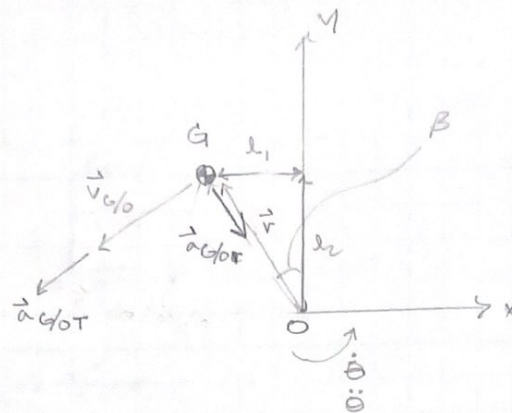


FOR TURRET LOCAL FRAME:



$$\vec{r} = -l_1 \hat{i} + l_2 \hat{j} \quad \beta = \tan^{-1}\left(\frac{l_1}{l_2}\right)$$

$$|\vec{r}| = \sqrt{l_1^2 + l_2^2}$$

$$\vec{v}_{G/O} = \vec{\omega} \times \vec{r} = (\dot{\theta} \hat{k}) \times (-l_1 \hat{i} + l_2 \hat{j})$$

$$\vec{v}_{G/O} = -l_2 \dot{\theta} \hat{i} + l_1 \dot{\theta} \hat{j}$$

$$|\vec{v}_{G/O}| = \dot{\theta} \sqrt{l_1^2 + l_2^2} = \dot{\theta} r$$

$$\vec{a}_{G/O} = \vec{\ddot{\theta}} \times \vec{r}$$

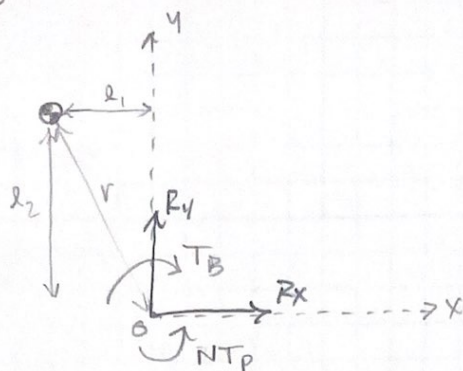
$$= (\ddot{\theta} \hat{k}) \times (-l_1 \hat{i} + l_2 \hat{j})$$

$$\vec{a}_{G/O} = -l_2 \ddot{\theta} \hat{i} - l_1 \ddot{\theta} \hat{j}$$

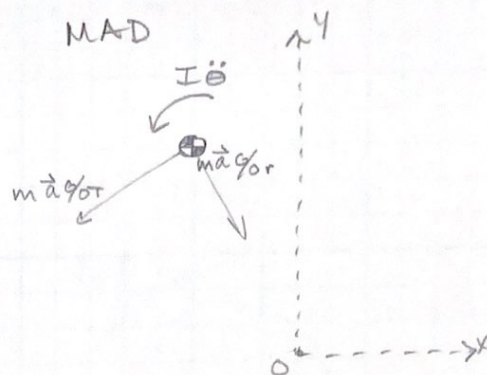


(3)

FBD



MAD



$$(\sum M_{FBD})_O = (\sum M_{MAD})_O$$

$$NT_P \hat{k} - TB \hat{k} = I \ddot{\theta} \hat{k} + \vec{r} \times \vec{a}_{g_{OT}m}$$

$$NT_P \hat{k} - \theta b \hat{k} = (I_{yy}) \ddot{\theta} \hat{k} + (-l_1 \hat{i} + l_2 \hat{j}) \times (-m l_2 \ddot{\theta} \hat{i} - l_1 m l_1 \ddot{\theta} \hat{j})$$

$$= (I_{yy} \ddot{\theta}) \hat{k} + m(l_1^2 \ddot{\theta} \hat{k} + l_2^2 \ddot{\theta} \hat{k})$$

$$NT_P - \theta b = (I_{yy} + m(l_1^2 + l_2^2)) \ddot{\theta}$$

$$NT_P - \theta b = (I_{yy} + m r^2) \ddot{\theta}$$

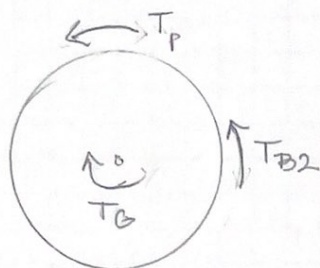
$$\textcircled{1} \quad \ddot{\theta} = -\theta \frac{b}{I_{yy} + m r^2} + \frac{N}{I_{yy} + m r^2} T_P$$

(4)

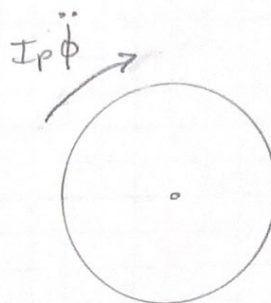
Determine Torque to Platter Through  
Pinion gear

Pinion gear:

FBD



MAD



$$\sum M_{FBD} = \sum M_{MAD}$$

$$-T_P - T_{B2} + T_G = -I_P \ddot{\phi}$$

$$T_P = -b_2 \dot{\phi} - I_P \ddot{\phi} + T_G$$

Assuming Motor Gearbox has no inertia/  
damping

$$T_G = 50 T_m = 50 \underbrace{K_t i_m}_{\text{Motor Torque}}$$

Gearbox torque



Motor Equations:

$$\frac{di_m}{dt} = -\frac{R}{L} i_m - \frac{K_v}{L} \Omega_m + \frac{1}{L} V_m$$

Let  $u$  represent the PWM % duty cycle

$$V_m = \frac{12V}{100} u$$

$$\frac{di_m}{dt} = -\frac{R}{L} i_m - \frac{K_v}{L} (N50) \dot{\theta} + \frac{1}{L} \frac{12}{100} u \quad (2)$$

Turret Pinion relationship:

$$\theta = N\phi \rightarrow \phi = \frac{1}{N}\theta$$

$$\dot{\theta} = N\dot{\phi} \quad \dot{\phi} = \frac{1}{N}\dot{\theta}$$

$$\ddot{\theta} = N\ddot{\phi} \quad \ddot{\phi} = \frac{1}{N}\ddot{\theta}$$

Sub into pinion EOM:

$$T_P = -b_2\dot{\phi} - I_P\ddot{\phi} + T_G$$

↓

$$T_P = -b_2\frac{1}{N}\dot{\theta} - I_P\frac{1}{N}\ddot{\theta} + T_G$$

Sub into eq (1)

$$\ddot{\theta} = \frac{-b_1}{I_{yy}+mr^2}\dot{\theta} + \frac{N}{I_{yy}+mr^2}\left(-\frac{b_2}{N}\dot{\theta} - \frac{I_P}{N}\ddot{\theta} + 50K_t \text{im}\right)$$

$$\ddot{\theta} = -\frac{b_1}{I_{yy}+mr^2}\dot{\theta} - \frac{b_2}{I_{yy}+mr^2}\dot{\theta} - \frac{I_P}{I_{yy}+mr^2}\ddot{\theta} + \frac{N50K_t}{I_{yy}+mr^2}\text{im}$$

$$\ddot{\theta}\left(\frac{I_{yy}+mr^2+I_P}{I_{yy}+mr^2}\right) = -\dot{\theta}\left(\frac{b_1+b_2}{I_{yy}+mr^2}\right) + \left(\frac{N50K_t}{I_{yy}+mr^2}\right)\text{im}$$

$$\boxed{\frac{d}{dt}\dot{\theta} = -\left(\frac{b_1+b_2}{I_{yy}+mr^2+I_P}\right)\dot{\theta} + \left(\frac{N50K_t}{I_{yy}+mr^2+I_P}\right)\text{im}} \quad (3)$$



State Equations:

$$\frac{d}{dt}\theta = \dot{\theta}$$

$$\frac{d}{dt}\dot{\theta} = -\left(\frac{b_1 + b_2}{I_{yy} + mr^2 + I_p}\right)\dot{\theta} + \left(\frac{NSOK_t}{I_{yy} + mr^2 + I_p}\right)i_m$$

$$\frac{d}{dt}i_m = -\left(\frac{NSOK_v}{L}\right)\dot{\theta} + \left(-\frac{R}{L}\right)i_m + \frac{12}{100L}u$$