

Normalization PIAFS

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1 Parameters

1.1 Pump beams

Physical quantity	name in the code	usual value	comment
λ_{UV}	IUV	248nm	Pump wavelength, $\in [200, 300]$
θ	theta	$0.17 \pi / 180$	half angle between prop beams
τ_{pulse}	tpulse	10ns	duration of the pump beam
ω_{UV}	nu	c/λ_{UV}	pump frequency
F_0	F0	$200mJ/cm^2$	pump fluence

1.2 ‘Derived quantities’

Physical quantity	name in the code	usual value	comment
k_{UV}	kUV	$2\pi/\lambda_{UV}$	pump beam wave vector
ω_{UV}	wUV	$k_{UV}c$	pump beam frequency
k_g	kg	$2k_{UV} \sin \theta$	grating wave vector
λ_g	lg	$2\pi/k_g$	grating wavelength
ω_g	wg	$k_g c_s$	grating frequency where c_s is the acoustic velocity for the initial conditions

1.3 Diffracted beam

Physical quantity	name in the code	usual value	comment
λ_{diff}	ldiff	532nm	Value article Michine & Yoneda
k_{diff}	kdiff	$2\pi/\lambda_{diff}$	

1.4 Gas conditions

Physical quantity	name in the code	usual value	comment
f_{CO_2}	fCO2	a few percents	CO_2 Fraction: if we have a mix of O_2 and CO_2 instead of pure CO_2
f_{O_2}	fO2	$1 - f_{CO_2}$	O_2 Fraction
f_{O_3}	fO3v	$\in [0, 0.3]$	O_3 Fraction, usually between 0 and 3% of the total gas concentration (we assume the total concentration is the O_2 concentration since $[O_2] \ll [O_3]$)
P_{tot}	Ptot	101325 Pa	O_2 Total gas pressure for 288 K
C_v	CvO2	$5/2 k_B$	Heat capacity for O_2
M_{O_2}	mmolO2	0.032 kg	O_2 Molar mass
γ	gamma	7/5	O_2 Heat capacity ratio
σ_{O_3}	sO3	$1.110^{-17} cm^{-2}$	ozone absorption cross-section in the center of the Hartley band
F_s	Fs	$h\nu/\sigma_{O_3}$	O_2 Saturation Fluence
n_{O_x}	n_Ox	$f_{O_x} P_{tot}/k_B/T_i$	Initial concentration in particle / m^{-3} of O_x where x is 2 or 3
$n_{h\nu_{max}}$	n_hnumax	$I_0/c/h/nu$	Initial photon concentration: Total laser energy divided by the energy of 1 photon
E_i	Ei	$P_{tot}/(\gamma - 1)/n_{O_2}$	Volumic initial gas internal energy in J
T_i	Ti	288 K	Initial temperature

1.5 Chemistry

Physical quantity	name in the code	usual value	comment
q	q0a, q0b etc	a few eV	O_2 Heat energy from reactions 0_a , 0_b etc
k	k0a, k0b etc	$10^{-18} - 10^{-12} m^3/s$	O_2 reaction rates from reactions 0_a , 0_b etc

2 Calculation of the viscous and heat conduction terms

From Acoustics, Allan D. Pierce, p589

Viscosity:

$$\frac{\mu}{\mu_0} = \left(\frac{T}{T_0} \right)^{3/2} \frac{T_0 + T_S}{T + T_S} \quad (1)$$

Thermal conductivity:

$$\frac{\kappa}{\kappa_0} = \left(\frac{T}{T_0} \right)^{3/2} \frac{T_0 + T_A e^{-T_B/T_0}}{T + T_A e^{-T_B/T}} \quad (2)$$

where μ_0 and κ_0 correspond to temperature T_0 . If these formulas hold for any given choice of T_0 , they also hold for any other choice of T_0 . The constants values are $T_S = 110.4K$, $T_A = 245.4K$, and $T_B = 27.6K$.

At 275K, $\mu_0 = 1.72 \times 10^{-4} g/cm^3$ and $\kappa_0 = 1.29 \times 10^{-5} cal/cm/s/K$

Bellow some values of μ/μ_0 and κ/κ_0 as a function of T, for the air.

T[K]	μ [kg/s/m]	μ/μ_0	κ [W/m/K]	κ/κ_0
280	1.75×10^{-5}	1.02	2.47×10^{-2}	1.022
290	1.8×10^{-5}	1.048	2558×10^{-2}	1.055
300	1.85×10^{-5}	1.076	2.62×10^{-2}	1.087
320	1.94×10^{-5}	1.13	2.78×10^{-2}	1.151
340	2.03×10^{-5}	1.183	2.93×10^{-2}	1.213
360	2.12×10^{-5}	1.234	3.08×10^{-2}	1.275
380	2.20×10^{-5}	1.283	3.22×10^{-2}	1.335
400	2.22×10^{-5}	1.332	3.34×10^{-2}	1.394

conductivity will be necessary for non linear situation where we have a consequent temperature modulation

The chemicals reactions in the bright interference fringes lead to a temperature modulation along x, thus an x dependence of μ and κ

Viscosity:

$$\frac{\mu(x)}{\mu_0} = \left(\frac{T(x)}{T_0} \right)^{3/2} \frac{T_0 + T_S}{T + T_S} \quad (3)$$

Thermal conductivity:

$$\frac{\kappa(x)}{\kappa_0} = \left(\frac{T(x)}{T_0} \right)^{3/2} \frac{T_0 + T_A e^{-T_B/T_0}}{T + T_A e^{-T_B/T}} \quad (4)$$

3 Normalizations

3.1 Basics

- Time normalized to acoustic frequency ω_g
- Space normalized to acoustic wave vector k_g
- Speed normalized to initial acoustic velocity c_s

3.2 Gas properties

- Density normalized to O_2 concentration n_{O_2}
- Pressure and energy normalized to $\omega_g n_{O_2} c_s$

In black the quantities in SI, in red the normalization.

First Euler equation:

$$\partial_t \frac{1}{\omega_g} \times \rho \frac{N_A}{M_{O_2} n_{O_2}} + \partial_x \frac{1}{k_g} \times \rho \frac{N_A}{M_{O_2} n_{O_2}} \times u \frac{1}{c_s} = 0 \quad (5)$$

Second Euler equation with viscous term:

$$\begin{aligned} \partial_t \frac{1}{\omega_g} \times \rho \frac{N_A}{M_{O_2} n_{O_2}} u \frac{1}{c_s} + \partial_x \frac{1}{k_g} \times \left(\rho \frac{N_A}{M_{O_2} n_{O_2}} \times u^2 \frac{1}{c_s^2} + p \frac{N_A}{n_{O_2} M_{O_2} c_s^2} \right) \\ = \partial_x \frac{1}{k_g} \left(\mu \frac{N_A}{M_{O_2} k_g \omega_g} \times \partial_x \frac{1}{k_g} \times u \frac{1}{c_s} \right) \end{aligned} \quad (6)$$

Third Euler equation with source term, viscous and heat conductivity term:

$$\begin{aligned} \partial_t \frac{1}{\omega_g} \times E \frac{N_A}{k_g n_{O_2} M_{O_2} c_s^2} + \partial_x \frac{1}{k_g} \times u \frac{1}{c_s} \times (E \frac{N_A}{k_g n_{O_2} M_{O_2} c_s^2} + p \frac{N_A}{k_g n_{O_2} M_{O_2} c_s^2}) \\ = \frac{Q}{\gamma - 1} \frac{N_A}{w_g^2 n_{O_2} M_{O_2} c_s} + \mu \frac{N_A}{M_{O_2} k_g \omega_g} \times \partial_x^2 \frac{1}{k_g^2} \times u \frac{1}{c_s} + \partial_x (\kappa \partial_x T) \end{aligned} \quad (7)$$

3.3 Chemistry

Normalisation of q and k:

$$Q \propto q \times k \times n^2.$$

$$q \frac{1}{k_g c_s^2} \times k \frac{n_{O_2}}{\omega_g} \times n^2 \frac{1}{n_{O_2}^2} \quad (8)$$

In the script, the values of q are initially in eV. qe is in J. We want q normalized to the initial internal energy. In the script, I use the normalisation e/E_i where E_i is the initial internal energy in J (not the volumic energy as in the Euler equation, hence the absence of n_{O_2} in the normalization).

Then the normalization for the chemistry equations are:

$$n_c = n \frac{1}{n_{O_2}} + \partial_t \frac{1}{\omega_g} \times (k \frac{n_{O_2}}{\omega_g} \times n_x \frac{1}{n_{O_2}} \times n_y \frac{1}{n_{O_2}} + \dots) \quad (9)$$

where n_c is the concentration of n at time n+1

4 Navier–Stokes Equations

The 1D Navier–Stokes equations in dimensional form (Tannehill & Anderson) are:

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} (\rho u) = 0, \quad (10a)$$

$$\frac{\partial}{\partial t} (\rho u) + \frac{\partial}{\partial x} (\rho u^2 + P) = \frac{\partial}{\partial x} \left[\frac{2}{3} \mu \left(2 \frac{\partial u}{\partial x} \right) \right], \quad (10b)$$

$$\frac{\partial E}{\partial t} + \frac{\partial}{\partial x} (E + P) u = \frac{\partial}{\partial x} \left[\frac{2}{3} \mu \left(2 \frac{\partial u}{\partial x} \right) u \right] + \frac{\partial}{\partial x} \left(\kappa \frac{\partial T}{\partial x} \right), \quad (10c)$$

where

$$E = \frac{P}{\gamma - 1} + \frac{1}{2} \rho u^2, \quad P = \rho R T. \quad (11)$$

Normalization Rewriting (10),

$$\frac{\rho_{\text{ref}}}{t_{\text{ref}}} \frac{\partial \tilde{\rho}}{\partial \tilde{t}} + \frac{\rho_{\text{ref}} c_s}{x_{\text{ref}}} \frac{\partial}{\partial \tilde{x}} (\tilde{\rho} \tilde{u}) = 0, \quad (12a)$$

$$\frac{\rho_{\text{ref}} c_s}{t_{\text{ref}}} \frac{\partial}{\partial \tilde{t}} (\tilde{\rho} \tilde{u}) + \frac{\rho_{\text{ref}} c_s^2}{x_{\text{ref}}} \frac{\partial}{\partial \tilde{x}} (\tilde{\rho} \tilde{u}^2 + \tilde{P}) = \frac{\mu_{\text{ref}} c_s}{x_{\text{ref}}^2} \frac{\partial}{\partial \tilde{x}} \left[\frac{2}{3} \tilde{\mu} \left(2 \frac{\partial \tilde{u}}{\partial \tilde{x}} \right) \right], \quad (12b)$$

$$\frac{\rho_{\text{ref}} c_s^2}{t_{\text{ref}}} \frac{\partial \tilde{E}}{\partial \tilde{t}} + \frac{\rho_{\text{ref}} c_s^3}{x_{\text{ref}}} \frac{\partial}{\partial \tilde{x}} (\tilde{E} + \tilde{P}) \tilde{u} = \frac{\mu_{\text{ref}} c_s^2}{x_{\text{ref}}^2} \frac{\partial}{\partial \tilde{x}} \left[\frac{2}{3} \tilde{\mu} \left(2 \frac{\partial \tilde{u}}{\partial \tilde{x}} \right) \tilde{u} \right] + \frac{\kappa_{\text{ref}} T_{\text{ref}}}{x_{\text{ref}}^2} \frac{\partial}{\partial \tilde{x}} \left(\tilde{\kappa} \frac{\partial \tilde{T}}{\partial \tilde{x}} \right), \quad (12c)$$

where the subscript ref denotes a reference quantity, and \tilde{cdot} are the normalized variables. Based on the previous section, we have the following basic quantities:

$$\begin{aligned} R &= \frac{N_A k_B}{M_{O_2}} \approx 259.7 \text{ J kg}^{-1} \text{ K}^{-1}, \quad c_p = 918.45 \text{ J kg}^{-1} \text{ K}^{-1} \text{ (O}_2 \text{ at } 288 \text{ K}), \\ x_{\text{ref}} &= \frac{1}{k_g}, \quad T_{\text{ref}} = T_i = 288 \text{ K}, \quad \rho_{\text{ref}} = \frac{P_{\text{tot}}}{R T_{\text{ref}}} = 1.356 \text{ kg m}^{-3}, \\ \mu_{\text{ref}} &= \mu_{O_2}(T_{\text{ref}}) = 1.99 \times 10^{-5} \text{ kg s}^{-1} \text{ m}^{-1}, \quad \kappa_{\text{ref}} = \kappa_{O_2}(T_{\text{ref}}) = 2.70 \times 10^{-2} \text{ W m}^{-1} \text{ K}^{-1}. \end{aligned} \quad (13)$$

and the following derived reference quantities:

$$c_s = \sqrt{\gamma R T_{\text{ref}}} = 323.59 \text{ m s}^{-1}, \quad t_{\text{ref}} = \frac{x_{\text{ref}}}{c_s}, \quad P_{\text{ref}} = \rho_{\text{ref}} c_s^2. \quad (14)$$

Thus, omitting the $\tilde{\cdot}$ symbol for convenience, (12) is:

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} (\rho u) = 0, \quad (15a)$$

$$\frac{\partial}{\partial t} (\rho u) + \frac{\partial}{\partial x} (\rho u^2 + P) = \left(\frac{\mu_{\text{ref}}}{\rho_{\text{ref}} c_s x_{\text{ref}}} \right) \frac{\partial}{\partial x} \left[\frac{2}{3} \mu \left(2 \frac{\partial u}{\partial x} \right) \right], \quad (15b)$$

$$\frac{\partial E}{\partial t} + \frac{\partial}{\partial x} (E + P) u = \left(\frac{\mu_{\text{ref}}}{\rho_{\text{ref}} c_s x_{\text{ref}}} \right) \frac{\partial}{\partial x} \left[\frac{2}{3} \mu \left(2 \frac{\partial u}{\partial x} \right) u \right] + \left(\frac{\kappa_{\text{ref}}}{\gamma R \rho_{\text{ref}} c_s x_{\text{ref}}} \right) \frac{\partial}{\partial x} \left(\kappa \frac{\partial T}{\partial x} \right). \quad (15c)$$

Note that

$$\left(\frac{\kappa_{\text{ref}}}{\gamma R \rho_{\text{ref}} c_s x_{\text{ref}}} \right) = \left(\frac{\kappa_{\text{ref}}}{\gamma R \mu_{\text{ref}}} \right) \left(\frac{\mu_{\text{ref}}}{\rho_{\text{ref}} c_s x_{\text{ref}}} \right) = \left(\frac{\kappa_{\text{ref}}}{(\gamma - 1) c_p \mu_{\text{ref}}} \right) \left(\frac{1}{Re} \right) = \frac{1}{(\gamma - 1) Pr Re}, \quad (16)$$

where Pr is the Prandtl number and Re is the Reynolds number. Therefore, the normalized Navier-Stokes equations (as implemented in PIAFS2D) are:

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} (\rho u) = 0, \quad (17a)$$

$$\frac{\partial}{\partial t} (\rho u) + \frac{\partial}{\partial x} (\rho u^2 + P) = \frac{1}{Re} \frac{\partial}{\partial x} \left[\frac{2}{3} \mu \left(2 \frac{\partial u}{\partial x} \right) \right], \quad (17b)$$

$$\frac{\partial E}{\partial t} + \frac{\partial}{\partial x} (E + P) u = \frac{1}{Re} \frac{\partial}{\partial x} \left[\frac{2}{3} \mu \left(2 \frac{\partial u}{\partial x} \right) u \right] + \frac{1}{(\gamma - 1) Pr Re} \frac{\partial}{\partial x} \left(\kappa \frac{\partial T}{\partial x} \right). \quad (17c)$$

Normalizing the equation of state (11),

$$P = \left(\frac{\rho_{\text{ref}} R T_{\text{ref}}}{\rho_{\text{ref}} c_s^2} \right) \rho T \Rightarrow \gamma P = \rho T. \quad (18)$$

The normalized coefficients of viscosity and conductivity are computed by normalizing (1) and (2):

$$\mu = \frac{T}{T_0}^{\frac{3}{2}} \left(\frac{T_0 + T_S}{T + T_S} \right), \quad \kappa = \frac{T}{T_0}^{\frac{3}{2}} \left(\frac{T_0 + T_A e^{-\frac{T_B}{T_0}}}{T + T_A e^{-\frac{T_B}{T}}} \right), \quad (19)$$

where the constants are all normalized by T_{ref} .

Implementation in PIAFS2D The following parameters should be specified in the `physics.inp` file:

$$Re = \frac{\rho_{\text{ref}} c_s x_{\text{ref}}}{\mu_{\text{ref}}} \approx \frac{1.36 \times 323.59 \times 6.65 \times 10^{-6}}{1.99 \times 10^{-5}} = 1.47 \times 10^2 \quad (\text{Reynolds number}) \quad (20a)$$

$$Pr = \frac{c_p \mu_{\text{ref}}}{\kappa_{\text{ref}}} \approx \frac{918.45 \times 1.99 \times 10^{-5}}{2.70 \times 10^{-2}} = 0.68 \quad (\text{Prandtl number}) \quad (20b)$$