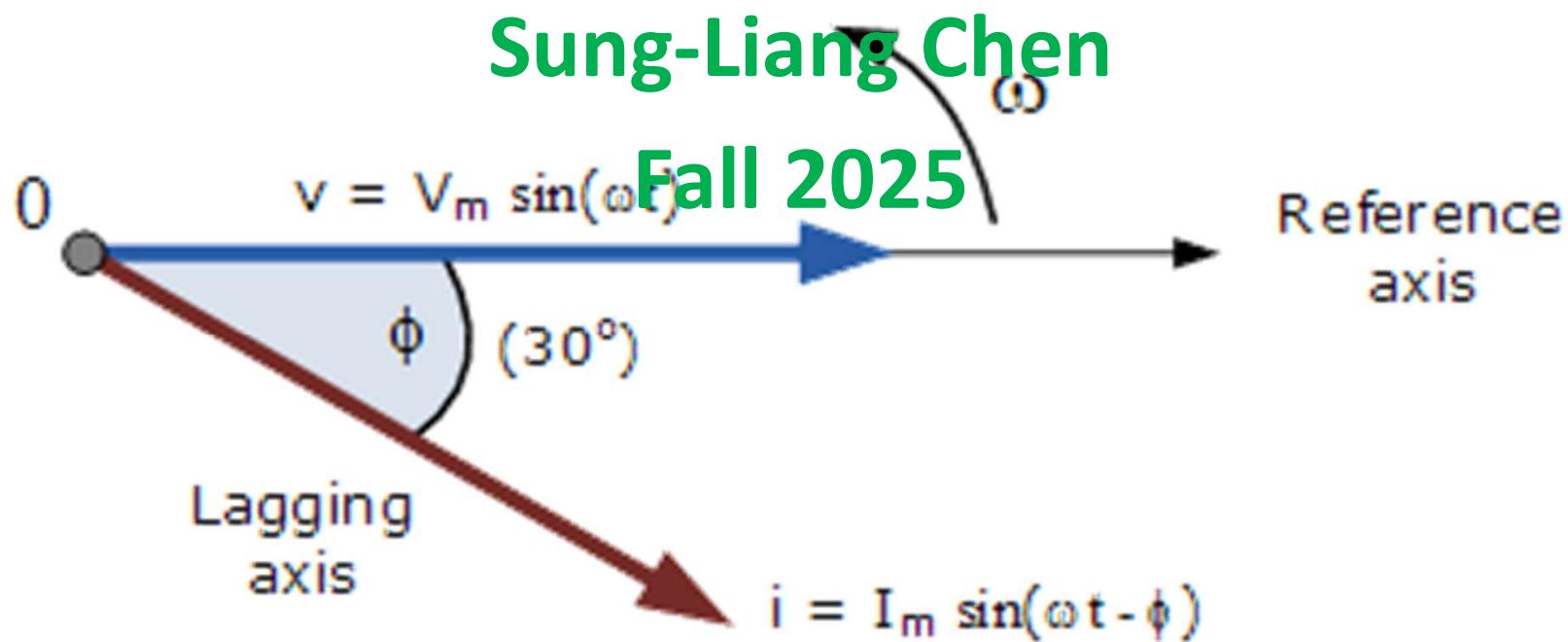


Chapter 9 Sinusoids and Phasors



9.1 Introduction

- Circuits driven by sinusoidal current or voltage sources are called alternating current (ac) circuits.
- We now begin the analysis of ac circuits.
- We are interested in sinusoidal **steady-state** response of ac circuits.

9.2 Sinusoids

A sinusoid is a signal that has the form of the sine or cosine function. For example,

$$v(t) = V_m \sin(\omega t + \phi)$$

where

V_m : amplitude

ω : angular frequency

ϕ : initial phase

Let us examine the two sinusoids

$$v_1(t) = V_m \sin \omega t$$

$$v_2(t) = V_m \sin(\omega t + \phi)$$

shown in Fig. 9.2.

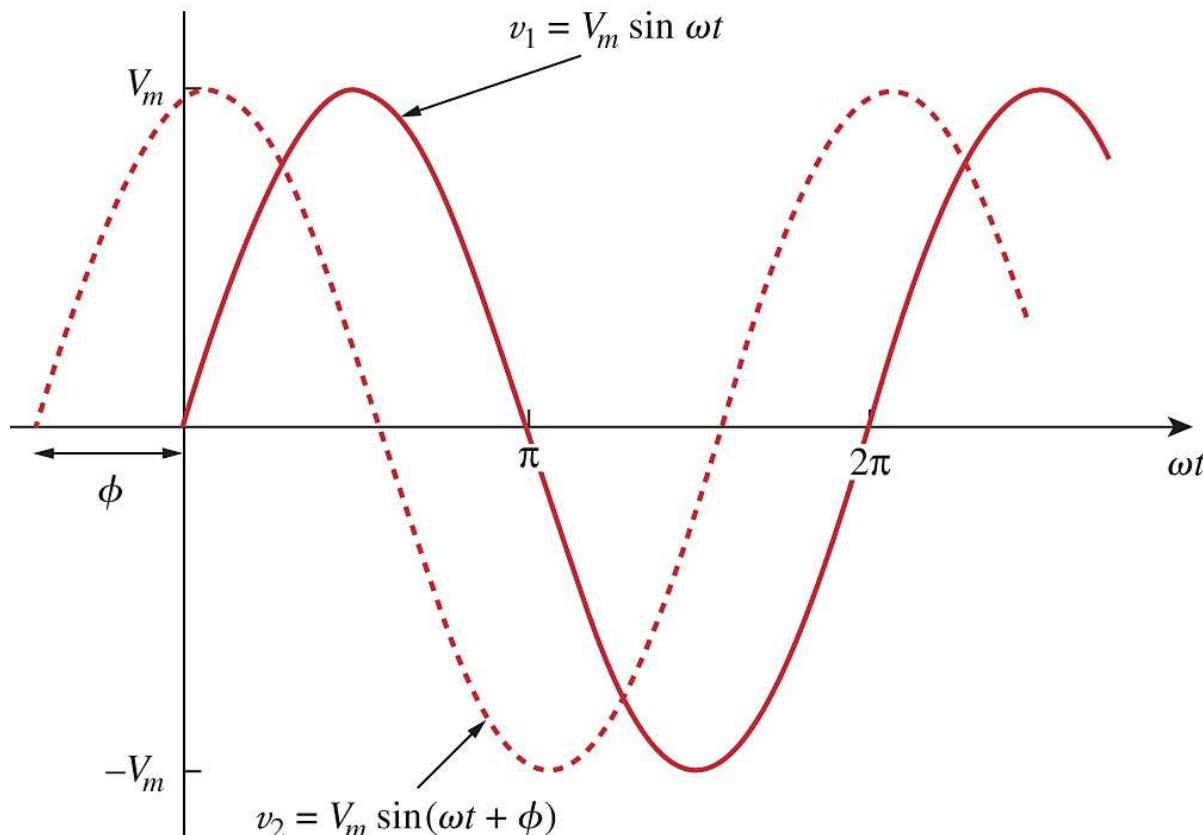


Figure 9.2 Two sinusoids with different phases.

The starting point of v_2 in Fig. 9.2 occurs first in time. Therefore, we say that v_2 leads v_1 by ϕ or that v_1 lags v_2 by ϕ . If $\phi \neq 0$, we say that v_1 and v_2 are *out of phase*. If $\phi = 0$, then v_1 and v_2 are said to be *in phase*.

9.3 Phasors

Sinusoids are easily expressed in terms of phasors, which are more convenient to work with than sine and cosine functions. A phasor is a complex number that represents the amplitude and phase of a sinusoid.

Given a sinusoid

$$v(t) = V_m \cos(\omega t + \phi)$$

$$= \operatorname{Re} \left(V_m e^{j(\omega t + \phi)} \right)$$

$$= \operatorname{Re} \left(V_m e^{j\phi} e^{j\omega t} \right)$$

$$= \operatorname{Re} \left(\tilde{V} e^{j\omega t} \right)$$

where $\tilde{V} = V_m e^{j\phi} = V_m \angle \phi$ is the phasor representation of the sinusoid $v(t)$.

Figure 9.7 shows the *sinor* $\tilde{V}e^{j\omega t} = V_m e^{j(\omega t + \phi)}$ on the complex plane. As time increases, the sinor rotates on a circle of radius V_m at an angular velocity ω in the counterclockwise direction. We may regard $v(t)$ as the projection of the sinor on the real axis.

$$\underline{\tilde{V}e^{j\omega t}} = V_m e^{j(\omega t + \phi)}$$

Sinor

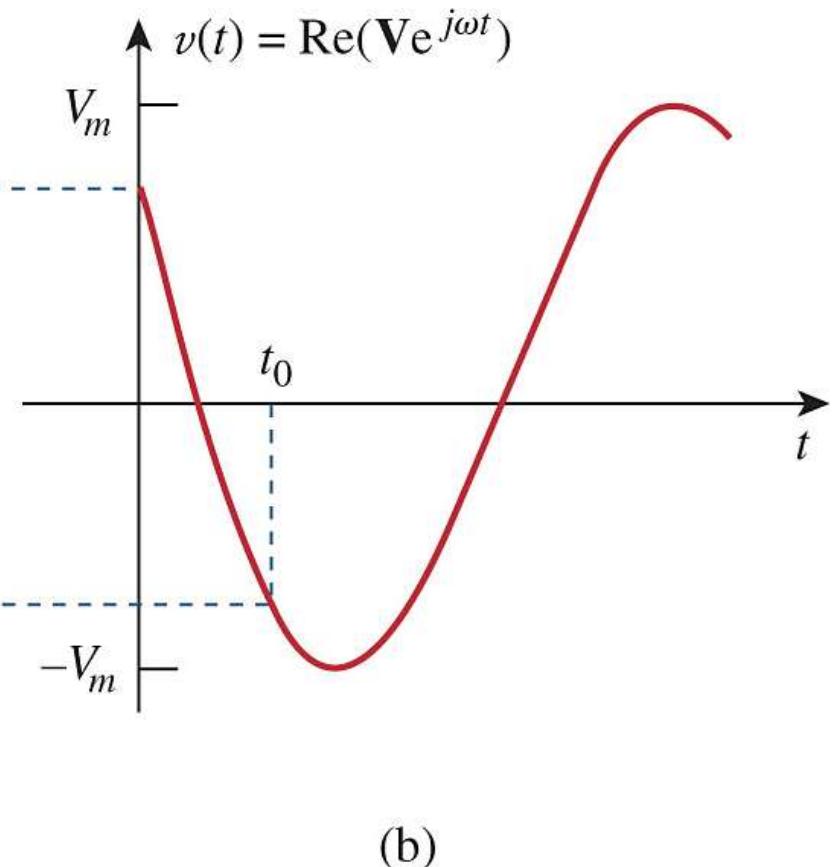
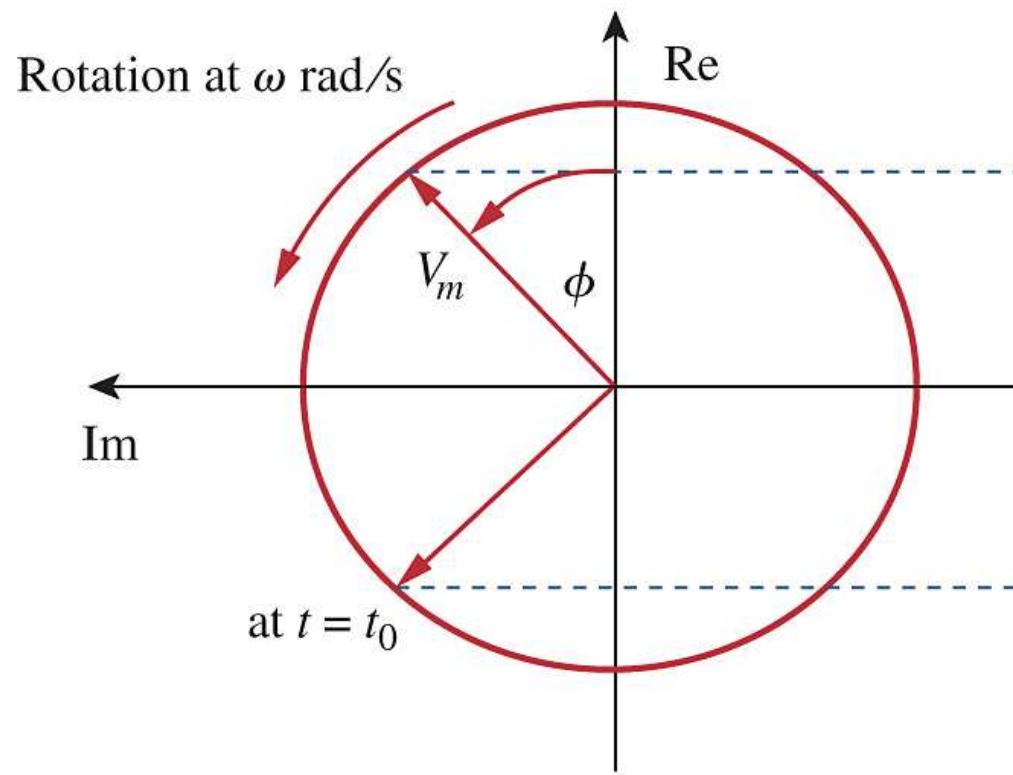


Figure 9.7 Representation of sinor: (a) sinor rotating counterclockwise, (b) its projection on the real axis, as a function of time.

$$\underline{\tilde{V}e^{j\omega t}} = V_m e^{j(\omega t + \phi)}$$

Sinor

The value of the sinor at time $t = 0$ is the phasor \tilde{V} . The sinor may be regarded as a rotating phasor. Thus, whenever a sinusoid is expressed as a phasor, the term $e^{j\omega t}$ is implicitly present.

Since a phasor has magnitude and phase ("direction"), it behaves as a vector. Figure 9.8 shows two phasors: $\tilde{V} = V_m \angle \phi$ and $\tilde{I} = I_m \angle -\theta$. Such a graphical representation of phasors is known as a *phasor diagram*.

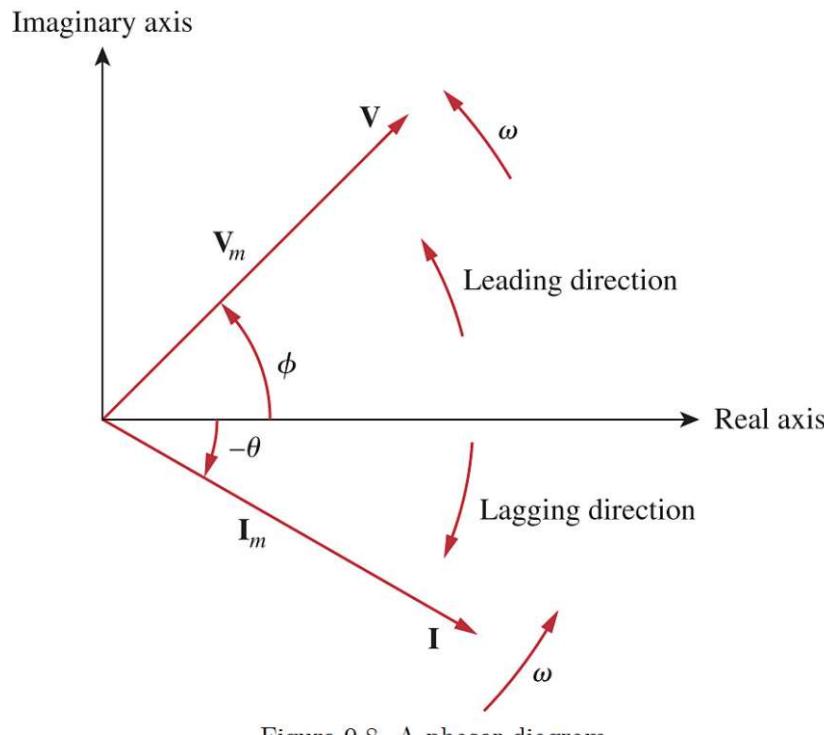


Figure 9.8 A phasor diagram.

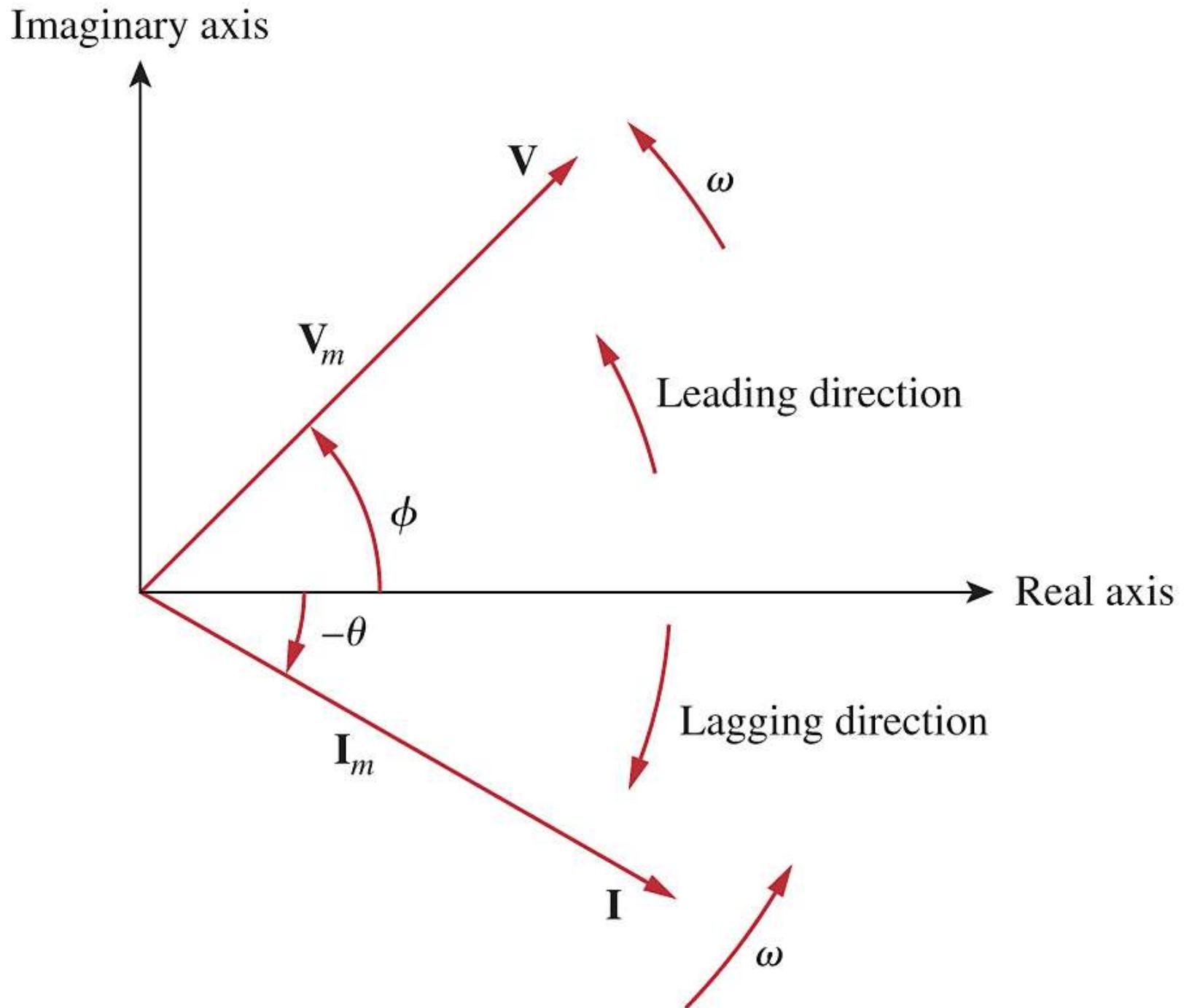


Figure 9.8 A phasor diagram.

In conclusion, a sinusoid has a time-domain representation $v(t) = V_m \cos(\omega t + \phi)$ and a phasor-domain representation $\tilde{V} = V_m \angle \phi$.

The phasor domain is also known as the frequency domain.

$$v(t) = V_m \cos(\omega t + \phi) \Leftrightarrow \tilde{V} = V_m \angle \phi$$

9.4 Phasor Relationships for Circuit Elements

We begin with the resistor. If the current through a resistor R is $i = \underline{I_m} \cos(\omega t + \underline{\phi})$, the voltage across it is given by Ohm's law as

$$v = iR = \underline{R} \underline{I_m} \cos(\omega t + \underline{\phi})$$

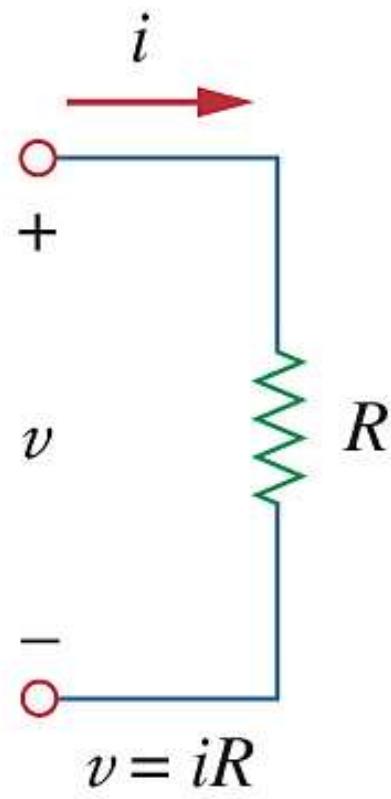
The phasor form of this voltage is

$$\tilde{V} = RI_m \angle \phi$$

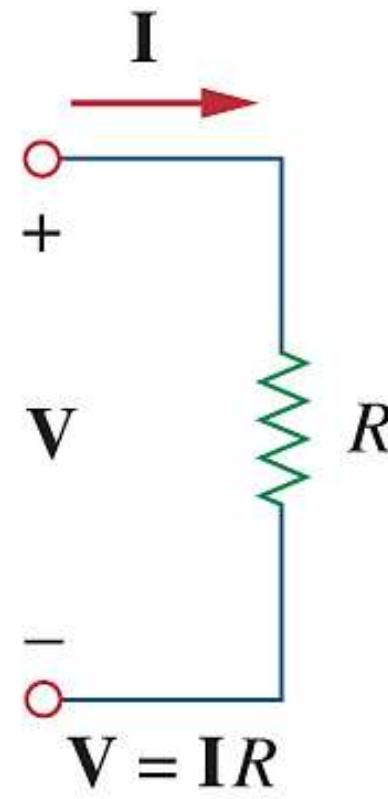
But the phasor representation of the current is $\tilde{I} = I_m \angle \phi$. Hence,

$$\tilde{V} = R\tilde{I}$$

showing the voltage-current relation for the resistor in the phasor domain continues to be Ohm's law, as in the time domain.



(a)



(b)

Figure 9.9 Voltage-current relations for a resistor in the (a) time domain, (b) frequency domain.

$$\tilde{V} = R\tilde{I}$$

$$\tilde{V} = RI_m \angle \phi \quad \tilde{I} = I_m \angle \phi$$

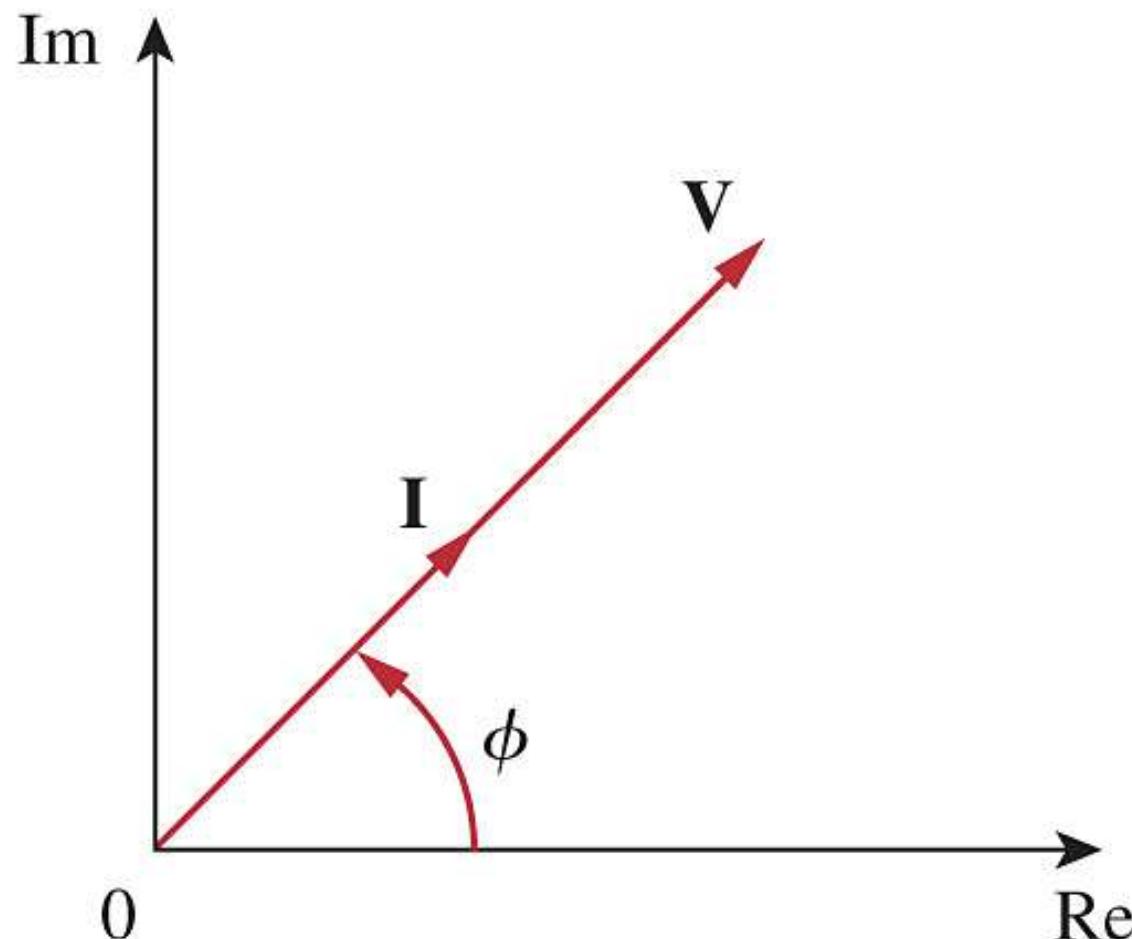


Figure 9.10 Phasor diagram for the resistor.

For the inductor L , if $i = I_m \cos(\omega t + \phi)$

$\Leftrightarrow \tilde{I} = I_m \angle \phi$, then

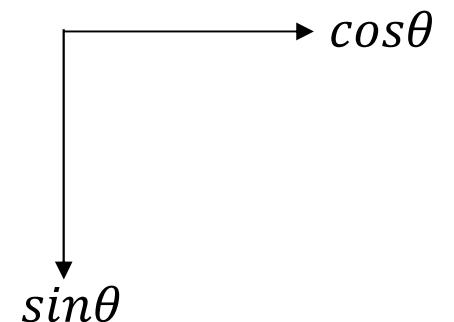
$$v = L \frac{di}{dt} = -\omega L I_m \sin(\omega t + \phi)$$

$$= \omega L I_m \cos(\omega t + \phi + 90^\circ) \Leftrightarrow$$

$$\tilde{V} = \omega L I_m \angle (\phi + 90^\circ) = j\omega L I_m \angle \phi$$

$$= j\omega L \tilde{I}$$

$$\angle 90^\circ = e^{j90^\circ} = j$$



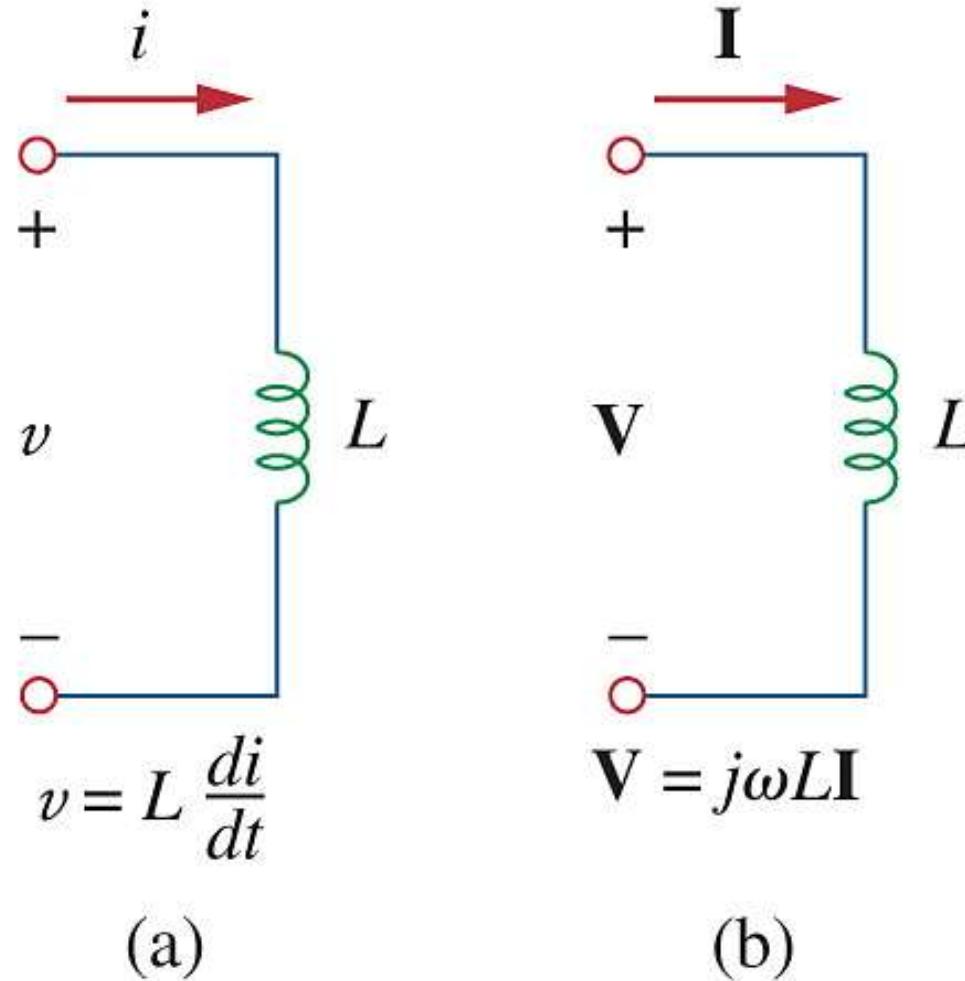


Figure 9.11 Voltage-current relations for an inductor in the (a) time domain, (b) frequency domain.

$$\tilde{I} = I_m \angle \phi \quad \tilde{V} = \omega L I_m \angle (\phi + 90^\circ) = j\omega L \tilde{I}$$

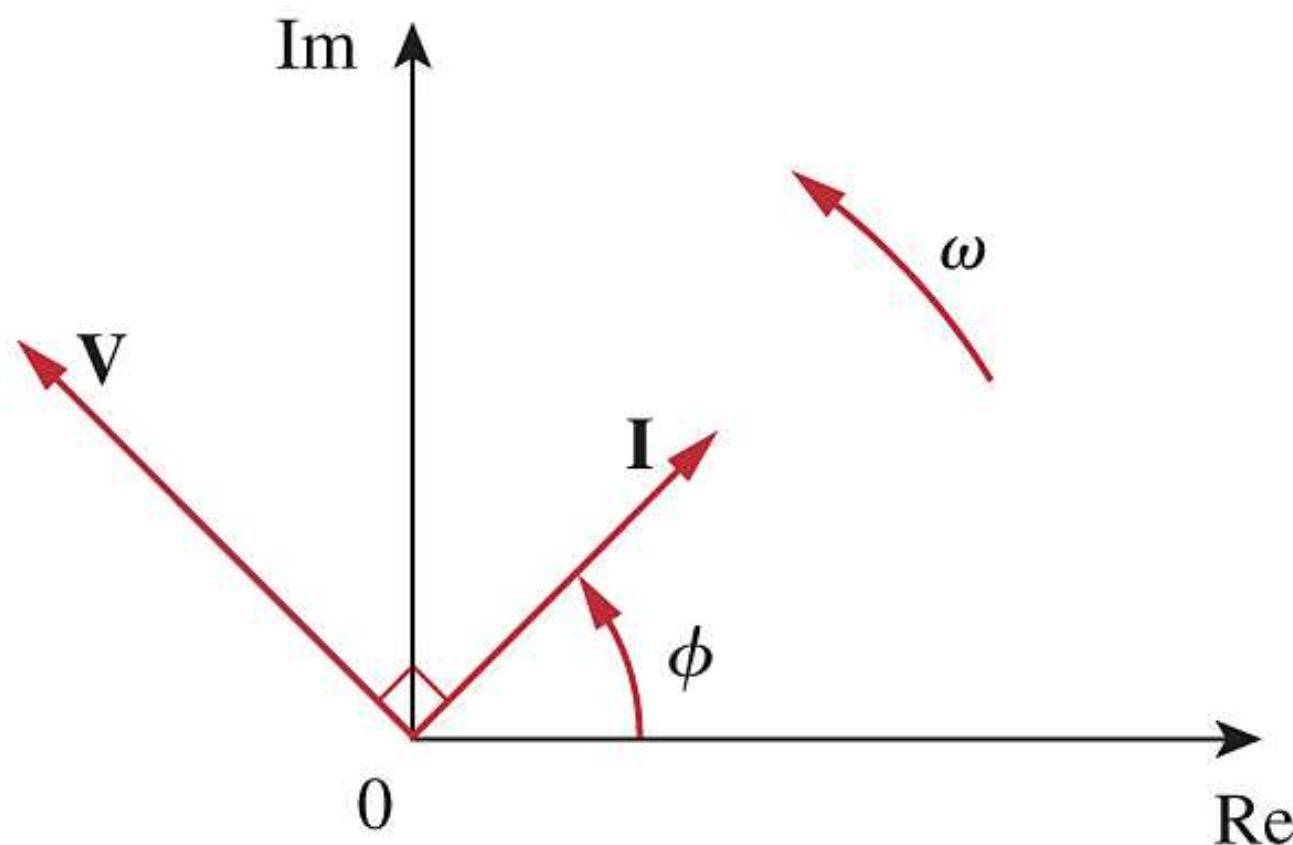
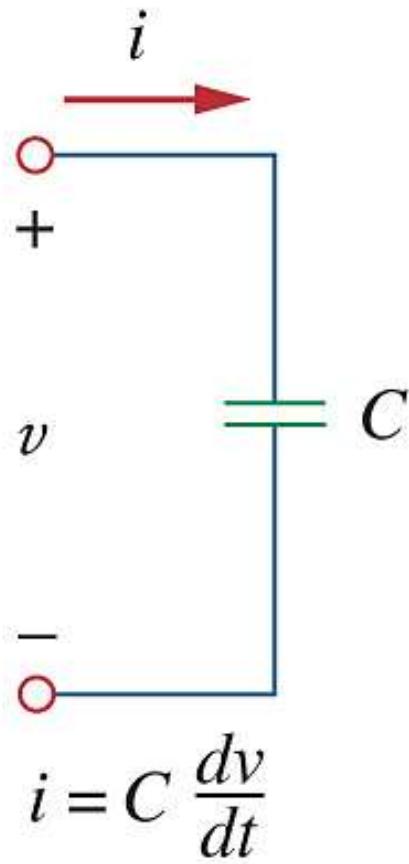


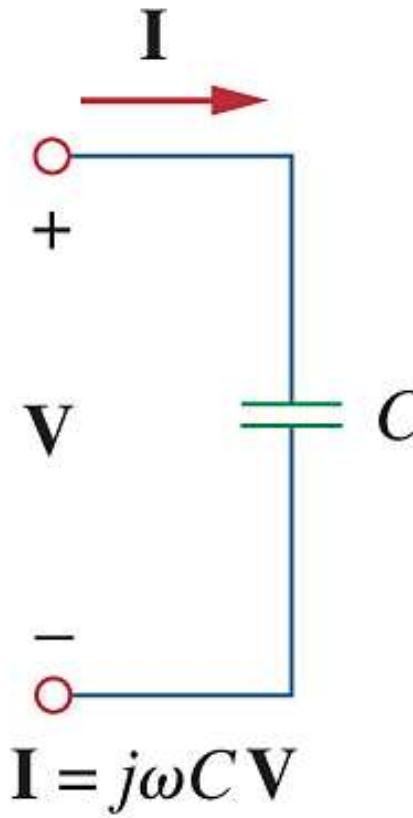
Figure 9.12 Phasor diagram for the inductor.

For the capacitor C , if $v = V_m \cos(\omega t + \phi)$
 $\Leftrightarrow \tilde{V} = V_m \angle \phi$, then

$$\begin{aligned} i &= C \frac{dv}{dt} = -\omega C V_m \sin(\omega t + \phi) \\ &= \omega C V_m \cos(\omega t + \phi + 90^\circ) \Leftrightarrow \\ \tilde{I} &= \omega C V_m \angle (\phi + 90^\circ) = j\omega C V_m \angle \phi \\ &= j\omega C \tilde{V} \end{aligned}$$



(a)



(b)

Figure 9.13 Voltage-current relations for a capacitor in the (a) time domain, (b) frequency domain.

$$\tilde{V} = V_m \angle \underline{\phi}$$

$$\tilde{I} = \omega C V_m \angle (\underline{\phi + 90^\circ}) = j\omega C \tilde{V}$$

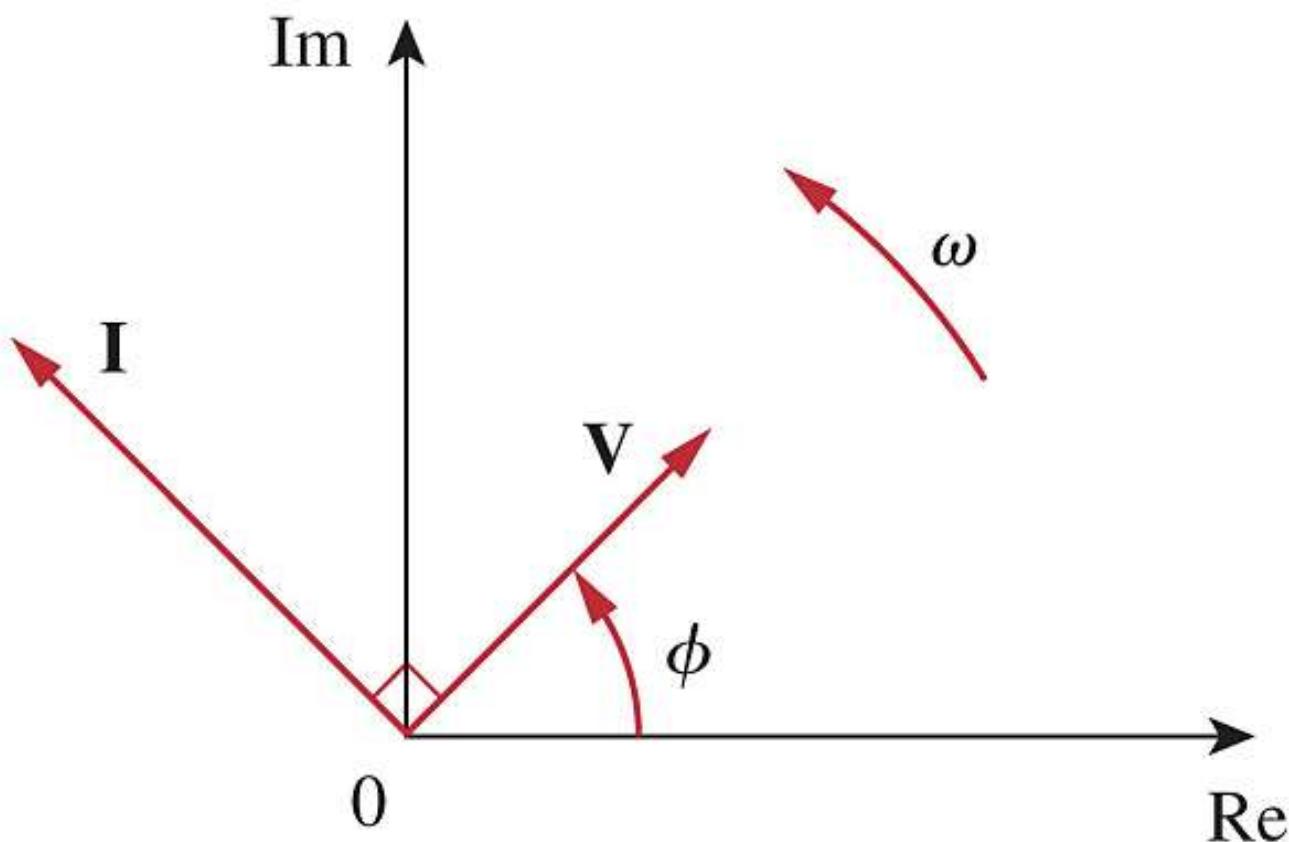


Figure 9.14 Phasor diagram for the capacitor.

TABLE 9.2

Summary of voltage - current relationships

Element	Time domain	Frequency domain
R	$v = Ri$	$\tilde{V} = R\tilde{I}$
L	$v = L \frac{di}{dt}$	$\tilde{V} = j\omega L\tilde{I}$
C	$i = C \frac{dv}{dt}$	$\tilde{V} = \frac{1}{j\omega C} \tilde{I}$

9.5 Impedance and Admittance

The impedance Z of a circuit is the ratio of the phasor voltage \tilde{V} to the phasor current \tilde{I} , measured in ohms (Ω).

$$Z = \frac{\tilde{V}}{\tilde{I}}$$

$$\boxed{\begin{aligned}\tilde{V} &= R\tilde{I} \\ \tilde{V} &= j\omega L\tilde{I} \\ \tilde{V} &= \frac{1}{j\omega C}\tilde{I}\end{aligned}}$$

For the three passive elements, we have $Z = R$, $Z = j\omega L$, and $Z = 1 / j\omega C$, respectively.

The admittance Y of a circuit is the ratio of the phasor current \tilde{I} to the phasor voltage \tilde{V} , measured in siemens (S).

$$Y = \frac{\tilde{I}}{\tilde{V}} = \frac{1}{Z}$$

$$\begin{aligned}\tilde{V} &= R\tilde{I} \\ \tilde{V} &= j\omega L\tilde{I} \\ \tilde{V} &= \frac{1}{j\omega C}\tilde{I}\end{aligned}$$

For the three passive elements, we have $Y = 1/R$, $Y = 1/j\omega L$, and $Y = j\omega C$, respectively.

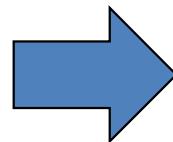
General definition of R

R : Resistance

G : Conductance

$$R = 1/G$$

(Real number)



Z : Impedance

Y : Admittance

$$Z = 1/Y$$

(Complex number)

The Ohm's law in phasor form is

$$\tilde{V} = Z\tilde{I} \text{ or } \tilde{I} = Y\tilde{V}$$

As a complex quantity, the impedance may be expressed in rectangular form or polar form

$$Z = R + jX = |Z| \angle \theta$$

where

R : resistance

X : reactance

If $X > 0$, we say that the impedance is inductive or lagging since current lags voltage; If $X < 0$, we say that the impedance is capacitive or leading because current leads voltage.

The impedance, resistance, and reactance are all measured in ohms.

$$\tilde{I} = I_m \angle \phi \quad \tilde{V} = \omega L I_m \angle (\phi + 90^\circ) = j\omega L \tilde{I}$$

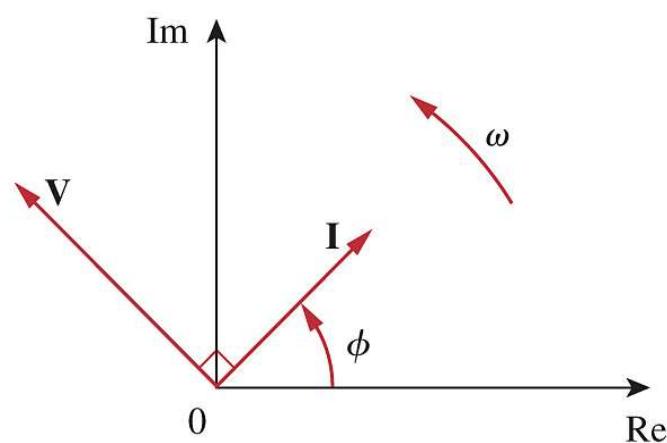


Figure 9.12 Phasor diagram for the inductor.

$$Z = R + jX$$

For an inductor, $Z = j\omega L$
 $\rightarrow X = \omega L > 0$
 \rightarrow Impedance is **inductive** or **lagging** (\mathbf{I} lags \mathbf{V})

$$\tilde{V} = V_m \angle \phi \quad \tilde{I} = \omega C V_m \angle (\phi + 90^\circ) = j\omega C \tilde{V}$$

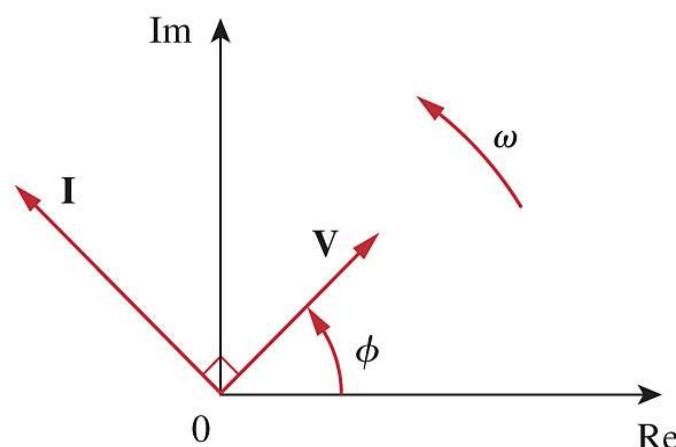


Figure 9.14 Phasor diagram for the capacitor.

$$Z = R + jX$$

For an inductor, $Z = 1/(j\omega C)$
 $\rightarrow X = -1/(\omega C) < 0$
 \rightarrow Impedance is **capacitive** or **leading** (\mathbf{I} leads \mathbf{V})

The admittance can be written as

$$Y = G + jB$$

where

G : conductance

B : susceptance

The admittance, conductance, and susceptance are all measured in siemens.

$$\left. \begin{array}{l} R: \text{resistance} \\ X: \text{reactance} \end{array} \right\} \text{Impedance } Z$$

$$\left. \begin{array}{l} G: \text{conductance} \\ B: \text{susceptance} \end{array} \right\} \text{Admittance } Y$$

9.6 Kirchhoff's Laws in the Frequency Domain

For KVL, Let v_1, v_2, \dots, v_n be the voltages around a closed loop. Then

$$\sum_{i=1}^n v_i = 0 \quad (9.51)$$

In sinusoidal steady state,

$$v_i = V_{mi} \cos(\omega t + \phi_i) = \operatorname{Re}(\tilde{V}_i e^{j\omega t})$$

$$\sum_{i=1}^n \operatorname{Re}(\tilde{V}_i e^{j\omega t}) = 0$$

$$\operatorname{Re}\left(\sum_{i=1}^n \tilde{V}_i e^{j\omega t}\right) = 0$$

but $e^{j\omega t} \neq 0$,

$$\sum_{i=1}^n \tilde{V}_i = 0$$

indicating that KVL holds for phasors.

For KCL, if i_1, i_2, \dots, i_n are the currents leaving or entering a closed surface in a circuit at time t , and $\tilde{I}_1, \tilde{I}_2, \dots, \tilde{I}_n$ are the phasor forms of i_1, i_2, \dots, i_n , then

$$\sum_{i=1}^n i_i = 0 \Rightarrow \sum_{i=1}^n \tilde{I}_i = 0$$

Since basic circuit laws, Kirchoff's and Ohm's, hold in phasor domain, it is not difficult to analyze ac circuits.

9.7 Impedance Combinations

For the N series-connected impedances shown in Fig. 9.18, the equivalent impedance at the input terminals is

$$Z_{eq} = \frac{\tilde{V}}{\tilde{I}} = \frac{\sum_{i=1}^N \tilde{V}_i}{\tilde{I}} = \sum_{i=1}^N \frac{\tilde{V}_i}{\tilde{I}} = \sum_{i=1}^N Z_i$$

KVL

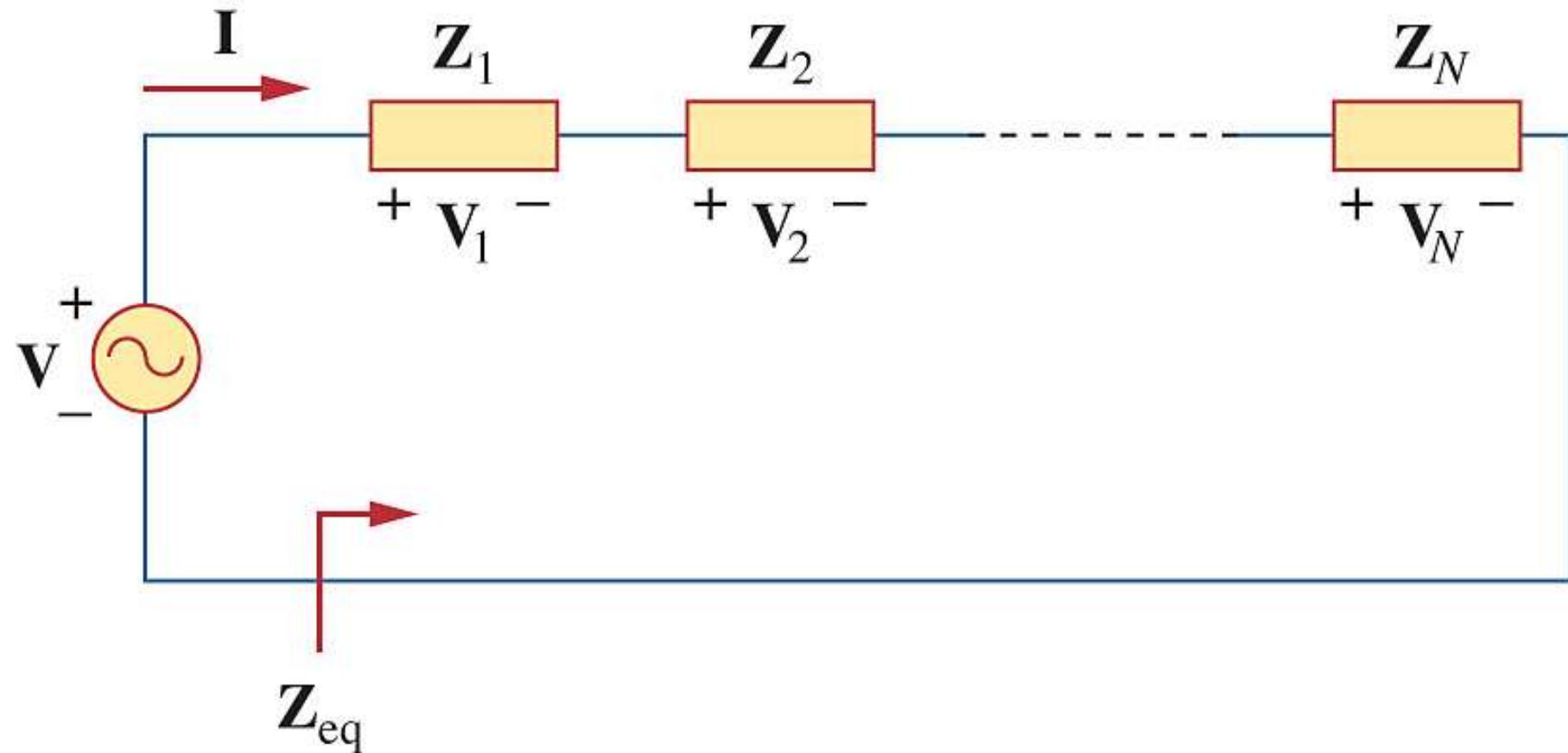


Figure 9.18 N impedances in series.

For the N parallel-connected impedances shown in Fig. 9.20, the equivalent admittance at the input terminals is

$$Y_{eq} = \frac{\tilde{I}}{\tilde{V}} = \frac{\sum_{i=1}^N \tilde{I}_i}{\tilde{V}} = \sum_{i=1}^N \frac{\tilde{I}_i}{\tilde{V}} = \sum_{i=1}^N Y_i$$

KCL

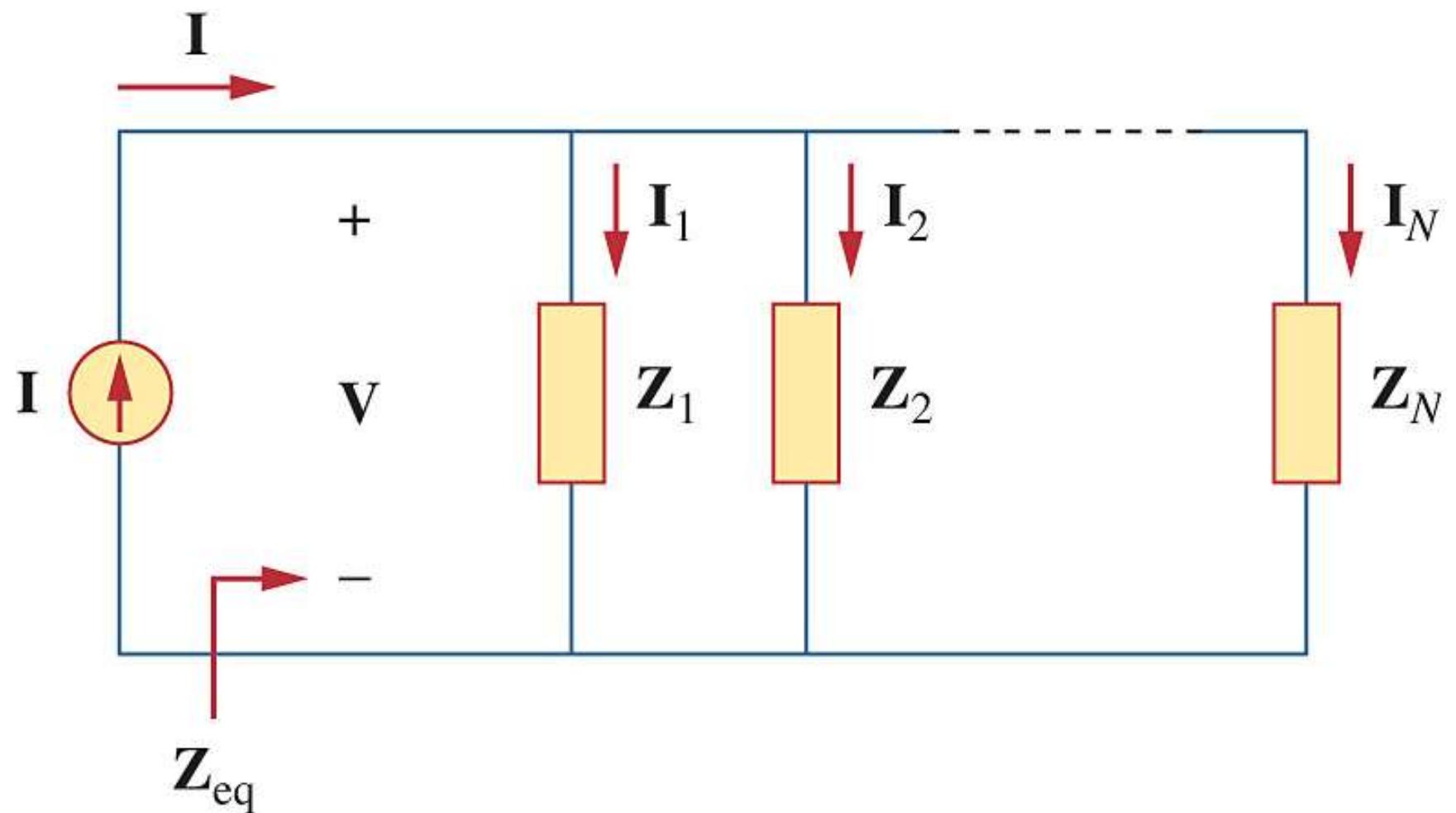


Figure 9.20 N impedances in parallel.

The delta-to-wye and wye-to-delta transformations that we applied to resistive circuits are also valid for impedances. With reference to Fig. 9.22, the conversion formulas are as follows:

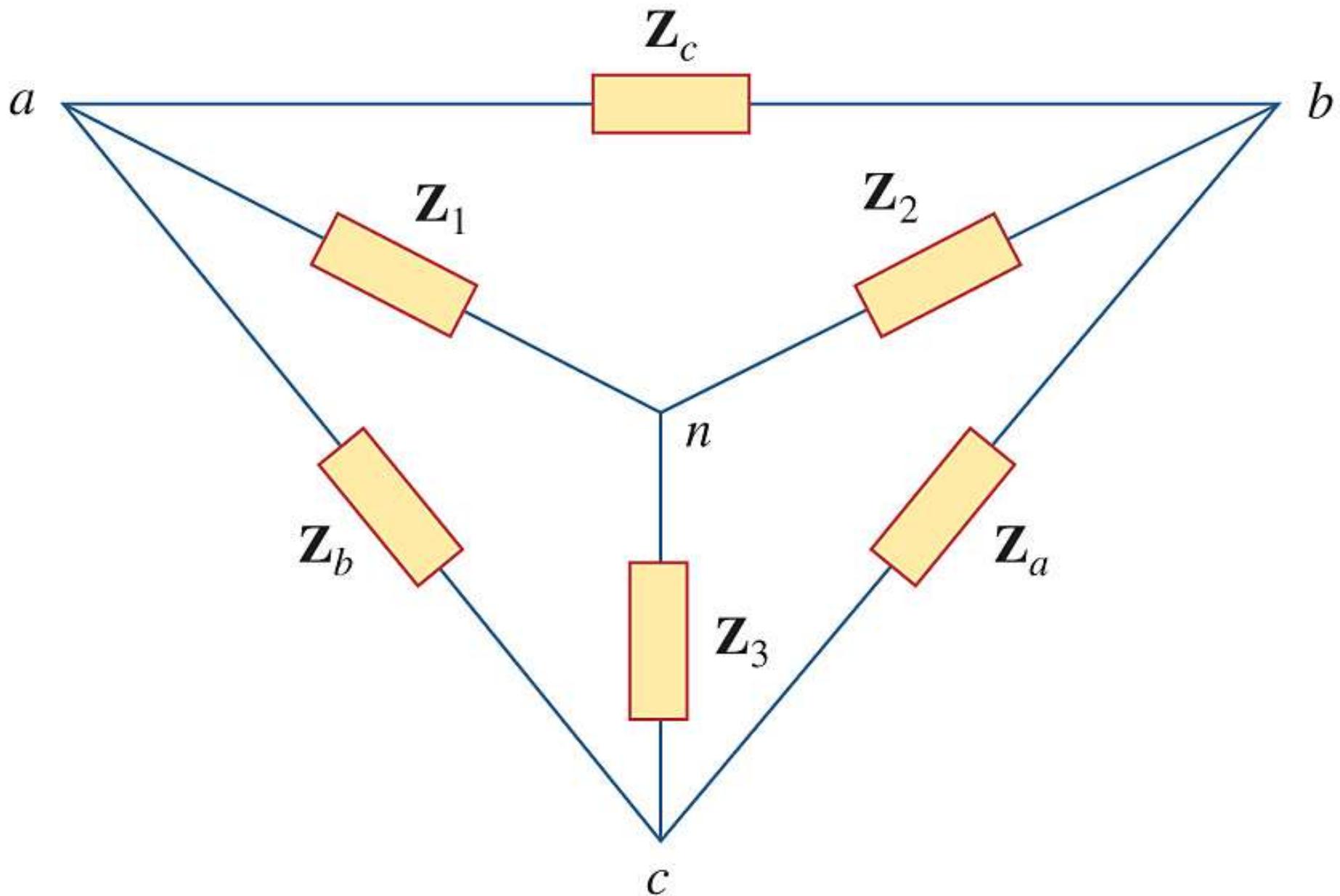


Figure 9.22 Superimposed wye and delta networks.

Y - Δ conversion:

$$Z_a = \frac{Z_1 Z_2 + Z_2 Z_3 + Z_3 Z_1}{Z_1}$$

$$Z_b = \frac{Z_1 Z_2 + Z_2 Z_3 + Z_3 Z_1}{Z_2}$$

$$Z_c = \frac{Z_1 Z_2 + Z_2 Z_3 + Z_3 Z_1}{Z_3}$$

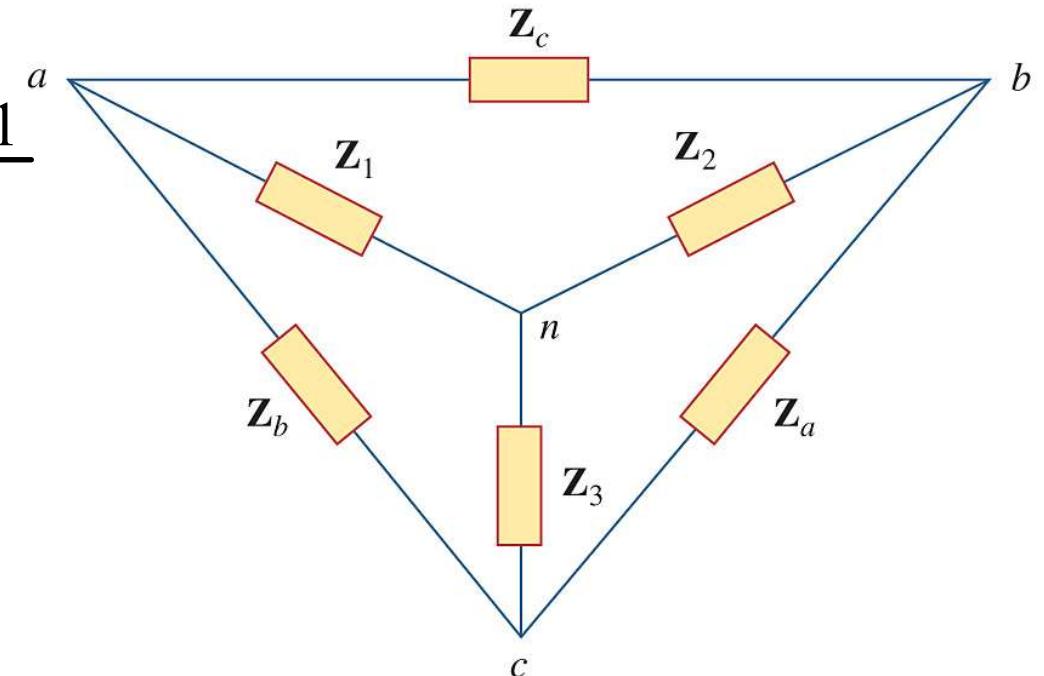


Figure 9.22 Superimposed wye and delta networks.

Δ - Y conversion:

$$Z_1 = \frac{Z_b Z_c}{Z_a + Z_b + Z_c}$$

$$Z_2 = \frac{Z_c Z_a}{Z_a + Z_b + Z_c}$$

$$Z_3 = \frac{Z_a Z_b}{Z_a + Z_b + Z_c}$$

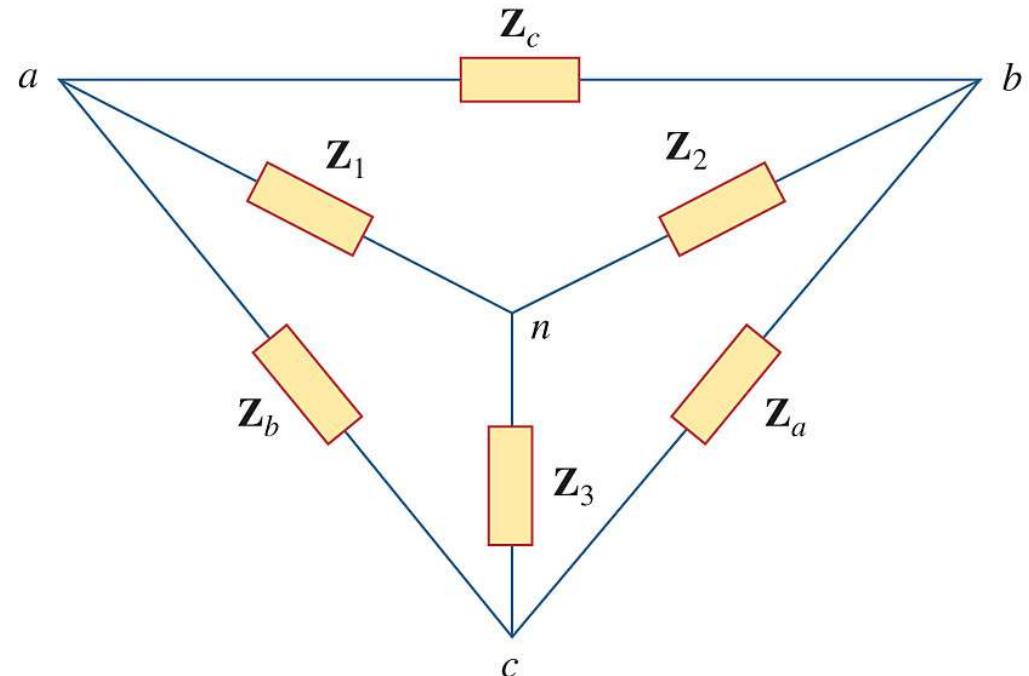


Figure 9.22 Superimposed wye and delta networks.

Practice Problem 9.10 Find the input impedance of the circuit in Fig. 9.24 at $\omega = 10 \text{ rad/s}$.

Solution :

$$8\text{-H inductor: } Z_1 = j10 \times 8 = j80 \text{ } (\Omega)$$

$$\begin{aligned} \text{0.5-mF capacitor: } Z_2 &= \frac{1}{j10 \times (0.5 \times 10^{-3})} \\ &= -j200 \text{ } (\Omega) \end{aligned}$$

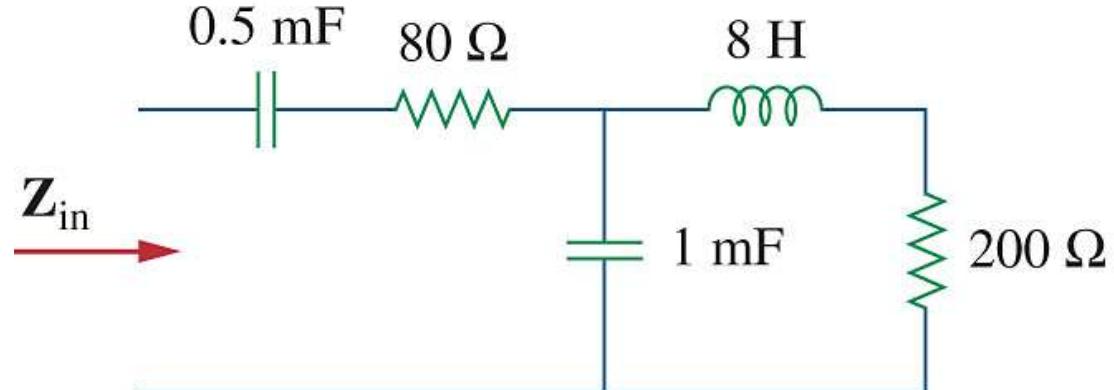


Figure 9.24

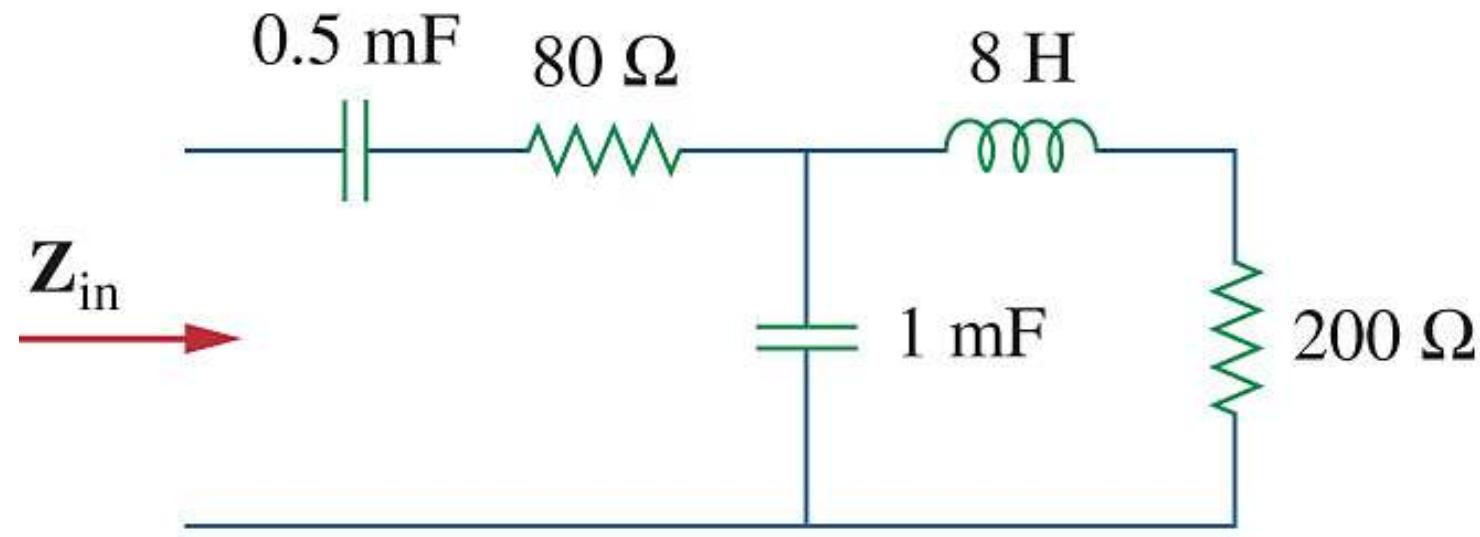


Figure 9.24

$$1\text{-mF capacitor: } Z_3 = \frac{1}{j10 \times (1 \times 10^{-3})}$$

$$= -j100 \text{ } (\Omega)$$

$$Z_{in} = Z_2 + 80 + Z_3 \parallel (Z_1 + 200)$$

where

$$Z_3 \parallel (Z_1 + 200) = (-j100) \parallel (j80 + 200)$$

$$= \frac{(-j100) \times (j80 + 200)}{(-j100) + (j80 + 200)}$$

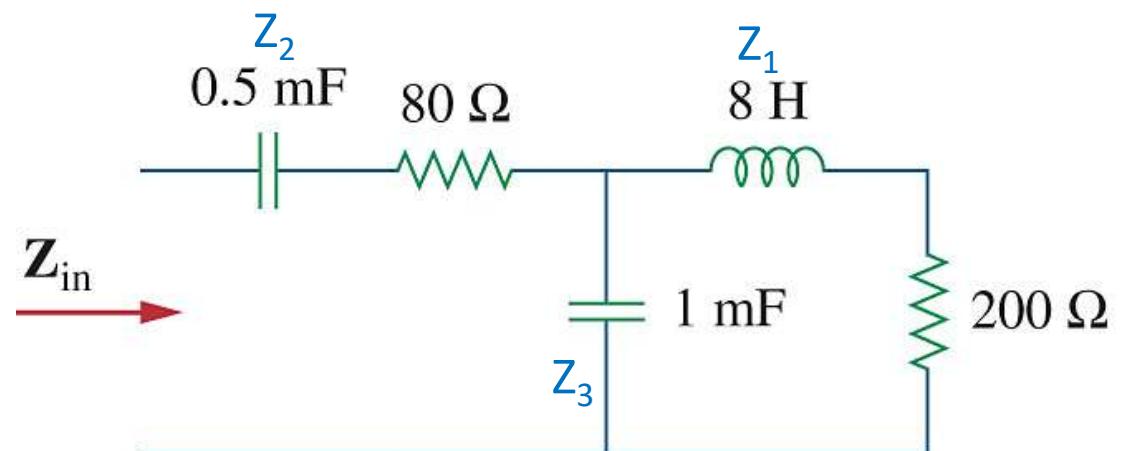


Figure 9.24

$$= \frac{(-j100) \times (200 + j80)}{200 - j20}$$

Rectangular form

$$\approx \frac{(100 \angle -90^\circ) \times 215.4066 \angle 21.80^\circ}{200.9975 \angle -5.71^\circ}$$

Polar form

$$\approx 107.1688 \angle -62.49^\circ$$

$$\approx 49.5016 - j95.0512 \text{ } (\Omega)$$

Rectangular form

$$Z_{in} = -j200 + 80 + 49.5016 - j95.0512$$

$$\approx 129.50 - j295.05 \text{ } (\Omega)$$

Practice Problem 9.11 Calculate v_o in the circuit of Fig. 9.27.

Solution :

0.5-H inductor: $Z_1 = j10 \times 0.5 = j5 \text{ } (\Omega)$

$\frac{1}{20}$ -F capacitor: $Z_2 = \frac{1}{j10 \times (1/20)} = -j2 \text{ } (\Omega)$

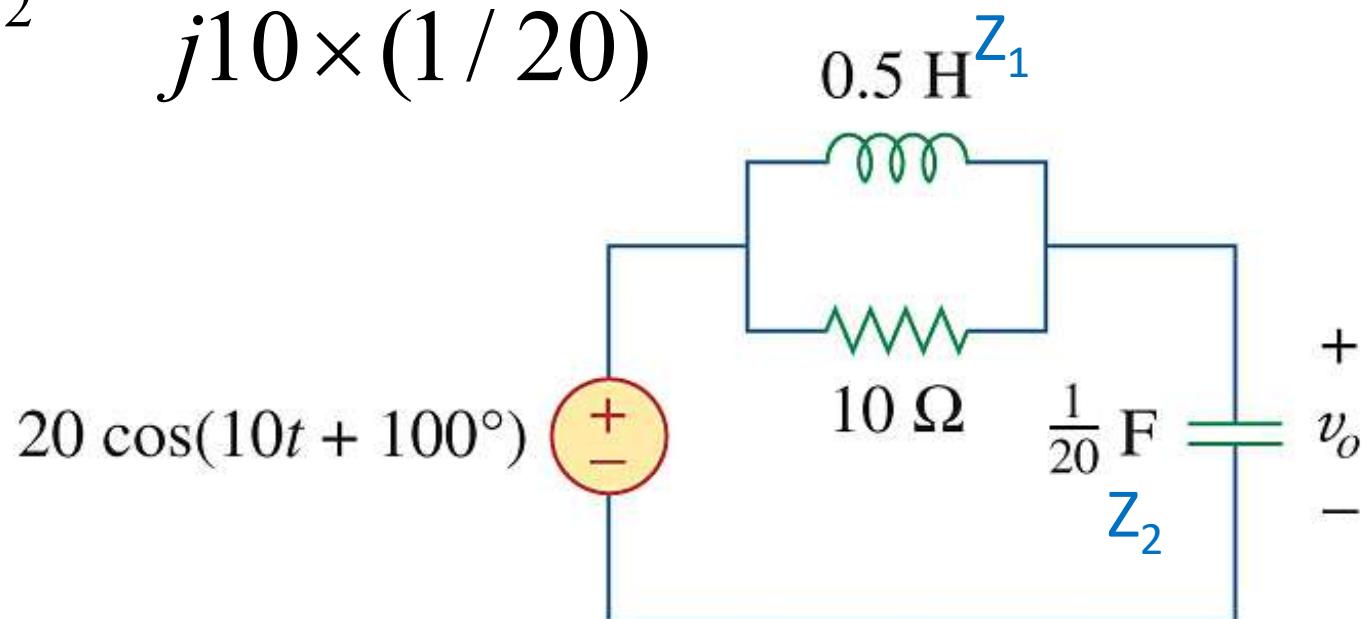


Figure 9.27

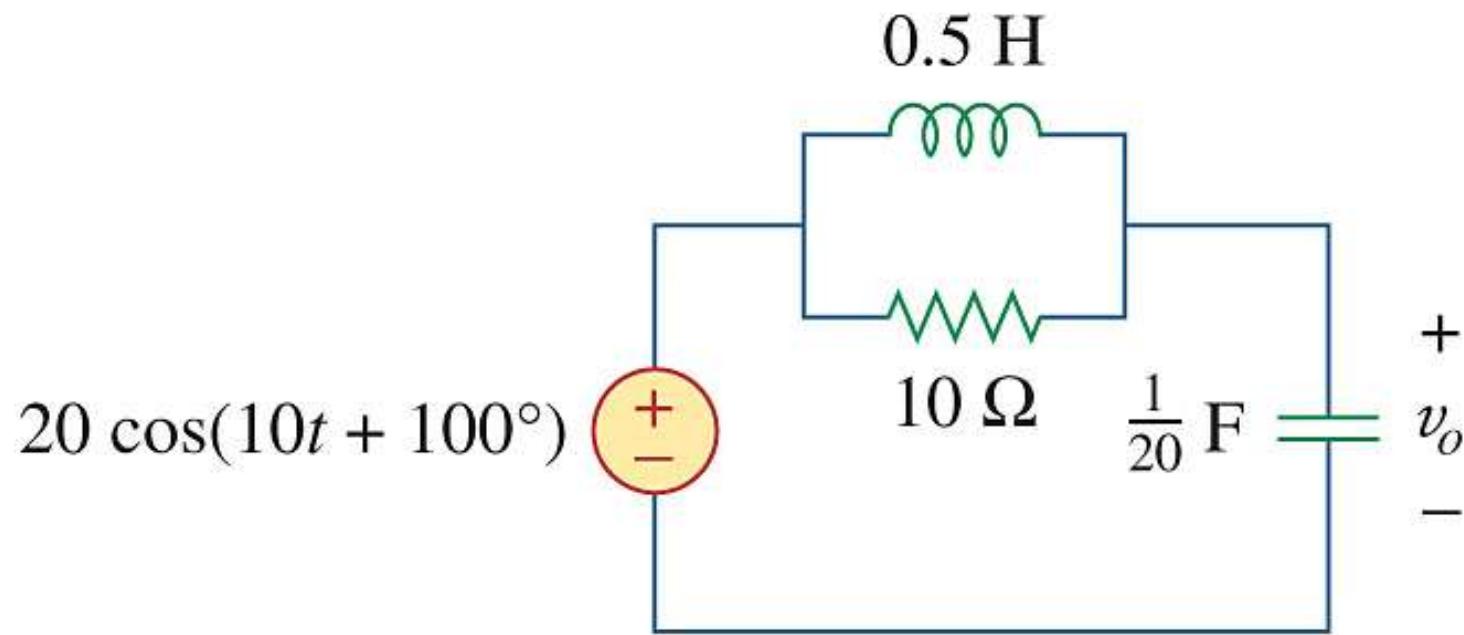


Figure 9.27

$$20 \cos(10t + 100^\circ) \text{ V} : 20 \angle 100^\circ \text{ V}$$

$$\tilde{V}_o = 20 \angle 100^\circ \times \frac{-j2}{-j2 + 10 \parallel j5}$$

Voltage division

$$10 \parallel j5 = \frac{10 \times j5}{10 + j5} = \frac{j10}{2 + j} = 2 + j4$$

$$\tilde{V}_o = 20 \angle 100^\circ \times \frac{-j2}{2 + j2} = 10\sqrt{2} \angle -35^\circ \text{ (V)}$$

$$v_o(t) = 10\sqrt{2} \cos(10t - 35^\circ) \text{ (V)}$$

$$20 \cos(10t + 100^\circ)$$

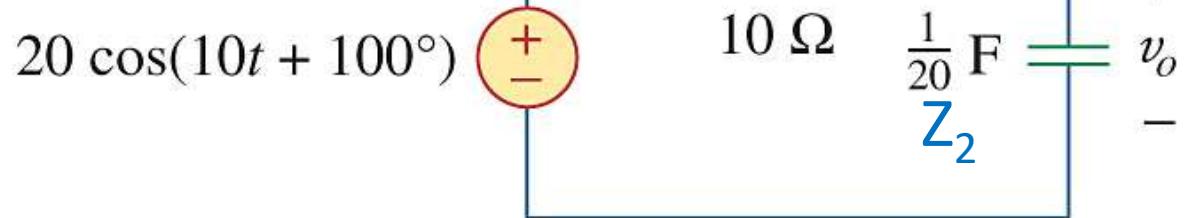


Figure 9.27

9.8 Applications

Phase - Shifters In Fig. 9.31(a),

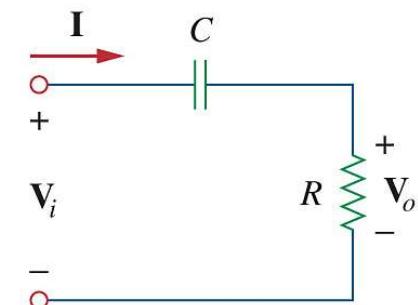
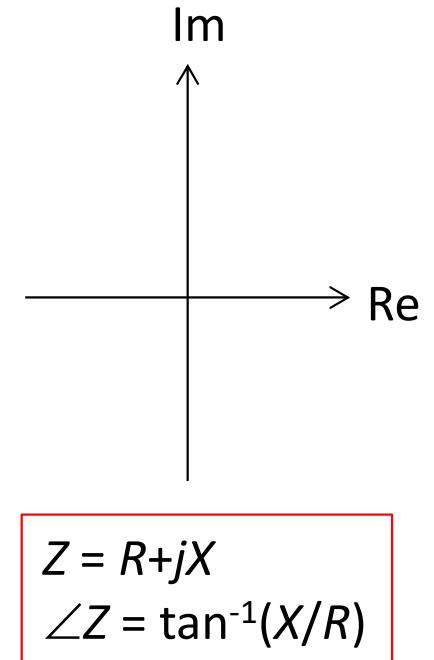
$$\tilde{V}_o = \tilde{V}_i \frac{R}{R + 1/(j\omega C)} = \tilde{V}_i \frac{R}{R - j(1/\omega C)}$$

$$= \tilde{V}_i \frac{R}{\sqrt{R^2 + (1/\omega C)^2}} \angle -\tan^{-1}(1/(\omega RC))$$

\tilde{V}_o leads \tilde{V}_i by $\theta = \tan^{-1}(1/(\omega RC))$,

$0^\circ < \theta < 90^\circ$, as shown in Fig. 9.32(a).

$$\begin{aligned}\angle \mathbf{V}_i + \theta &= \angle \mathbf{V}_o \\ \angle \mathbf{V}_o &> \angle \mathbf{V}_i\end{aligned}$$



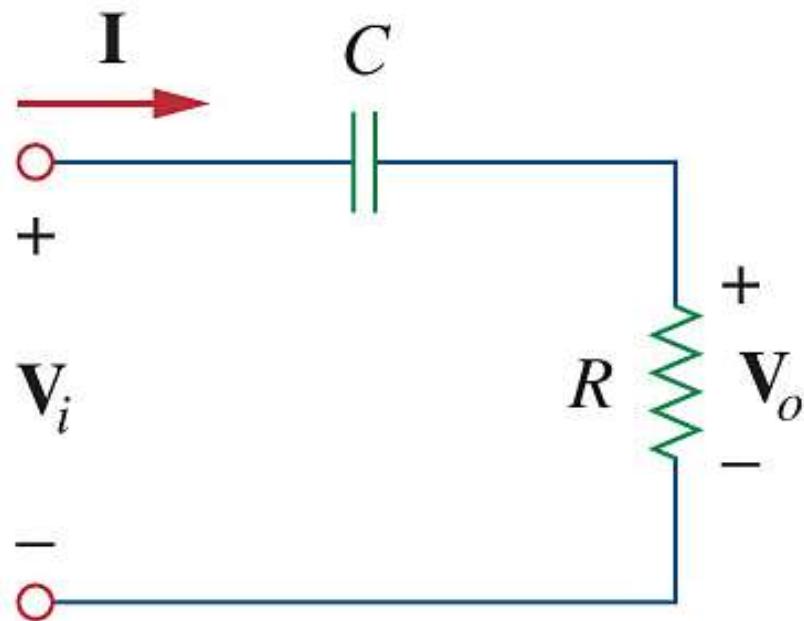


Figure 9.31(a) Series RC shift circuit: leading output.

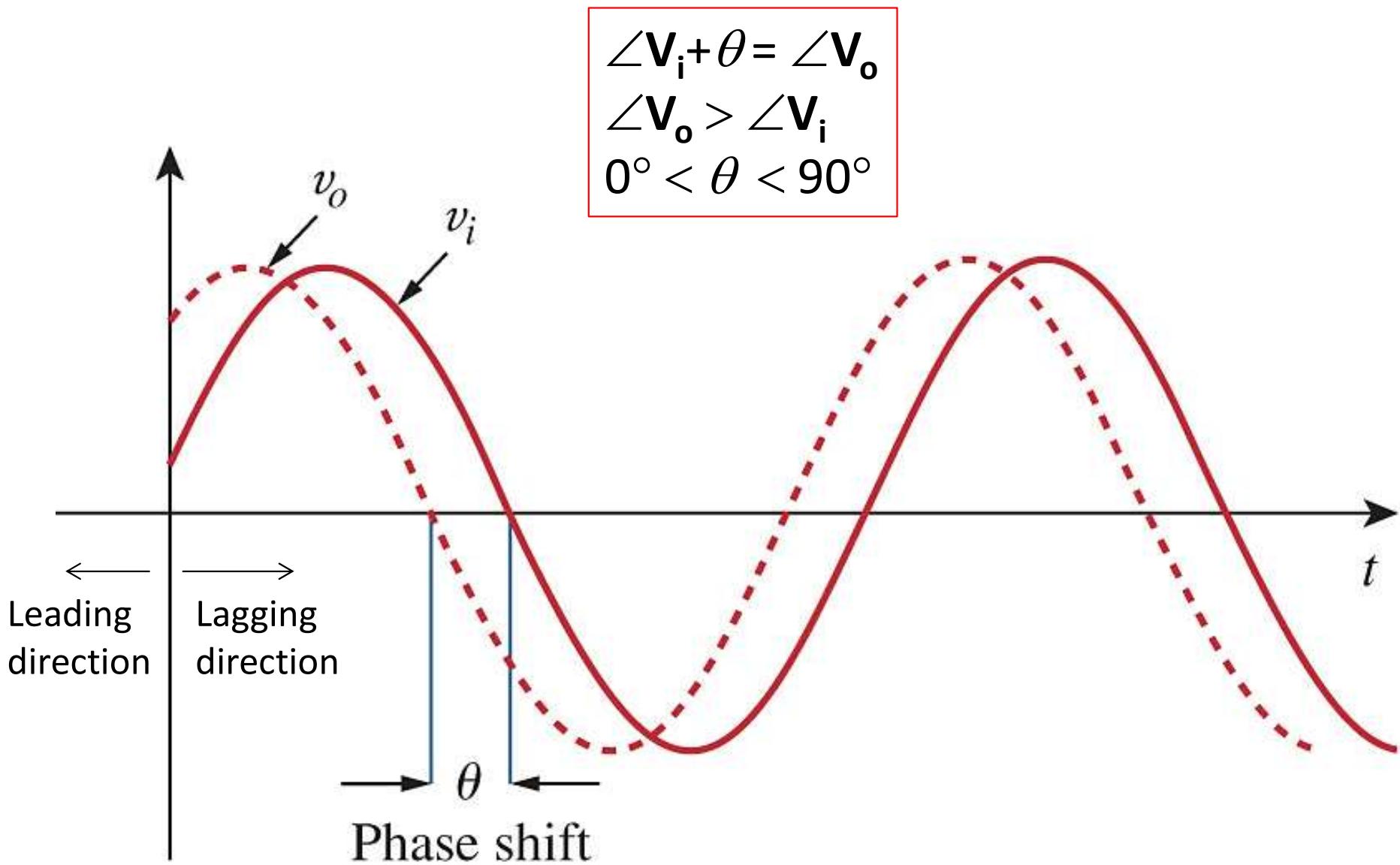


Figure 9.32(a) Phase shift in RC circuits: leading output.

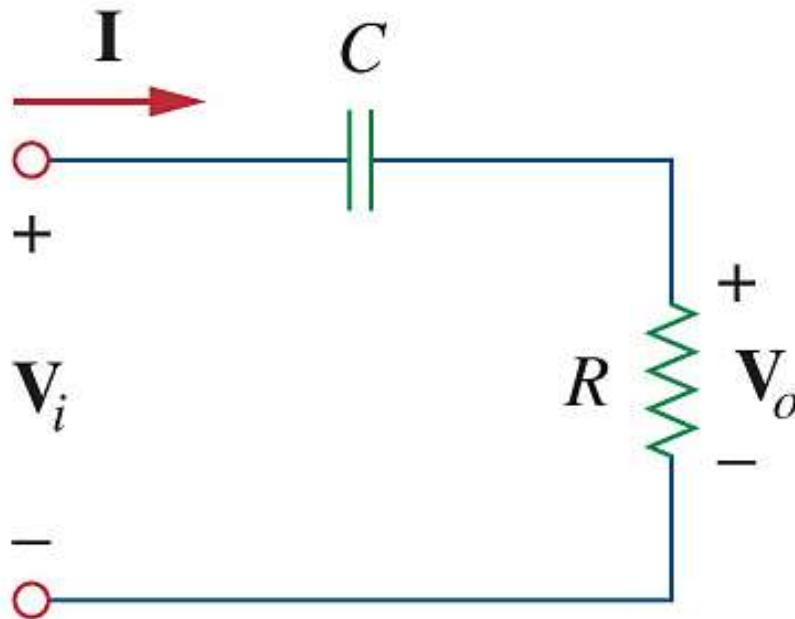


Figure 9.31(a) Series RC shift circuit: leading output.

Another way to check the leading/lagging relation:

$$(1) V_o = IR \rightarrow \angle I = \angle V_o$$

$$(2) V_i = IZ = I(R + 1/j\omega C) \rightarrow -90^\circ < \angle Z < 0 \rightarrow \angle I > \angle V_i$$

(3) Thus, $\angle V_o > \angle V_i$, leading output

Issue of 90° shift:

To produce 90° shift, $\omega RC \rightarrow 0$

$$|\tilde{V}_o| = \frac{1}{\sqrt{1 + \left(\frac{1}{j\omega RC}\right)^2}} |\tilde{V}_i| = \frac{1}{\sqrt{1 + (\infty)^2}} |\tilde{V}_i| \rightarrow 0$$

No output voltage!

\tilde{V}_o leads \tilde{V}_i by $\theta = \tan^{-1}(1 / (\omega RC))$

$$\begin{aligned} \tilde{V}_o &= \tilde{V}_i \frac{R}{R + 1/(j\omega C)} = \tilde{V}_i \frac{R}{R - j(1/\omega C)} \\ &= \tilde{V}_i \frac{R}{\sqrt{R^2 + (1/\omega C)^2}} \angle -\tan^{-1}(1/(\omega RC)) \end{aligned}$$

In Fig. 9.31(b),

$$\tilde{V}_o = \tilde{V}_i \frac{1/(j\omega C)}{R + 1/(j\omega C)} = \tilde{V}_i \frac{1}{1 + j\omega RC}$$
$$= \tilde{V}_i \frac{1}{\sqrt{1 + (\omega RC)^2} \angle \tan^{-1}(\omega RC)}$$

\tilde{V}_o lags \tilde{V}_i by $\theta = \tan^{-1}(\omega RC)$, $0^\circ < \theta < 90^\circ$,
as shown in Fig. 9.32(b).

$$\begin{aligned}\angle \mathbf{V}_i - \theta &= \angle \mathbf{V}_o \\ \angle \mathbf{V}_o &< \angle \mathbf{V}_i\end{aligned}$$

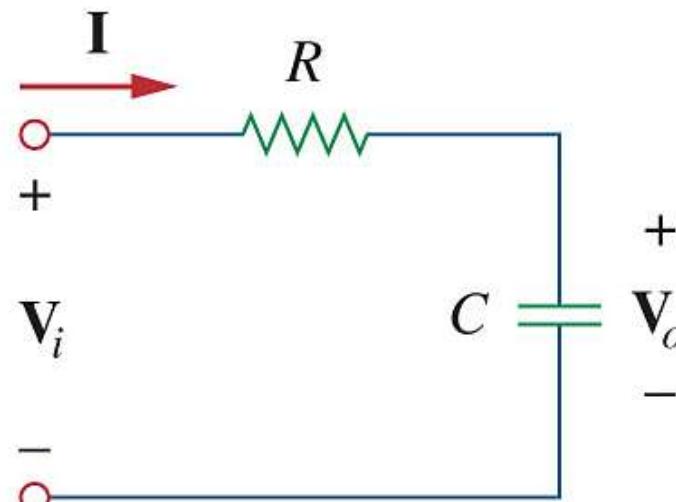


Figure 9.31(b) Series RC shift circuit: lagging output.⁵⁶

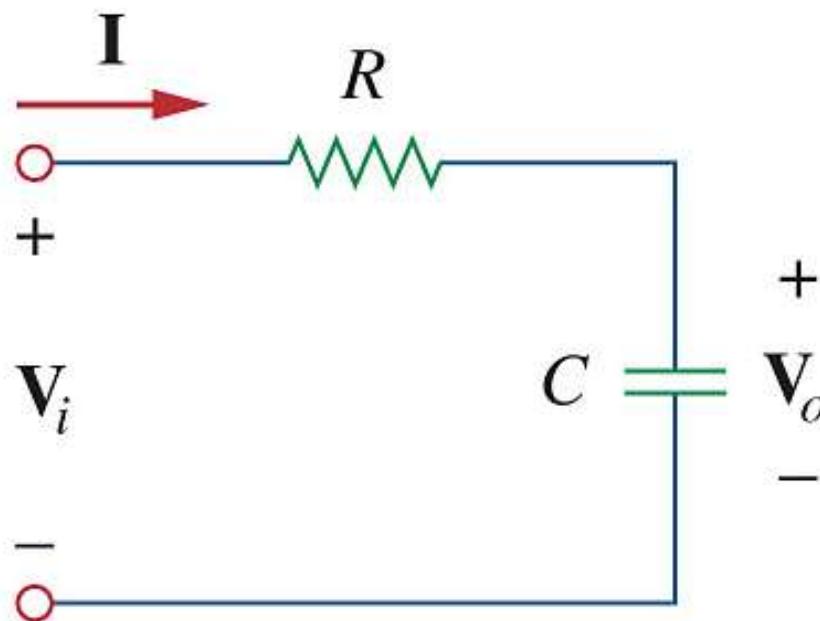


Figure 9.31(b) Series RC shift circuit: lagging output.

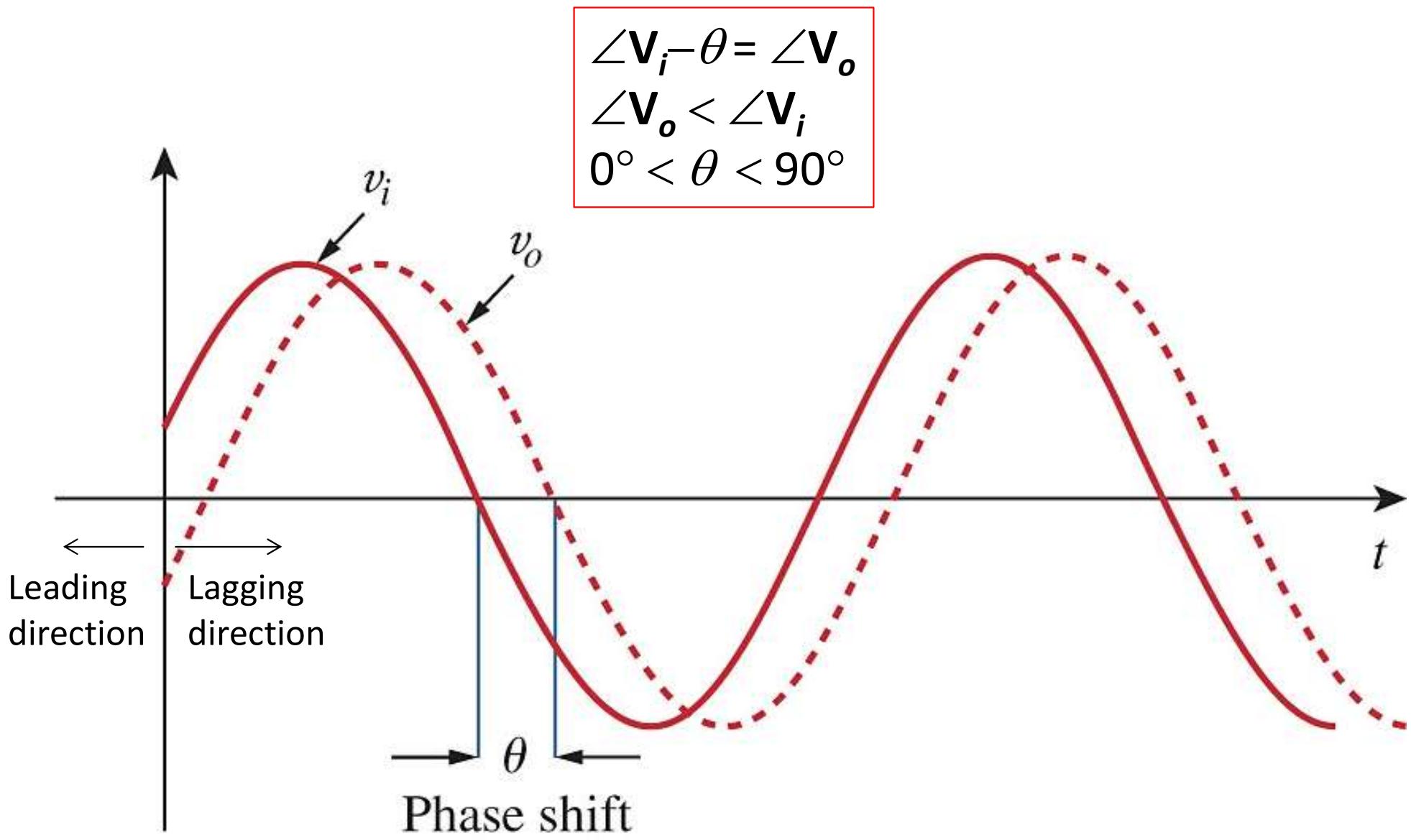


Figure 9.32(b) Phase shift in RC circuits: lagging output.

Practice Problem 9.13 Design an RC circuit to provide a phase shift of 90° leading.

Solution :

We need two stages, with each stage providing a phase shift of 45° .

Select $R_1 = R_2 = 20 \Omega$,

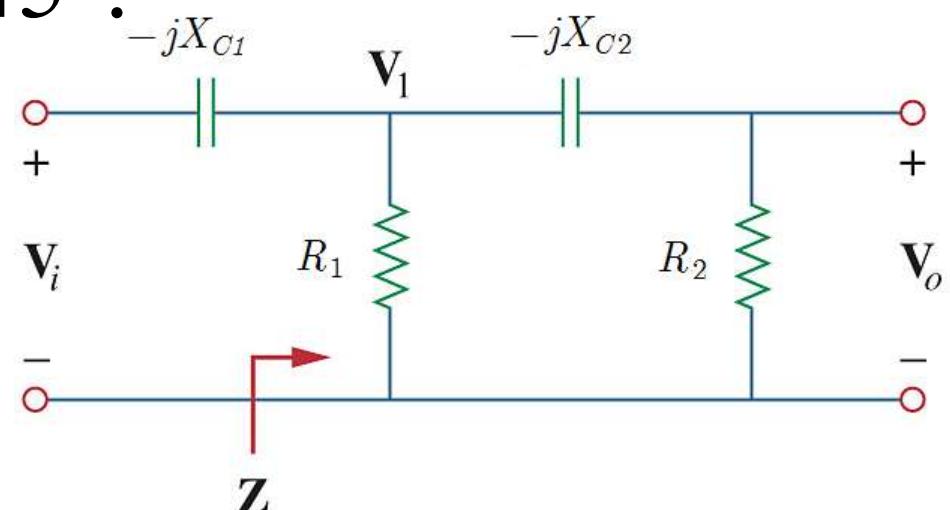


Figure 9.33 An RC phase shift circuit with 90° leading phase shift; for Example 9.13. ⁵⁹

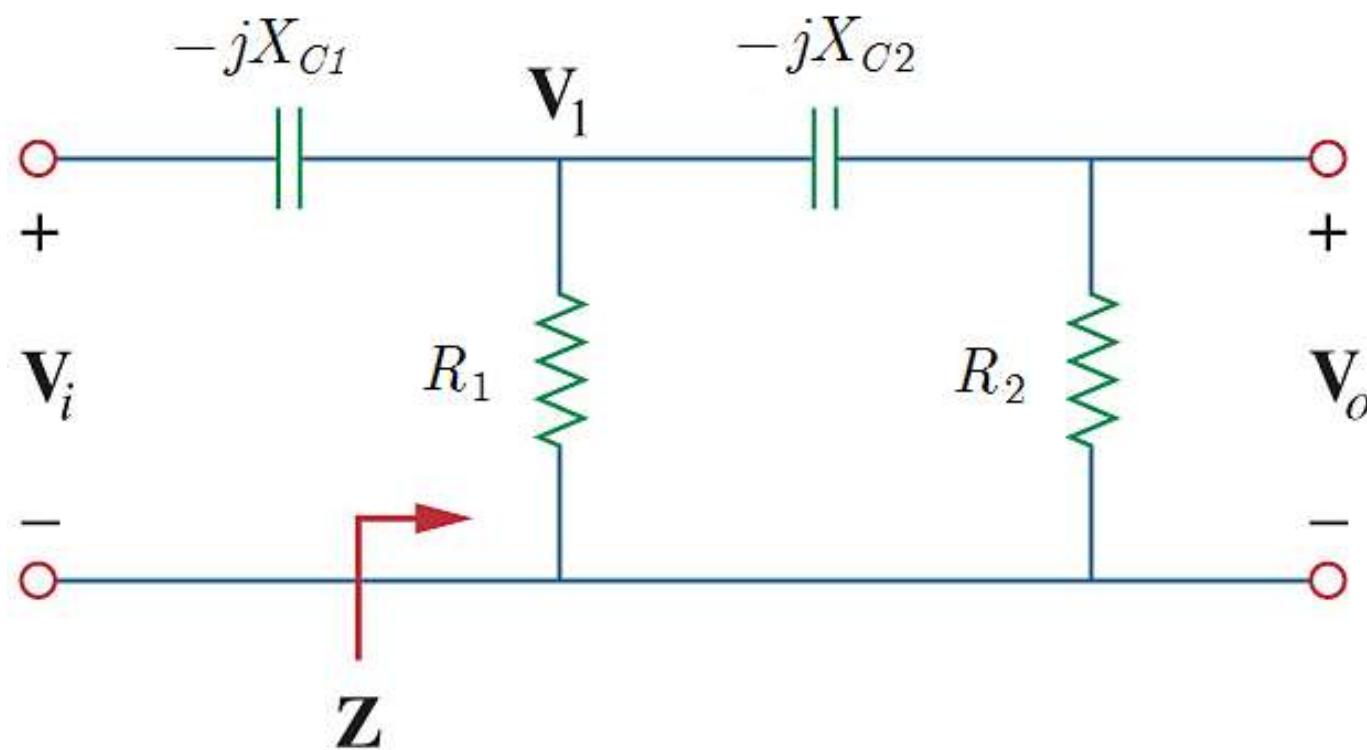


Figure 9.33 An RC phase shift circuit with 90° leading phase shift; for Example 9.13.

$$\tilde{V}_o = \tilde{V}_1 \frac{20}{20 - jX_{C2}} = \tilde{V}_1 \frac{20(20 + jX_{C2})}{20^2 + X_{C2}^2}$$

If $X_{C2} = 20 \Omega$, then the second stage produces a 45° phase shift.

$$Z = 20 \parallel (20 - j20) = \frac{20 \times (20 - j20)}{20 + (20 - j20)}$$

$$= 12 - j4 \text{ } (\Omega)$$

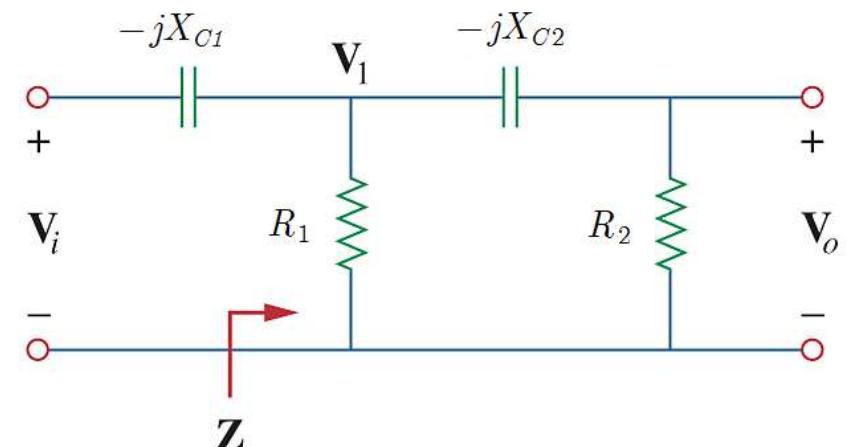


Figure 9.33 An RC phase shift circuit with 90° leading phase shift; for Example 9.13.

$$\tilde{V}_1 = \tilde{V}_i \frac{Z}{-jX_{C1} + Z} = \tilde{V}_i \frac{12 - j4}{12 - j(4 + X_{C1})}$$

$$= \tilde{V}_i \frac{(12 - j4)(12 + j(4 + X_{C1}))}{12^2 + (4 + X_{C1})^2}$$

$$= \tilde{V}_i \frac{(160 + 4X_{C1}) + j(12X_{C1})}{12^2 + (4 + X_{C1})^2}$$

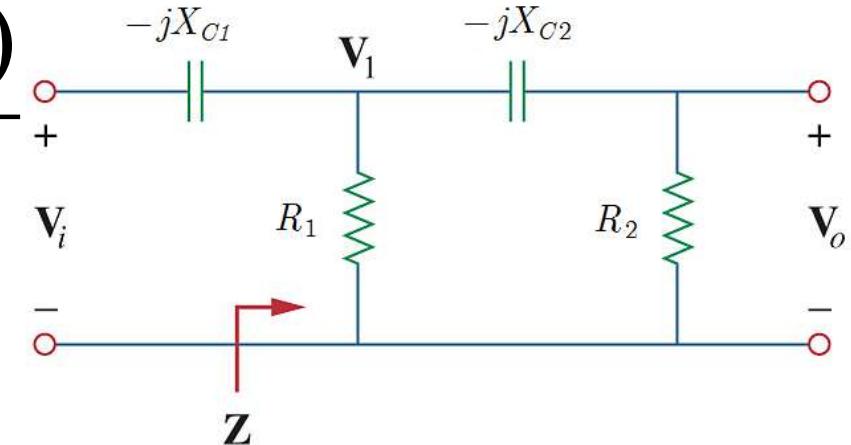


Figure 9.33 An RC phase shift circuit with 90° leading phase shift; for Example 9.13.

For the first stage to produce another 45° ,

we require $160 + 4X_{C1} = 12X_{C1}$, i.e.,

$X_{C1} = 20 \Omega$.

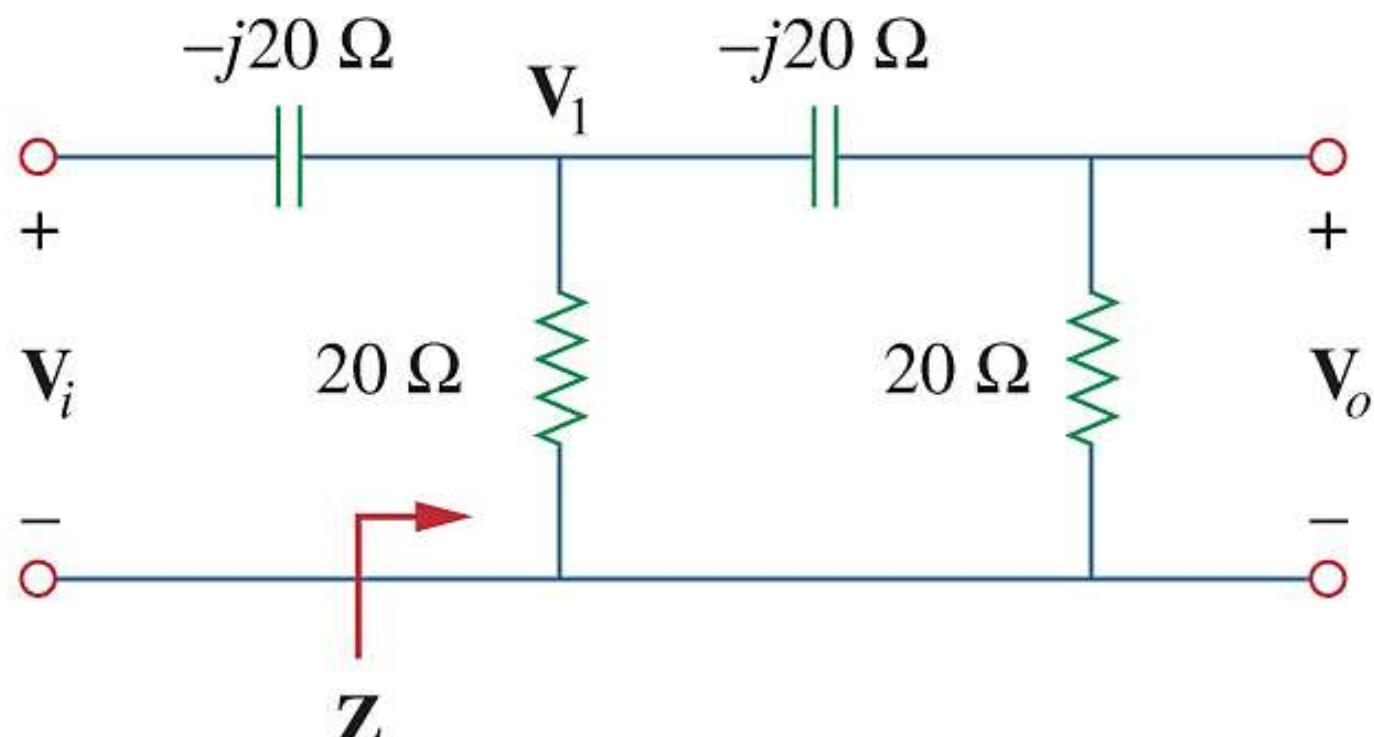


Figure 9.33

