathbf{I}_c) = 0$  and  $\mathbf{V}_{nN} = \mathbf{Z}_n \mathbf{I}_n = 0$

**While the line current is the current in each line, the phase current is the current in each phase of the source or load.**



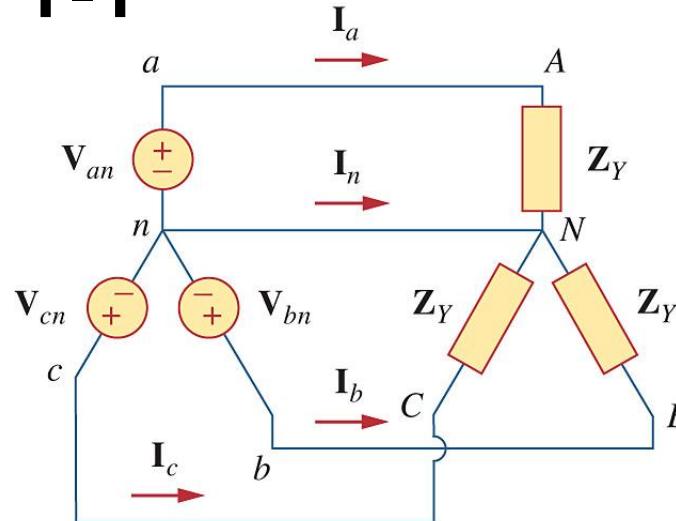
**In Y-Y connected system, the line current is the same as the phase current.**

An alternative way of analyzing a **balanced Y-Y system** is to do so on a **per phase basis**.



The single-phase analysis yields the line current  $I_a = \frac{V_{an}}{Z_Y}$

# Summary of balanced Y-Y



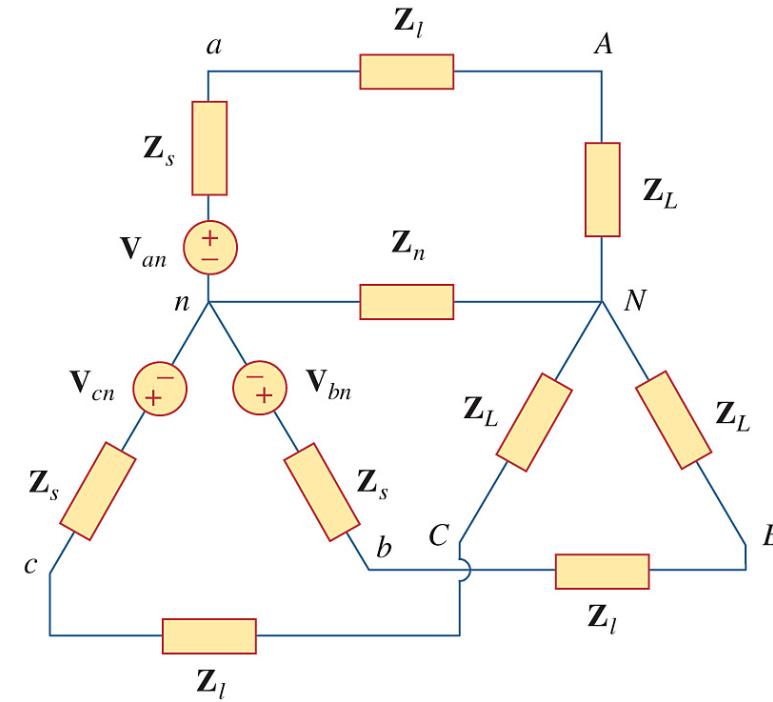
Summary of phase and line voltages/currents for balanced three-phase systems.<sup>1</sup>

Connection	Phase voltages/currents	Line voltages/currents
Y-Y	$\mathbf{V}_{an} = V_p \angle 0^\circ$ $\mathbf{V}_{bn} = V_p \angle -120^\circ$ $\mathbf{V}_{cn} = V_p \angle +120^\circ$ Same as line currents	$\mathbf{V}_{ab} = \sqrt{3} V_p \angle 30^\circ$ $\mathbf{V}_{bc} = \mathbf{V}_{ab} \angle -120^\circ$ $\mathbf{V}_{ca} = \mathbf{V}_{ab} \angle +120^\circ$ $\mathbf{I}_a = \mathbf{V}_{an}/\mathbf{Z}_Y$ $\mathbf{I}_b = \mathbf{I}_a \angle -120^\circ$ $\mathbf{I}_c = \mathbf{I}_a \angle +120^\circ$

Positive or abc sequence is assumed.

**Practice Problem 12.2** A Y-connected balanced three-phase generator with an impedance of  $0.4 + j0.3 \Omega$  per phase is connected to a Y-connected balanced load with an impedance of  $24 + j19 \Omega$  per phase. The line joining the generator and the load has an impedance of  $0.6 + j0.7 \Omega$  per phase. Assuming a positive sequence for the source voltages and that  $\tilde{V}_{an} = 120\angle30^\circ$  V, find the line voltages and the line currents.

**Practice Problem 12.2** A Y-connected balanced three-phase generator with an impedance of  $0.4 + j0.3 \Omega$  per phase is connected to a Y-connected balanced load with an impedance of  $24 + j19 \Omega$  per phase. The line joining the generator and the load has an impedance of  $0.6 + j0.7 \Omega$  per phase. Assuming a positive sequence for the source voltages and that  $\tilde{V}_{an} = 120\angle 30^\circ$  V, find the line voltages and the line currents.



# Line voltages by follow the definition

**Practice Problem 12.2** A Y-connected balanced three-phase generator with an impedance of  $0.4 + j0.3 \Omega$  per phase is connected to a Y-connected balanced load with an impedance of  $24 + j19 \Omega$  per phase. The line joining the generator and the load has an impedance of  $0.6 + j0.7 \Omega$  per phase. Assuming a positive sequence for the source voltages and that  $\tilde{V}_{an} = 120\angle 30^\circ$  V, find the line voltages and the line currents.

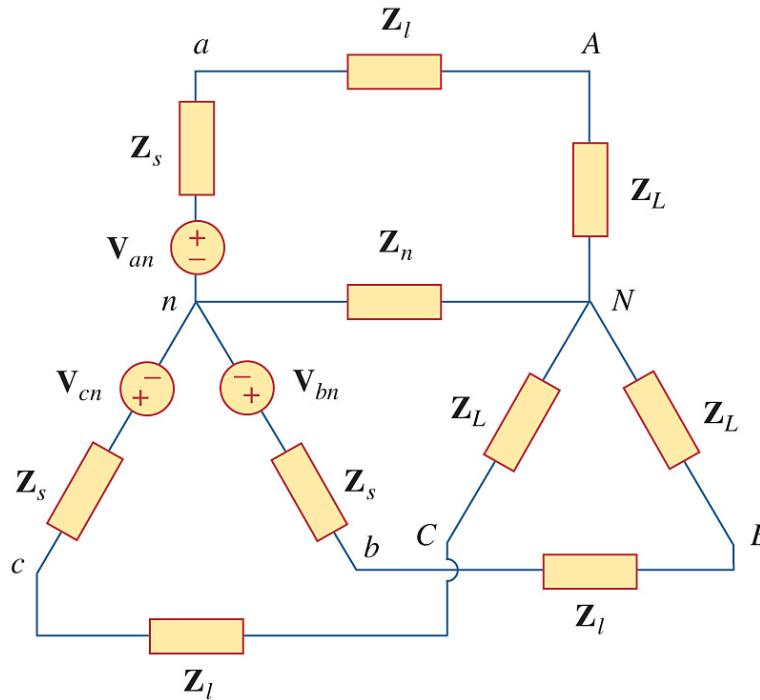
The "ideal" line voltages are

$$\tilde{V}_{ab} = \tilde{V}_{an}\sqrt{3}\angle 30^\circ = 120\angle 30^\circ \times \sqrt{3}\angle 30^\circ$$

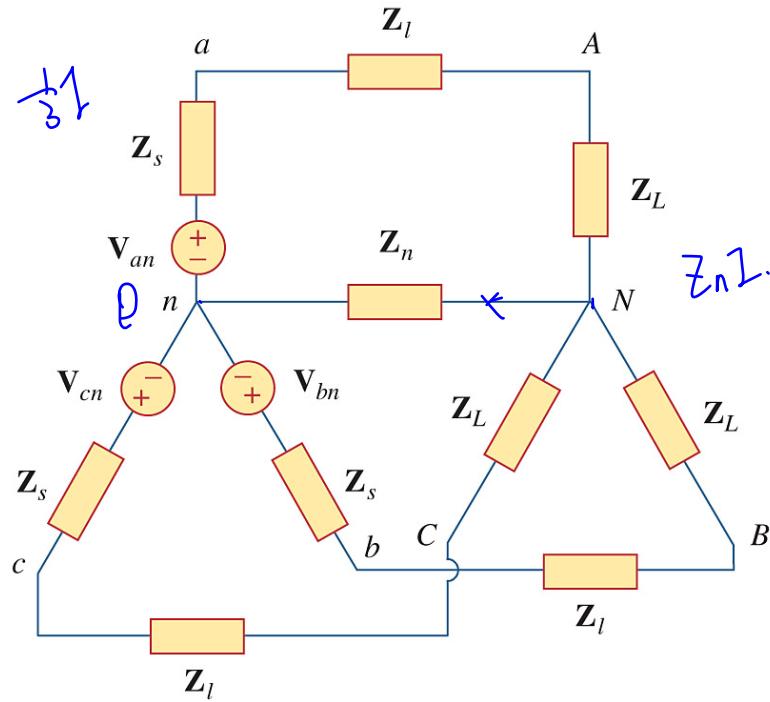
$$\approx 207.8461\angle 60^\circ \text{ (V)}$$

$$\tilde{V}_{bc} = \tilde{V}_{ab}\angle -120^\circ = 207.8461\angle -60^\circ \text{ (V)}$$

$$\tilde{V}_{ba} = \tilde{V}_{ab}\angle -240^\circ = 207.8461\angle -180^\circ \text{ (V)}$$



## Line currents



$$V_{an} - Z_n I = \text{blue } Z \angle$$

$$Z_Y = Z_s + Z_n + Z_L = (0.4 + j0.3) + (24 + j19) + (0.6 + j0.7) = 25 + j20 \text{ } (\Omega)$$

$$\tilde{I}_a = \frac{\tilde{V}_{an}}{Z_Y} = \frac{120\angle 30^\circ}{25 + j20} \approx \frac{120\angle 30^\circ}{32.0156\angle 38.66^\circ}$$

$$\approx 3.7482\angle -8.66^\circ \text{ (A)}$$

$$\tilde{I}_b = \tilde{I}_a \angle -120^\circ = 3.7482\angle -128.66^\circ \text{ (A)}$$

$$\tilde{I}_c = \tilde{I}_a \angle -240^\circ = 3.7482\angle -248.66^\circ \text{ (A)}$$

## Alternatively, by the equations

The "ideal" line voltages are

$$\tilde{V}_{ab} = \tilde{V}_{an}\sqrt{3}\angle 30^\circ = 120\angle 30^\circ \times \sqrt{3}\angle 30^\circ$$

$$\approx 207.8461\angle 60^\circ \text{ (V)}$$

$$\tilde{V}_{bc} = \tilde{V}_{ab}\angle -120^\circ = 207.8461\angle -60^\circ \text{ (V)}$$

$$\tilde{V}_{ba} = \tilde{V}_{ab}\angle -240^\circ = 207.8461\angle -180^\circ \text{ (V)}$$

Note that for a balanced system, the other two voltages/currents can be quickly obtained by their **phase relation**.

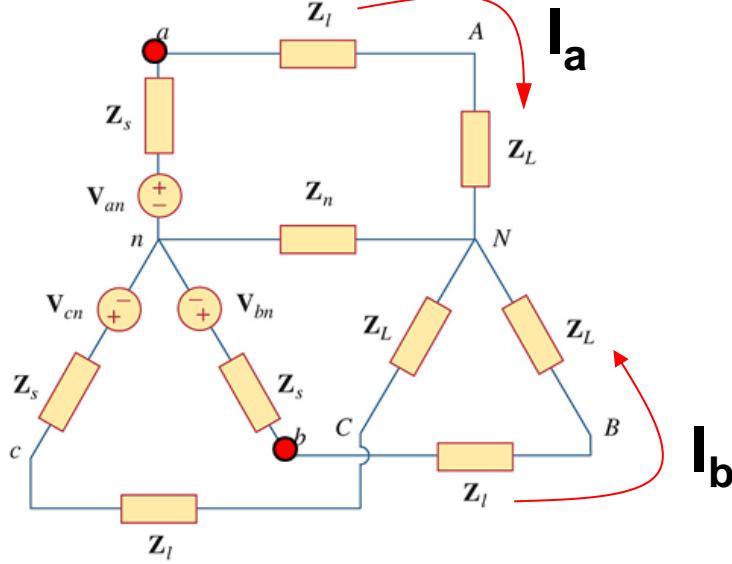
## Line current

$$Z_Y = Z_s + Z_l + Z_L = (0.4 + j0.3) + (24 + j19) \\ + (0.6 + j0.7) = 25 + j20 \text{ } (\Omega)$$

$$\tilde{I}_a = \frac{\tilde{V}_{an}}{Z_Y} = \frac{120\angle 30^\circ}{25 + j20} \approx \frac{120\angle 30^\circ}{32.0156\angle 38.66^\circ} \\ \approx 3.7482\angle -8.66^\circ \text{ (A)}$$

$$\tilde{I}_b = \tilde{I}_a \angle -120^\circ = 3.7482\angle -128.66^\circ \text{ (A)}$$

$$\tilde{I}_c = \tilde{I}_a \angle -240^\circ = 3.7482\angle -248.66^\circ \text{ (A)}$$



The line voltages seen from the generator terminals are

$$\begin{aligned}
 \tilde{V}_{ab} &= \tilde{I}_a(Z_l + Z_L) - \tilde{I}_b(Z_l + Z_L) \\
 &= \tilde{I}_a \sqrt{3} \angle 30^\circ (Z_l + Z_L) \\
 &= \frac{\tilde{V}_{an}}{Z_Y} \sqrt{3} \angle 30^\circ (Z_l + Z_L) = \tilde{V}_{ab} \left( \frac{Z_l + Z_L}{Z_Y} \right)
 \end{aligned}$$

Line voltage  $V_{ab}$

$$= 207.8461 \angle 60^\circ \times \left( \frac{24.6 + j19.7}{25 + j20} \right)$$

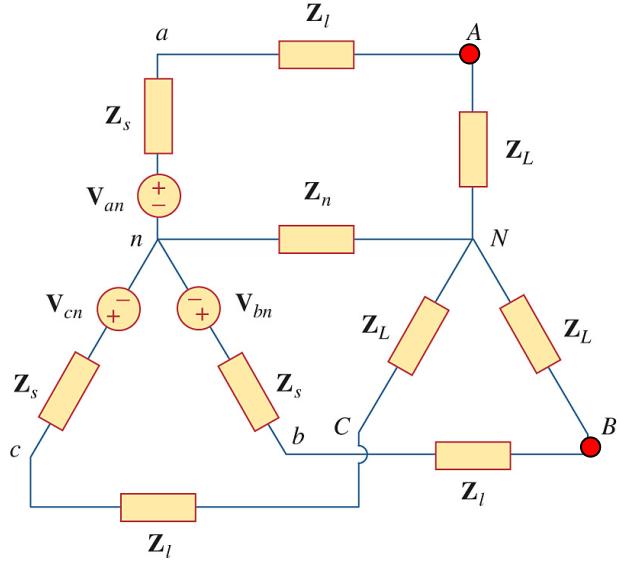
$$\approx 207.8461 \angle 60^\circ \times \frac{31.5159 \angle 38.69^\circ}{32.0156 \angle 38.66^\circ}$$

$$\approx 204.6020 \angle 60.03^\circ \text{ (V)}$$

$$\tilde{V}_{bc} = 204.6020 \angle -59.97^\circ \text{ (V)}$$

$$\tilde{V}_{ca} = 204.6020 \angle -179.97^\circ \text{ (V)}$$

Slightly lower magnitude and angles compared to the ideal line voltages.



The line voltages seen from the load terminals are

$$\tilde{V}_{AB} = \tilde{I}_a Z_L - \tilde{I}_b Z_L$$

$$I_a = 3.7482 \angle -8.66$$

$$I_b = 3.7482 \angle -8.66$$

$$Z_L = 14 + j19 = 30.61 \angle 38.37$$

$$V_{AB} = 198.72 \angle 59.71$$

$$V_{BC} = 198.72 \angle -60.29$$

$$V_{CA} = 198.72 \angle -180.29$$

The line voltages seen from the load

terminals are

$$V_{AN} - V_{BN}$$

$$I_a - I_b = I_a \sqrt{3} \angle 30^\circ = V_{an}/Z_Y \sqrt{3} \angle 30^\circ = V_{ab}/Z_Y$$

$$\tilde{V}_{AB} = \tilde{I}_a Z_L - \tilde{I}_b Z_L = \tilde{V}_{ab} \frac{Z_L}{Z_Y}$$

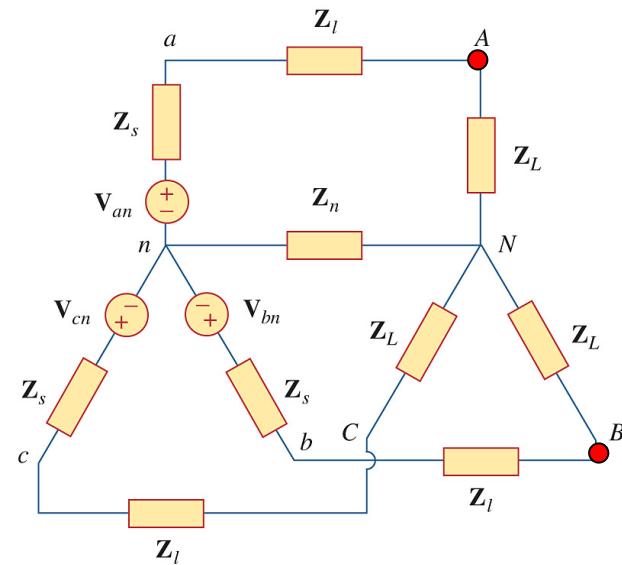
$$= 207.8461 \angle 60^\circ \times \left( \frac{24 + 19}{25 + j20} \right)$$

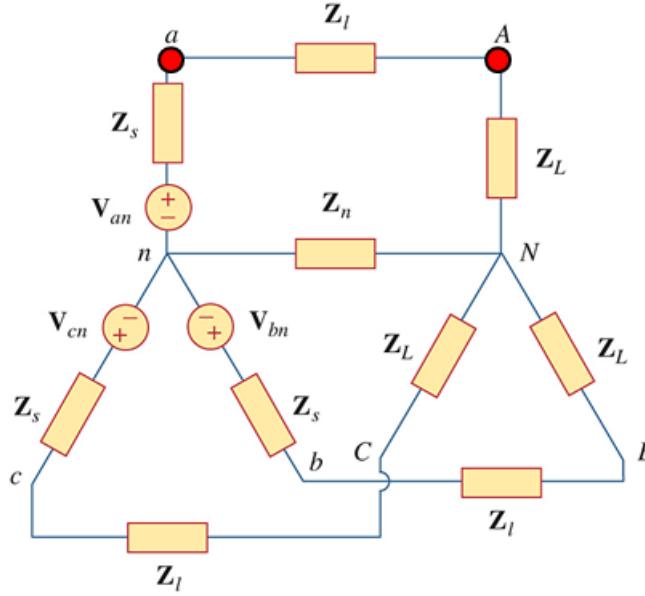
$$\approx 207.8461 \angle 60^\circ \times \frac{30.6105 \angle 38.37^\circ}{32.0156 \angle 38.66^\circ}$$

$$\approx 198.7242 \angle 59.71^\circ \text{ (V)}$$

$$\tilde{V}_{BC} \approx 198.7242 \angle -60.29^\circ \text{ (V)}$$

$$\tilde{V}_{CA} \approx 198.7242 \angle -180.29^\circ \text{ (V)}$$





The line voltage drops are

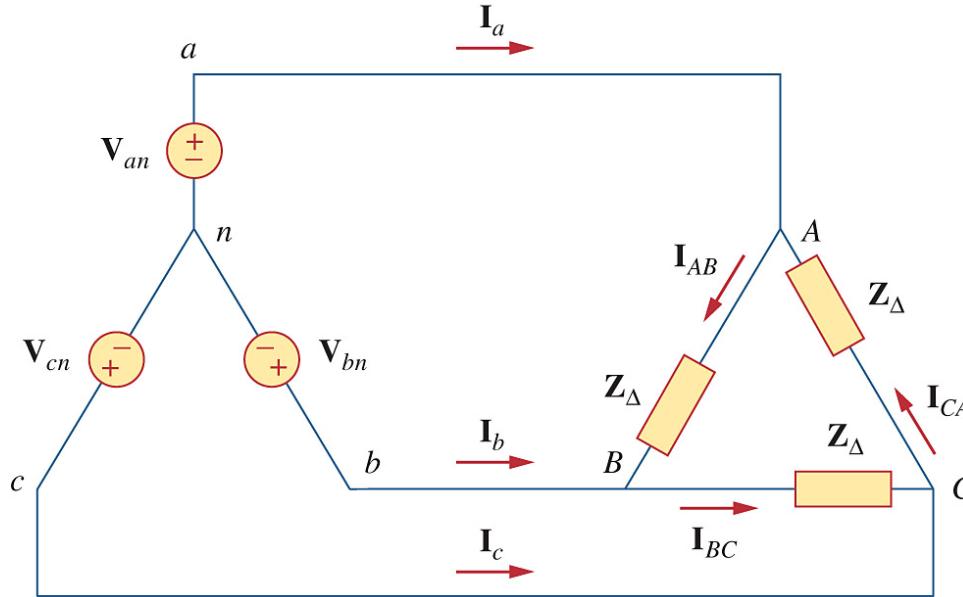
$$\tilde{I}_a Z_l = 3.7482 \angle -8.66^\circ \times (0.6 + j0.7)$$

$$\approx 3.4558 \angle 40.74^\circ \text{ (V)}$$

$$\tilde{I}_b Z_l = 3.4558 \angle -79.26^\circ \text{ (V)}$$

$$\tilde{I}_c Z_l = 3.4558 \angle -199.26^\circ \text{ (V)}$$

## 12.4 Balanced Wye-Delta Connection



**A balanced Y- $\Delta$  system** consists of a balanced Y-connected source feeding a balanced  $\Delta$ -connected load.

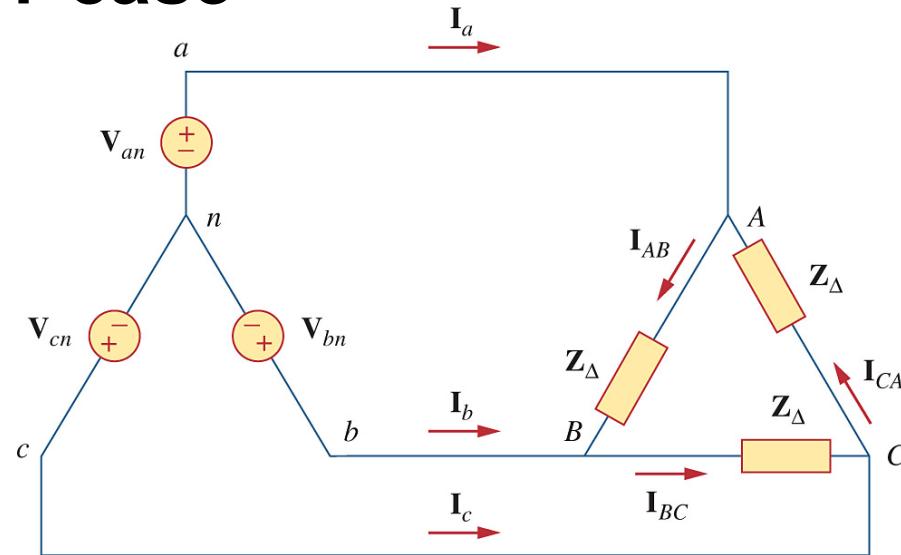
# Phase voltages: same as Y-Y case

Assume that

$$\tilde{V}_{an} = V_p \angle 0^\circ$$

$$\tilde{V}_{bn} = V_p \angle -120^\circ$$

$$\tilde{V}_{cn} = V_p \angle -240^\circ$$



The line voltages are

$$\tilde{V}_{ab} = \sqrt{3}V_p \angle 30^\circ = \tilde{V}_{an}\sqrt{3}\angle 30^\circ = \tilde{V}_{AB}$$

$$\tilde{V}_{bc} = \tilde{V}_{ab} \angle -120^\circ = \tilde{V}_{BC}$$

$$\tilde{V}_{ca} = \tilde{V}_{ab} \angle -240^\circ = \tilde{V}_{CA}$$

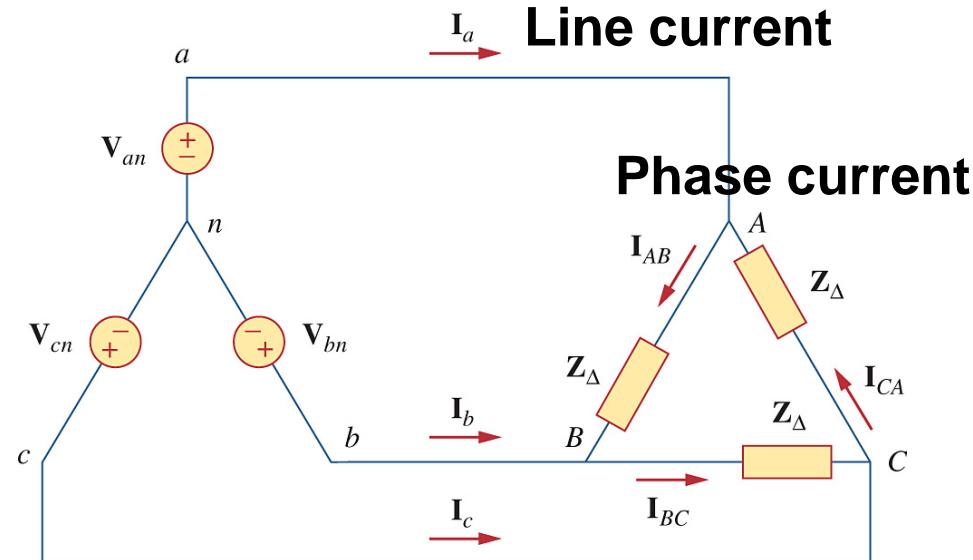
# Phase currents

The phase currents are

$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_{\Delta}}$$

$$\tilde{I}_{BC} = \frac{\tilde{V}_{BC}}{Z_{\Delta}} = \tilde{I}_{AB} \angle -120^\circ$$

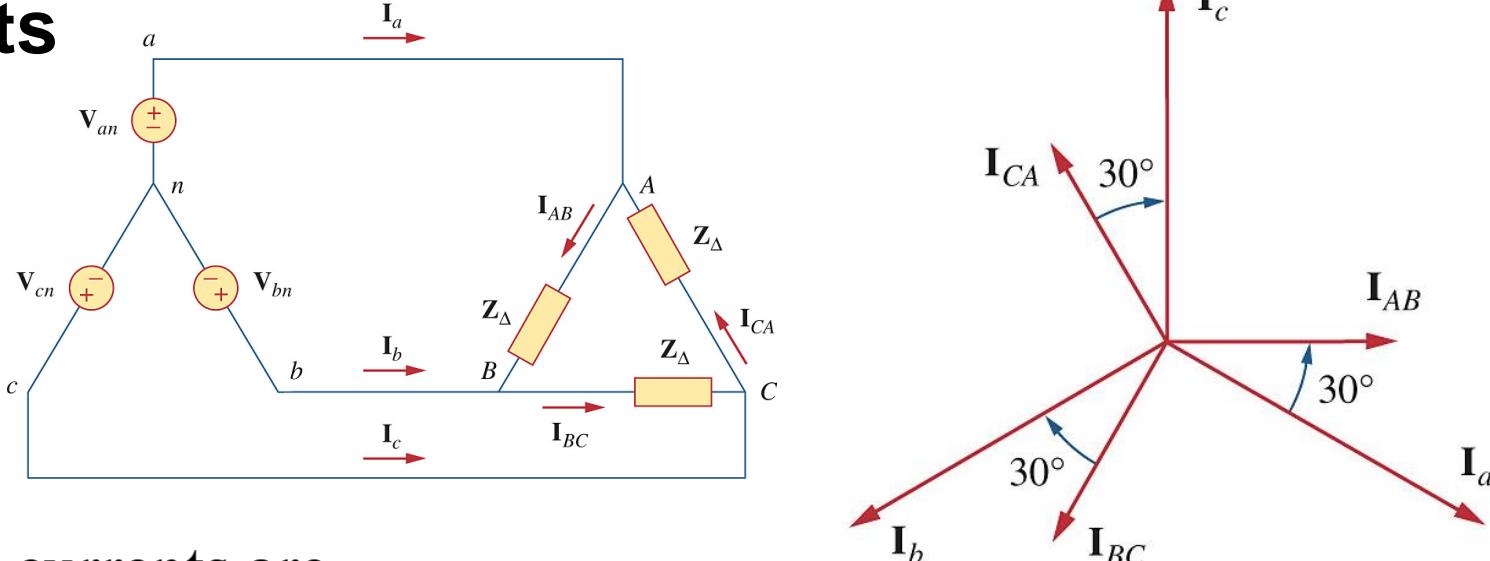
$$\tilde{I}_{CA} = \frac{\tilde{V}_{CA}}{Z_{\Delta}} = \tilde{I}_{AB} \angle -240^\circ$$



$$Z_Y = \frac{Z_{\Delta}}{3}$$

While the **line current** is the current in each line, the **phase current** is the current in each phase of the source or load.

# Line currents



The line currents are

$$\tilde{I}_a = \tilde{I}_{AB} - \tilde{I}_{CA} = \tilde{I}_{AB} \sqrt{3} \angle -30^\circ$$

$$\tilde{I}_b = \tilde{I}_{BC} - \tilde{I}_{AB} = \tilde{I}_{BC} \sqrt{3} \angle -30^\circ = \tilde{I}_a \angle -120^\circ$$

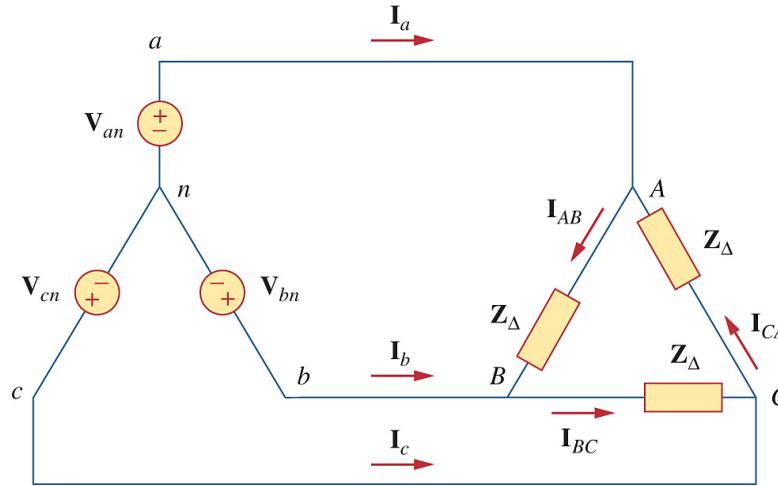
$$\tilde{I}_c = \tilde{I}_{CA} - \tilde{I}_{BC} = \tilde{I}_{CA} \sqrt{3} \angle -30^\circ = \tilde{I}_a \angle -240^\circ$$

showing that

$$I_L = \sqrt{3} I_p \quad I_L = |\tilde{I}_a| = |\tilde{I}_b| = |\tilde{I}_c|, \quad I_p = |\tilde{I}_{AB}| = |\tilde{I}_{BC}| = |\tilde{I}_{CA}|$$

$$\boxed{\begin{aligned}\tilde{I}_{AB} &= \frac{\tilde{V}_{AB}}{Z_\Delta} \\ \tilde{I}_{BC} &= \frac{\tilde{V}_{BC}}{Z_\Delta} = \tilde{I}_{AB} \angle -120^\circ \\ \tilde{I}_{CA} &= \frac{\tilde{V}_{CA}}{Z_\Delta} = \tilde{I}_{AB} \angle -240^\circ\end{aligned}}$$

# Summary of balanced Y- $\Delta$

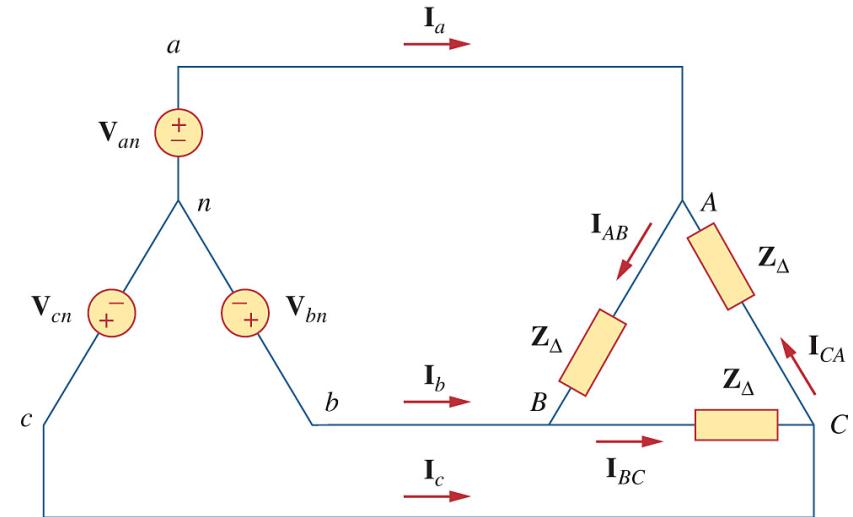


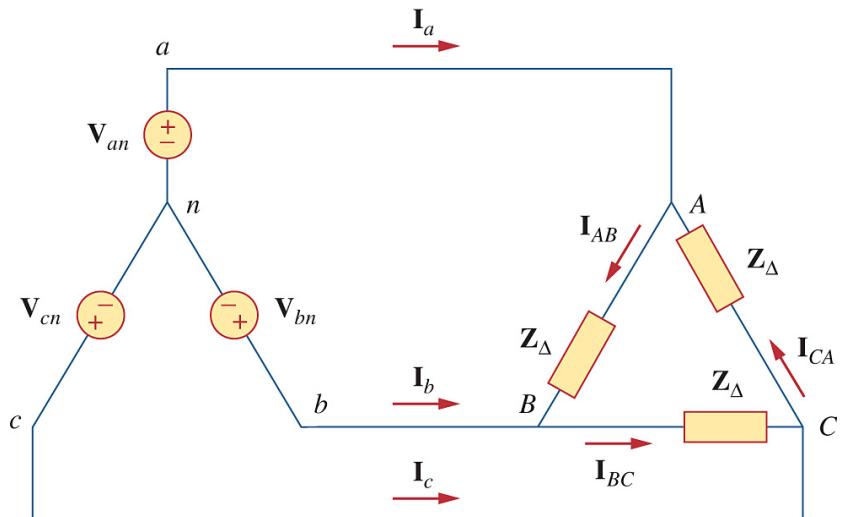
Summary of phase and line voltages/currents for balanced three-phase systems.<sup>1</sup>

Connection	Phase voltages/currents	Line voltages/currents
Y- $\Delta$	$\mathbf{V}_{an} = V_p \angle 0^\circ$ $\mathbf{V}_{bn} = V_p \angle -120^\circ$ $\mathbf{V}_{cn} = V_p \angle +120^\circ$ $\mathbf{I}_{AB} = \mathbf{V}_{AB}/Z_\Delta$ $\mathbf{I}_{BC} = \mathbf{V}_{BC}/Z_\Delta$ $\mathbf{I}_{CA} = \mathbf{V}_{CA}/Z_\Delta$	$\mathbf{V}_{ab} = \mathbf{V}_{AB} = \sqrt{3}V_p \angle 30^\circ$ $\mathbf{V}_{bc} = \mathbf{V}_{BC} = \mathbf{V}_{ab} \angle -120^\circ$ $\mathbf{V}_{ca} = \mathbf{V}_{CA} = \mathbf{V}_{ab} \angle +120^\circ$ $\mathbf{I}_a = \mathbf{I}_{AB} \sqrt{3} \angle -30^\circ$ $\mathbf{I}_b = \mathbf{I}_a \angle -120^\circ$ $\mathbf{I}_c = \mathbf{I}_a \angle +120^\circ$

Positive or abc sequence is assumed.

**Practice Problem 12.3** One line voltage of a balanced Y-connected source is  $\tilde{V}_{AB} = 240\angle -20^\circ \text{ V}$ . If the source is connected to a  $\Delta$ -connected load of  $20\angle 40^\circ \Omega$ , find the phase and line currents. Assume the  $abc$  sequence.





$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_\Delta} = \frac{240\angle -20^\circ}{20\angle 40^\circ} = 12\angle -60^\circ \text{ (A)}$$

$$\tilde{I}_{BC} = \tilde{I}_{AB} \angle -120^\circ = 12\angle -180^\circ \text{ (A)}$$

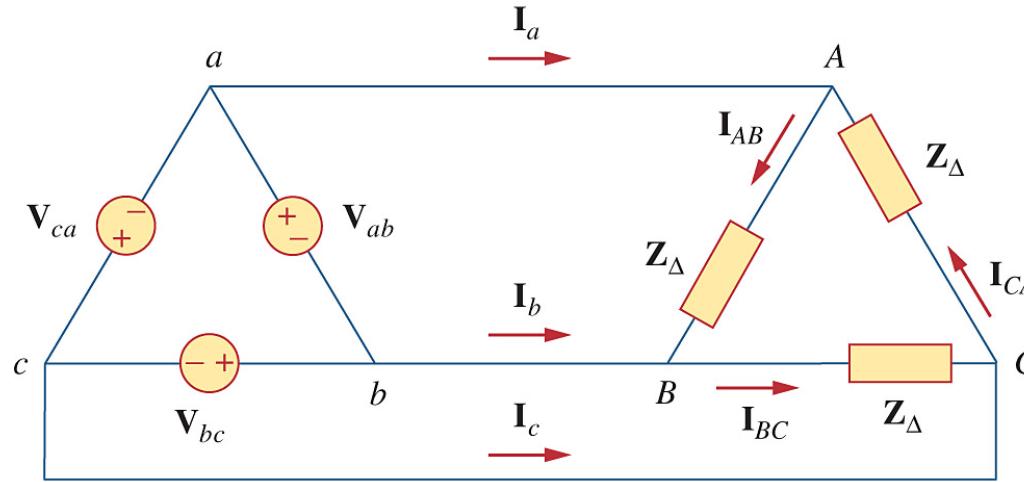
$$\tilde{I}_{CA} = \tilde{I}_{AB} \angle +120^\circ = 12\angle 60^\circ \text{ (A)}$$

$$\tilde{I}_a = \tilde{I}_{AB} \sqrt{3} \angle -30^\circ \approx 20.7846 \angle -90^\circ \text{ (A)}$$

$$\tilde{I}_b = \tilde{I}_a \angle +240^\circ = 20.7846 \angle 150^\circ \text{ (A)}$$

$$\tilde{I}_c = \tilde{I}_a \angle +120^\circ = 20.7846 \angle 30^\circ \text{ (A)}$$

## 12.5 Balanced Delta-Delta Connection



A **balanced  $\Delta$ - $\Delta$  system** is one in which both the balanced source and balanced load are  $\Delta$ -connected.

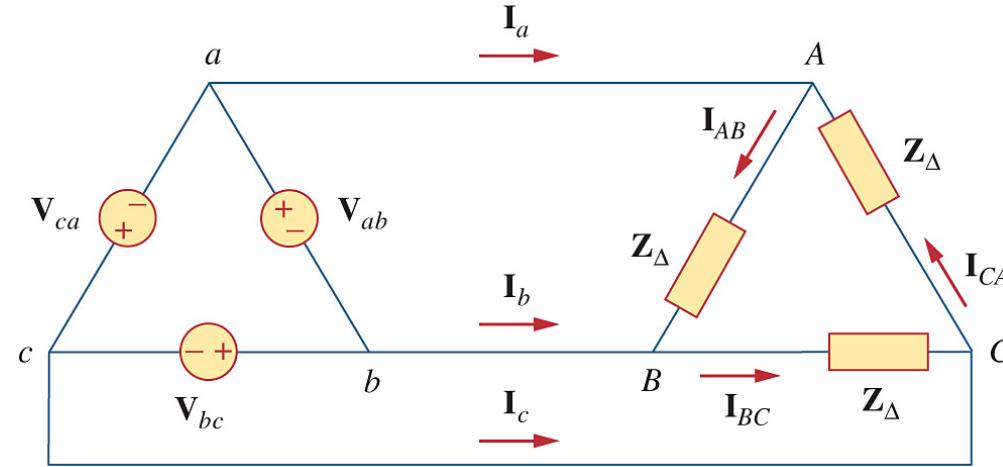
# Phase and line voltages

Assume that

$$\tilde{V}_{ab} = V_p \angle 0^\circ$$

$$\tilde{V}_{bc} = V_p \angle -120^\circ$$

$$\tilde{V}_{ca} = V_p \angle +120^\circ$$

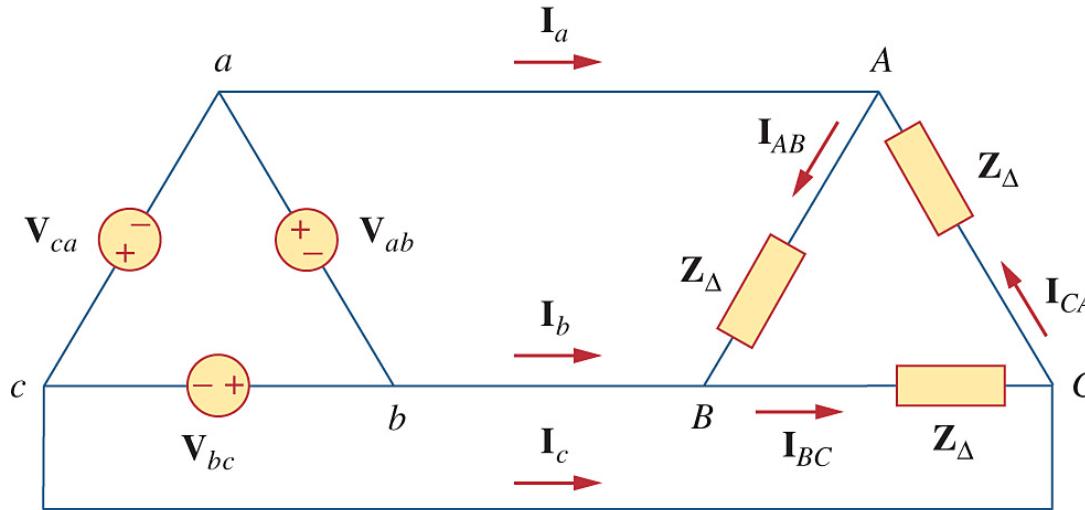


**Phase voltage = Line voltage**

Phase voltage = Voltage across the impedances

$$\tilde{V}_{ab} = \tilde{V}_{AB}, \tilde{V}_{bc} = \tilde{V}_{BC}, \tilde{V}_{ca} = \tilde{V}_{CA}$$

# Phase current



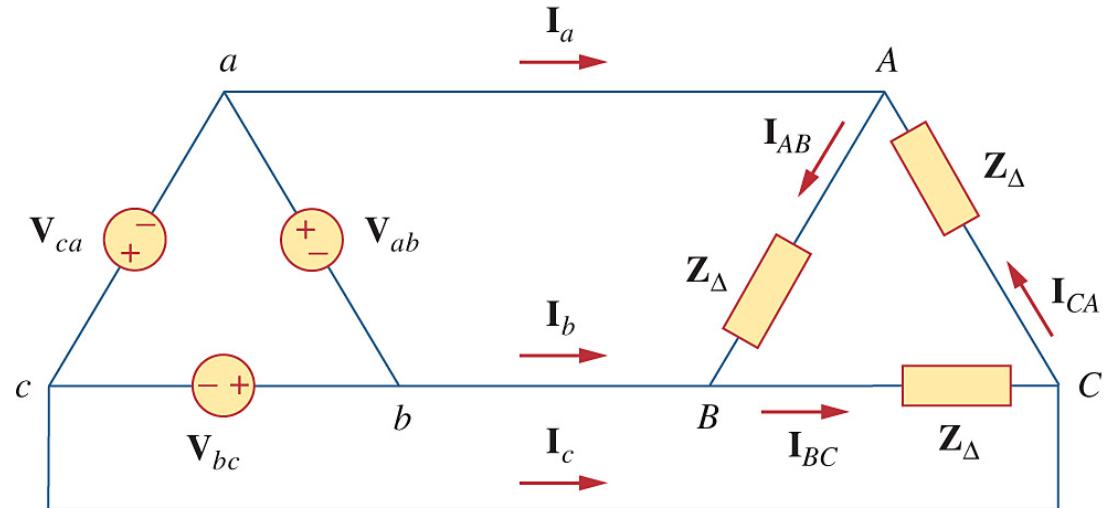
The phase currents are

$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_\Delta}$$

$$\tilde{I}_{BC} = \frac{\tilde{V}_{BC}}{Z_\Delta} = \tilde{I}_{AB} \angle -120^\circ$$

$$\tilde{I}_{CA} = \frac{\tilde{V}_{CA}}{Z_\Delta} = \tilde{I}_{AB} \angle +120^\circ$$

# Line current



The line currents are

$$\tilde{I}_a = \tilde{I}_{AB} - \tilde{I}_{CA} = \tilde{I}_{AB}\sqrt{3}\angle -30^\circ$$

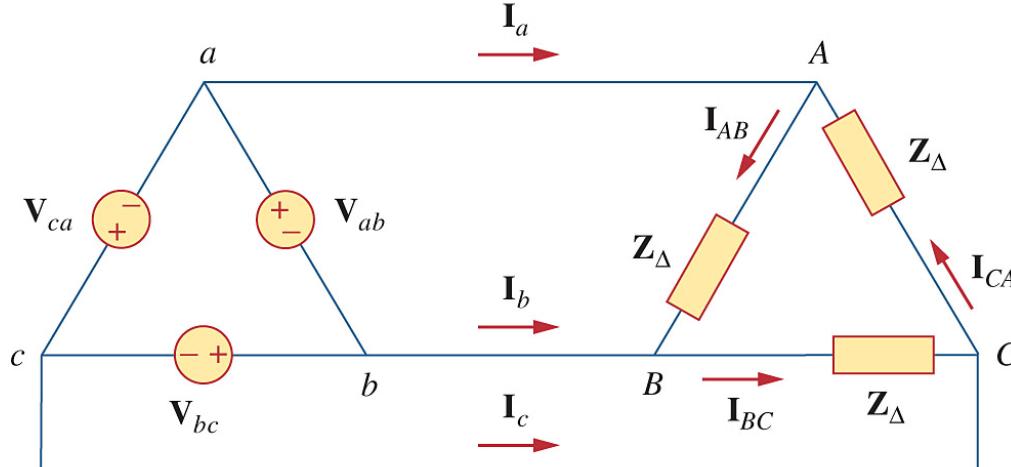
$$\tilde{I}_b = \tilde{I}_{BC} - \tilde{I}_{AB} = \tilde{I}_{BC}\sqrt{3}\angle -30^\circ = \tilde{I}_a\angle -120^\circ$$

$$\tilde{I}_c = \tilde{I}_{CA} - \tilde{I}_{BC} = \tilde{I}_{CA}\sqrt{3}\angle -30^\circ = \tilde{I}_a\angle -240^\circ$$

showing that

$$I_L = \sqrt{3}I_p \quad I_L = |\tilde{I}_a| = |\tilde{I}_b| = |\tilde{I}_c|, \quad I_p = |\tilde{I}_{AB}| = |\tilde{I}_{BC}| = |\tilde{I}_{CA}|$$

# Summary of balanced $\Delta$ - $\Delta$



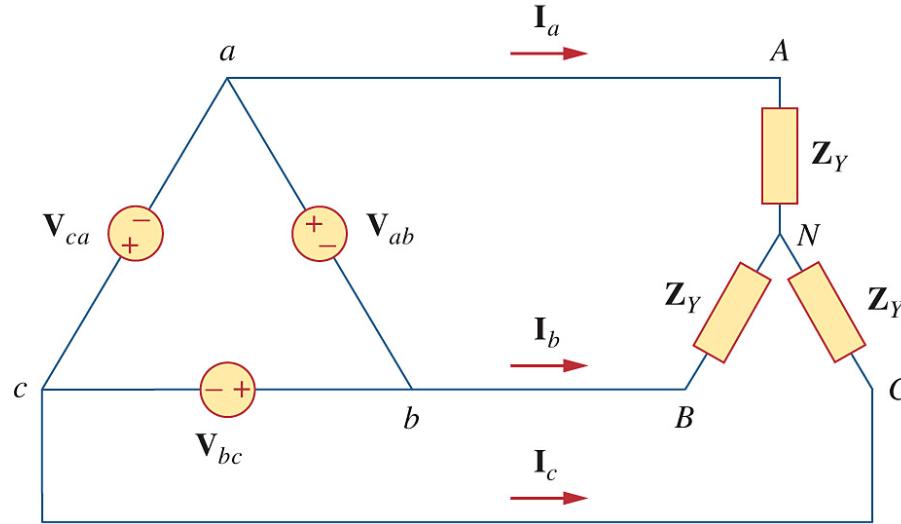
Summary of phase and line voltages/currents for balanced three-phase systems.<sup>1</sup>

Connection	Phase voltages/currents	Line voltages/currents
$\Delta$ - $\Delta$	$V_{ab} = V_p \angle 0^\circ$ $V_{bc} = V_p \angle -120^\circ$ $V_{ca} = V_p \angle +120^\circ$ $I_{AB} = V_{ab}/Z_\Delta$ $I_{BC} = V_{bc}/Z_\Delta$ $I_{CA} = V_{ca}/Z_\Delta$	Same as phase voltages $I_a = I_{AB}\sqrt{3} \angle -30^\circ$ $I_b = I_a \angle -120^\circ$ $I_c = I_a \angle +120^\circ$

Positive or abc sequence is assumed.



## 12.6 Balanced Delta-Wye Connection



**A balanced  $\Delta$ -Y system** consists of a balanced  $\Delta$ -connected source feeding a balanced  $Y$ -connected load.

**\*In  $\Delta$ -connected source:**  
**Phase voltages = Line voltages**

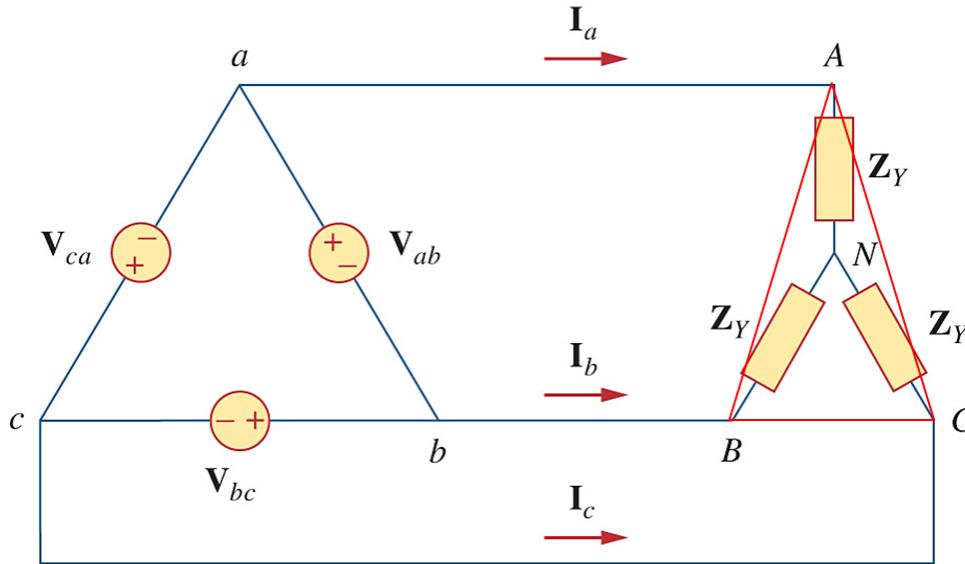
# Line current

Assume that

$$\tilde{V}_{ab} = V_p \angle 0^\circ$$

$$\tilde{V}_{bc} = V_p \angle -120^\circ$$

$$\tilde{V}_{ca} = V_p \angle +120^\circ$$



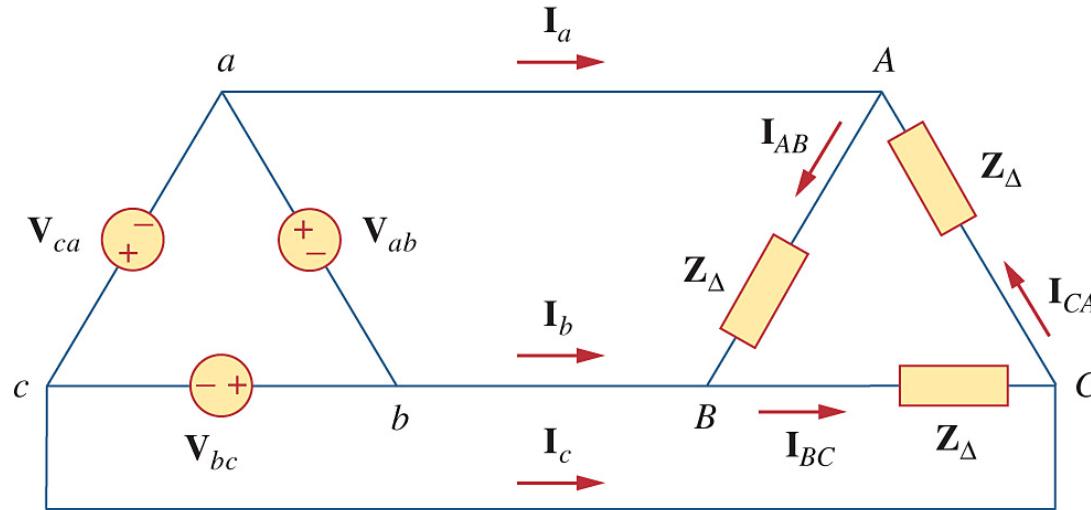
Replace the Y-connected load with its equivalent Δ-connected load. **Line current (e.g.  $I_a$ )** in a Δ-connected load is:

$$\tilde{I}_a = \tilde{I}_{AB} \sqrt{3} \angle -30^\circ = \frac{\tilde{V}_{AB}}{Z_\Delta} \sqrt{3} \angle -30^\circ$$

$$Z_\Delta = 3Z_Y$$
$$Z_Y = Z_\Delta / 3$$

$$= \frac{\tilde{V}_{ab}}{3Z_Y} \sqrt{3} \angle -30^\circ = \frac{\tilde{V}_{ab}}{\sqrt{3}Z_Y} \angle -30^\circ$$

## Recall: $\Delta$ - $\Delta$ Phase current



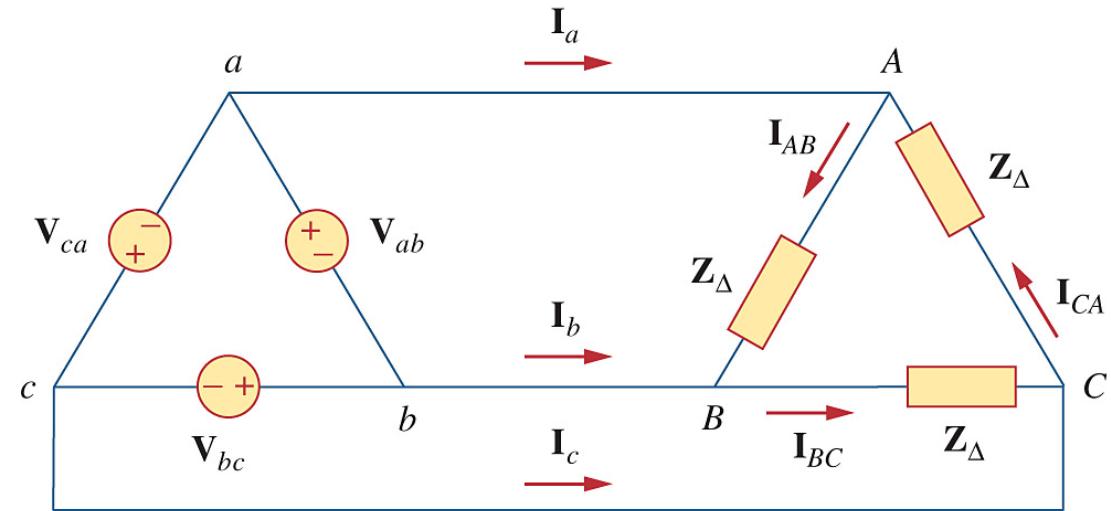
The phase currents are

$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_{\Delta}}$$

$$\tilde{I}_{BC} = \frac{\tilde{V}_{BC}}{Z_{\Delta}} = \tilde{I}_{AB} \angle -120^\circ$$

$$\tilde{I}_{CA} = \frac{\tilde{V}_{CA}}{Z_{\Delta}} = \tilde{I}_{AB} \angle +120^\circ$$

## Recall: $\Delta$ - $\Delta$ Line current



The line currents are

$$\tilde{I}_a = \tilde{I}_{AB} - \tilde{I}_{CA} = \tilde{I}_{AB}\sqrt{3}\angle -30^\circ$$

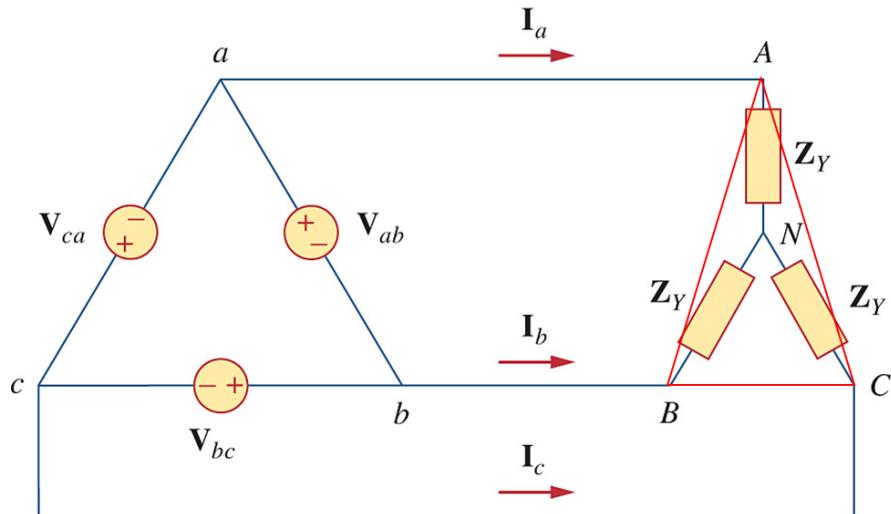
$$\tilde{I}_b = \tilde{I}_{BC} - \tilde{I}_{AB} = \tilde{I}_{BC}\sqrt{3}\angle -30^\circ = \tilde{I}_a\angle -120^\circ$$

$$\tilde{I}_c = \tilde{I}_{CA} - \tilde{I}_{BC} = \tilde{I}_{CA}\sqrt{3}\angle -30^\circ = \tilde{I}_a\angle -240^\circ$$

showing that

$$I_L = \sqrt{3}I_p \quad I_L = |\tilde{I}_a| = |\tilde{I}_b| = |\tilde{I}_c|, \quad I_p = |\tilde{I}_{AB}| = |\tilde{I}_{BC}| = |\tilde{I}_{CA}|$$

# Line current



$$\tilde{I}_a = \frac{\tilde{V}_{ab}}{\sqrt{3}Z_Y} \angle -30^\circ$$

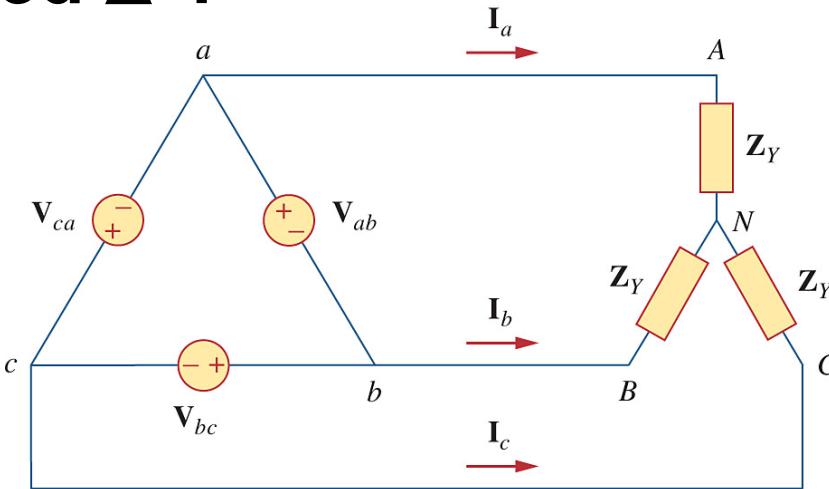
$$\tilde{I}_b = \frac{\tilde{V}_{bc}}{\sqrt{3}Z_Y} \angle -30^\circ = \tilde{I}_a \angle -120^\circ$$

$$\tilde{I}_c = \frac{\tilde{V}_{ca}}{\sqrt{3}Z_Y} \angle -30^\circ = \tilde{I}_a \angle +120^\circ$$

$$\begin{aligned}\tilde{V}_{ab} &= V_p \angle 0^\circ \\ \tilde{V}_{bc} &= V_p \angle -120^\circ \\ \tilde{V}_{ca} &= V_p \angle +120^\circ\end{aligned}$$

In **Y-connected load**,  
Phase currents = Line currents

# Summary of balanced $\Delta$ -Y



Summary of phase and line voltages/currents for balanced three-phase systems.<sup>1</sup>

Connection	Phase voltages/currents	Line voltages/currents
$\Delta$ -Y	$V_{ab} = V_p \angle 0^\circ$ $V_{bc} = V_p \angle -120^\circ$ $V_{ca} = V_p \angle +120^\circ$ Same as line currents	Same as phase voltages $I_a = \frac{V_p \angle -30^\circ}{\sqrt{3}Z_Y}$ $I_b = I_a \angle -120^\circ$ $I_c = I_a \angle +120^\circ$

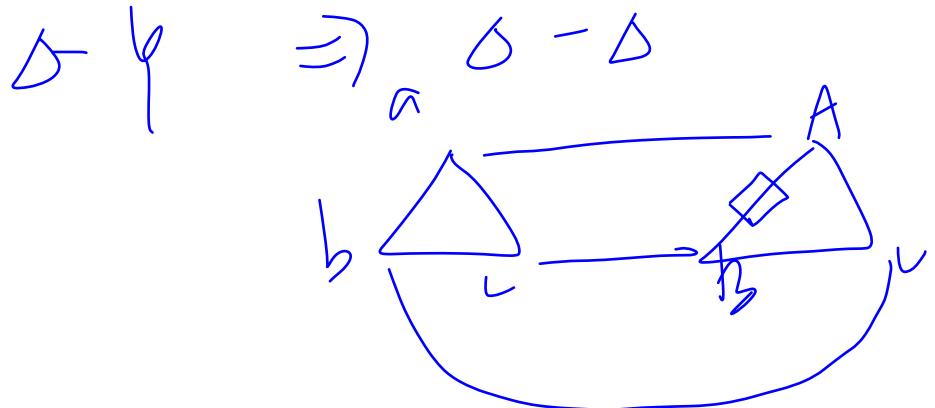
Positive or abc sequence is assumed.

In a balanced  $\Delta$ -Y circuit,  $V_{ab} = 240 \angle 15^\circ$  and  $Z_Y = (12 + j15) \Omega$ . Calculate the line currents.

### Practice Problem 12.5

**Answer:**  $7.21 \angle -66.34^\circ$  A,  $7.21 \angle +173.66^\circ$  A,  $7.21 \angle 53.66^\circ$  A.

$$Z_\Delta = 3Z_Y$$
$$Z_Y = Z_\Delta / 3$$



$$Z_\Delta = 3Z_Y = 9(4 + j5)$$

$$I_{AB} = \frac{V_{AB}}{Z_\Delta} = \frac{V_{ab}}{3Z_Y}$$

$$I_B \text{ } V \quad I_A \text{ } V$$

$$I_a = I_{AB} - I_{CB}$$

## 12.7 Power in a Balanced System

### Three phase system - Advantage 1:

We begin by examining the **instantaneous power** absorbed by the load (time domain). For a **Y-connected load**, the phase voltages in the abc sequence are

$$v_{AN} = \sqrt{2}V_p \cos \omega t$$

$$v_{BN} = \sqrt{2}V_p \cos(\omega t - 120^\circ)$$

$$v_{CN} = \sqrt{2}V_p \cos(\omega t + 120^\circ)$$

Phase voltage  $V_p$  is the  
rms value

→ Peak value:  $\sqrt{2}V_p$

If  $Z_Y = Z\angle\theta$ , the phase currents are

$$i_a = \sqrt{2}I_p \cos(\omega t - \theta)$$

$$i_b = \sqrt{2}I_p \cos(\omega t - \theta - 120^\circ)$$

$$i_c = \sqrt{2}I_p \cos(\omega t - \theta + 120^\circ)$$

$\mathbf{I} = \mathbf{V}/\mathbf{Z}$   
 $\rightarrow \angle \mathbf{I} = \angle \mathbf{V} - \angle \mathbf{Z}$

The total instantaneous power is

$$P = P_a + P_b + P_c$$

$$= v_{AN} i_a + v_{BN} i_b + v_{CN} i_c$$

$$= 3V_p I_p \cos \theta$$

$$\begin{aligned}
 &= 2V_p I_p [\cos \omega t \cos(\omega t - \theta) \\
 &\quad + \cos(\omega t - 120^\circ) \cos(\omega t - \theta - 120^\circ) \\
 &\quad + \cos(\omega t + 120^\circ) \cos(\omega t - \theta + 120^\circ)] \\
 &= 2V_p I_p \left\{ \frac{\cos \theta + \cos(2\omega t - \theta)}{2} \right. \\
 &\quad + \frac{\cos \theta + \cos(2\omega t - \theta - 240^\circ)}{2} \\
 &\quad \left. + \frac{\cos \theta + \cos(2\omega t - \theta + 240^\circ)}{2} \right\} \\
 &= 3V_p I_p \cos \theta
 \end{aligned}$$

$$P = P_a + P_b + P_c = 3V_p I_p \cos \theta$$

Thus, **the total instantaneous power** in a balanced three-phase system is **constant** – it does not change with time as the instantaneous power of each phase does.

**This result is true whether the load is Y- or Δ-connected.** This is one important reason for using a three-phase system to generate and distribute power.

The advantage over a single-phase AC system: **constant p(t)**

Since the total instantaneous power is independent of time,

$$Z_Y = Z \angle \theta \quad \theta \text{ is the power factor angle}$$

- (i) **Average power** per phase  $P_p$  for the Y- or  $\Delta$ -connected load is  $\frac{P}{3}$ , or  $P_p = V_P I_P \cos\theta$
- (ii) **Reactive power** per phase is  $Q_p = V_P I_P \sin\theta$
- (iii) **Apparent power** per phase is  $|S_p| = V_P I_P$
- (iv) **Complex power** per phase is  $S_p = P_p + jQ_p = V_P I_P^*$
- (v) **Total average power** by AC power conservation is  $P = P_a + P_b + P_c = 3P_p = 3V_P I_P \cos\theta$

## The total average power:

For a Y-connected load (with Y-connected source),

$$I_L = I_P \text{ but } V_L = \sqrt{3}V_P$$

For a  $\Delta$ -connected load (with  $\Delta$ -connected source),

$$I_L = \sqrt{3}I_P \text{ but } V_L = V_P$$

$$\text{Thus, } 3V_p I_P \cos\theta = \sqrt{3}V_L I_L \cos\theta$$

$V_p$ : phase voltage  
 $I_p$ : phase current

$V_L$ : line voltage  
 $I_L$ : line current

**The total average power:**

$$P = 3P_p = 3V_p I_p \cos\theta = \sqrt{3}V_L I_L \cos\theta$$

**The total reactive power:**

$$Q = 3Q_p = 3V_p I_p \sin\theta = \sqrt{3}V_L I_L \sin\theta$$

**The total complex power:**

$$S = 3S_p = 3V_p I_p^* = 3I_p^2 Z_p = \frac{3V_p^2}{Z_p^*}$$

where  $Z_p$  is the load impedance per phase.

$$S = P + jQ = 3V_p I_p \cos\theta + j3V_p I_p \sin\theta = \sqrt{3}V_L I_L \cos\theta + j\sqrt{3}V_L I_L \sin\theta$$

$V_p$ ,  $I_p$ ,  $V_L$ , and  $I_L$  are **all rms values** and that  $\theta$  is the angle of the load impedance or the angle between the phase voltage and the phase current.

Recall:

$$Z_Y = Z \angle \theta, \quad \theta = \angle V_p - \angle I_p$$

$\theta$  is the power factor angle

**The total average power:**

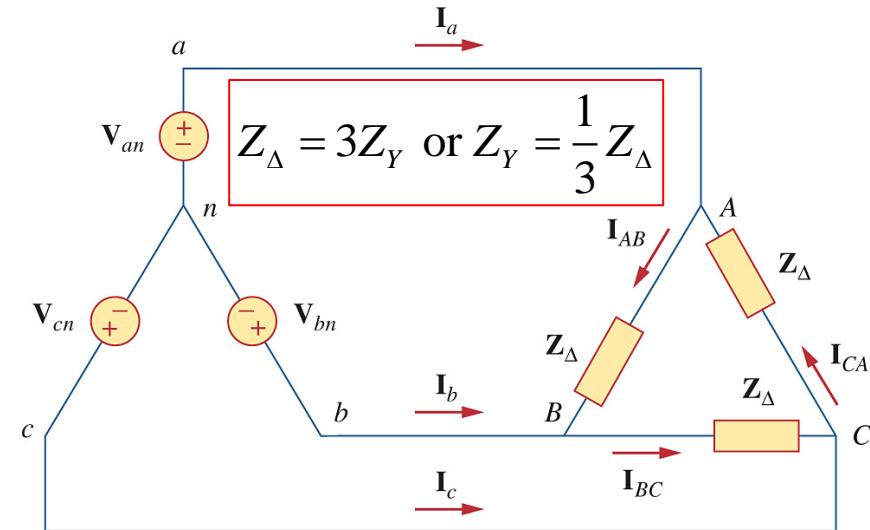
For a Y-Y connection,  $I_L = I_P$  but  $V_L = \sqrt{3}V_P$

For a  $\Delta$ - $\Delta$  connection,  $I_L = \sqrt{3}I_P$  but  $V_L = V_P$

$$P = 3P_P = 3V_p I_P \cos\theta = \sqrt{3}V_L I_L \cos\theta$$

**How about other connections?**

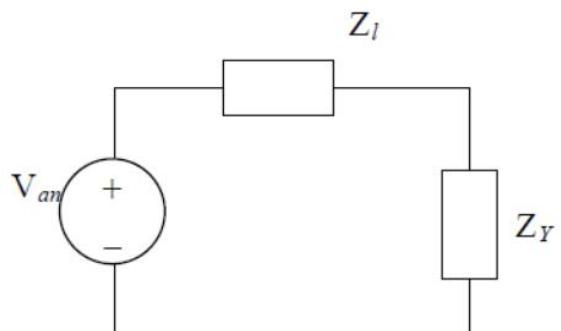
- 12.29** A balanced three-phase Y- $\Delta$  system has  $\mathbf{V}_{an} = 240 \angle 0^\circ$  V rms and  $\mathbf{Z}_\Delta = 51 + j45 \Omega$ . If the line impedance per phase is  $0.4 + j1.2 \Omega$ , find the total complex power delivered to the load.



- 12.29** A balanced three-phase Y- $\Delta$  system has  $\mathbf{V}_{an} = 240 \angle 0^\circ$  V rms and  $\mathbf{Z}_\Delta = 51 + j45 \Omega$ . If the line impedance per phase is  $0.4 + j1.2 \Omega$ , find the total complex power delivered to the load.



**Replace the delta load with a Y load,  $\mathbf{Z}_Y = \mathbf{Z}_\Delta / 3$**

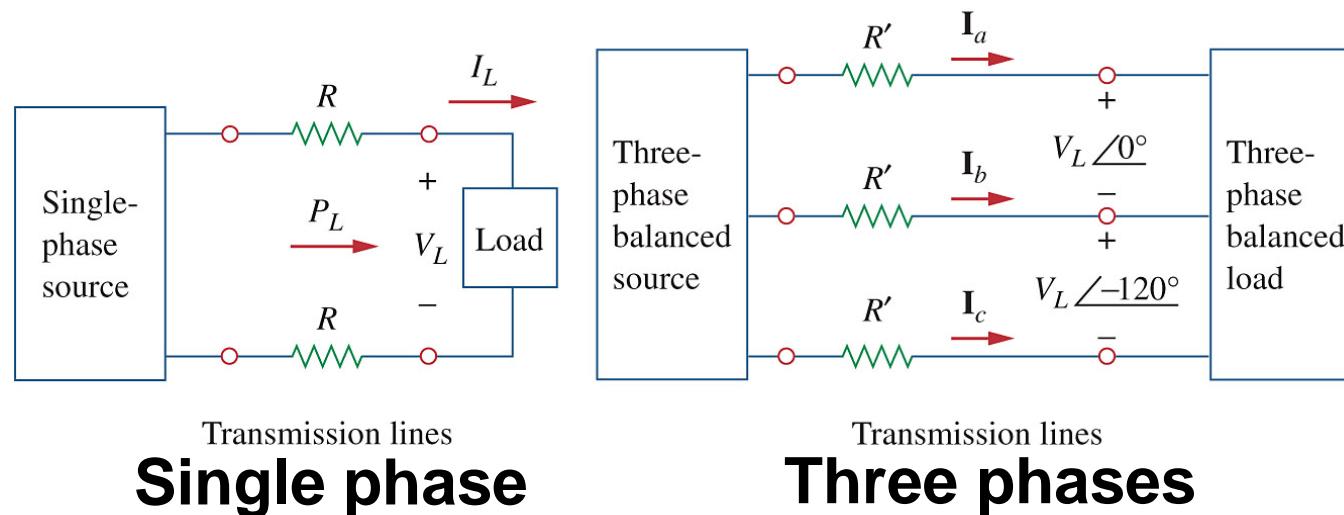


$$\mathbf{I}_a = \mathbf{V}_{an} / |\mathbf{Z}_Y + \mathbf{Z}_l| = 240 / |17 + j15 + 0.4 + j1.2| = 240 / |17.4 + j16.2| = 240 / 23.77 = 10.095$$

$$\begin{aligned} \mathbf{S} &= 3[(\mathbf{I}_a)^2(17 + j15)] = 3 \times 101.91(17 + j15) \\ &= [5.197 + j4.586] \text{ kVA.} \end{aligned}$$

## Three phase system - Advantage 2:

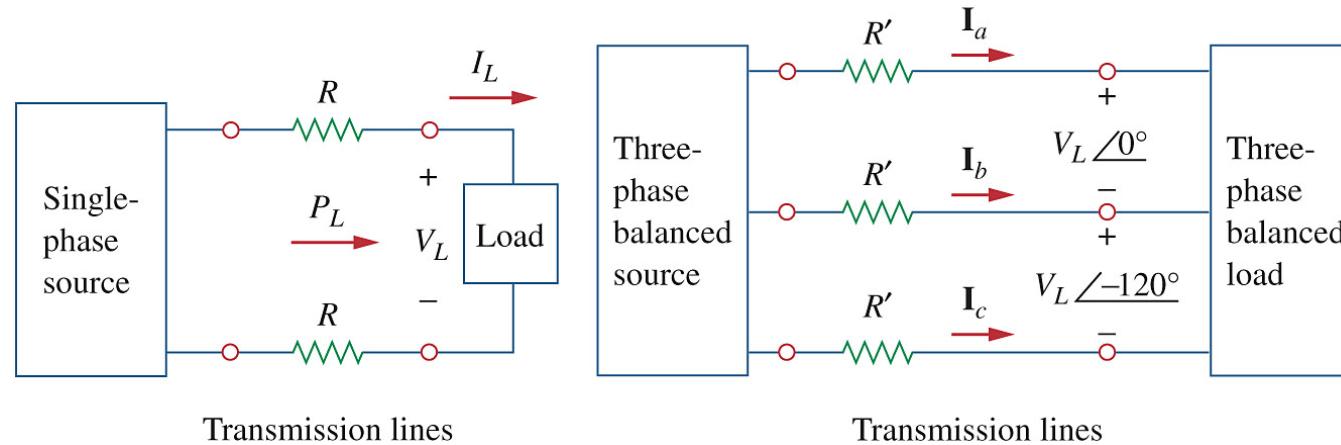
The three-phase system uses a lesser amount of wire than the single-phase system for the same line voltage  $V_L$  and **the same absorbed power  $P_L$**  → Economical



1. The same total power delivered  $P_L$
2. The same line voltage  $V_L$

## Recall: Average power in the rms form in Chapter 11

$$P = \frac{1}{2}V_m I_m \cos(\theta_v - \theta_i) = V_{\text{rms}} I_{\text{rms}} \cos(\theta_v - \theta_i)$$



Assume that the load is purely resistive

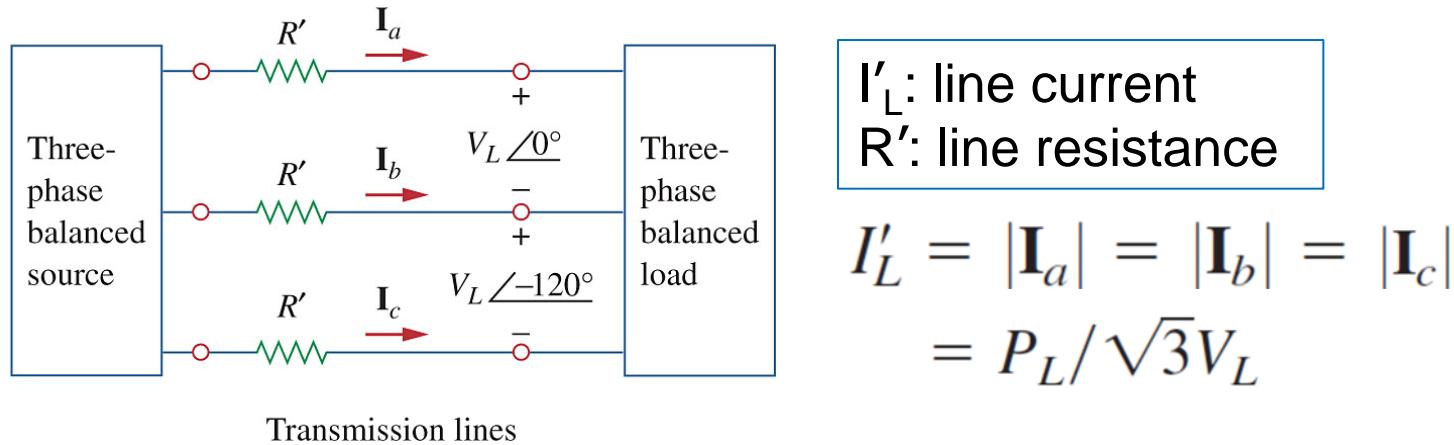
For the single-phase **two-wire system**,  $P_L = V_L I_L$ , the power loss in the two wires is

$$P_{\text{loss}} = 2I_L^2 R = 2\left(\frac{P_L}{V_L}\right)^2 R$$

**2 wires**

## Recall: Average power in the rms form in Chapter 11

$$P = \frac{1}{2}V_m I_m \cos(\theta_v - \theta_i) = V_{\text{rms}} I_{\text{rms}} \cos(\theta_v - \theta_i)$$



For the three-phase wire system,  $P_L = \sqrt{3}V_L I_L'$ , the power loss in **the three wires** is

$$P'_{\text{loss}} = 3I_L'^2 R' = 3 \left( \frac{P_L}{\sqrt{3}V_L} \right)^2 R' = \left( \frac{P_L}{V_L} \right)^2 R' \quad \boxed{\text{3 wires}}$$

The equations show that for **the same total power delivered  $P_L$  and the same line voltage  $V_L$** ,

$$P_{loss} = 2I_L^2 R = 2 \left( \frac{P_L}{V_L} \right)^2 R \quad \boxed{2 \text{ wires}}$$

$$P'_{loss} = 3I'_L^2 R' = 3 \left( \frac{P_L}{\sqrt{3}V_L} \right)^2 R' = \left( \frac{P_L}{V_L} \right)^2 R' \quad \boxed{3 \text{ wires}}$$

$$\frac{P_{loss}}{P'_{loss}} = \frac{2R}{R'} = \frac{2\rho l / (\pi r^2)}{\rho l / (\pi r'^2)} = \frac{2r'^2}{r^2}$$

$$R = \frac{\rho L}{A}$$

$\rho$  = resistivity  
 $L$  = length  
 $A$  = cross sectional area

where  $\rho$  is resistivity;  $l$  is length of transmission line; and  $r$  is radius of the transmission line

If we consider **the same power loss** in both systems,

$$\frac{P_{loss}}{P'_{loss}} = \frac{2r'^2}{r^2} = 1 \text{ thus, } r^2 = 2r'^2$$

Two wires  
Material volume needed

Two wires

Three wires

$$\frac{\text{Material for single-phase}}{\text{Material for three-phase}} = \frac{2(\pi r^2 l)}{3(\pi r'^2 l)} = \frac{2r^2}{3r'^2} = \frac{4}{3}$$



<https://www.energy.gov/sites/prod/files/2015/12/f28/united-states-electricity-industry-primer.pdf>

The second major advantage of three-phase systems for power distribution: **Economical**

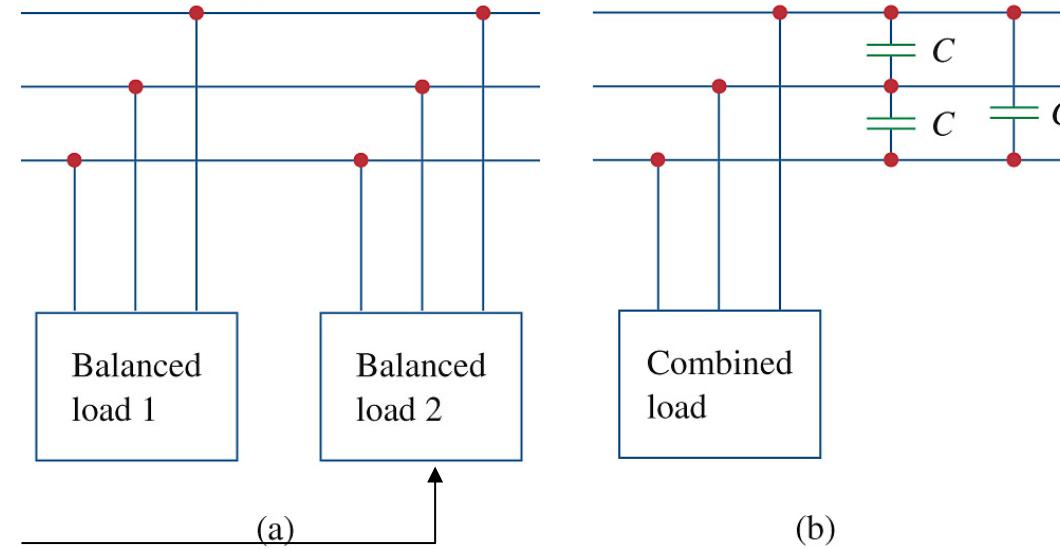
## **Summary of the advantages of 3-φ system**

1. The total instantaneous power in a balanced three-phase system is constant.
2. The material (transmission line) to deliver the same power and to tolerate the same loss needed is  $\frac{3}{4}$  times less.

## Example 12.8

$$\begin{aligned}S &= P + jQ = 3V_P I_P \cos \theta + j3V_P I_P \sin \theta \\&= \sqrt{3}V_L I_L \cos \theta + j\sqrt{3}V_L I_L \sin \theta\end{aligned}$$

Two balanced loads are connected to a 240-kV rms 60-Hz line, as shown in Fig. 12.22(a). Load 1 draws 30 kW at a power factor of 0.6 lagging, while load 2 draws 45 kVAR at a power factor of 0.8 lagging. Assuming the *abc* sequence, determine: (a) the complex, real, and reactive powers absorbed by the combined load, (b) the line currents, and (c) the kVAR rating of the three capacitors  $\Delta$ -connected in parallel with the load that will raise the power factor to 0.9 lagging and the capacitance of each capacitor.



30kW  
pf=0.6 lagging

45kVAR  
pf=0.8 lagging

Figure 12.22 (a) The original balanced loads, (b) the combined load with improved power factor.

Load 1:

30kW

$\text{pf}=0.6$  lagging

Load 2:

45kVAR

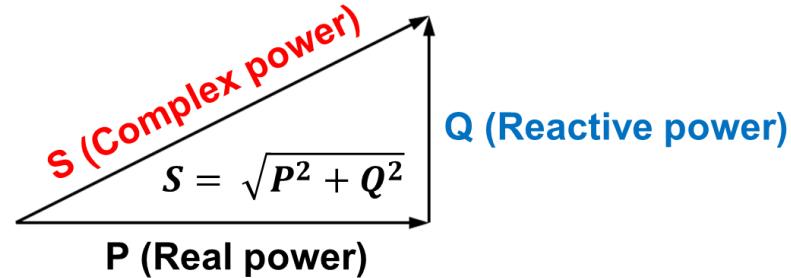
$\text{pf}=0.8$  lagging

$V_L = 240\text{kV}, 60 \text{ Hz}$

$$\begin{aligned} S &= P + jQ = 3V_P I_P \cos \theta + j3V_P I_P \sin \theta \\ &= \sqrt{3}V_L I_L \cos \theta + j\sqrt{3}V_L I_L \sin \theta \end{aligned}$$

## (a) S, P, Q

Load 1: 30kW, pf=0.6 lagging



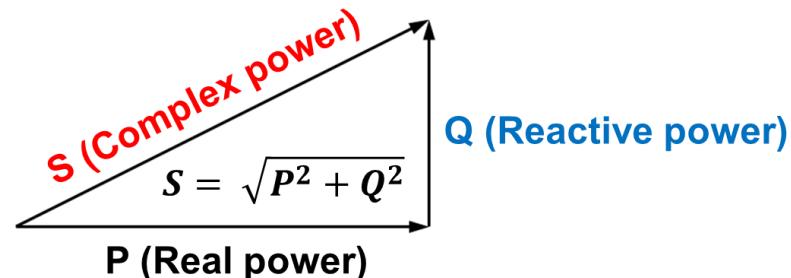
$$\cos \theta_1 = 0.6 \rightarrow \theta_1 = 53.13^\circ$$

$$\tan 53.13^\circ = Q/P$$

$$\text{Thus, } Q = 40\text{k [VAR]}$$

$$\mathbf{S}_1 = 30\text{k} + \mathbf{j}40\text{k [VA]}$$

Load 2: 45kVAR, pf=0.8 lagging



$$\cos \theta_2 = 0.8 \rightarrow \theta_2 = 36.87^\circ$$

$$\tan 36.87^\circ = Q/P$$

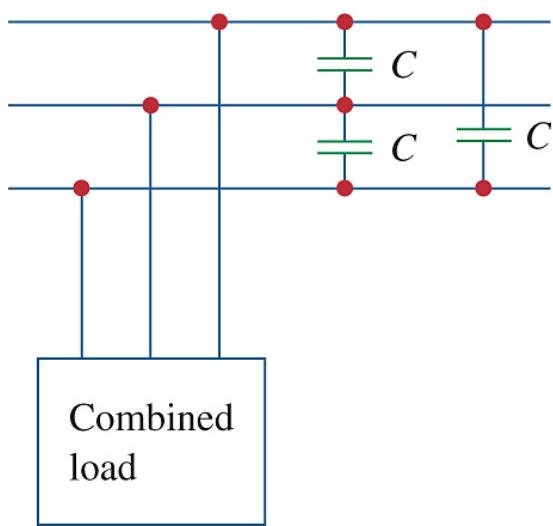
$$\text{Thus, } P = 60\text{k [W]}$$

$$\mathbf{S}_1 = 60\text{k} + \mathbf{j}45\text{k [VA]}$$

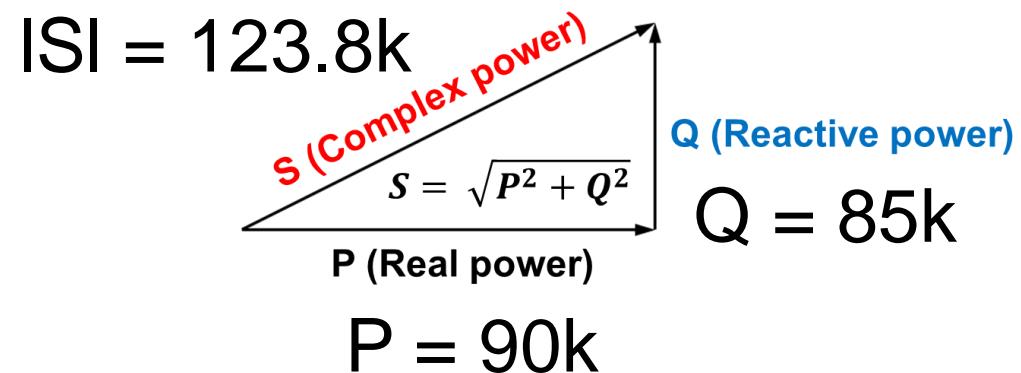
Complex power absorbed by the combined load, therefore, is

$$\mathbf{S} = 90\text{k} + \mathbf{j}85\text{k [VA]} \text{ where } P = 90\text{kW} \text{ and } Q = 85\text{kVA}$$

## (b) Line currents



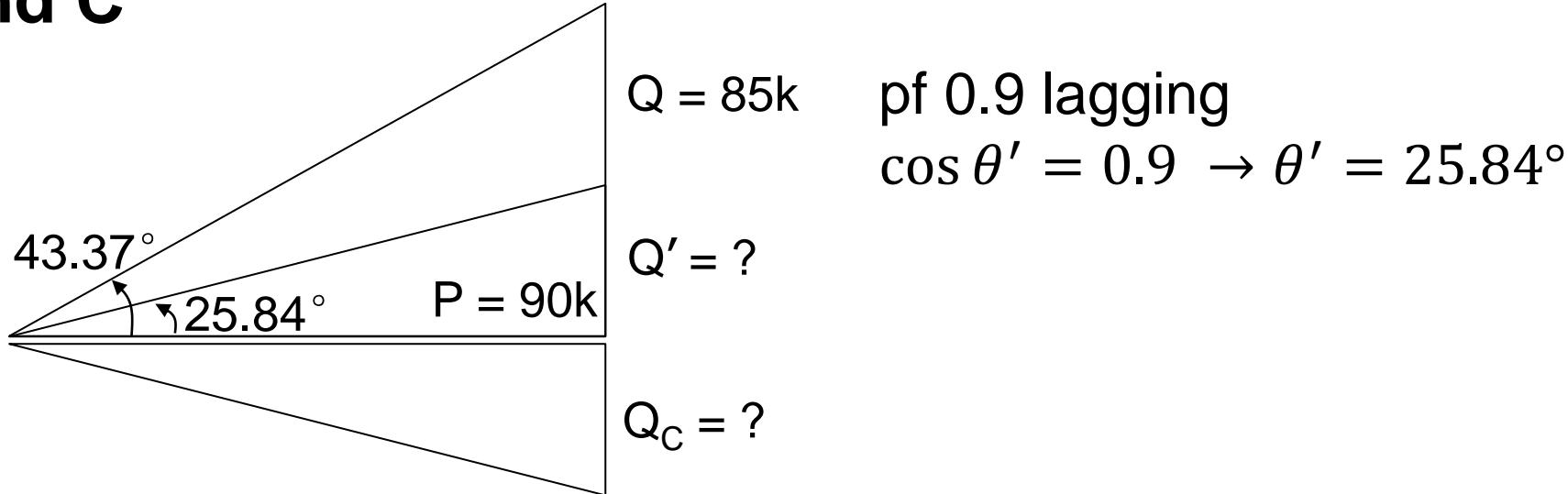
240 kV rms 60-Hz line  $\rightarrow V_L = 240 \text{ kV}$   
S from (a) is  $90\text{k} + j85\text{k}$



$$P = \sqrt{3}V_L I_L \cos \theta \rightarrow 90\text{k} = \sqrt{3} 240\text{k} I_L \frac{90}{123.8}$$

Thus,  $I_L = 0.296 \text{ A}$  or  $0.296 \text{ mA}$

### (c) $Q_C$ and $C$



$$Q' \rightarrow \tan 25.84 = \frac{Q'}{P(90k)} \rightarrow Q' = 43.56k$$

$$Q_C = Q - Q' = 85k - 43.56k = \mathbf{41.44k \text{ VAR}}$$

→ Each capacitor has an effect of 13.81k VAR

$Q_C = I^2X = \omega CV^2$  for purely capacitive case, and thus,

$$C = \frac{Q_C}{\omega(=2\pi f)V^2} = \mathbf{6.36 \times 10^{-10} [F]}$$