20°C

10,000 kg/h

Given:

Air in a large building is kept warm by heating it with steam in a heat exchanger. Saturated water vapor enters the unit at 35°C at a rate of 10,000 kg/hr and leaves as saturated liquid at 32°C. Air at 1 atm enters the unit at 20°C and leaves at 30°C at about the same pressure.

$$T_1 := 35 \, ^{\circ}\text{C}$$
 $T_2 := 32 \, ^{\circ}\text{C}$ $m'_s := 10000 \, \frac{\text{kg}}{\text{hr}}$ $T_3 := 20 \, ^{\circ}\text{C}$ $T_4 := 30 \, ^{\circ}\text{C}$ $P_{sir} := 1 \, \text{atm}$

Required:

Determine the rate of entropy generated during this process.

Solution:

Starting with an entropy balance for a steady flow device shows

$$\frac{d}{dt}S_{sys} = \Sigma S'_{in} - \Sigma S'_{out} + S'_{gen}$$

$$0 = \Sigma S'_{in} - \Sigma S'_{out} + S'_{gen}$$

$$S'_{gen} = \Sigma S'_{out} - \Sigma S'_{in} = m'_{s} \cdot s_{2} + m'_{air} \cdot s_{4} - m'_{s} \cdot s_{1} - m'_{air} \cdot s_{3} = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot \left(s_{4} - s_{3}\right)$$

If the air is assumed to behave as an ideal gas with a constant specific heat, the rate of entropy generation becomes

$$S'_{gen} = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot \left(c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{4}}{P_{3}}\right)\right)$$

Knowing the pressure of the air remains constant throughout the process, the rate of entropy generation becomes

$$S'_{gen} = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot \left(c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right)\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{P_{air}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) = m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{pavg} \cdot \ln\left(\frac{T_{4}}{P_{air}}\right) + R \cdot \ln\left(\frac{P_{air}}{P_{air}}\right) + R \cdot \ln\left(\frac{P_$$

Going to Table A-4 @ $T_1 = 35.00$ °C and $X_1 = 1$ shows

$$s_1 := 8.3517 \frac{\text{kJ}}{\text{kg K}}$$
 $h_1 := 2564.6 \frac{\text{kJ}}{\text{kg}}$

Going to Table A-4 @ $T_2 = 32.00$ °C and $X_2 = 0$ shows that interpolation is needed.

$$\begin{split} T_a &:= 30 \text{ °C} & T_b := 35 \text{ °C} \\ s_a &:= 0.4368 \; \frac{\text{kJ}}{\text{kg K}} \qquad s_b := 0.5051 \; \frac{\text{kJ}}{\text{kg K}} \qquad h_a := 125.74 \; \frac{\text{kJ}}{\text{kg}} \qquad h_b := 146.64 \; \frac{\text{kJ}}{\text{kg}} \\ s_2 &:= \frac{T_2 - T_a}{T_b - T_a} \cdot \left(s_b - s_a\right) + s_a = 0.4641 \; \frac{\text{kJ}}{\text{kg K}} \qquad h_2 := \frac{T_2 - T_a}{T_b - T_a} \cdot \left(h_b - h_a\right) + h_a = 134.1 \; \frac{\text{kJ}}{\text{kg}} \end{split}$$

The mass flow rate of the air may be found by performing an <u>energy balance</u> on the system. This is shown below for a steady flow device with negligible changes in KE and PE.

$$\frac{d}{dt} E_{sys} = \Sigma E'_{in} - \Sigma E'_{out}$$

$$0 = m'_{sin} \cdot h_1 + m'_{airin} \cdot h_3 - m'_{sout} \cdot h_2 - m'_{airout} \cdot h_4$$

Realizing the steam and air mass streams remain constant, the energy balance becomes

$$0 = m'_{s} \cdot (h_{1} - h_{2}) + m'_{air} \cdot (h_{3} - h_{4})$$

Solution (contd.):

Solving for the mass flow rate of the air shows

$$m'_{air} = \frac{m'_s \cdot \left(h_2 - h_1\right)}{h_3 - h_4}$$

Assuming air has a constant specific heat over the range of the process, the mass flow rate of air becomes

$$m'_{air} = \frac{m'_{s} \cdot \left(h_{2} - h_{1}\right)}{c_{pavg} \cdot \left(T_{3} - T_{4}\right)}$$

Going to Table A-2(a) @ air shows

$$c_{p,avg} \coloneqq 1.005 \frac{\text{kJ}}{\text{kg K}}$$

The mass flow rate of air may then be found by

$$m'_{air} := \frac{m'_{s} \cdot (h_{2} - h_{1})}{c_{p,avg} \cdot (T_{3} - T_{4})} = 671.8 \frac{\text{kg}}{\text{s}}$$

The rate of entropy generation is then found to be

$$S'_{gen} := m'_{s} \cdot \left(s_{2} - s_{1}\right) + m'_{air} \cdot c_{p,avg} \cdot \ln\left(\frac{T_{4}}{T_{3}}\right) = 0.7364 \frac{\text{kW}}{\text{K}}$$