6.2 UAS Model and Control

The key feature of *Movement Automaton* is to interface *continuous-control signal* as the *discrete command chain*. Following topics are introduced in this section:

- 1. Movement Automaton Background (sec. 6.2.1) the listing of related work and similar approaches to ours.
- 2. Specialization of Hybrid Automaton (sec. 6.2.2) the specialization of the hybrid automaton to fulfill control/approximation roles in our approach.
- 3. Formal Movement Automaton Definition (sec. 6.2.3) the formal definition of movement automaton used in our approach.
- 4. Used UAS Nonlinear Model (sec. 6.2.4) simple plane model used in this work as controlled plant.
- 5. Used Movement Automaton (sec. 6.2.5) movement automaton for UAS Nonlinear Model constructed from scratch.
- 6. Segmented Movement Automaton (sec. 6.2.6) for more complex systems the State Space can be separated into Segments and segment movement automaton is used to generate thick reference trajectory.
- 7. Reference Trajectory Generator (sec. 6.2.7) other use of Movement Automaton as predictor for reference trajectory calculation.

6.2.1 Movement Automaton Background

Movement Automaton is basic interface approach for discretization of trajectory evolution or control input for any continuous or discrete system model.

Main function of Movement Automaton is for system given by equation state = f(time, state, input) with initial state $state_0$ to generate reference trajectory state(t) or control $signal\ input(t)$.

Using Movement Automaton as Control Proxy will provide us with discrete command chain interface. This will reduce the non deterministic element from Evasive trajectory generation, by reducing infinite maneuver set to finite movement set.

Non determinism of Avoidance Maneuver have been discussed as an issue in following works:

- 1. Newton gradient method for evasive car maneuvers [1].
- 2. Non-holistic methods for trajectory generation [2].
- 3. Stochastic approach to elliptic trajectories generation [3].

Examples of Movement Automaton Implementation as Control Element can be mentioned as follows:

- 1. Control of traffic flow [4].
- 2. Complex air traffic collision situation resolution system [5, 6].
- 3. SAA/DAA capable avoidance system [7].

6.2.2 Specialization of Hybrid Automaton

Definition 1. Movement Primitive:

States from Hybrid automaton can be taken as Movements in Movement Automaton. MovementPrimitive (eq. 6.1) is describing the Movement behaviour as transfer function VectorField enriched with parameters.

$$MovementPrimitive(vectorField, minimalDuration, parameters) \\ VectorField: SystemState \times parameters \rightarrow SystemState$$
 (6.1)

Example: Let say that UAS system is given as position = velocity, then let us have two MovementPrimitives:

- 1. Stay minimalTime = 1s, $parameters = \{\}$, VectorField : position = 0.
- 2. Move minimalTime = 1s, $parameters = \{velocity\}$, VectorField : position = velocity.

Trajectory from Movement Primitives: The UAS should Move for 5s with velocity 10m/s, then Stay for 10s, then move for 7s with velocity 4m/s, with initial position $position_0 = 0$ and initial time $t_0 = 1$ The standard approach is to derive transfer function $position = \Theta(...)$

$$position(t) = \Theta(\dots) \begin{cases} t \in [0,5] &: 10 \times t + position(0) \\ t \in (5,15] &: 0 \times (t-5) + position(5) \\ t \in (15,22] &: 4 \times (t-15) + position(15) \end{cases}$$
(6.2)

The example given by (eq. 6.2) is fairly primitive, but imagine UAS system given by nonlinear dynamics $\dot{x} = f(x, u, t)$ [8]. Then defining transfer function for given command chain can be impossible.

Definition 2. Movement Transition:

System state can be different than intended movement application, the notion of Transition is therefore introduced as stabilizing element in movement chaining (eq. 6.3).

$$Transition: MovementPrimitive \times SystemState \rightarrow MovementPrimitive$$
 (6.3)

Trajectory with Transitions: Introducing two transitions Transition(Move, Stay) and Transition(Stay, Move) reflecting periods when vehicle stop moving or speed-up to desired velocity. The transfer function (eq. 6.2) can be rewritten as combination of MovementPrimitives (eq. 6.1) and Transitions (eq. 6.3):

$$Transition(Stay, Move), Move(5s, 10m/s),$$

$$Transition(Move, Stay), Stay(10s),$$

$$Transition(Stay, Move), Move(7s, 4m/s) \quad (6.4)$$

Note. There are two types of *MovementPrimitives*:

- 1. Stationary when system state is considered neutral and they are considered as entry point for automaton.
- 2. Dynamic when the system state is considered evolving and they needs to be terminated with stationary transition.

Movement Mapping Example: Transition/MovementPrimitive pairs (eq. 6.3) can be mapped into movements (eq. 6.5).

$$Move(5s, 10m/s) : Transition(Stay, Move), Move(5s, 10m/s),$$

 $Stay(10s) : Transition(Move, Stay), Stay(10s),$ (6.5)
 $Move(7s, 4m/s) : Transition(Stay, Move), Move(7s, 4m/s)$

Definition 3. Movement:

Movement can consist from multiple Transitions (eq. 6.3) and one MovementPrimitive (eq. 6.1), the duration of MovementPrimitive can be shortened by Transitions duration. Movement is defined as follows:

$$Movement \begin{pmatrix} initialState, \\ initialTime[0..1], \\ duration, \\ parameters[0..1] \end{pmatrix} = Chain \begin{pmatrix} InitialTransition(...)[0..*], \\ MovementPrimitive \begin{pmatrix} transitionState, \\ remainingDuration, \\ parameters \end{pmatrix} \\ LeaveTransition(...)[0..*], \end{pmatrix}$$
(6.6)

Chain function connects multiple initial Transitions which are applied at initialState at initialTime. Then own MovementPrimitive (eq. 6.1) is invoked with transitionnsState. Transitions state is state changed by Initial Transitions. After Movement Primitive there can be Leave Transitions Movement

Minimal Movement Time: Given by (eq. 6.7) for *movement* is given as sum of *MovementPrimitive* (eq. 6.1) minimal time, and *Transition* (eq. 6.3) in/out combined minimal time.

$$minimalTime(Movement) = \frac{minimalTime(MovementPrimitive) +}{\max_{in/out} \{time(Transition)\}}$$
(6.7)

Movement Chaining: Movements can be chained and applied to initial system state to generate system trajectory. Example of trajectory is given by (eq. 6.2). Movements are reversibly obtained by participation such trajectory into Movement primitives and Transitions. Then sample Trajectory for $n \in \mathbb{N}^+$ movements looks like (eq. 6.8).

```
Trajectory(t_{0}) = State(t_{0})
Trajectory(t_{0}, t_{1}] = Movement_{1}(Trajectory(t_{0}), t_{0}, duration_{1}, parameters_{1})
Trajectory(t_{1}, t_{2}] = Movement_{2}(Trajectory(t_{1}), t_{1}, duration_{2}, parameters_{2})
Trajectory(t_{2}, t_{3}] = Movement_{3}(Trajectory(t_{2}), t_{2}, duration_{3}, parameters_{3})
\vdots
Trajectory(t_{n-1}, t_{n}] = Movement_{n}(Trajectory(t_{n-1}), t_{n-1}, duration_{n}, parameters_{n})
(6.8)
```

Given Trajectory at time t_0 is given as initial State of System. For time interval (t_0, t_1) , which length is equal to $duration_1$, the State is given by $Movement_1$ with $parameters_1$ and base time t_0 . This behaviour continues for movements $2, \ldots, n$.

Definition 4. Movement Buffer:

Movements can be chained into Buffer with assumption of continuous movement execution. Continuous movement executions each movement in chain (eq. 6.8) is executed in time interval $\tau_i = (t_{i-1}, t_i]$ where i is movement order and \forall Movement_i starting time is t_0 or t_{i-1} from previous movement. With given assumption Buffer is given as (eq. 6.9) with parameters t_{i-1} , t_i omitted, due t_0 and duration_i dependency.

$$Buffer = \{Movement_i(duration_i, parameters_i)\} i \in \mathbb{N}^+$$
(6.9)

Definition 5. Movement Automaton Trajectory:

Let say system State $\in \mathbb{R}^n$ which Trajectory is defined by movement chaining (eq. 6.8), applied on some initial time $t_0 \in \mathbb{R}^+$ and final time $t_f = t_0 + \sum_{i=1}^{I} duration_i$, with movements contained in Buffer (eq. 6.9) is given as Trajectory (eq. 6.10).

$$Trajectory(t_0, State(t_0), Buffer) \ or \ Trajectory(State_0, Buffer) \ if \ t_0 = 0$$
 (6.10)

Note. The space dimension of Trajectories is \mathbb{R}^{n+1} if the space dimension of state Space is \mathbb{R}^n , because Trajectory space contains evolution of Space in time interval $T[t_0, t_f]$.

The transformation from transfer function (eq. 6.2) to trajectory (eq. 6.10) is natural, only set of Movement primitives (eq. 6.1) and set of Transitions (eq. 6.3) is required.

State Projection: Trajectory (eq. 6.10) is naturally evolution of space over time, then there exists StateProjection function (eq. 6.11) which returns State for specific Time.

$$StateProjection: Trajectory \times Time \rightarrow State(Time)$$
 (6.11)

6.2.3 Formal Movement Automaton Definition

Definition 6. Movement Automaton is given as follow:

$$InitialState :\in \mathbb{R}^h, h \in \mathbb{N}^+$$
(6.12)

$$System: \dot{State} = f(Time, State, Input) \ or \ vectorField$$
 (6.13)

$$Primitives = \left\{ MovementPrimitive_i \begin{pmatrix} vectorField, \\ minimalDuration, \\ parameters \end{pmatrix} \right\} i \in \mathbb{N}^+ \quad (6.14)$$

$$Transitions = \left\{ Transition_j \begin{pmatrix} MovementPrimitive_l, \\ MovementPrimitive_k \end{pmatrix}_{k \neq l} \right\} j \in N^+$$
 (6.15)

$$Primitives = \begin{cases} MovementPrimitive_{i} & (vectorField, \\ minimalDuration,) \end{cases} i \in \mathbb{N}^{+} \quad (6.14)$$

$$Transitions = \begin{cases} Transition_{j} & (MovementPrimitive_{l}, \\ MovementPrimitive_{k}) \end{cases} j \in \mathbb{N}^{+} \quad (6.15)$$

$$Movements = \begin{cases} Movement_{m} & (Transition_{o}[0..*], \\ MovementPrimitive_{p} \\ Transition_{r}[0..*], \end{cases} m \in \mathbb{N}^{+} \quad (6.16)$$

$$Buffer = \{Movement_s(duration_s, parameters_s)\} s \in \mathbb{N}^+$$
(6.17)

$$Executed = \{Movement_s(duration_s, parameters_t)\} t \in \mathbb{N}^+$$
(6.18)

$$Builder: Movement \times Movement Primitive \rightarrow Movement$$
 (6.19)

$$Trajectory: InitialState \times Movement^u \rightarrow State \times Time, u \in N^+$$
 (6.20)

$$StateProjection: Trajectory \times Time \rightarrow State(Time)$$
 (6.21)

System (eq. 6.13) is given in form of differential equations $\dot{x} = f(t, x, u)$ or other transformable equivalent, with initial state (eq. 6.12).

Movements (eq. 6.8) are defined as sequence of necessary initial transitions (eq. 6.15), movement primitive (eq. 6.14), and, leave transitions (6.15).

Buffer contains a set of movement primitives (eq. 6.14) to be executed in order to achieve desired goal. Builder (eq. 6.19) assures that first movement primitive (eq. 6.1) from Buffer (eq. 6.17) is transformed into next movement (eq. 6.16) based on current movement (eq. 6.16).

The system trajectory (eq. 6.20) is defined in (eq. 6.10). State projection (eqs. 6.11,6.21) is giving State variable for time $t \in [t_0, t_{max}]$ where t_m ax is given by:

$$t_{max} = t_0 + \sum_{i=1,u} Buffer.Movement(i).movementDuration$$
 (6.22)

Note. From Continuous Reach set to Movement Automaton Control Reach Set:

The reach set R (6.23) for system $\partial/\partial t$ state = model(state, input) with initial state $state_0 = state(t_i)$ in time interval $[t_i, t_{i+1}[$ is with existing control strategy $input(t) \in ControlStrategy(t)$. The reach set $R(state_0, t_0, t_1)$ where $t_1 > t_0$.

$$R(state_0, t_0, t_1) = \bigcup \{state(s) : input(s) \in ControlStrategy(s), s \in (t_0, t_1]\}$$
 (6.23)

The reach set \Re (6.24) of the system under the control of the movement automation consist from the set of trajectories Trajectory(initialState, buffer), which are executed in constrained time period $[t_i, t_{i+1}]$.

$$ReachSet(state_0, t_i, t_{i+1}) =$$

$$\{Trajectory(state_0, buffer) : duration(buffer) \le (t_{i+1} - t_i)\} \quad (6.24)$$

Note. Weak Invariance:

When the UAS is under the control of the movement automaton for the obstacle avoidance problem, by design of the avoidance algorithm, the trajectories of the UAV will not intersect any threat. This means that the controlled system $\partial/\partial t$ state = model(state, input) is weakly invariant with respect to the complement of the threats, and with respect to the free space. A pair (state, SafeSpace), where $\partial/\partial t$ state = model(state, input) and SafeSpace is a closed set, is weakly invariant if there exist controls such that a trajectory starting inside $State_0 \in SafeSpace$ remains inside $State(t) \in SafeSpace$ [9].

6.2.4 Used UAS Nonlinear Model

Motivation: Simplified rigid body kinematic model will be used. This model have decoupled roll, yaw and pitch angles. The focus is on *reach set approximation methods*, therefore *UAS model* is simplified.

State Vector (eq. 6.25) defined as positional state in euclidean position in right-hand euclidean space, where x, y, z can be abstracted as latitude, longitude, altitude.

$$state = [x, y, z, roll, pitch, yaw]^{T}$$
(6.25)

Input Vector (eq. 6.26) is defined as linear velocity of UAS v and angular speed of rigid body $\omega_{roll}, \omega_{pitch}, \omega_{yaw}$.

$$input = [v, \omega_{roll}, \omega_{pitch}, \omega_{yaw}]^T$$
 (6.26)

Velocity distribution function (eq. 6.27) is is defined trough standard rotation matrix and linear velocity v, oriented velocity $[v_x, v_y, v_z]$ given by (eq. 6.28).

$$\begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix} = \begin{bmatrix} v\cos(pitch)\cos(yaw) \\ v\cos(pitch)\sin(yaw) \\ -v\sin(pitch) \end{bmatrix}$$
(6.27)

UAS Nonlinear Model (eq. 6.28) is given by first order equations:

$$\frac{\partial x}{\partial time} = v \cos(pitch) \cos(yaw); \qquad \frac{\partial roll}{\partial time} = \omega_{roll};
\frac{\partial y}{\partial time} = v \cos(pitch) \sin(yaw); \qquad \frac{\partial pitch}{\partial time} = \omega_{pitch};
\frac{\partial z}{\partial time} = -v \sin(pitch); \qquad \frac{\partial yaw}{\partial time} = \omega_{yaw};$$
(6.28)

6.2.5 Used Movement Automaton for UAS Model

Motivation: An *UAS Nonlinear Model* (eq. 6.28) can be modeled by *Movement Automaton* (def. 6).

Movement Primitives by (def. 1) are given as (eq. 6.1). To define primitives the minimal time is 1s. The maximal duration is also 1s.

Assumption 1. Let assume that transition time of roll, pitch, yaw, linear velocity is 0s.

Under the assumption (as. 1) the movement transitions (def. 2) have 0 duration.

Note. The assumption (as. 1) can be relaxed under condition that path tracking controller exists.

Movements (def. 3) for *fixed step k* we start with discretization of the input variables. The *linear velocity* in text step is given:

$$v(k+1) = v(k) + \delta v(k) \tag{6.29}$$

The roll, pitch, yaw for next step are given

$$roll(k+1) = roll(k) + \delta roll(k)$$

$$pitch(k+1) = pitch(k) + \delta pitch(k)$$

$$yaw(k+1) = yaw(k) + \delta yaw(k)$$
(6.30)

The $\delta v(k)$ is velocity change, $\delta roll(k)$, $\delta pitch(k)$, $\delta yaw(k)$, are orientation changes for current discrete step k. If the duration of transition is 0s (as. 1) then 3D trajectory evolution in discrete time is given as:

$$x(k+1) = x(k) + v(k+1)\cos(pitch(k+1))\cos(yaw(k+1)) = \delta x(k)$$

$$y(k+1) = y(k) + v(k+1)\cos(pitch(k+1))\sin(yaw(k+1)) = \delta y(k)$$

$$z(k+1) = z(k) - v(k+1)\sin(pitch(k+1)) = \delta z(k)$$

$$time(k+1) = time(k) + 1 = \delta time(k)$$
(6.31)

The $\delta x(k)$, $\delta y(k)$, $\delta z(k)$ are positional differences depending on *input vector* for given discrete time k:

$$input(k) = \begin{bmatrix} \delta x(k), \delta y(k), \delta z(k), \delta v(k), \\ \delta roll(k), \delta pitch(k), \delta yaw(k), \delta time(k) \end{bmatrix}^{T}$$

$$(6.32)$$

The *state vector* for discrete time is given:

$$state(k) = \begin{bmatrix} x(k), y(k), z(k), v(k), \\ roll(k), pitch(k), yaw(k), time(k) \end{bmatrix}^{T}$$

$$(6.33)$$

The nonlinear model (eq. 6.28) is then reduced to *linear discrete model* (eq. 6.34) given by *apply movements* function (eq. 6.29, 6.30, 6.31).

$$state(k+1) = applyMovement(state(k), input(k))$$
 (6.34)

Movement Set for linear discrete model (eq. 6.34) is defined as set of extreme unitary movements on main axes (tab. 6.1) and diagonal axes (tab. 6.2).

input(movement)	Straight	Down	Up	Left	Right
$\delta x(k)[m]$	1.00	0.98	0.98	0.98	0.98
${\delta y(k)[m]}$	0	0	0	0.13	-0.13
$\delta z(k)[m]$	0	-0.13	0.13	0	0
$\delta roll(k)[^{\circ}]$	0	0	0	0	0
$\delta pitch(k)[^{\circ}]$	0	15°	-15°	0	0
$\overline{\delta yaw(k)[^{\circ}]}$	0	0	0	15°	-15°

Table 6.1: Input values for main axes movements.

input(movement)	Down-Left	Down-Right	Up-Left	Up-Right
$\delta x(k)[m]$	0.76	0.76	0.76	0.76
$\delta y(k)[m]$	-0.13	0.13	0.13	-0.13
$\delta z(k)[m]$	-0.13	-0.13	0.13	0.13
$\overline{\delta roll(k)[^{\circ}]}$	0	0	0	0
$\overline{\qquad \qquad \delta pitch(k)[^{\circ}]}$	-15°	-15°	15°	15°
$\overline{\delta yaw(k)[^{\circ}]}$	15°	-15°	15°	-15°

Table 6.2: Input values for diagonal axes movements.

Note. Movement set in shorten form is given as

$$MovementSet = \begin{cases} Straight, Left, Right, Up, Down, \\ DownLeft, DownRight, UpLeft, UpRight \end{cases}$$
 (6.35)

Trajectory by (def. 5) for initial time time = 0, initial state state(0) and Movement Buffer (from def. 4):

$$Buffer \in MovementSet^*(eq.6.35), \quad |Buffer| \in \mathbb{N}$$
 (6.36)

Trajectory (eq. 6.37) is then given as the time-series of discrete states:

$$Trajectory(state(0), Buffer) = \begin{cases} state(0) + \sum_{j=0}^{i-1} input(movement(j)) : \\ i \in \{1 \dots |Buffer| + 1\}, \\ movement(\cdot) \in Buffer \end{cases}$$
(6.37)

Trajectory (eq. 6.37) is ordered set of states bounded to discrete time $0 \dots n$, where n is member count of *Buffer*. Trajectory set has n+1 members:

$$Trajectory(state(0), Buffer) =$$

$$\begin{cases}
state(0) = state(0) + \{\} \\
state(1) = state(0) + input(movement(1)) \\
state(2) = state(0) + input(movement(1)) + input(movement(2)) \\
\vdots = \vdots \\
state(n) = state(0) + input(movement(1)) + \dots + input(movement(n))
\end{cases} (6.38)$$

State Projection (eq. 6.39) for the *Trajectory* (eq. 6.37) is given as follow:

$$StateProjection(Trajectory, time) = Trajectory.getMemberByIndex(time + 1)$$

$$(6.39)$$

Note. Movement Automaton for system (eq. 6.28) with given (as. 1) is established with all related properties (sec. 6).

6.2.6 Segmented Movement Automaton

Motivation: Constructing *Movement Automaton* for more complex system can be tedious. Used *Movement Automaton* for *UAS system* (6.28) has decoupled control which is not true for most of the copters/planes [8].

Partitioning UAS State Space: Proposed movement automaton is defined by its Movement set (tab. 6.1,6.2). Those can be scaled depending on maneuverability in the *Initial state state*(0):

- 1. $Climb/Descent Rate \ \delta pitch_{max}(k)$ the maximal climb or descent rate for Up/Down movements.
- 2. Turn Rate $\delta yaw_{max}(k)$ the maximal turn rate for Left/Right movement.
- 3. Acceleration $\delta v_{max}(k)$ the maximal acceleration in cruising speed range.

Definition 7. State Space partition Maneuverability is depending on Initial State. There can not be the infinite count of Movement Automatons.

The state space $StateSpace \in \mathbb{R}^n$ can be separated into two exclusive subsets:

$$StateSpace = [ImpactStates, NonImpactingStates]$$
 (6.40)

The Impacting states are states which bounds the Maneuverability: $\delta pitch_{max}(k)$, $\delta yaw_{max}(k)$, $\delta v_{max}(k)$. For each impact state is possible to define upper and lower boundary:

 $\forall impactState \in ImpactStates, \exists :$

$$lower(impactState) \le value(impactState) \le upper(impactState)$$
 (6.41)

The bounded interval of impact state can be separated into distinctive impact state segments like follow:

 $impactState \in [lower, upper]:$

```
\{[lower, separator_1[\dots \cup \dots [separator_i, separator_{i+1}[\dots \cup \dots ] \\ \dots \cup \dots [separator_n, upper]]\} = \\ = impactStateIntervals(impactState) \quad (6.42)
```

Note. The interval length depends on model dynamics. The rule of thumb is to keep maximal climb/descend/turn/acceleration rates near constant value.

When partitioning of all impact States finishes, the count of partitions is given as product of count of partitions for each member of Impact States:

$$partitionCount = \prod_{impactState \in}^{ImpactStates} |impactStateIntervals(impactState)|$$
 (6.43)

Note. Try to keep the count of partitions to minimum, each new interval increases the count of partitions geometrically.

There is finite number n of Impacting States, these are separated into impactState—Intervals_i with respective index $i \in 1...n$. The segment with index defining position used impacting state intervals is given as constrained space:

$$Segment(index) = \begin{bmatrix} impactState_1 \in impactStateIntervals_1[index_1], \\ \vdots \\ impactState_n \in impactStateIntervals_n[index_n], \\ \vdots \\ NonImpactingStates \end{bmatrix}$$
(6.44)

Each Segment covers one of impacting state intervals combination, because the original intervals are exclusive, also Segments are exclusive. The union of all segments covers State Space:

$$StateSpace = \bigcup_{\substack{\forall index \in |impactStateIntervals|^n}} Segment(index)$$
 (6.45)

Segmented Movement Automaton: The segmentation of state space is done in (def. 7) any state belongs exactly to Segment of State Space. For each Segment in State Space it is possible to assess: $Climb/Descent\ Rate\ \delta pitch_{max}(k)$, $Turn\ Rate\ \delta yaw_{max}(k)$, and, $Acceleration\ \delta v_{max}(k)$.

Definition 8. Movement Automaton for Segment(index)

For for Model(eq. 6.34) with State (eq. 6.33) the input vector (eq. 6.32) is for position [x, y, z] and velocity defined like:

$$\delta x(k) = (v(k) + \delta v(k)) \cos(\delta pitch(k)) \cos(\delta yaw(k))$$

$$\delta y(k) = (v(k) + \delta v(k)) \cos(\delta pitch(k)) \sin(\delta yaw(k))$$

$$\delta z(k) = -(v(k) + \delta v(k)) \cos(\delta pitch(k))$$

$$\delta v(k) \in [-\delta v(k)_{max}, \delta v(k)_{max}]$$
(6.46)

The acceleration $\delta v(k)$ is in interval $[-\delta v(k)_{max}, \delta v(k)_{max}]$, usually set to 0 ms^{-1} . The change of the orientation angles for *Movement Set* (eq. 6.35) is given in (tab. 6.3,6.4).

input(movement)	Straight	Down	Up	Left	Right
$\delta roll(k)[^{\circ}]$	0	0	0	0	0
$\delta pitch(k) [^{\circ}]$	0	$\delta pitch_{max}$	$-\delta pitch_{max}$	0	0
$\delta yaw(k)[^{\circ}]$	0	0	0	δyaw_{max}	$-\delta yaw_{max}$

Table 6.3: Orientation input values for main axes movements.

input(movement)	Down-Left	Down-Right	Up-Left	Up-Right
$\delta roll(k)[^{\circ}]$	0	0	0	0
$\delta pitch(k) [^{\circ}]$	$-\delta pitch_{max}$	$-\delta pitch_{max}$	$\delta pitch_{max}$	$\delta pitch_{max}$
$\delta yaw(k)[^{\circ}]$	δyaw_{max}	$-\delta yaw_{max}$	δyaw_{max}	$-\delta yaw_{max}$

Table 6.4: Orientation input values for diagonal axes movements.

Note. The Trajectory is calculated same as in (eq. 6.37). The State Projection is given as in (eq. 6.39).

Then the Movement Automaton for Segment \in State Space is defined.

Definition 9. Segmented Movement Automaton For system with segmented state space (eq. 6.45) there is for each state(k) in StateSpace injection function:

$$Active Movement Automaton: State Space \rightarrow Movement Automaton$$
 (6.47)

Selecting appropriate movement automaton implementation (def. 8) for state(k) \in Segment \subset State Space. The mapping function (eq. 6.47) is injection mapping every state(k) to Segment then Movement Automaton Implementation. The trajectory generated is then given:

$$Trajectory \begin{pmatrix} state(0), \\ Buffer \end{pmatrix} = \begin{cases} state(0) + \dots \\ \sum_{j=0}^{i-1} ActiveMovementAutomaton(state(j-1)). \\ input(movement(j)) \\ i \in \{1 \dots |Buffer| + 1\}, \\ movement(\cdot) \in Buffer \end{cases}$$
 (6.48)

6.2.7 Reference Trajectory Generator

Reference Trajectory Generator: Segmented Movement Automaton (def. 9) with trajectory function (eq. 6.48) is used as reference trajectory generator for complex systems.

There is assumption that precise *path tracking* implementation exist for such system which with *thick reference trajectory* gives similar results to *plain movement automaton control*.

The Reference trajectory (eq. 6.49) for Planned movement set is given as projection of Trajectory time series to position time series [x, y, z, t]:

$$ReferenceTrajectory: Trajectory \begin{pmatrix} state(now), \\ Planned \end{pmatrix} \rightarrow \begin{bmatrix} x_{ref} \in \mathbb{R}^{|Planned|} \\ y_{ref} \in \mathbb{R}^{|Planned|} \\ z_{ref} \in \mathbb{R}^{|Planned|} \\ t_{ref} \in \mathbb{R}^{|Planned|} \end{bmatrix}$$
(6.49)

Predictor: The Reference Trajectory Generator (eq. 6.49) can be also used as predictor.

Note. The Segmented Movement Automaton (def. 9) is used in this work with one Segment equal to State space with input function given by (6.1, 6.2). The predictor used in Reach set computation is given by (eq. 6.49).

Bibliography

- [1] Ondřej Šantin and Vladimir Havlena. Combined partial conjugate gradient and gradient projection solver for mpc. In *Control Applications (CCA)*, 2011 IEEE International Conference on, pages 1270–1275. IEEE, 2011.
- [2] Frangois G Pin and Hubert A Vasseur. Autonomous trajectory generation for mobile robots with non-holonomic and steering angle constraints. Technical report, Oak Ridge National Lab., 1990.
- [3] Ralph G Andrzejak, G Widman, K Lehnertz, C Rieke, P David, and CE Elger. The epileptic process as nonlinear deterministic dynamics in a stochastic environment: an evaluation on mesial temporal lobe epilepsy. *Epilepsy research*, 44(2-3):129–140, 2001.
- [4] Yoshiaki Kuwata, Justin Teo, Gaston Fiore, Sertac Karaman, Emilio Frazzoli, and Jonathan P How. Real-time motion planning with applications to autonomous urban driving. *IEEE Transactions on Control Systems Technology*, 17(5):1105–1118, 2009.
- [5] Emilio Frazzoli. Robust hybrid control for autonomous vehicle motion planning. PhD thesis, Massachusetts Institute of Technology, 2001.
- [6] Emilio Frazzoli, Munther A Dahleh, and Eric Feron. Trajectory tracking control design for autonomous helicopters using a backstepping algorithm. In *American Control Conference*, 2000. Proceedings of the 2000, volume 6, pages 4102–4107. IEEE, 2000.
- [7] Alojz Gomola, João Borges de Sousa, Fernando Lobo Pereira, and Pavel Klang. Obstacle avoidance framework based on reach sets. In *Iberian Robotics conference*, pages 768–779. Springer, 2017.
- [8] Thor I Fossen. Mathematical models for control of aircraft and satellites. Department of Engineering Cybernetics Norwegian University of Science and Technology, 2011.
- [9] Franco Blanchini. Set invariance in control. Automatica, 35(11):1747–1767, 1999.