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# Implementation of an Alternate Chemistry Library into OpenFOAM™

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# Implementation of an Alternate Chemistry Library into OPENFOAM™

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# Outline

## 1 Introduction/Motivation

Current status  
CANTERA  
Desired behaviour

## 2 Implementation

Alternate Chemistry Library  
Transient Solver  
Steady Solver  
Other topics

## 3 Results Plug Flow Reactor

Transient PFR  
Steady-state PFR

## 4 Results Sydney Bluff-Body Flame (HM1)

Results HM1  
Discussion HM1

## 5 Conclusion

Summary  
Availability  
Outlook/Future Work  
Acknowledgements



# The chemistryModel-class

- Part of the OPENFOAM<sup>TM</sup>-distribution
  - Solves a set of chemical reactions and returns a **reaction-rate**
  - Used in the solvers dieselFoam and reactingFoam
- Chemical reactions can be specified in two formats:
  - A generic OPENFOAM<sup>TM</sup>-format (allows the inclusion of non-standard reaction rates)
  - The CHEMKIN<sup>TM</sup>-format which is very "FORTRAN"
- Both formats are converted to the same internal representation
- ... and are solved using a number of different solvers



# CANTERA

CANTERA [1] is a open-source chemical kinetics package

- Very **flexible** and easy to handle
- Important functions for chemical species, (heterogeneous) kinetics, equilibrium, transport, diffusion, heat conduction are available and efficiently implemented
- Kernel written in C++; accessible via PYTHON, MATLAB, FORTRAN and of course C/C++
- Good CHEMKIN<sup>TM</sup>-Lexer
- A set of ideal reactors is available
- Uses the CVODE-Solver of the Sundials Suite [2] for integration of the ODEs.



## Goals of this work

As mentioned in the Milan presentation [3], CANTERA would be beneficial for the development of solvers for reacting flows:

- Flexible exchange of **chemistry engines** without the necessity to change the solver
- Easy access to **thermochemical functions**
- Better **stability** (JANAF-error)
- Stationary chemistry solver



# The Alternate Chemistry Library

- A Library that provides a **framework** for adding **further chemistry solvers**
- Should require only **minimal changes** to existing solvers
  - Solvers should be implementation-agnostic (by using the RunTime-selection mechanism)
- This is achieved by replacing the `chemistryModel` object (usually called `chemistry`) in the solvers with a `autoPtr<alternateChemistryModel>`
  - Direct subclassing of `chemistryModel` is not possible because necessary properties are `private`
  - Usually every call `chemistry.xxxx()` is replaced by a `chemistry().xxxx()`



# Interface

- Only a **small part** of the original chemistryModel-interface is needed by the solvers:
  - solve** Solve the reaction system
  - RR** Access the reaction rates
  - tc** Access the chemical time-scale
- Only these have to be implemented by a new chemical solver class
- In addition to these the methods
  - calcDQ** for the calculation of  $dQ$
  - tf** Access the flow time-scale (described later)were added to the interface





# chemistryModelProxy

- Provides access to the functionality of the original chemistryModel-class
- Has a private chemistryModel-object
- Calls are passed through to the chemistryModel-object
  - `solve()` and `tc()`
  - `calcDQ()` implemented after example from original solvers
- With this chemistry model implementation the solver is equivalent to the original reactingFoam

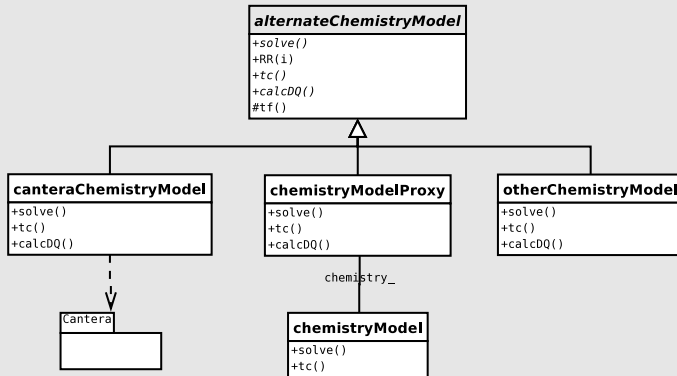


# The CANTERA-model

- Implements interface to the CANTERA-package
- Requires the thermoType to be a `hMixtureThermo<CanteraMixture>`
  - Instead of the usual `hMixtureThermo<reactingMixture>`
  - Currently required to have consistent calculations of the mixture and the chemistry
  - Calculation of thermophysical properties is done in `CanteraThermo` a wrapper to the CANTERA-class `IdealGasMix`
- Reactions are read from a `cti`-file (CANTERA Input)
  - Also the thermophysical data of the species. Thus the requirement on the thermoType
- Calculations in `solve()` are done via the `Reactor/ReactorNet`-classes of CANTERA
  - Solution of the ODEs is done via `CVODE`



# Class overview



## alternateReactingFoam

Solver almost unchanged. Basis: reactingFoam. Remember the Chalmers **PaSR-Model** for turbulent combustion:

$$\kappa = \frac{dT + tc}{dT + tc + tk} \quad (1)$$

Where  $tc$  is the **chemical time scale** and  $tk$  is the **turbulent time scale**.

- Implementation of  $tc()$ -method for the CANTERA calculation necessary.
- For the CANTERA solver no ODE solver from OF necessary (choice of the ODE solver in chemistryProperties doesn't have any effect).



# alternateSteadyReactingFoam

Steady solvers are a must when simulating **large-scale chemical reactors** or **burners**.

Necessary changes from the transient case:

- Usage of the SIMPLE-algorithm for  $p$ - $U$ -coupling
- Coupling of chemistry to the flow-time
- **Stabilization** of the solution by reduction of  $\kappa$  if  $|Y_i^{old} - Y_i^{new}|$  is too large (only at start-up!)



## Flow time scale

In **unsteady** calculations  $Co < 1$  and integration time equals  $dT$ .  
For **steady-state** solvers  $Co \gg 1$ . So we limit the integration time by the residence time in the cell  $i$ :

$$tf_i = \frac{D_i}{U_i} \quad (2)$$

and hence we substitute  $dT$  in (1) by  $df$ :

$$\kappa = \frac{tf + tc}{tf + tc + tk} \quad (3)$$



We define the **flow time scale**  $tf$ .

# CVODE

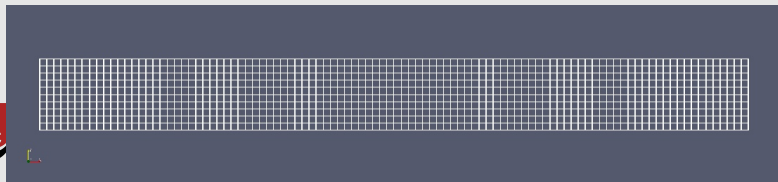
An OF library that makes use of the CVODE-Solver of the Sundials Suite [2] was written.



## Plug flow reactor (PFR) test case

Simple test case, which is easily comparable to ideal PFR models as available in CHEMKIN<sup>TM</sup> or CANTERA:

- Ignitable premixed composition at inlet:  $Y_{H_2} = 0.009$ ,  $Y_{O_2} = 0.026$ ,  $Y_{Ar} = 0.965$ ,  $T = 1600$  K,  $p = 1$  bar
- Tube idealized as 2D-domain  $x_{max} = 1$  m,  $y_{max} = 0.1$  m, 10×100 cells, inlet left patch, outlet right patch, upper and lower patch symmetry
- $H_2 - O_2$  mechanism with 9 species and 27 reactions





## PFR alternateReactingFoam

For the **transient simulations** we were interested in

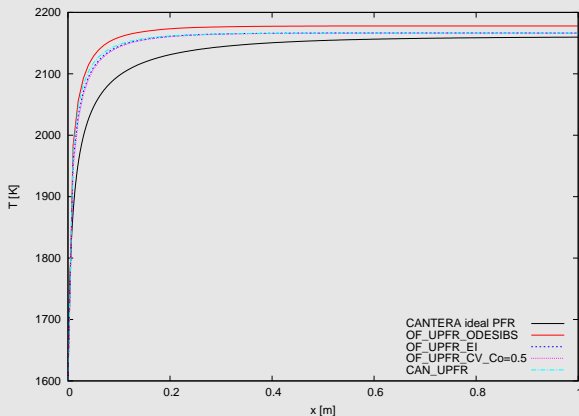
- Behaviour of the CANTERA chemistry library
- Choice of ODE solvers and their performance

All plots were done along the **x direction**. The ideal Solution was obtained by calculating the time into a position with  $U$  and  $\rho$ .

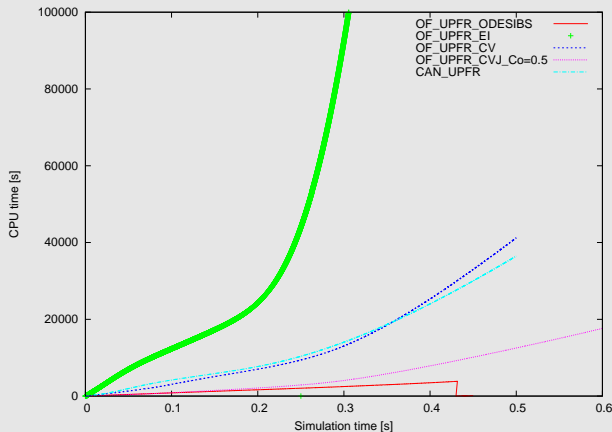


# PFR alternateReactingFoam ODE-solvers (T)

ODESIBS: ODE SIBS; EI: Euler Implicit; CV: CVODE



# PFR alternateReactingFoam ODE CPUTime



## PFR alternateReactingFoam Summary

Transient PFR results:

- With implementation of CANTERA chemistry and tc() results for both chemistry engines give **identical results** for PFR.
- ODE SIBS results deviate slightly from the others (EI, CV) (due to semi-implicitness?)
- CVODE more stable than SIBS, EI but sometimes slower
- CVODE benefits from **larger integration steps** (internal time-stepping). → So use higher Co, if results aren't affected.
- Compared to ideal reactor solvers are 'faster' and there is a temperature difference of 5 K. Possibly induced by discretisation errors or idealisation.



## PFR alternateSteadyReactingFoam

The following aspects for the runs of the **steady-state simulations** are of particular interest:

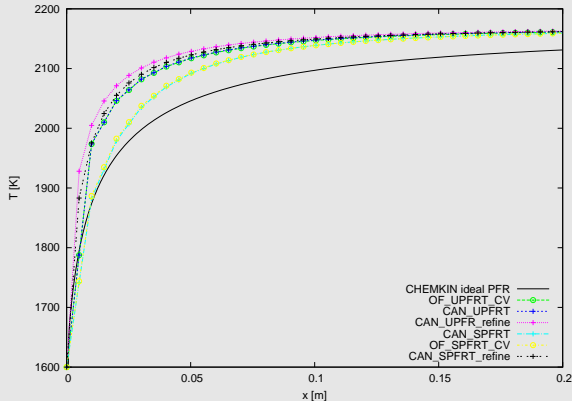
- A** Performance and stability of the steady-state implementation in relation to transient case and the ideal case.
- B** Influence of the implementation of  $\kappa$
- C** Influence of  $C_{mix}$

Plots are similar to the transient ones but scaling was changed.



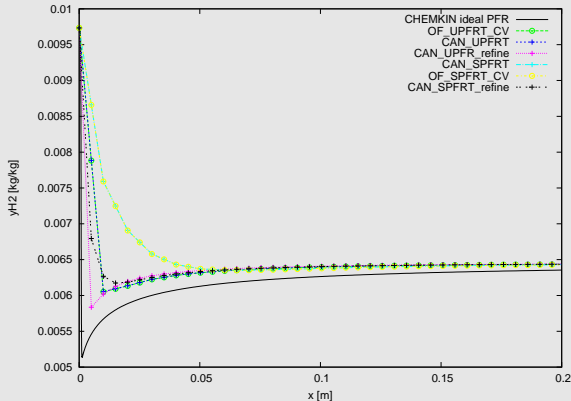
# PFR alternateSteadyReactingFoam (T)

A Transient vs. steady



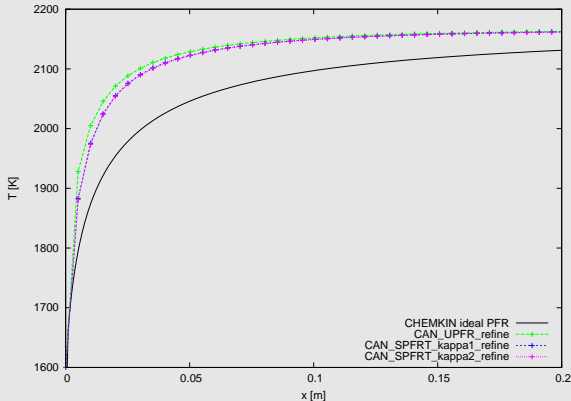
# PFR alternateSteadyReactingFoam (H2)

A Transient vs. steady



# PFR alternateSteadyReactingFoam (T)

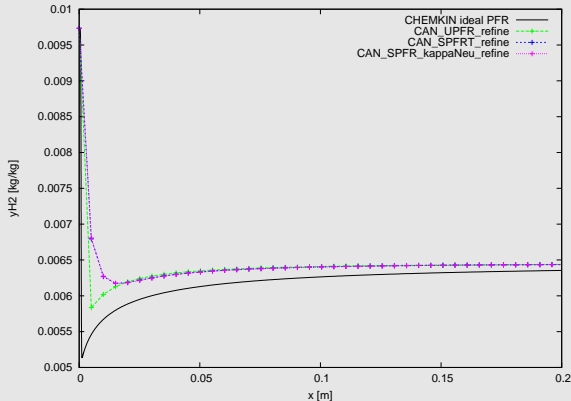
B Influence of  $\kappa$





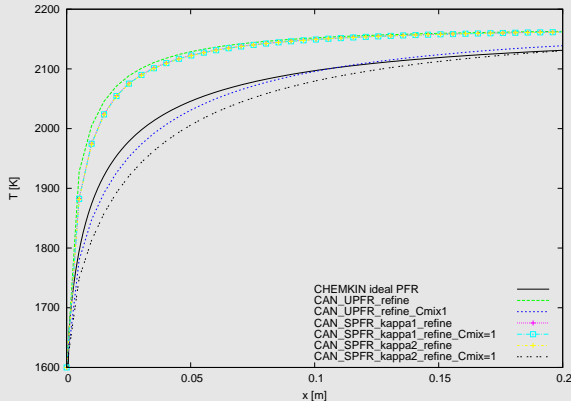
# PFR alternateSteadyReactingFoam (H2)

## B Influence of $\kappa$



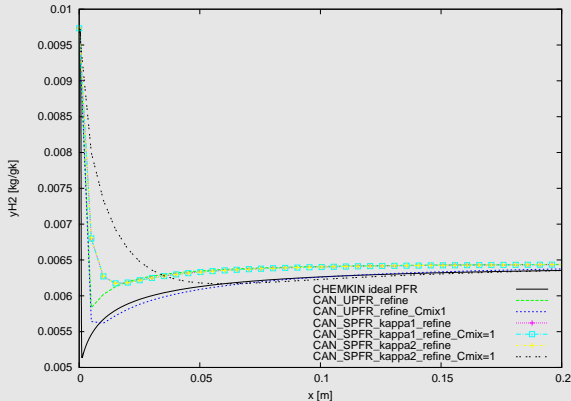
# PFR alternateSteadyReactingFoam (T)

C Influence of  $C_{mix}$



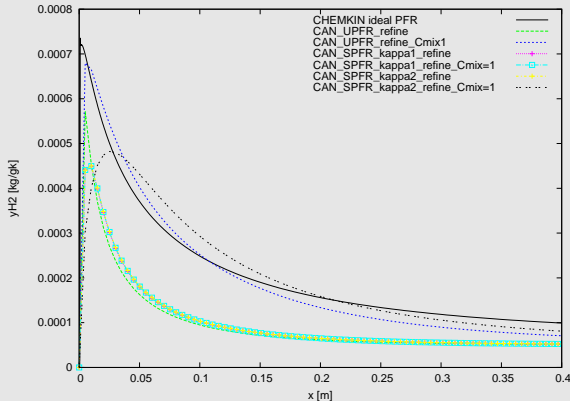
# PFR alternateSteadyReactingFoam (H2)

## C Influence of $C_{mix}$



# PFR alternateSteadyReactingFoam (OH)

## C Influence of $C_{mix}$



## PFR Steady Summary

A:

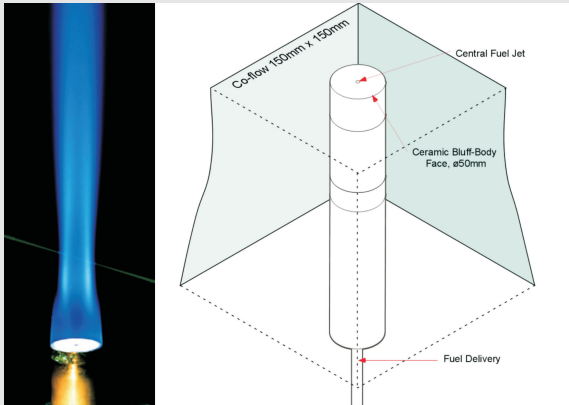
- Transient/Steady solutions do **not agree totally** but **refinement reduces deviation**

B+C:

- Definition of new  $\kappa$  according to (3) brings no changes for small values of  $C_{mix}$ . But for  $C_{mix}=1$  the solution seems closer to ideal solution.
- However, no clear conclusion could be drawn.

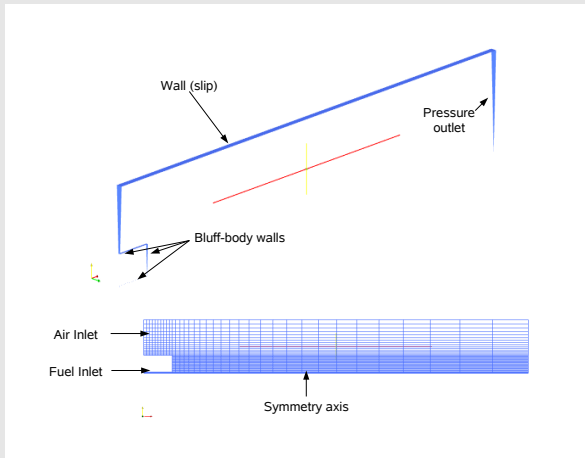


# Sydney Bluff-body Flame (HM1)



Data from Sandia bluff-body flame HM1 conducted at Sydney university [4].

## HM1 case set-up



## HM1 set-up

Boundary Conditions:

- **Diameters:**  $D_{jet} = 3.6\text{mm}$ ;  $D_{channel} = 150\text{mm}$  (300mm),  
 $D_{bluffbody} = 50\text{mm}$
- **Turbulence:** 8.5 % (2.5%) turbulence intensity , 0.135 mm  
(5.625 mm) mixing length for jet (co-flow)
- **Mesh:** from blockMesh with 1095

Inlet conditions:

- HM1:  $U_{jet} = 118\text{m/s}$   $U_{coflow} = 40\text{m/s}$

Other models:

- $k - \epsilon$  turbulence model, ATRMech (reduced GRI 3.0)
- OF used KRR4 ODE solver for chemistry



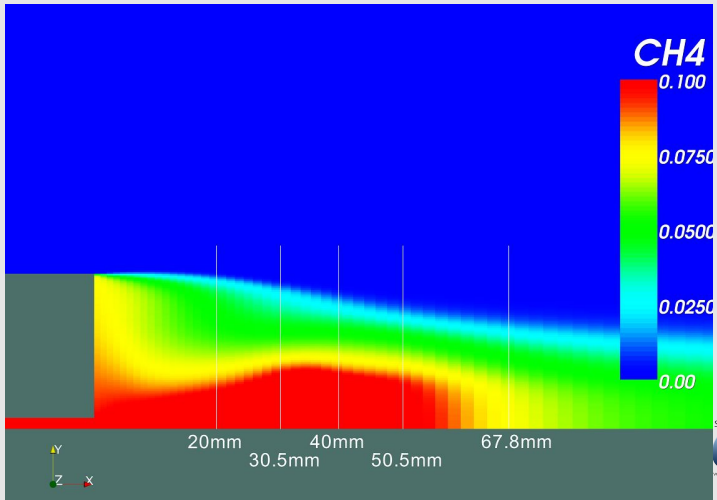


## HM1 Plots & Points of Measurement

- Plots of **radius** against measurement **values (Exp HM1)** at different **x-positions** are shown together with simulation results.
- **EDC** refers to the EDCSimpleFoam solver [3].
- **CAN** and **OF** mark CANTERA- and OPENFOAM<sup>TM</sup>-solution
- **K1** and **K2** stands for  $\kappa_1$  and  $\kappa_2$



## HM1 Plots & Points of Measurement

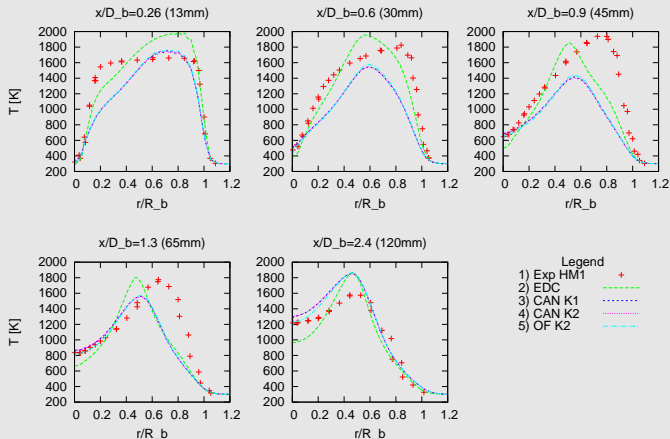


Strömungsforschung GmbH

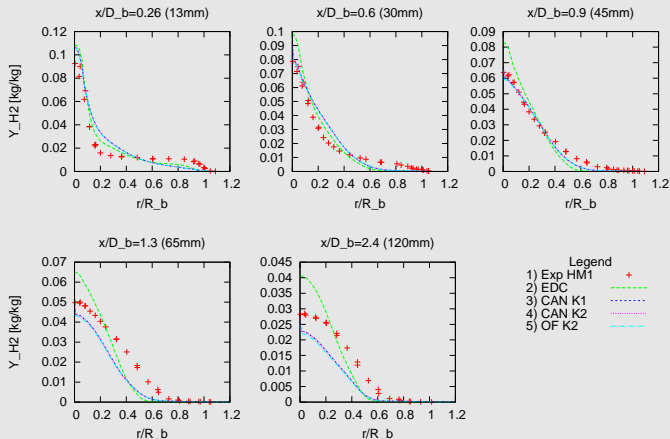
**CE**  
Computational Engineering



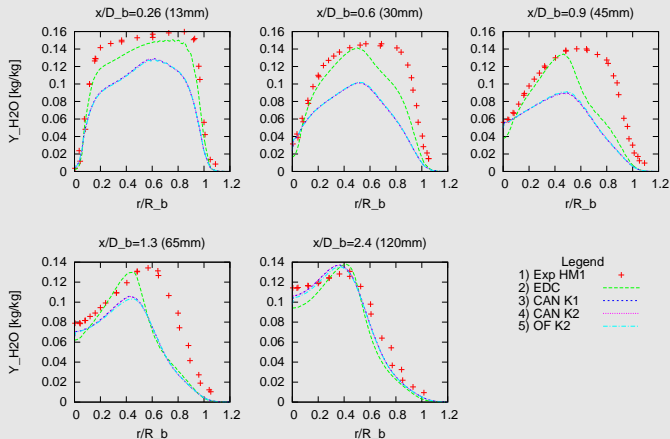
# HM1 results T



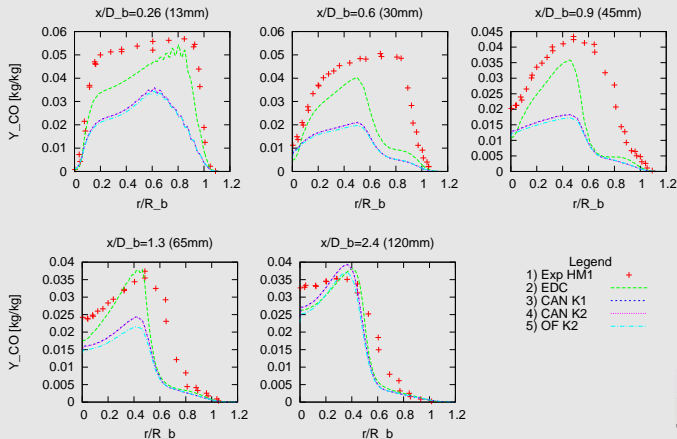
# HM1 results H2



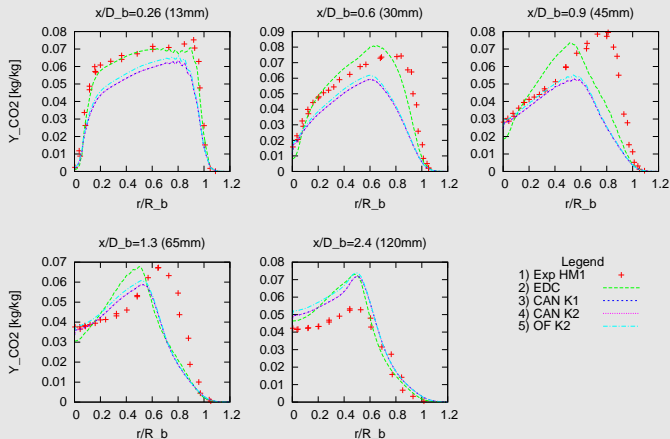
# HM1 results H2O



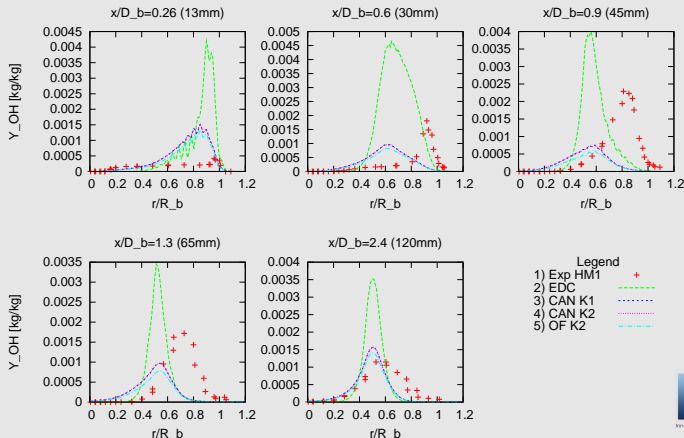
# HM1 results CO



# HM1 results CO2



# HM1 results OH





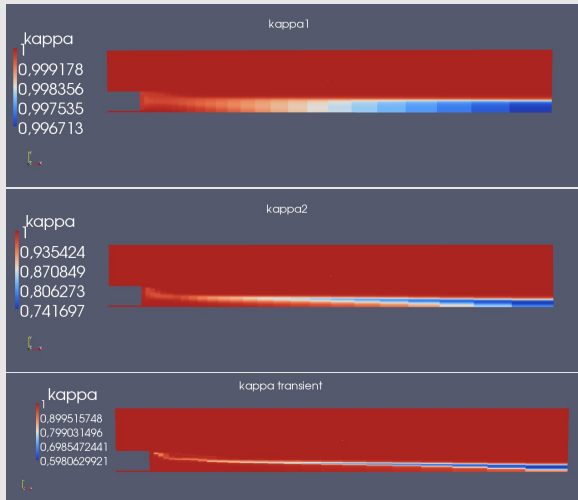
## Discussion HM1

Why are all the results **so similar**? (No influence of  $\kappa$ -implementation or Cmix (not shown))

- In case Cmix=0.005 no difference in  $\kappa$  notable - too fast mixing as in PFR case.
- Furthermore, in the domain **close to the inlets**  $\kappa \approx 1$  in every case and influence of Cmix can only be seen **further downstream** where no measurements are available.
- Comparison with **transient simulation** of HM1 indicates that  $\kappa_2$  seems more appropriate (see next slide)
- Still, further testing is needed



## HM1 comparison $\kappa_1, \kappa_2$ for $C_{mix}=1$



## Conclusion HM1

- Flame was rendered with **acceptable quality** by the new solvers
- Steady solvers are **very robust** if the right ODE solvers are used (CVODE for CANTERA, KRR4 for OF)
- Checking of  $dY_i$  provides further stability and prevents composition from being driven to unphysical states.
- Solutions for a finer grid (20000 cells) are still not available - flame **blows off** very easily.



# Summary

The implementation of the CANTERA chemistry into OPENFOAM™ can be considered successful and provides:

- A **flexible interface** to access a wide range of thermophysical data, and chemistry functions
- Robust **solvers** for transient and steady-state calculations
- Valuable **test-cases** for validation and further investigation
- **Collaborators** are welcome to test the code and contribute own developments.



## How to get the library

- The libraries and solvers presented here will be made available on the openfoam-extend-SVN on [sourceforge.net](http://sourceforge.net)

**Libraries** Two independent libraries:

**alternateChemistryModel** The general framework an the OPENFOAM™-interface

**canteraChemistryModel** The interface to CANTERA

**Solvers** The steady and the transient solver with the test-cases PFR and HM1

- URL will be given on the WIKI
- Interfaces to other **chemistry libraries**, more **solvers**, critique, and improvements are encouraged



## Future Work

There is always room for improvement:

- Both chemistry solvers read the same input files
  - Converter between `CANTERA` and `OPENFOAM™`-format
- Make the `CANTERACHEMISTRYMODEL` independent of `canteraMixture`
- Implementation of reduction/tabulation techniques for more time-efficient solution.
- More combustion models.



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