

## Time-stepping approach to large-scale linear algebra

Jean-Christophe Loiseau



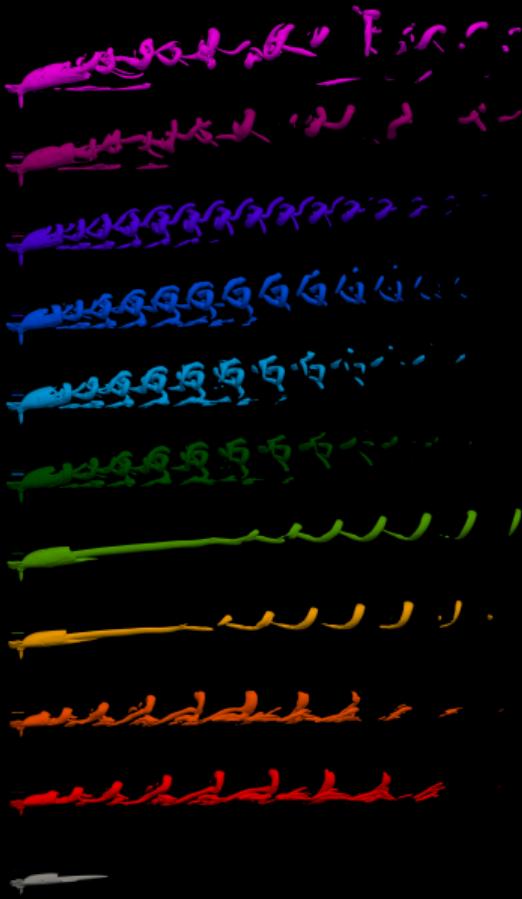
Ricardo Frantz



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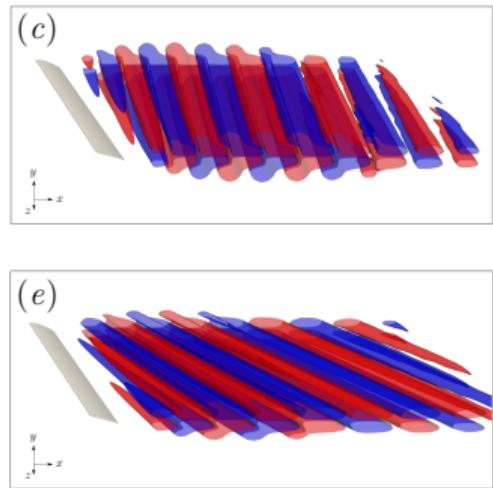
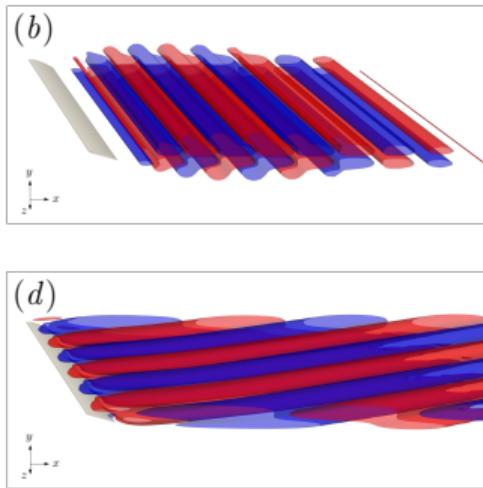
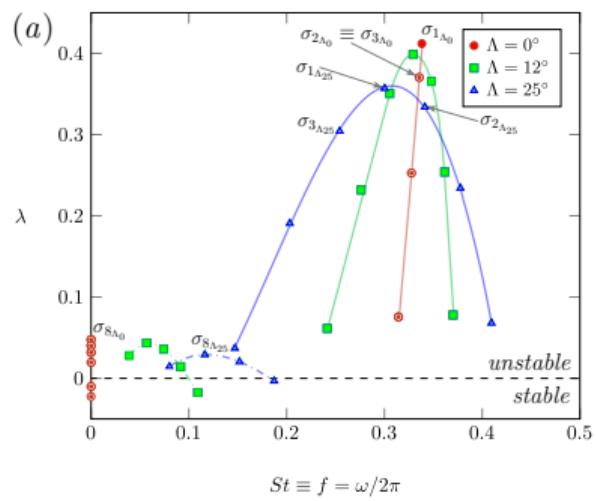


Jean-Christophe Robinet



**Hydrodynamic stability** : Set of tools to investigate the first stages of transition to turbulence.

Primarily a numerical linear algebra issue for large-scale dynamical systems such as discretized PDEs.



Dynamics  $f : \mathbb{R} \times \mathbb{R}^n \times \mathbb{R}^p \rightarrow \mathbb{R}^n$

$$\dot{\mathbf{X}} = f(t, \mathbf{X}, \mu)$$

State vector  $\mathbf{X} \in \mathbb{R}^n$

**Flow map**  $\varphi_\tau : \mathbb{R}^n \times \mathbb{R}^p \rightarrow \mathbb{R}^n$

$$\mathbf{X}_{k+1} = \boxed{\varphi_\tau}(\mathbf{X}_k, \boldsymbol{\mu})$$

**How to compute fixed points or periodic orbits of the system and study their linear stability properties given only a time-stepper ?**

## Fixed points

*Continuous time*

$$f(\mathbf{X}, \boldsymbol{\mu}) = \mathbf{0}$$

*Discrete time*

$$\varphi_\tau(\mathbf{X}, \boldsymbol{\mu}) - \mathbf{X} = \mathbf{0} \quad \forall \tau$$

## Linearized system

*Continuous time*

$$\dot{\mathbf{x}} = \mathbf{L} \mathbf{x}$$

Jacobian matrix  $\in \mathbb{R}^{n \times n}$

*Discrete time*

$$\mathbf{x}_{k+1} = \exp(\tau \mathbf{L}) \mathbf{x}_k$$

Exponential Propagator  $\in \mathbb{R}^{n \times n}$

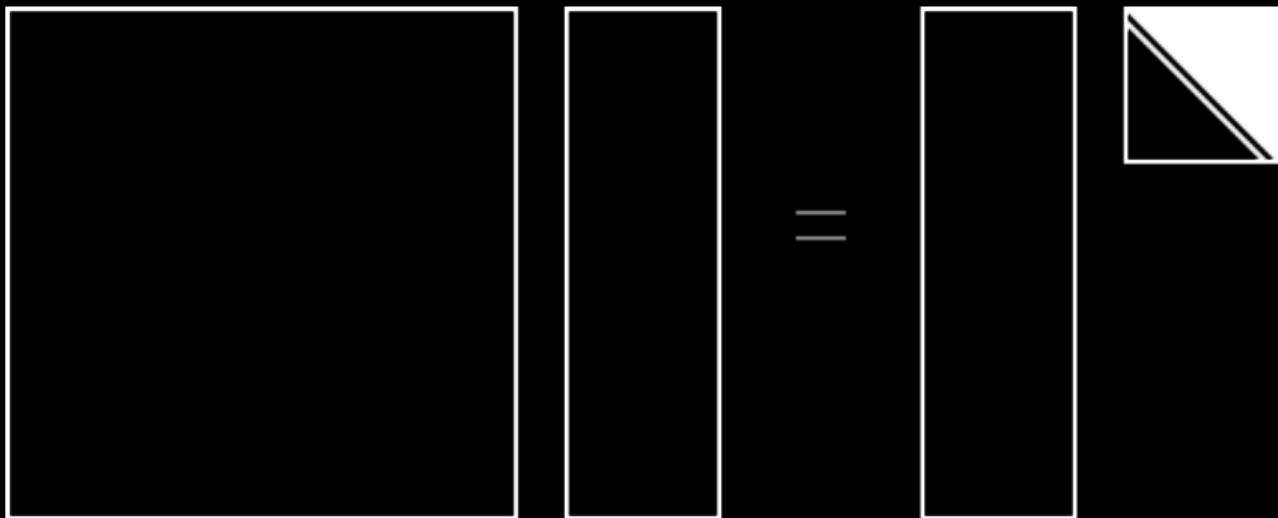
## Arnoldi factorization



Alexei Krylov



Cornelius Lanczos



## Generalized Minimal Residual Method

**Require:**  $x_0, A, b$

**Ensure:**  $\|Ax - b\|_2^2 \leq \varepsilon$

$$r \leftarrow b - Ax_0$$

$$q_1 \leftarrow r / \|r\|_2$$

**for**  $k = 1, 2, \dots$  **do**

$$y \leftarrow Aq_k$$

**for**  $j = 1, 2, \dots, k$  **do**

$$h_{jk} \leftarrow q_j^T y$$

$$y \leftarrow y - h_{jk} q_j$$

**end for**

$$h_{k+1,k} = \|y\|_2$$

$$q_{k+1} = y / h_{k+1,k}$$

$$\text{minimize } \|Hc - e_1\|_2 \|r\|_2$$

$$x_k \leftarrow x_0 + Q_k c$$

**end for**



Youssef Saad

# Fixed point computation

$$\mathcal{F}(\mathbf{X}, \boldsymbol{\mu}) \equiv \varphi_{\tau}(\mathbf{X}, \boldsymbol{\mu}) - \mathbf{X} = \mathbf{0}$$

$$\mathbf{J} \equiv \exp(\tau \mathbf{L}) - \mathbf{I}$$

## Newton-GMRES solver for fixed point computation

**Require:**  $\mathbf{X}$

**Ensure:**  $\|\mathbf{F}(\mathbf{X})\| \leq \varepsilon$

$\mathbf{r} \leftarrow \mathcal{F}(\mathbf{X}_0)$

**while**  $\|\mathbf{r}\| \geq \varepsilon$  **do**

$\delta\mathbf{x} \leftarrow \text{gmres}(\mathbf{F}', \mathbf{r})$

$\mathbf{X} \leftarrow \mathbf{X} + \delta\mathbf{x}$

$\mathbf{r} \leftarrow \mathbf{F}(\mathbf{X})$

**end while**

- The product  $\exp(\tau \mathbf{L}) \mathbf{x}$  can easily be computed with a time-stepper.
- Good performances even without preconditionning!
- Extension to periodic orbits is straightforward.



Espen Åkervik

## Selective Frequency Damping

$$\dot{\mathbf{X}} = f(t, \mathbf{X}, \boldsymbol{\mu}) - \chi (\mathbf{X} - \mathbf{Y})$$

$$\dot{\mathbf{Y}} = \omega_c (\mathbf{X} - \mathbf{Y})$$

Filter's gain

Filter's cutoff frequency

## BoostConv

Corrected state

$$\tilde{\mathbf{x}}_{t+1} = \mathbf{x}_{t+1} - \mathbf{Y}\mathbf{Y}^\dagger (\mathbf{x}_{t+1} - \tilde{\mathbf{x}}_t) + \mathbf{X}\mathbf{Y}^\dagger (\mathbf{x}_{t+1} - \tilde{\mathbf{x}}_t)$$

Predicted state



Vincenzo Citro



Standard test case in the incompressible hydrodynamic stability community. Here, we solve it with the spectral element solver Nek5000 + nekStab.



- From  $Re = 40 \rightarrow Re = 70$ .
- 2000 spectral elements.
- 3<sup>rd</sup> order-accurate EXT/BDF scheme.
- Helmholtz solver tolerance set to  $10^{-12}$ .
- Pressure Poisson solver tolerance set to  $10^{-10}$ .

**Coarse mesh :** 32 000 grid points with  $\Delta t = 0.025$

	<b>SFD</b>	<b>BootConv</b>	<b>Newton-GMRES</b>	<b>Newton-GMRES (dyn. tol.)</b>
<b>Time</b>	42 s	30 s	65 s	30 s
<b>RAM Usage</b>	0.3 Gb	0.4 Gb	1.8 Gb	0.5 Gb

**Intermediate mesh** : 72 000 grid points with  $\Delta t = 0.01$

	<b>SFD</b>	<b>BootConv</b>	<b>Newton-GMRES</b>	<b>Newton-GMRES (dyn. tol.)</b>
<b>Time</b>	230 s ( $\times 6$ )	235 s ( $\times 8$ )	370 s ( $\times 6$ )	230 s ( $\times 8$ )
<b>RAM Usage</b>	0.3 Gb	0.4 Gb	1.8 Gb	0.8 Gb

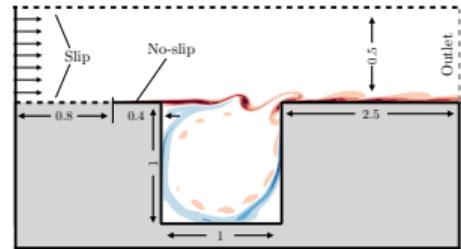
**Fine mesh :** 128 000 grid points with  $\Delta t = 0.005 =$

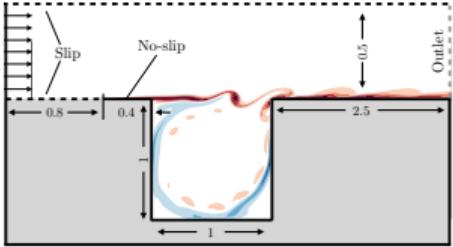
	<b>SFD</b>	<b>BootConv</b>	<b>Newton-GMRES</b>	<b>Newton-GMRES (dyn. tol.)</b>
<b>Time</b>	884 s ( $\times 3.8$ )	1260 s ( $\times 5$ )	1370 s ( $\times 3.7$ )	774 s ( $\times 3.6$ )
<b>RAM Usage</b>	0.4 Gb	0.6 Gb	2.9 Gb	0.8 Gb

Another relatively standard test-case for flow control and reduced-order modeling<sup>a</sup>. A branch of discrete eigenvalues eventually become unstable.

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<sup>a</sup>Merci Denis !





- From  $Re = 4000 \rightarrow Re = 4500$ .
- 4000 spectral elements.
- 3<sup>rd</sup> order-accurate EXT/BDF scheme.
- Helmholtz solver tolerance set to  $10^{-12}$ .
- Pressure Poisson solver tolerance set to  $10^{-10}$ .

**Coarse mesh :** 64 000 grid points with  $\Delta t = 0.0025$

	<b>SFD</b>	<b>BootConv</b>	<b>Newton-GMRES</b>	<b>Newton-GMRES (dyn. tol.)</b>
<b>Time</b>	975 s	1600 s	600 s	400 s
<b>RAM Usage</b>	0.3 Gb	0.4 Gb	1.8 Gb	0.5 Gb

**Intermediate mesh :** 144 000 grid points with  $\Delta t = 0.001$

	<b>SFD</b>	<b>BootConv</b>	<b>Newton-GMRES</b>	<b>Newton-GMRES (dyn. tol.)</b>
<b>Time</b>	3120 s ( $\times 3.2$ )	NA	500 s ( $\times 1$ )	400 s ( $\times 1$ )
<b>RAM Usage</b>	0.4 Gb		1.8 Gb	0.8 Gb

**Fine mesh :** 256 000 grid points with  $\Delta t = 0.0006$

	<b>SFD</b>	<b>BootConv</b>	<b>Newton-GMRES</b>	<b>Newton-GMRES (dyn. tol.)</b>
<b>Time</b>	$10^4$ s ( $\times 3.5$ )	NA	1900 s ( $\times 3.8$ )	1500 s ( $\times 3.8$ )
<b>RAM Usage</b>	0.6 Gb		2.9 Gb	0.8 Gb

$$\begin{aligned}\exp(\tau \mathbf{L}) - \mathbf{I} &\simeq (\mathbf{I} + \tau \mathbf{L}) - \mathbf{I} \\ &\propto \mathbf{L}\end{aligned}$$

$$\text{spec}(\mathbf{L}) \in \mathcal{D} = \{z : \text{Re}(z) \leq -\delta\}$$

$$\text{spec}(\mathbf{J}) \in \mathcal{D}' = \{z : |z + 1| \leq \exp(-\tau\delta)\}$$

The residual  $\varepsilon$  after  $k$  iterations can be upper bounded by

$$\varepsilon \leq \kappa(\mathbf{V}) \exp(-k\tau\delta)$$

with  $\kappa(\mathbf{V})$  the condition number of the eigenbasis.

The number of iterations  $k$  needed to reach a given tolerance  $\varepsilon$  is given by

$$k \leq \frac{1}{\tau\delta} \log \left( \frac{\kappa(\mathbf{V})}{\varepsilon} \right).$$

This bound is however overly pessimistic. If  $p$  eigenvalues are unstable,  $\mathcal{O}(p)$  extra iterations are needed.

# Linear stability analyses

# Spectral decomposition

$$\exp(\tau \mathbf{L}) \mathbf{v} = \mathbf{v}\mu$$

- Matrix-vector product computed with a time-stepper.
- Eigenvalues of interest already have the largest magnitude.
- No other spectral transformation needed for fast convergence of iterative solvers.

**Krylov subspace dimension : 128**

<b>Mesh</b>	<i>Coarse</i>	<i>Intermediate</i>	<i>Fine</i>
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<b># of conv. ev.</b>	2	2	2
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<b>Time</b>	30 s	210 s	800 s
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**Krylov subspace dimension : 192**

<b>Mesh</b>	<i>Coarse</i>	<i>Intermediate</i>	<i>Fine</i>
<hr/>			
<b># of conv. ev.</b>	4	10	10
<b>Time</b>	54 s	324 s	1140 s

**Krylov subspace dimension : 256**

<b>Mesh</b>	<i>Coarse</i>	<i>Intermediate</i>	<i>Fine</i>
<hr/>			
<b># of conv. ev.</b>	6	10	10
<b>Time</b>	80 s	418 s	1520 s

Suppose  $\mu_i$  is an isolated eigenvalue such that the rest of the spectrum is enclosed in the disk

$$\mathcal{D} = \{z : |z - c| < \rho\},$$

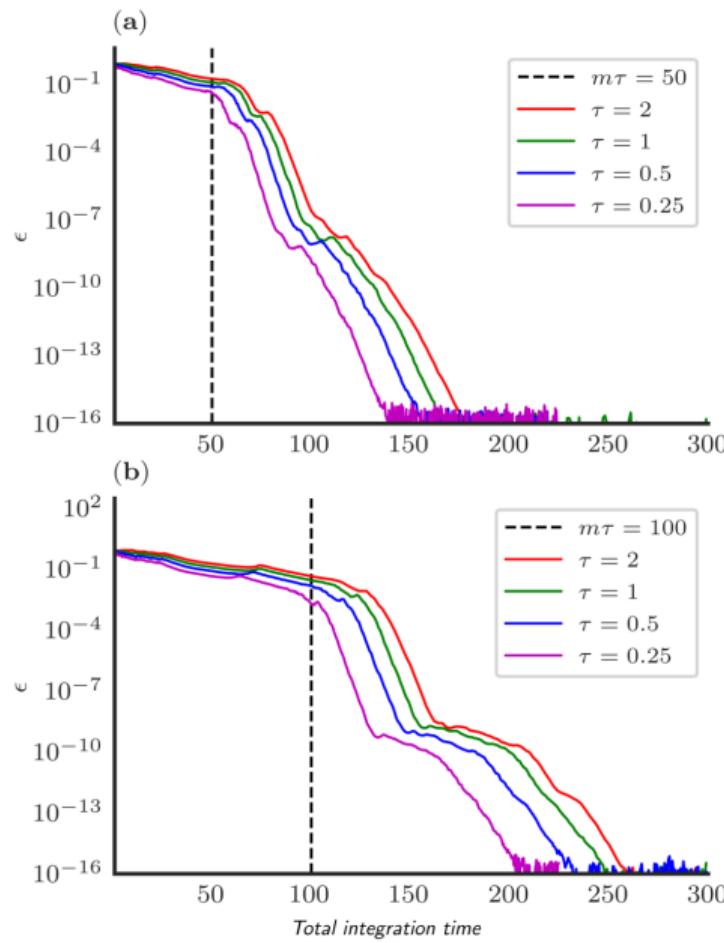
i.e. a disk centered in  $c$  and of radius  $\rho$ .

Upper bound for the residual  $\varepsilon_i$  associated to  $\mu_i$  after a  $k$ -step Arnoldi factorization is given by

$$\varepsilon_i \leq \kappa(\mathbf{V}) \left( \frac{\rho}{|\mu_i - c|} \right)^k.$$

The further apart  $\mu_i$  is from the rest of the spectrum, the faster it converges.

- The larger  $\tau$ , the larger the gap between  $\mu_i$  and the rest of the spectrum.
- The larger  $\tau$ , the fewer iterations are needed to converge the leading eigenspectrum.
- The larger  $\tau$ , the more expensive each matrix-vector product is.



For a random starting vector, the number of Krylov iterations before convergence is proportional to the flow-through time.

# Adjoint sensitivity analysis

**Adjoint operator**

$$\langle \mathbf{y} | \mathbf{Lx} \rangle = \langle \mathbf{L}^\dagger \mathbf{y} | \mathbf{x} \rangle$$

**Sensitivity to baseflow modification**

$$\nabla_{\mathbf{U}} \lambda = - (\nabla \mathbf{u})^H \cdot \mathbf{u}^\dagger + \nabla \mathbf{u}^\dagger \cdot \mathbf{u}^*$$

## Sensitivity to a steady force

$$\nabla_{\mathbf{F}} \lambda = \mathbf{U}^\dagger$$

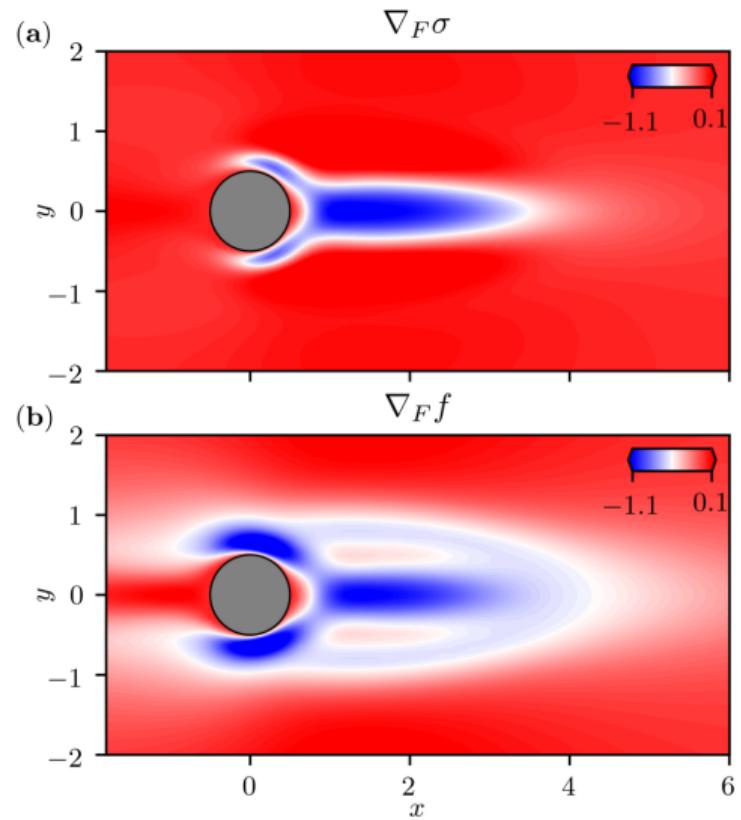
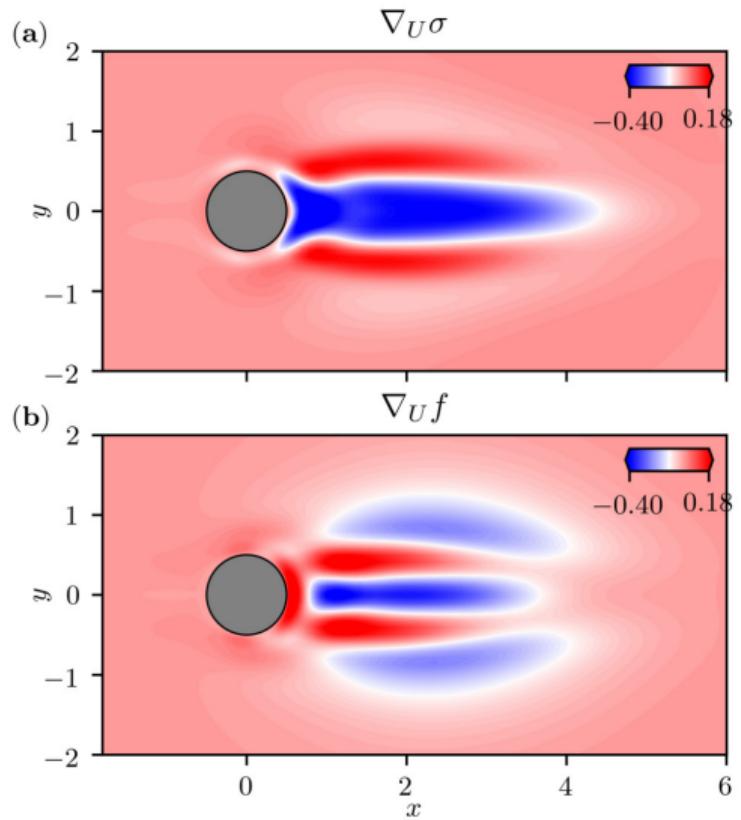


$$\mathbf{L}^\dagger \mathbf{U}^\dagger = \nabla_{\mathbf{U}} \lambda$$

$$\dot{\mathbf{x}} = \mathbf{L}^\dagger \mathbf{x} + \mathbf{b}$$

$$\mathbf{x}(\tau) = \exp(\tau \mathbf{L}^\dagger) \mathbf{x}_0 + \int_0^\tau \exp((\tau - t) \mathbf{L}^\dagger) \mathbf{b} dt$$

$$(\mathbf{I} - \exp(\tau \mathbf{L}^\dagger)) \mathbf{x} = \int_0^\tau \exp((\tau - t) \mathbf{L}^\dagger) \mathbf{b} dt$$



# What's next ?

- Linear optimal perturbation analysis is a straightforward extension with the operator being

$$\mathbf{A} = \exp(\tau \mathbf{L}^\dagger) \exp(\tau \mathbf{L}).$$

- Resolvent analysis can also be cast in this framework although it requires being a bit more careful.

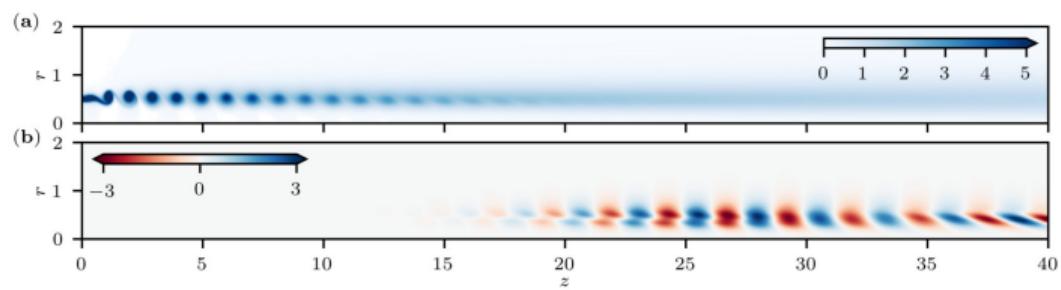
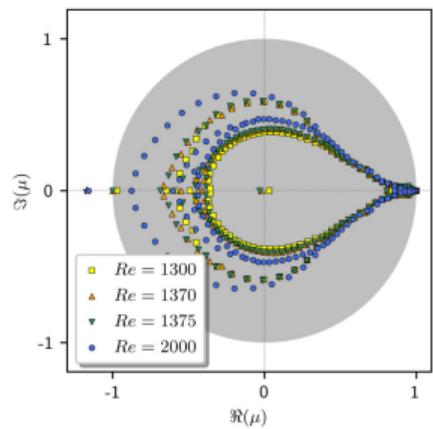
$$\begin{aligned} & \underset{\mathbf{x}}{\text{maximize}} && \|\exp(\tau \mathbf{L})\mathbf{x}\|_{\mathbf{W}}^2 \\ & \text{subject to} && \|\mathbf{x}\|_{\mathbf{W}}^2 = 1 \end{aligned}$$

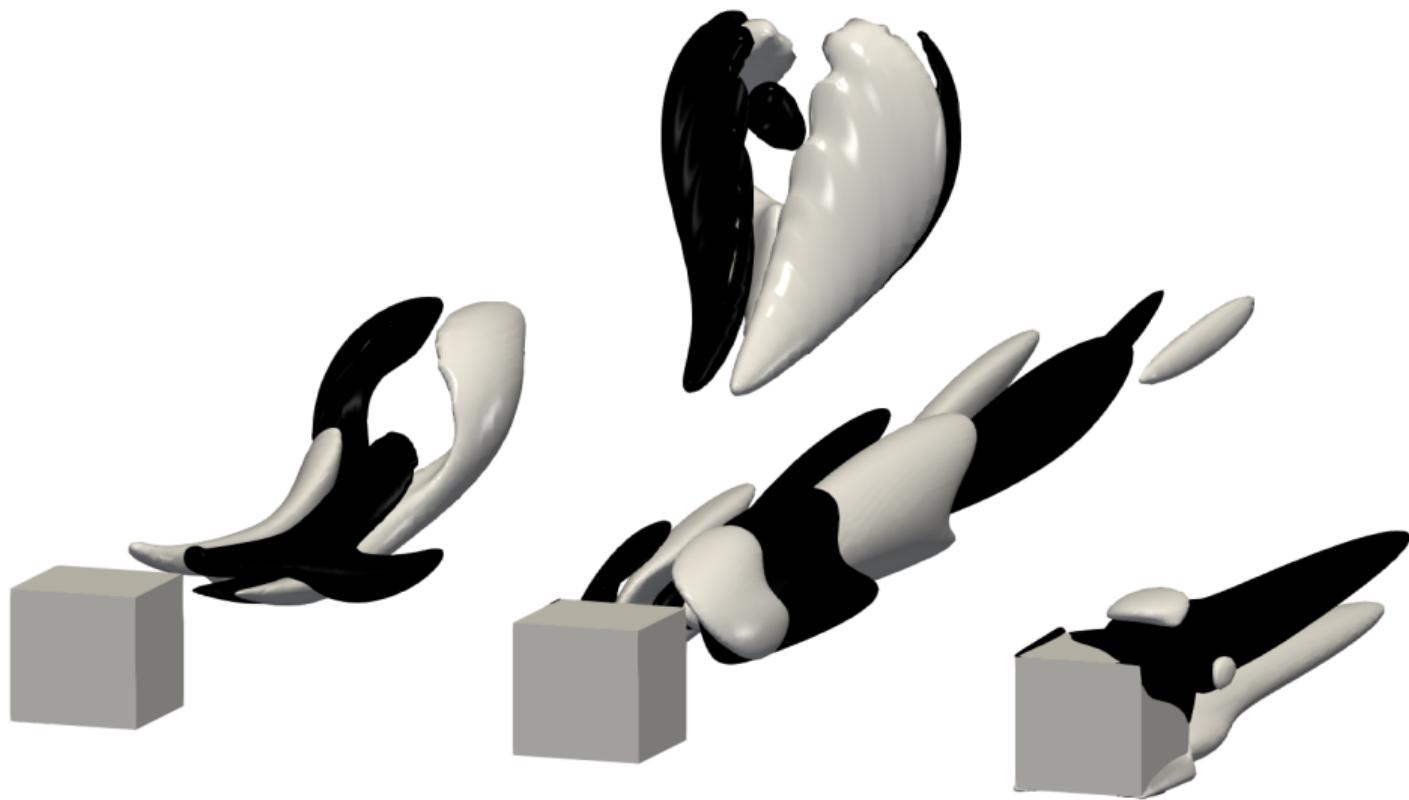
- Extension to compute (unstable) periodic orbits, satisfying

$$\mathbf{X} - \varphi_\tau(\mathbf{X}) = 0 \quad \text{for } \tau = k\tau^*$$

is also straightforward.

- The same applies to computing the eigenvalues of the monodromy matrix for Floquet analysis.





Quantitative comparison of the matrix-forming vs. time-stepper approaches using the exact same solver is still lacking.

If you have some extra \$\$\$ to use for this, please be my guest. You know how to get in touch with me !





<https://loiseaujc.github.io/>



<https://loiseau-jc.medium.com/>



@loiseau\_jc

**Thank you for your attention!**

**Any question?**