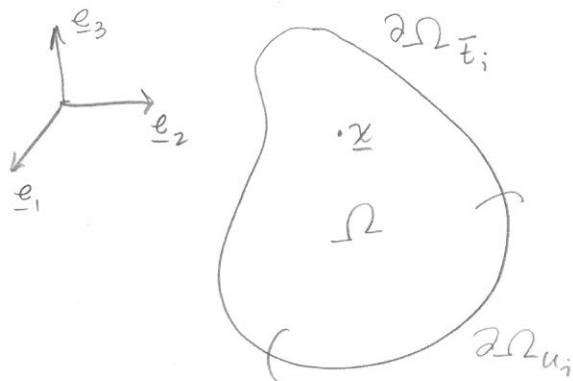


12.01 Hyperbolic Linear PDEs in vector unknowns. - Linear Elastodynamics in 3D.



$$\left. \begin{aligned} \partial\Omega &= \partial\Omega_{u_i} \cup \partial\Omega_{\bar{f}_i} \\ \partial\Omega_{u_i} \cap \partial\Omega_{\bar{f}_i} &= \emptyset \end{aligned} \right\} i=1,2,3$$

mass density

Strong Form: Given: $u_i^g, \bar{f}_i, f_i, u_{i0}, v_{i0}, \sigma_{ij} = C_{ijkl} \epsilon_{kl}, \rho$
 $\epsilon_{kl} = \frac{1}{2} \left(\frac{\partial u_k}{\partial x_l} + \frac{\partial u_l}{\partial x_k} \right)$

find: $u_i(\underline{x}, t)$ such that:

$$\rho \frac{\partial^2 u_i}{\partial t^2} = \sigma_{ij,j} + f_i \quad \text{in } \Omega \times [0, T]$$

Boundary Conditions: $u_i(\underline{x}, t) = u_i^g(\underline{x}, t) \quad @ \quad \underline{x} \in \partial\Omega_{u_i}$

$$\sigma_{ij} n_j = \bar{f}_i(\underline{x}, t) \quad @ \quad \underline{x} \in \partial\Omega_{\bar{f}_i}$$

Initial Conditions: $u_i(\underline{x}, 0) = u_{i0}(\underline{x}) \quad \forall \underline{x} \in \Omega$

$$\dot{u}_i(\underline{x}, 0) = v_{i0}(\underline{x}) \quad \forall \underline{x} \in \Omega$$

Weak Form: Find $u_i \in \mathcal{S} = \{u_i \mid u_i = u_i^g \text{ on } \partial\Omega_{u_i}\}$
 such that $\forall w_i \in \mathcal{V} = \{w_i \mid w_i = 0 \text{ on } \partial\Omega_{u_i}\}$

$$\int_{\Omega} w_i \rho \frac{\partial^2 u_i}{\partial t^2} dV + \int_{\Omega} w_{i,j} \sigma_{ij} dV = \int_{\Omega} w_i f_i dV + \sum_{i=1}^3 \int_{\partial\Omega_{\bar{f}_i}} w_i \bar{f}_i dS$$

12.02 Hyperbolic PDEs in vector unknowns, in 3D - Linear Elastodynamics

Find $u_i^h \in \mathcal{S}^h \subset \mathcal{S}$; $\mathcal{S}^h = \{u_i^h \in H^1(\Omega) \mid u_i^h = u_i^g \text{ on } \partial\Omega_{u_i}\}$

Such that $\forall w_i^h \in \mathcal{V}^h \subset \mathcal{V}$; $\mathcal{V}^h = \{w_i^h \in H^1(\Omega) \mid w_i^h = 0 \text{ on } \partial\Omega_{u_i}\}$

$$\underbrace{\int_{\Omega} w_i^h \rho \frac{\partial^2 u_i^h}{\partial t^2} dV}_{\text{Inertia}} + \underbrace{\int_{\Omega} w_i^h \sigma_{ij}^h \delta_{ij} dV}_{\substack{\text{Elasticity} \\ C_{ijkl} \epsilon_{kl}}} = \underbrace{\int_{\Omega} w_i^h f_i dV + \sum_{i=1}^3 \int_{\partial\Omega_{\bar{f}_i}} w_i^h \bar{f}_i dS}_{\text{External Forces}} \quad \left. \vphantom{\int_{\Omega} w_i^h \rho \frac{\partial^2 u_i^h}{\partial t^2} dV} \right\} \text{FINITE-DIMENSIONAL WEAK FORM.}$$

$$\underline{C}^T \underline{M} \ddot{\underline{d}} + \underline{C}^T \underline{K} \underline{d} = \underline{C}^T \underline{F}$$

Form of \underline{M} : Consider $\int_{\Omega} w_i^h \rho \frac{\partial^2 u_i^h}{\partial t^2} dV = \sum_e \int_{\Omega^e} w_i^h \rho \frac{\partial^2 u_i^h}{\partial t^2} dV$

12.03 The element Integral:

$$\int_{\Omega^e} w_i^h \rho \frac{\partial^2 u_i^h}{\partial t^2} dV = \sum_{A,B} C_{e,i}^A \left(\int_{\Omega^e} \rho N^A N^B dV \right) \ddot{d}_{e,i}^B$$

Recall sum on i

$$= \sum_{A,B} C_{e,i}^A \left(\int_{\Omega^e} \rho N^A N^B \delta_{ij} dV \right) \ddot{d}_{e,i}^B$$

$$\langle C_{e,1}^2, C_{e,2}^2, C_{e,3}^2 \rangle$$

$$= \langle C_e^{1T}, C_e^{2T}, \dots, C_e^{n_{ne}T} \rangle$$

$$\int_{\Omega^e} \rho N^1 N^1 dV \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\dots \int_{\Omega^e} \rho N^A N^B dV \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \dots$$

\underline{M}_e

size

$$[n_{ne} \times n_{sd}] \times [n_{ne} \times n_{sd}]$$

$$\begin{bmatrix} \ddot{d}_e^1 \\ \ddot{d}_e^2 \\ \vdots \\ \ddot{d}_e^{n_{ne}} \end{bmatrix}$$

Assembly proceeds as before over global degrees of freedom.

$$\underline{M} \ddot{\underline{d}} + \underline{K} \underline{d} = \underline{F}$$

$$\underline{d}(0) = \underline{d}_0$$

$$\dot{\underline{d}}(0) = \underline{v}_0 = \left\{ \begin{matrix} v_0(x^A) \\ \vdots \end{matrix} \right\}$$

specified for every degree of freedom.

12.04

The matrix-vector problem of linear elastodynamics

$$\underline{M} \ddot{\underline{d}} + \underline{K} \underline{d} = \underline{F}$$

$$\underline{d}(0) = \underline{d}_0$$

$$\dot{\underline{d}}(0) = \underline{v}_0$$

Including the effect of structural damping:

$$\underset{\substack{\uparrow \\ \text{damping} \\ \text{matrix}}}{\underline{C}} = a \cdot \underline{M} + b \cdot \underline{K} \quad \left. \vphantom{\underline{C}} \right\} \text{Rayleigh Damping}$$

where a & b
are constants

Elastodynamics with structural damping:

$$\underline{M} \ddot{\underline{d}} + \underline{C} \dot{\underline{d}} + \underline{K} \underline{d} = \underline{F} \quad \text{with } \dot{\underline{d}}(0) = \underline{v}_0 \text{ \& \& } \ddot{\underline{d}}(0) = \underline{v}_0$$

Time Discretization: $[0, T] = \cup [t_0, t_1] \dots [t_{N-1}, \underbrace{t_N}_T]$

\underline{d}_n : time-discrete approximation to $\underline{d}(t_n)$

Time-discretized matrix-vector equation:

$$\underline{M} \underset{\substack{\uparrow \\ \text{acceleration}}}{\underline{a}_{n+1}} + \underline{C} \underline{v}_{n+1} + \underline{K} \underline{d}_{n+1} = \underline{F}_{n+1}$$

Newmark Family of algorithms for 2nd order ODEs:

For $\gamma \in [0, 1]$; $2\beta \in [0, 1]$

$$\underline{d}_{n+1} = \underline{d}_n + \Delta t \underline{v}_n + \frac{\Delta t^2}{2} \left((1-2\beta) \underline{a}_n + 2\beta \underline{a}_{n+1} \right)$$

$$\underline{v}_{n+1} = \underline{v}_n + \Delta t \left((1-\gamma) \underline{a}_n + \gamma \underline{a}_{n+1} \right)$$

The α -method:

Predictors: $\tilde{\underline{d}}_{n+1} = \underline{d}_n + \Delta t \underline{v}_n + \frac{\Delta t^2}{2} (1-2\beta) \underline{a}_n$

$$\tilde{\underline{v}}_{n+1} = \underline{v}_n + \Delta t (1-\gamma) \underline{a}_n$$

Correctors: $\underline{d}_{n+1} = \tilde{\underline{d}}_{n+1} + \left(\Delta t^2 \cdot \beta \underline{a}_{n+1} \right)$
 $\underline{v}_{n+1} = \tilde{\underline{v}}_{n+1} + \left(\Delta t \gamma \underline{a}_{n+1} \right)$ } Correctors.

Substituting,

$$\underline{M} \underline{a}_{n+1} + \underline{C} \left[\tilde{\underline{v}}_{n+1} + \Delta t \gamma \underline{a}_{n+1} \right] + \underline{K} \left[\tilde{\underline{d}}_{n+1} + \Delta t^2 \beta \underline{a}_{n+1} \right] = \underline{F}_{n+1}$$

$$\Rightarrow \left[\underline{M} + \underline{C} \Delta t \gamma + \underline{K} \Delta t^2 \beta \right] \underline{a}_{n+1} = \underline{F}_{n+1} - \underline{C} \tilde{\underline{v}}_{n+1} - \underline{K} \tilde{\underline{d}}_{n+1}$$

To get \underline{a}_0 , use equation:

$$\underline{M} \underline{a}_0 = \underline{F}_0 - \underbrace{\underline{C} \underline{v}_0}_{\text{known}} - \underbrace{\underline{K} \underline{d}_0}_{\text{known}}$$

12.05 Analysis is based on the eigenvalue problem:

$$\omega^2 \underline{M} \underline{\Psi} = \underline{K} \underline{\Psi}$$

ω : natural frequency of oscillation. $\underline{\Psi}$: \underline{M} -orthogonal eigenvectors, $l=1, \dots, n_{df}$

$$\underline{d} = \sum_l \underline{d}^l \underline{\Psi}^l$$

Reduction to n_{df} single d.o.f modal equations of the time-exact ODE

$$\ddot{d}^l + 2\xi_l^h \omega_l^h \dot{d}^l + (\omega_l^h)^2 d^l = 0 \quad (\text{homogeneous case.})$$

ω_l^h : finite-dimensional (spatially discretized) natural frequencies

$$\xi_l^h = \frac{a}{\omega_l^h} + b \omega_l^h \quad \} \text{ Modal damping ratio.}$$

Rewrite 2ND-ORDER ODE as two 1ST-ORDER ODEs:

$$\underline{y} = \begin{Bmatrix} d \\ \dot{d} \end{Bmatrix}$$

Time-discretized problem in modal form:

$$a_{n+1}^l + 2\xi_l^h \omega_l^h v_{n+1}^l + (\omega_l^h)^2 d_{n+1}^l = 0 \quad (\text{homogeneous problem})$$

Newmark family Equations relate $d_{n+1}^l, v_{n+1}^l, a_{n+1}^l$

12.06 Reduction to two 1ST-ORDER ODEs:

$$\underbrace{\underline{y}_{n+1}}_{\begin{Bmatrix} d_{n+1} \\ v_{n+1} \end{Bmatrix}} = \underbrace{\underline{A}}_{\substack{\uparrow \\ \begin{Bmatrix} d_n \\ v_n \end{Bmatrix} \\ \text{2x2 amplification} \\ \text{matrix.}}} \underline{y}_n + \underline{L}_n$$

NOTE: Suppressing Mode Number Index, l .

Stability: $2\beta \geq \gamma \geq 1/2 \rightarrow \text{Unconditional Stability}$

$\gamma \geq 1/2$
 $0 \leq \beta \leq \gamma/2$ } Conditional Stability.

$$\omega^h \Delta t \leq \Omega_{\text{crit}}$$

$$\Omega_{\text{crit}} = \xi^h (\gamma - 1/2) + \left[\frac{\gamma}{2} - \beta + (\xi^h)^2 (\gamma - 1/2) \right]^{1/2}$$

damping when $\xi^h > 0$.

$$\text{Undamped critical frequency: } \Omega_{\text{crit}}^u = \left(\frac{\gamma}{2} - \beta \right)^{-1/2}$$

$$\Omega_{\text{crit}}^u \leq \Omega_{\text{crit}}$$

Ω_{crit}^u is a more stringent condition on $\omega^h \Delta t$

Method	Type	β	γ	Ω_{crit}^u	order of Accuracy
Trapezoidal Rule	Implicit	$1/4$	$1/2$	uncond.	2
Linear Acceleration		$1/6$	$1/2$	$2\sqrt{3}$	2
Average Acceleration		$1/12$	$1/2$	$\sqrt{6}$	2
Central Difference	Explicit	0	$1/2$	2	2

12.07 Stability Analysis is based on an eigenvalue analysis of the amplification matrix. A

$$\underline{y}_{n+1} = \underset{\uparrow}{\underline{A}} \underline{y}_n + \underline{L}_n$$

Define the spectral radius of A: $r(\underline{A}) = \max_i |\lambda_i(\underline{A})|$ $\{i=1,2\}$
 \uparrow
eigen values of A

Stability: $r \leq 1$ if λ_1, λ_2 are distinct.
eigenvectors of A
are linearly independent.

$$= \max_{i=1,2} \sqrt{\lambda_i(\underline{A}) \cdot \underbrace{\overline{\lambda_i(\underline{A})}}_{\text{complex conjugate of } \lambda_i(\underline{A})}}$$

$r < 1$ if $\lambda_1 = \lambda_2$
eigenvectors of A are linearly dependent.

(1) Linearly independent eigen vectors:

$$\underline{y}_{n+1} = \underline{A} \underline{y}_n; \quad \underline{y}_n = \underline{A} \underline{y}_{n-1}, \quad \underline{y}_{n-1} = \dots$$

$$\vdots$$

$$\underline{y}_{n+1} = \underline{A}^{n+1} \underline{y}_0$$

$$\underline{A} = \underline{P} \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} \underline{P}^{-1} \Rightarrow \underline{A}^n = \underbrace{\underline{P} \begin{bmatrix} \lambda_1^n & 0 \\ 0 & \lambda_2^n \end{bmatrix} \underline{P}^{-1}}_{\text{bounded}}$$

(2) Linearly dependent eigenvectors:

$$\underline{A} = \underline{Q} \begin{bmatrix} \lambda & 1 \\ & \lambda \end{bmatrix} \underline{Q}^{-1}$$

$$\Rightarrow \underline{A}^n = \underline{Q} \begin{bmatrix} \lambda^n & n \cdot \lambda^{n-1} \\ & \lambda^n \end{bmatrix} \underline{Q}^{-1}$$

$\lambda = 1$ then this term becomes n .

Off-diagonal term diverges as n .

Solving of λ : $\lambda^2 - 2A_1\lambda + A_2 = 0$

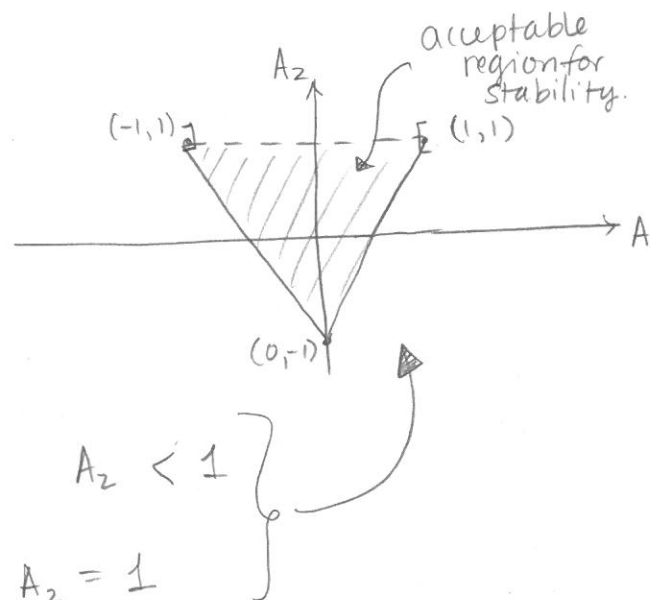
$$A_1 = \frac{1}{2} \text{trace}(\underline{A})$$

$$A_2 = \det(\underline{A})$$

$$\rightarrow \lambda_1, \lambda_2 = A_1 \pm \sqrt{A_1^2 - A_2}$$

Stability in terms of A_1 & A_2 :

$$\left. \begin{aligned} -\frac{(A_2+1)}{2} &\leq A_1 \leq \frac{(A_2+1)}{2} && \text{if } A_2 < 1 \\ -1 < A_1 < 1 &&& \text{if } A_2 = 1 \end{aligned} \right\}$$



12.08 Stability conditions on \underline{A} :

$$A_1 = \frac{1}{2} \text{trace}(\underline{A}) \quad \& \quad A_2 = \det(\underline{A})$$

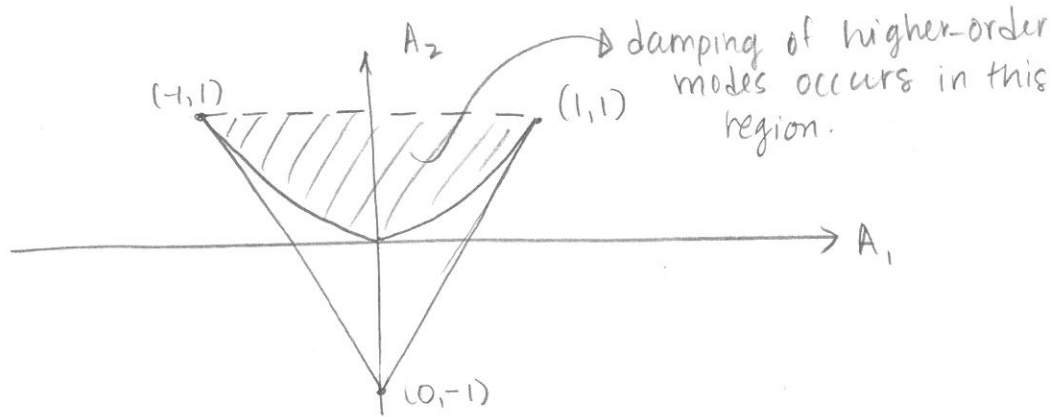
$$\lambda_1, \lambda_2 = A_1 \pm \sqrt{A_1^2 - A_2}$$

$$r = \max_{i=1,2} \sqrt{\lambda_i \cdot \bar{\lambda}_i}$$

$$r \leq 1$$

High-order Modes are nondecaying if λ_1, λ_2 are purely real.

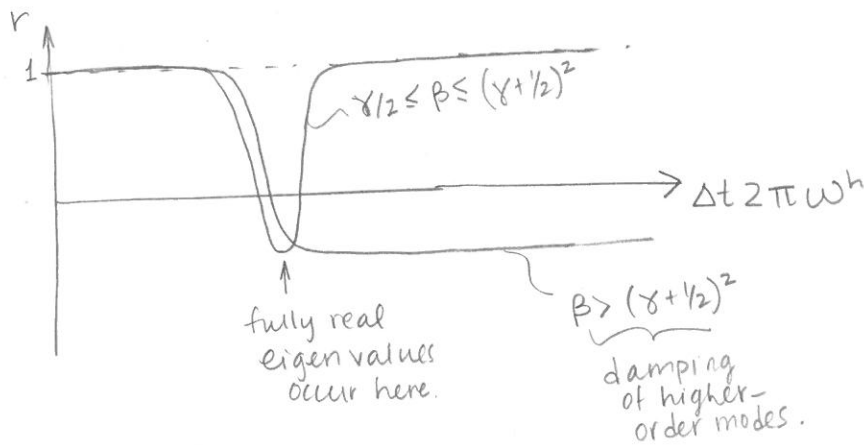
Need $A_1^2 - A_2 < 0$ for damping of higher-order modes.



Stability Requirement: $\beta \geq \frac{\gamma}{2}$ } unconditional

$\beta \geq \frac{(\gamma + \frac{1}{2})^2}{4}$ } damping of higher-order modes.

→ Spectral Radius:



Consistency:

$\underline{y}_{n+1} = \underline{A} \underline{y}_n + \underline{L}_n$ } inhomogeneous problem.
& time-discrete modal equation.

$\underline{y}(t_{n+1}) = \underline{A} \underline{y}(t_n) + \underline{L}_n + \Delta t \underline{\tau}(t_n)$ } time-exact modal eqn..
substituted.

Consistency Requires $\underline{\tau} = \underline{c} \cdot \Delta t^k$, $\begin{cases} \tau_1(t_n) \\ \tau_2(t_n) \end{cases} = \begin{cases} c_1 \\ c_2 \end{cases} \Delta t^k$, $k < 0$, c_1, c_2 are constants

k : order of accuracy.

Lax Theorem: Consistency and Stability \Rightarrow Convergence

$$\underline{e}_{n+1} = \underline{A}^{n+1} \underline{e}_0 - \sum_{i=0}^n \Delta t \underline{A}^i \underline{\tau}(t_n)$$

$$\lim_{\Delta t \rightarrow 0} \underline{e}_{n+1} = \underline{0}$$