

Mathematical Modeling and Optimization of Ion Transport Membrane for Oxygen Separation from Air

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Introduction and Background on Air Separation

- > There is a growing demand for high purity oxygen (oxy-combustion) as a replacement for air in combustion and gasification processes.
- ➤ Energy-related emissions have been growing in importance recently due to them accounting for roughly 68 percent of greenhouse gas emissions.
- In comparison to Air-Combustion, Oxy-combustion processes have exhibited lower harmful CO2 and NOx emissions and higher overall combustion efficiency, due to a drop in heat loss (as a result of lower mass flow rates) out of the stack.
- The main air separation technologies used currently to produce high purity (99%>) oxygen are Cryogenic Air Separation, Pressure or Vacuum Swing Absorption (PSA or VSA respectively), as well as, membrane technologies.
- In comparison to cryogenic air separation, ITM technologies exhibit lower electricity costs attributed to the lack of a need for much (if any) external electrical loadings to drive the separation process.
- > Approximately 1520 mol/s of oxygen is required for a 620 MWe IGCC power plant.

Ion Transport Membrane Modeling and Optimization

> An Ion Transport Membrane (ITM) consists of a shell and tube setup where surface ion exchange reaction/permeation occur simultaneously.

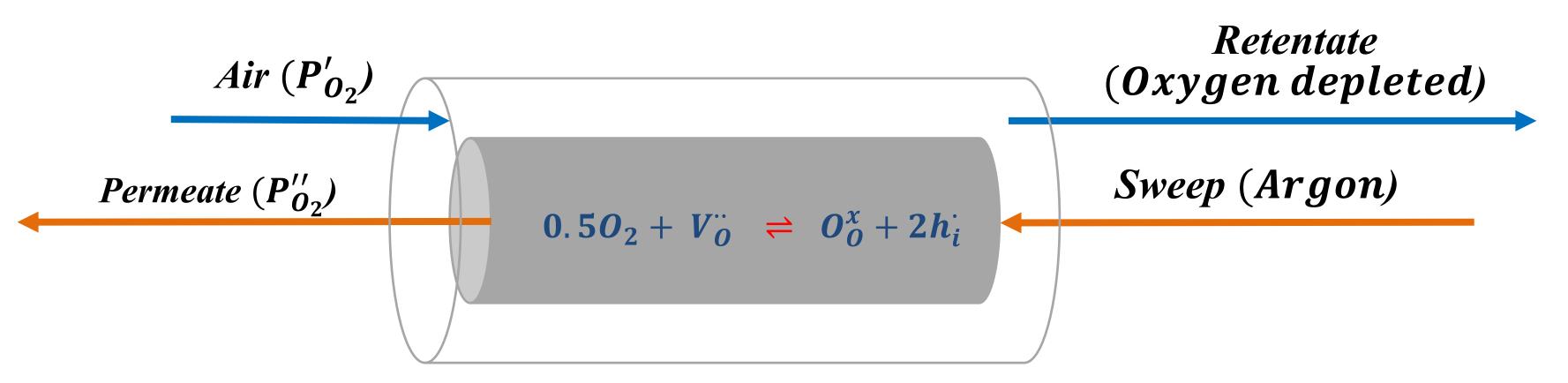
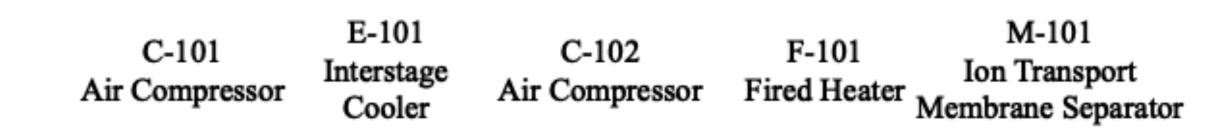


Figure 1: Ion Transport Membrane



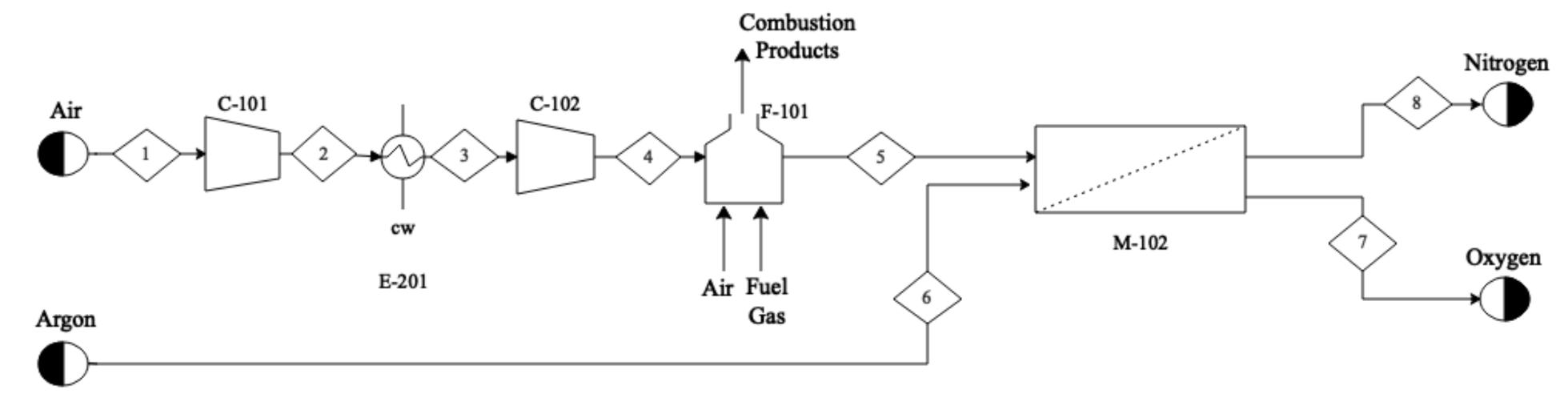


Figure 2: OITM based air separation unit

<u>Table 1:</u> Values for cost parameters objective function

$A_r(M)$	8.92
Air(\$/Kmol)	0.11
$_{o_2}(\fine 0)$	960
\$ _{NG} (\$/GJ)	3.95
$m(m^2)$	1000
Op (hours)	7880

*Based on LHV of natural gas of 0.7935 GJ/mol ** Price at pressure of 3.3 barg > Oxygen permeation rate equation for perovskite membrane material $La_{0.6}Sr_{0.4}Co_{0.8}Fe_{0.2}O_{3-\alpha}$ (LSCF)*

$$\frac{\partial N_{O_2}}{\partial l} = \frac{k_r \left[\left(p'_{O_2} \right)^{0.5} - \left(p''_{O_2} \right)^{0.5} \right]}{\frac{(p''_{O_2})^{0.5}}{2\pi R_O} + \frac{k_f \ln(\frac{R_O}{R_i})(p'_{O_2})^{0.5}(p''_{O_2})^{0.5}(p''_{O_2})^{0.5}}{\pi D_v} + \frac{(p'_{O_2})^{0.5}}{2\pi R_{in}}$$

Results

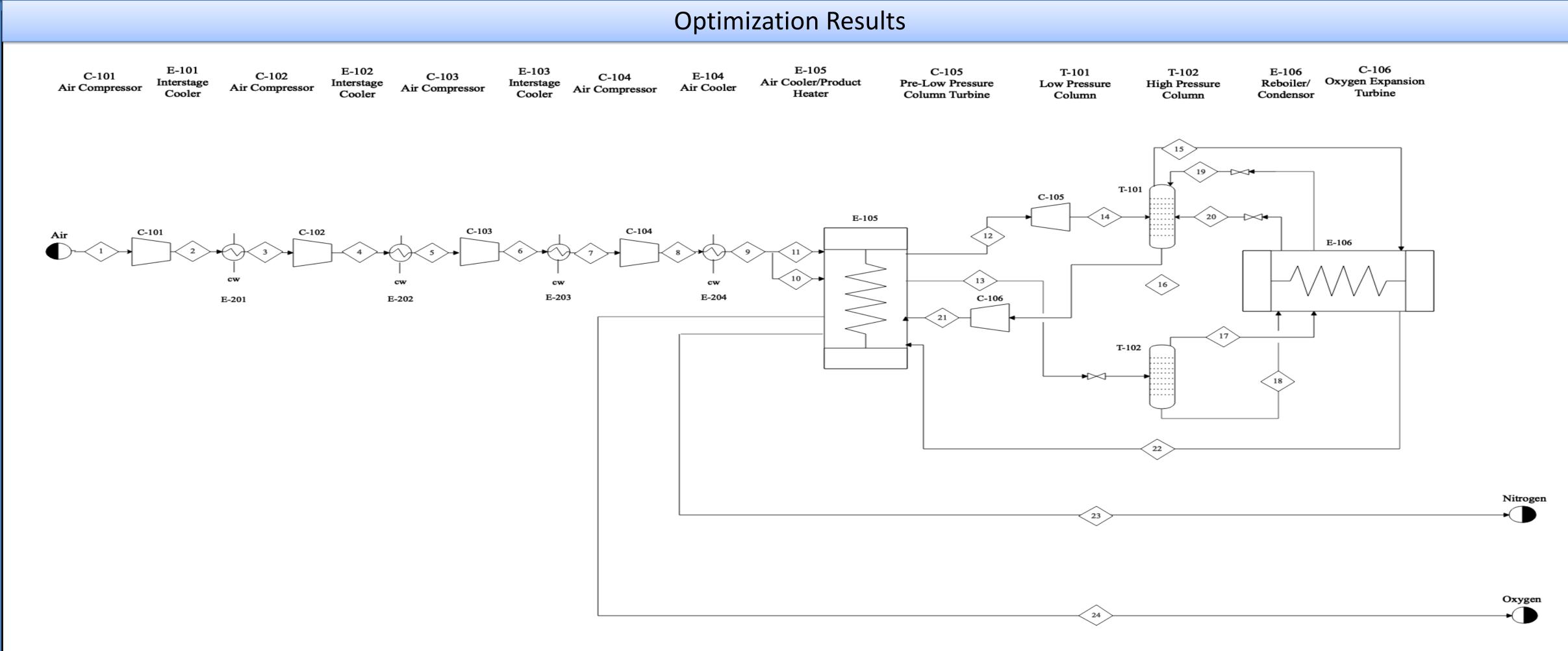


Figure 3: Cryogenic ASU unit PFD

Table 2: Base case economic evaluations

Unit Type	Capital Cost (Thousands of	Comparison with Literature
	dollars)	(Thousands of dollars)**
Cryogenic ASU	125,900	113,000
OITM based ASU*	158,600	182,000

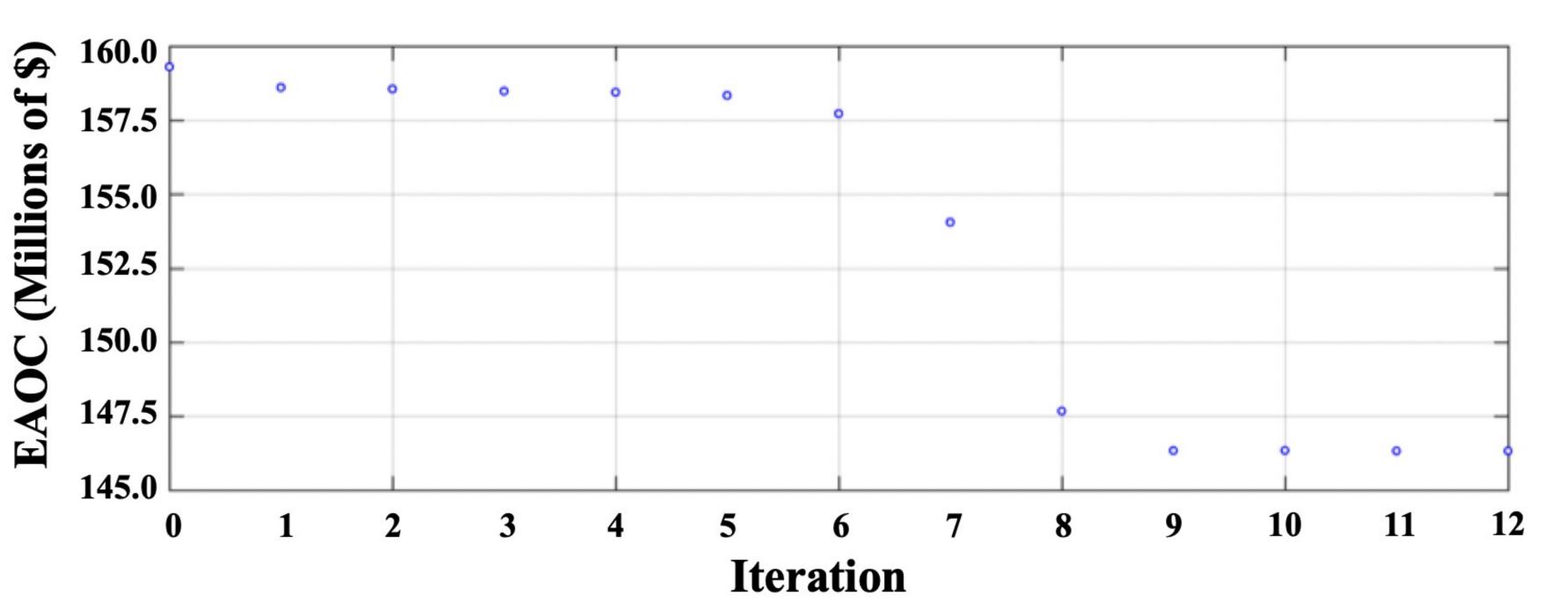


Figure 4: Preliminary optimization results for ITM ASU

Conclusion and Future Directions

- > A membrane reactor model was developed and integrated into an ASU to be economically evaluated
- > Constrained optimization problem was formulated, permitting the systematic selection of optimal reactor design through more efficient membrane utilization.
- > A Cryogenic ASU simulation was economically evaluated and altered in order to match the IGCC specifications found in the literature***
- These models may be integrated into larger power plant simulations and evaluated for further research on the economic and environmental validity of OITM technology
- > Future work will consider application to operability and process control studies.

Acknowledgements

The authors gratefully acknowledge the Donors of the American Chemical Society Petroleum Research Fund and the National Science Foundation CAREER Award 1653098 REU Supplement for partial support of this research. Also, acknowledgement is made to the financial support from West Virginia University.

Research sponsored through the NSF-REU program funding under Dr. Lima's Control, Optimization and Design of Energy Systems (CODES) research group.